

I N S T I T U T E
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H Y D R O L O G Y


A REVIEW OF THE FLOOD STUDIES REPORT
RAINFALL-RUNOFF MODEL PARAMETER
ESTIMATION EQUATIONS

by

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ABSTRACT

The Flood Studies Report, published in 1975, presents a method of design flood estimation based on a rainfall-runoff model and a statistically-derived rainfall input. At the heart of the rainfall-runoff model (the unit hydrograph and losses model) are equations relating model parameters to physical and climatological features of the drainage basin that can be abstracted from maps. These parameter estimation equations have been reviewed in the light of an expanded data set and experience gained in ten years' application of the procedure. New equations are presented that ease application and prove more robust under extreme conditions.

 Natural
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REPORT NO 94

June 1985

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1 INTRODUCTION

The Flood Studies Report (NERC, 1975) presented two methods of design flood estimation suitable for use at ungauged sites. One of these is based on a rainfall-runoff model and uses a statistically derived rainfall event as input to give an estimate of the flood magnitude of required return period. Since publication of the report more event data have been collected and analysed enabling a review of the method and in particular its parameter estimation equations. The collection of new data was partly a response to comments made at the Flood Studies Conference (Institution of Civil Engineers, 1975) and was an attempt to collect more data on catchments which had provided few events to the published analyses and also data from extra catchments of types not represented in the FSR data set. This report contains the background to the development of the revised set of recommendations summarised in Flood Studies Supplementary Report Number 16.

At this stage in the life of the Flood Studies Report (FSR) it was thought best to introduce improvements whilst maintaining as much as possible of the existing methodology; if changes were to be recommended then they should be easily slotted in to the present framework. This restriction implies a review of the model parameter estimation equations only and this is what was undertaken. The opportunity of such a review has been taken to consolidate all recommendations concerned with the rainfall-runoff method previously published in the FSR and the Flood Studies Supplementary Reports (FSSR's). In addition, the choice of dependent and independent variables used in the regression analyses has been appraised in an attempt to ease the abstraction of catchment characteristics and solve problems encountered in application under extreme conditions.

The analyses presented in this report parallel those given in the FSR and indeed assume a certain knowledge of the FSR (Volume I, Chapter 6 in particular*) The model used in analysis, the unit hydrograph and losses model, comprising a loss rate rainfall separation changing with catchment wetness and unit hydrograph derivation using matrix inversion with smoothing, is exactly as used previously in the FSR.

2 DATA

The data required for this study are of two types: catchment characteristics obtained from maps and event parameters obtained from observations and analyses. For those catchments and events used in the FSR, these data already existed in a well collated form. For new events, flow, rainfall and soil moisture deficit data were collected and processed as required before analysis. Each event yielded parameters relating to the event, such as rainfall and antecedent flow, and model parameters, such as unit hydrograph time to peak and percentage runoff. Where the new events were from catchments for which event data had not previously been collected then the pertinent catchment characteristics were abstracted.

*References to the Flood Studies Report will be given in the form Volume, chapter, section eg FSR I,6.1

To aid the storage, collation and analysis of these data a computer data base management system, the Flood Event Data Archive, was developed. This facility, which is described in Appendix B, contained many features not available at the time of the FSR. To aid abstraction of catchment characteristics, catchment boundaries were digitised and stored, thus enabling the production of computer constructed maps with precisely located catchments. The accuracy of these maps showed up many discrepancies in maps used for the FSR and led to the checking of all map derived catchment characteristics. Similarly, the new event analyses revealed that the haste with which the original analyses had been performed had allowed many events to pass the data checking stage that had poorly defined rainfalls or a possible snowmelt contribution. All event data were inspected and coded as being of quality suitable for derivation of a unit hydrograph, only suitable for assessing volumes of rainfall and flow, or of poor quality and not suitable for use in the current study.

These reviews, it was hoped, left a well organised and carefully vetted data set ready for the next stage in the analysis, the generalisation of the model parameters to the ungauged site.

Two tables in Appendix A contain the data. Table A.1 lists all the catchment characteristics abstracted for catchments in this study. Because previously derived values have been reviewed, values may differ from those published earlier. Table A.2 gives the event information and contains both event details and derived model parameters.

At the start of the second phase of data collection it had been hoped that a large increase in the total number of useful events would result. The outcome was somewhat disappointing; although over 900 new events were selected, fewer events were available for unit hydrograph analysis than had been used in the FSR. The table below summarises data availability.

TABLE 2.1 NUMBER OF EVENTS AND CATCHMENTS FOLLOWING DATA VALIDATION

Events	Total (including rejects)	2564 (1631)
	Volume analysis	1910 (1488)
	Unit hydrograph	1306 (1351)
Catchments	Total (at least one event)	210 (138)
	With at least one unit hydrograph event	181
	With at least five volume analysis events	174 - 1822 events
	With at least five unit hydrograph events	128 - 1159 events

Figures in brackets are for the equivalent FSR data set

The table shows that only half of all events selected were suitable for unit hydrograph modelling and that on many catchments only a few events were available (82 of the 210 catchments were providing less than five events suitable for full analysis). The new data set is larger in terms of numbers of catchments and events suitable for volume analysis and there has been a very small decrease in events suitable for unit hydrograph analysis. That there should be any decrease

at all having collected so much new data reflects the very much more stringent checking and acceptability criteria that were applied in the review.

Before deriving the ungauged catchment regressions a small data set was withdrawn to provide an independent sample for testing. This comprised six catchments with 59 events, 42 of which were suitable for unit hydrograph studies. Table 2.2 details the test data set.

TABLE 2.2 THE TEST DATA SET

Catchment	unit hydrograph events	loss study events
19001	5(5)	5(5)
29001	7(6)	9(6)
39012	6(8)	11(10) *
40004	11(15)	15(15)
54016	4(12)	7(16)
67010	9(12)	12(12)
Total	42(58)	59(64)

Figures in brackets are for the equivalent FSR data set

*Replaces 29003 withdrawn in FSR

3 UNIT HYDROGRAPH PARAMETER ESTIMATION

The parameters abstracted from the derived unit hydrographs were peak in hours (T_p), peak in cumecs per 100 sq km (Q_p), and the width of the peak (W), in hours; their definitions are shown graphically in Figure 3.1. If in analysis a data interval other than one hour was used an adjustment was applied to give equivalent one hour unit hydrograph parameter values (FSR I, 6.4.8).

The FSR showed the strong interdependence of the unit hydrograph parameter values and gives expressions for Q_p and W in terms of T_p alone. Figures 3.2 and 3.3 show catchment average values of Q_p and W plotted against T_p with the lines representing the FSR equations superimposed. As can be seen the equations fit the data reasonably well and there seems to be no need for change. Table 3.1 gives details of regression equations fitted to the new and the original data sets but are intended for information only and are not recommended for use.

Users of the FSR will be aware that the loss model recommended for design use is a percentage one yet a loss rate based model has been used in analysis.

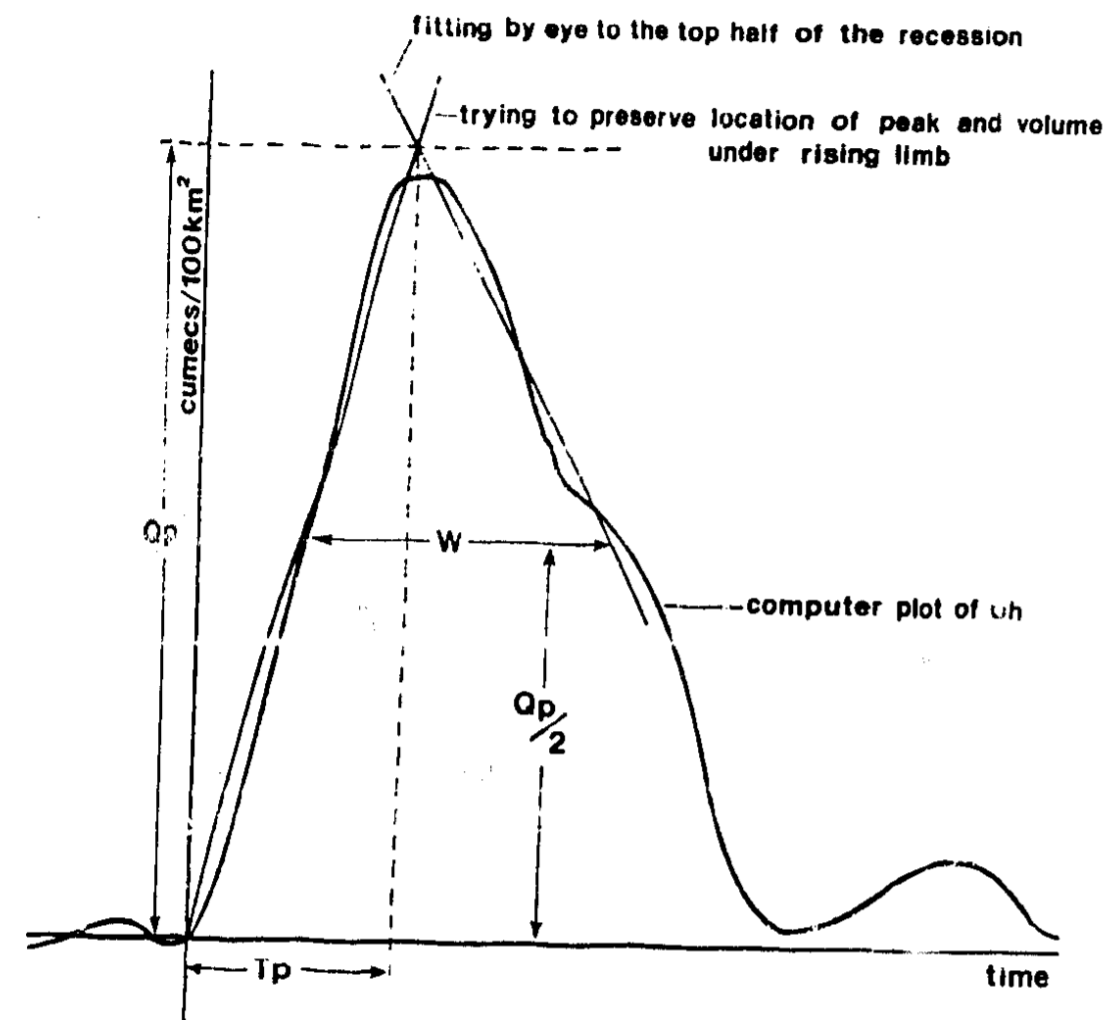


FIGURE 3.1 Definition and fitting of the FSR parameters of the unit hydrograph T_p , Q_p and W

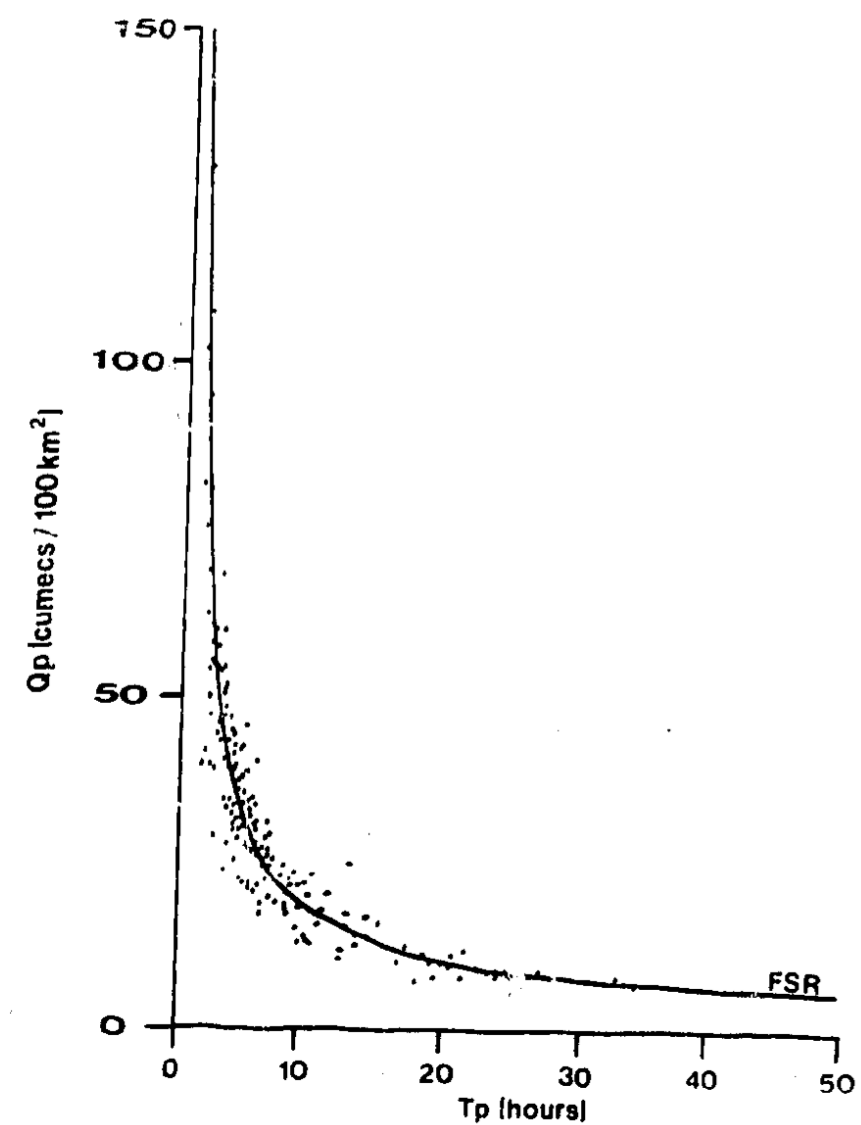


FIGURE 3.2 Catchment average values of Q_p plotted against T_p

TABLE 3.1 REGRESSION OF SECONDARY UNIT HYDROGRAPH PARAMETERS

Dependent variable : $Q_p T_p$						
Independent variable	Estimate	se	t	R^2	see observations	
Catchment averages						
T_p	2.809	0.392	7.17	0.229	347	175
Constant	157.1	4.130	38.03	-	-	-
FSR						
T_p	2.587	0.407	6.35	0.241	334	129
Constant	162.2	4.832	33.6	-	-	-
Dependent variable : W/T_p						
Catchment averages						
T_p	- 0.0154	0.00354	4.35	0.10	0.314	175
Constant	1.483	0.0374	38.6	-	-	-
FSR						
T_p	- 0.00834	0.00325	2.57	0.049	0.267	129
Constant	1.399	0.0386	36.2	-	-	-

Headings in this and subsequent tables contain the following abbreviations

- se standard error of the coefficient
- t t statistic
- R^2 coefficient of determination
- see standard error of the estimate
- sfe standard factorial error of the estimate.
- RMS root mean square

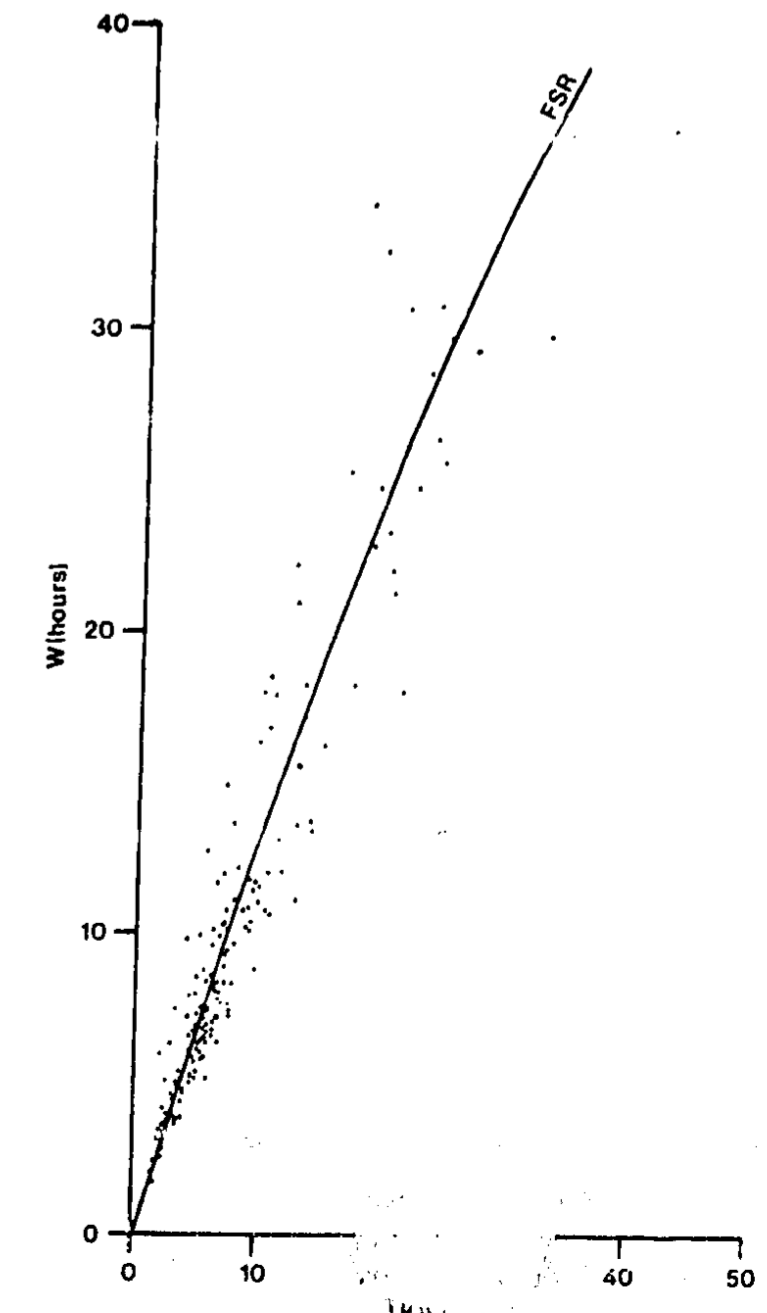


FIGURE 3.3 Catchment average values of W plotted against T_p

The interaction between unit hydrograph shape and loss model is such that an adjustment must be applied to allow for the change in rainfall separation technique. FSR I,6.5.9 details the effect this may have. The simplifying assumption of using a triangular unit hydrograph and modifying the QpTp relationship given in FSR I,6.5.2 is still considered valid as the original equations relating internal parameters are given support by the new data set.

In the FSR, Tp is estimated from a regression equation that has stream slope, urban fraction, mainstream length and RSMD as the independent variables. The meanings of the first three of these are obvious, although it is important that they are abstracted in the prescribed manner (FSR I,4.2). RSMD is an effective 5 year return period 1 day rainfall that is laborious to calculate and easy to mis-calculate. Since it is highly correlated with SAAR, the standard period average annual rainfall, which is much easier to derive, it was decided to replace RSMD with SAAR if this could be achieved without loss of accuracy in estimation.

The use of Tp, the 1-hour unit hydrograph time to peak, can also cause problems in application of the estimation equation on fast responding catchments. In such cases the required data interval may be a half or quarter hour and the 1-hour Tp must be adjusted. As the lower bound of estimated Tp's is zero it is clearly possible for adjusted Tp's to be negative, although it is more likely that they will just be unreasonably small. This problem can be avoided by developing a regression equation for time to peak of the instantaneous unit hydrograph. Whereas the 1-hour unit hydrograph represents the response to 10 mm of rainfall occurring in one hour, the instantaneous unit hydrograph is the response of an equal, but instantaneous, rainfall at the start of the hour. The time to peak of the instantaneous unit hydrograph Tp(0) can be estimated from the 1-hour time to peak, Tp(1), by $Tp(0) = Tp(1) - 1/2$.

Table 3.2 gives details of regression equations derived from the new data set and incorporating these amendments. While the equations based on the new data set and using Tp(1)-1/2 as the independent variable appear inferior to the original FSR equation the change in independent variable makes the comparison almost meaningless. In terms of estimating Tp(1) then the RMS errors from using equation 1 and equation 3 (in Table 3.2) are 4.03 and 4.00 respectively; the equations perform equally well. Replacing RSMD by SAAR has not led to any loss in accuracy in estimating Tp. Equation 4 in Table 3.2 gives details of a regression identical in form to Equation 3 only on a restricted data set; only catchments averages coming from at least five events were included. This considerably reduces the number of observations and the fit of the equation is slightly better than before. The coefficients differ by less than one standard deviation between regression equations. If catchments with more than 5% urbanisation are excluded from the data set then the resulting three variable equation has coefficients very similar to those shown in Table 3.2.

It has therefore been possible to incorporate the desired changes in the Tp estimation equation without any loss in accuracy; the recommendation is that Tp(T), where T is the required data interval, should be estimated from

$$Tp(0) = 283.0 S1085^{-0.33} (1+URBAN)^{-2.16} SAAR^{-0.54} MSL^{0.23} \quad 3.1$$

$$Tp(T) = Tp(0) + T/2 \quad 3.2$$

Figure 3.4 shows observed catchment average values of Tp(1) plotted against values estimated from the above equations.

For situations where stage data are available, but no rating exists to

TABLE 3.2 REGRESSION OF Tp ON CATCHMENT CHARACTERISTICS

Dependent variable : log(Tp(1))							
Independent variable	Estimate	se	t	R ²	see	sfe	observations
1. FSR							
Log(S1085)	- 0.381	0.066	5.77	0.780	0.150	1.41	130
Log(1+URBAN)	- 1.995	0.284	7.02	-	-	-	-
Log(RSMD)	- 0.417	0.118	3.52	-	-	-	-
Log(MSL)	0.139	0.050	2.77	-	-	-	-
Constant	1.669	0.140	11.91	-	-	-	-
Note: MSL forced into this four-variable equation.							
Dependent variable : log(Tp(1)-1/2)							
2. Catchment averages							
Log(S1085)	- 0.288	0.063	4.59	0.742	0.17	1.48	175
Log(1+URBAN)	- 2.152	0.298	7.20	-	-	-	-
Log(RSMD)	- 0.653	0.128	5.09	-	-	-	-
Log(MSL)	0.249	0.047	5.25	-	-	-	-
Constant	1.804	0.159	11.33	-	-	-	-
3. Catchment averages							
Log(S1085)	- 0.327	0.0597	5.47	0.736	0.17	1.48	175
Log(1+URBAN)	- 2.164	0.303	7.15	-	-	-	-
Log(SAAR)	- 0.538	0.115	4.69	-	-	-	-
Log(MSL)	0.228	0.0465	4.89	-	-	-	-
Constant	2.452	0.299	8.21	-	-	-	-
4. Catchments with at least 5 events							
Log(S1085)	- 0.272	0.062	4.36	0.800	0.15	1.41	125
Log(1+URBAN)	- 2.156	0.0317	6.80	-	-	-	-
Log(SAAR)	- 0.619	0.124	4.99	-	-	-	-
Log(MSL)	0.308	0.053	5.78	-	-	-	-
Constant	2.553	0.318	8.04	-	-	-	-

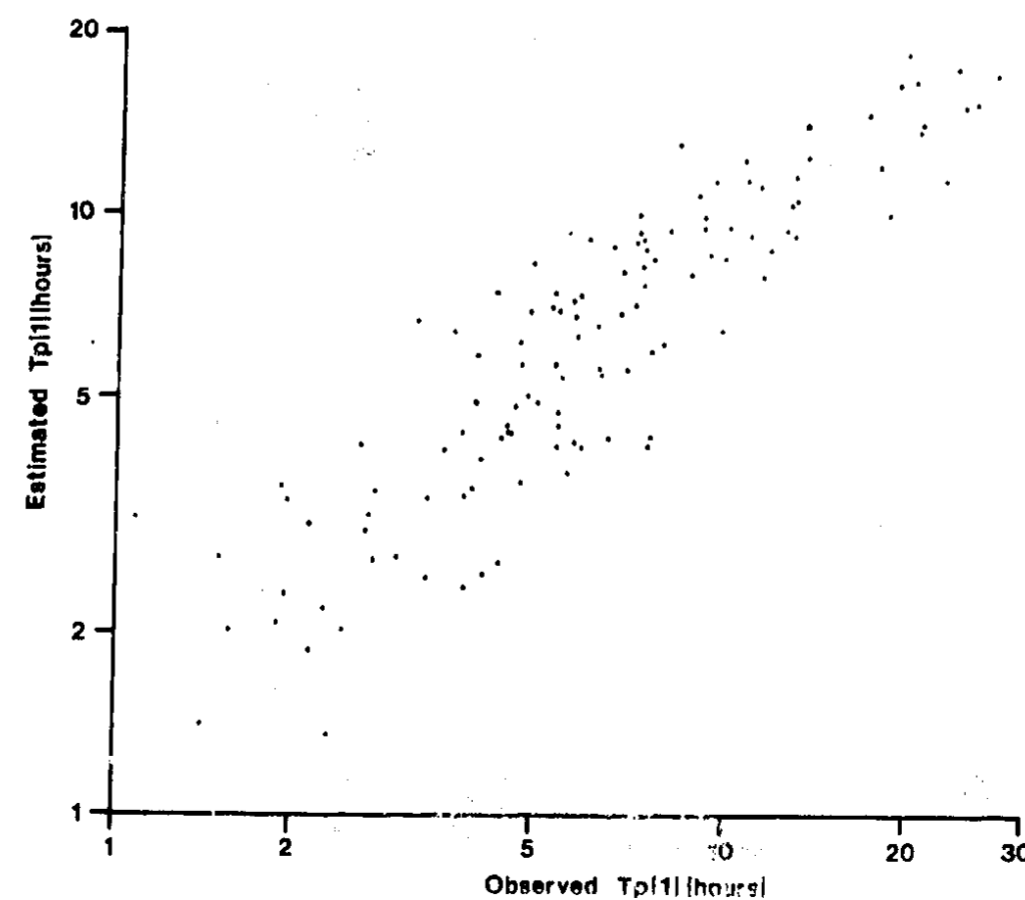


FIGURE 3.4

Estimated against observed (catchment average) values of the 1 hour unit hydrograph time to peak

obtain flows, the FSR gives an equation which can be used to estimate T_p from the catchment lag, as defined in FSR I,6.4.2. The equation is

$$T_p(1) = 0.9 \text{ Lag} \quad 3.3$$

Figure 3.5 shows catchment average values of Lag against T_p for the new data set; also plotted on this figure is the FSR equation, which represents the observed data reasonably well. However, the use of equation 3.3 would be inconsistent with the earlier recommendation to estimate $T_p(T)$ via $T_p(0)$ and could lead to the same problems in estimating time to peaks on quickly responding catchments. $T_p(0)$ may be estimated from the catchment lag using

$$T_p(0) = 0.604 \text{ Lag}^{1.144} \quad 3.4$$

which has been derived by regression analysis using catchment average data. Table 3.3 gives details of regression analyses on the new data set.

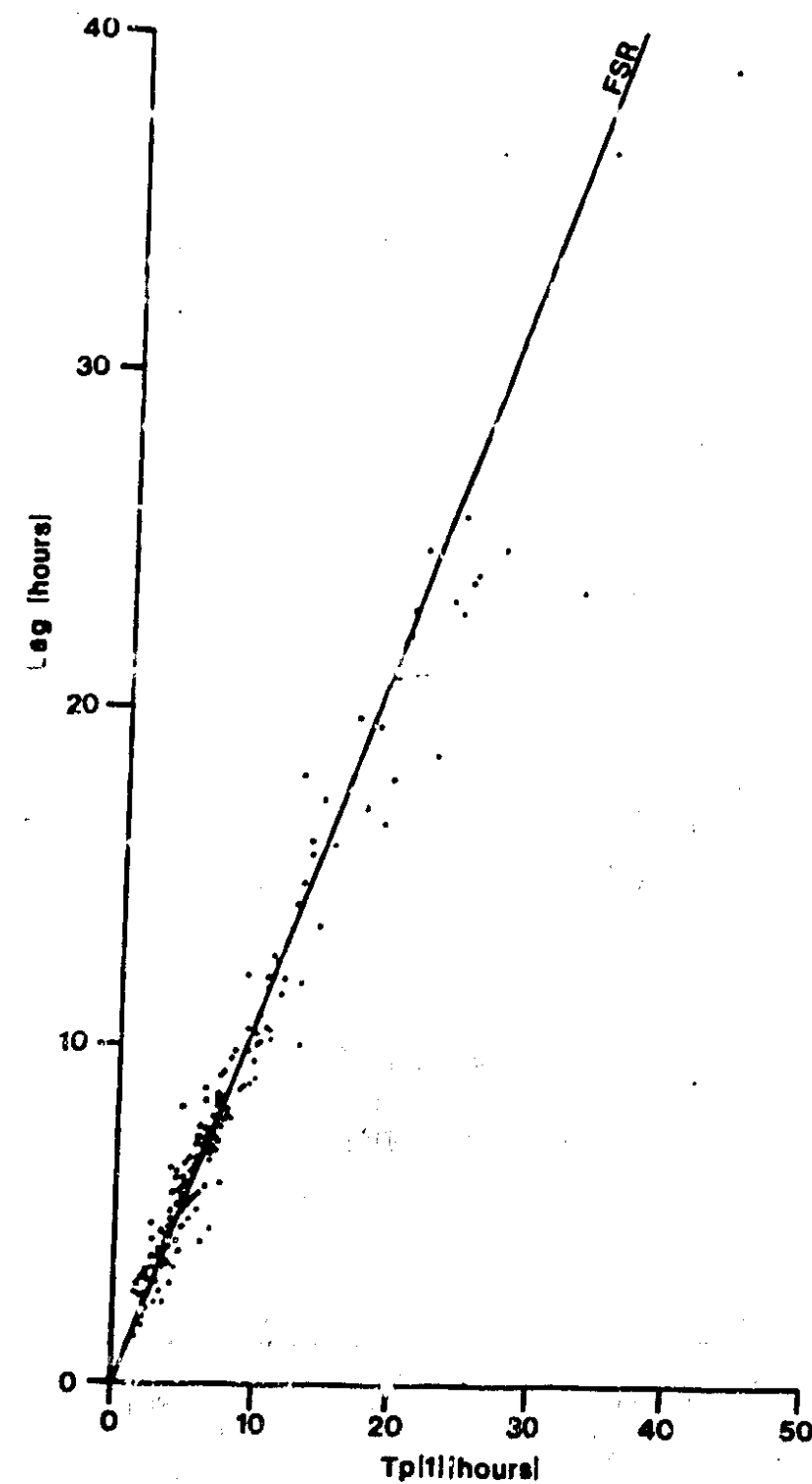


FIGURE 3.5
Catchment average values of
Lag plotted against T_p

TABLE 3.3 REGRESSION OF T_p ON LAG

Dependent variable : $\text{Log}(T_p(1))$								
Independent variable	Estimate	se	t	R^2	see	sfe	observations	
1. FSR								
Log(Lag)	0.99	0.174	57.01	0.962	0.061	1.15	129	
Constant	- 0.36			-	-	-	-	
2. All catchments								
Log(Lag)	1.041	0.0216	48.14	0.930	0.0790	1.20	175	
Constant	- 0.085	0.0194	4.39	-	-	-	-	
3. All events								
Log(Lag)	0.973	0.0145	67.05	0.78	0.158	1.44	1264	
Constant	- 0.042	0.0127	3.34	-	-	-	-	
Dependent variable $\text{Log}(T_p(1) - 1/2)$ /								
4. All catchments								
Log(Lag)	1.144	0.025	46.41	0.926	0.090	1.23	175	
Constant	- 0.219	0.022	9.91	-	-	-	-	

4 PERCENTAGE RUNOFF ESTIMATION

In the FSR the estimation of percentage runoff is seen as the most important and yet most uncertain part of the design flood estimation procedure. The usefulness of local data in refining percentage runoff estimates cannot be emphasized too strongly. While the equations presented below are applicable in situations in which no data are available they should be considered as a basis for preliminary flood estimation only.

Variations in percentage runoff can be divided into two components. On a single catchment, percentage runoff will vary with storm characteristics (depth, duration and profile of rainfall) and with catchment state at the onset of rainfall (what stores or deficits of water exist in the catchment eg. soil moisture, surface storage). Thus we expect a larger percentage response from a large storm on a wet catchment than from a small storm on a dry one. When percentage runoffs are compared between catchments then these 'dynamic' variations are superimposed on physical (constant) differences between the basins (soils, geology, land use etc). A catchment located on chalk will give very much lower runoff than one situated on clay. While it is easy to express these intuitive concepts in this general way, in practice it is difficult to define precise relationships supported by real data. This is because of the difficulties in collecting event data that cover the full range of combinations of catchment state, storm variability and catchment type, and in finding suitable indices for these variables. Difficulties may also accrue from a poor choice of rainfall-runoff model or poor model parameterisation but in the present context these are considered relatively unimportant.

The FSR presents an equation that assesses percentage runoff as a standard term, dependent on a soil index and the urban fraction, and a dynamic term that varies with total storm depth (P) and a catchment wetness index (CWI).

The resulting model for PR is represented by the three equations

$$SPR = 10S1 + 30S2 + 37S3 + 47S4 + 53S5 \quad 4.9$$

$$PR_{\text{rural}} = SPR + 0.25(CWI-125) + 0.13(P - 40) \quad 4.10$$

$$PR = PR_{\text{rural}} (1-0.3 \text{ URBAN}) + 21.0 \text{ URBAN} \quad 4.11$$

These equations represent a slight improvement over the PR formulae given in the FSR and in FSSR 5. The two main differences between the new equations and those presented in the FSR are the reduction in response from type 1 soils and the increase in magnitude of the dynamic terms. The first of these is explained by looking at the catchments located mainly on type 1 soils. Over half of the catchments mainly located on type 1 soils that were analysed in the FSR had significant urban areas (>10% urbanisation) and yet no adjustment was made prior to calibration of the SOIL index; the current analysis does have such a correction and gives a lower natural response. The increase in the dynamic term coefficients is again seen as a product of the urban adjustment and partly perhaps because of the combined fitting of soil and CWI multipliers.

The three equations 4.9 - 4.11 give a percentage runoff estimation method based on the current data set and data from small urban (sewered) catchments. While their accuracy is limited (see. of 15%) they are thought to provide a sound blend of empirical analysis and hydrological theory and could be used with due caution in conditions similar to those used to derive the equations. Restriction on their application is warranted on catchments where there is a large urban fraction and especially where this is concentrated rather than distributed throughout the catchment. The dynamic conditions encountered in the data set cover the full range of values for CWI that are likely to be experienced in even the most extreme design case; the same cannot be said for the event rainfalls of which less than 2% are greater than 100 mm. This introduces reservations over extrapolating equation 4.10 to apply to rainfall totals much greater than 100 mm. Unfortunately this is unavoidable when seeking to estimate probable maximum floods (PMF's) for which the design rainfall may be as high as 400 mm. Clearly these relationships derived from common events are not easily extrapolated to extreme situations. In estimating PMF's it is necessary to consider the general philosophy behind the estimate which in the case of the FSR was a reasonable maximisation of all contributory factors. The absolute maximum for percentage runoff is 100% so it seems reasonable to limit percentage runoff to this value under the most extreme conditions likely to occur, say a rainfall of 400 mm on a catchment with a CWI of 200 mm and, if possible, to approach this limit asymptotically.

It is therefore recommended that the rainfall term in equation 4.10 be replaced by

$$0 \quad \text{for } P < 40 \text{ mm}$$

$$\text{and } 0.45(P-40)^{0.7} \quad \text{for } P > 40 \text{ mm}$$

This adjustment gives close agreement with the fitted equation (4.10) over the rainfall range 30 mm - 110 mm and yields 99.5% runoff from an event of 400 mm occurring on a soil type 5 catchment with CWI of 200 mm. This form of relationship will also alleviate problems of negative percentage runoffs estimated for small events on catchments with mainly type 1 soils. Although this is a most unlikely occurrence in design use it could happen in other applications and indeed should be expected in conditions where the percentage runoff is less than the standard error of estimate of the PR equation. Users who are concerned

about the arbitrary nature and dubious conception of this correction should remember that estimates of PR using the regression equation have a standard error of estimate of 15%.

The percentage runoff model can therefore be summarised by the equations

$$PR_{\text{rural}} = SPR + DPR_{\text{CWI}} + DPR_{\text{RAIN}} \quad 4.12$$

where

$$SPR = 10S1 + 30S2 + 37S3 + 47S4 + 53S5 \quad 4.9$$

$$DPR_{\text{CWI}} = 0.25 (CWI-125) \quad 4.13$$

$$DPR_{\text{RAIN}} = \begin{cases} 0.45(P-40)^{0.7} & \text{for } P > 40 \text{ mm} \\ 0 & \text{for } P \leq 40 \text{ mm} \end{cases} \quad 4.14$$

$$PR = PR_{\text{rural}} (1 - 0.3 \text{ URBAN}) + 21.0 \text{ URBAN} \quad 4.11$$

Figure 4.1 shows catchment average values of percentage runoff estimated using these equations plotted against the observed values.

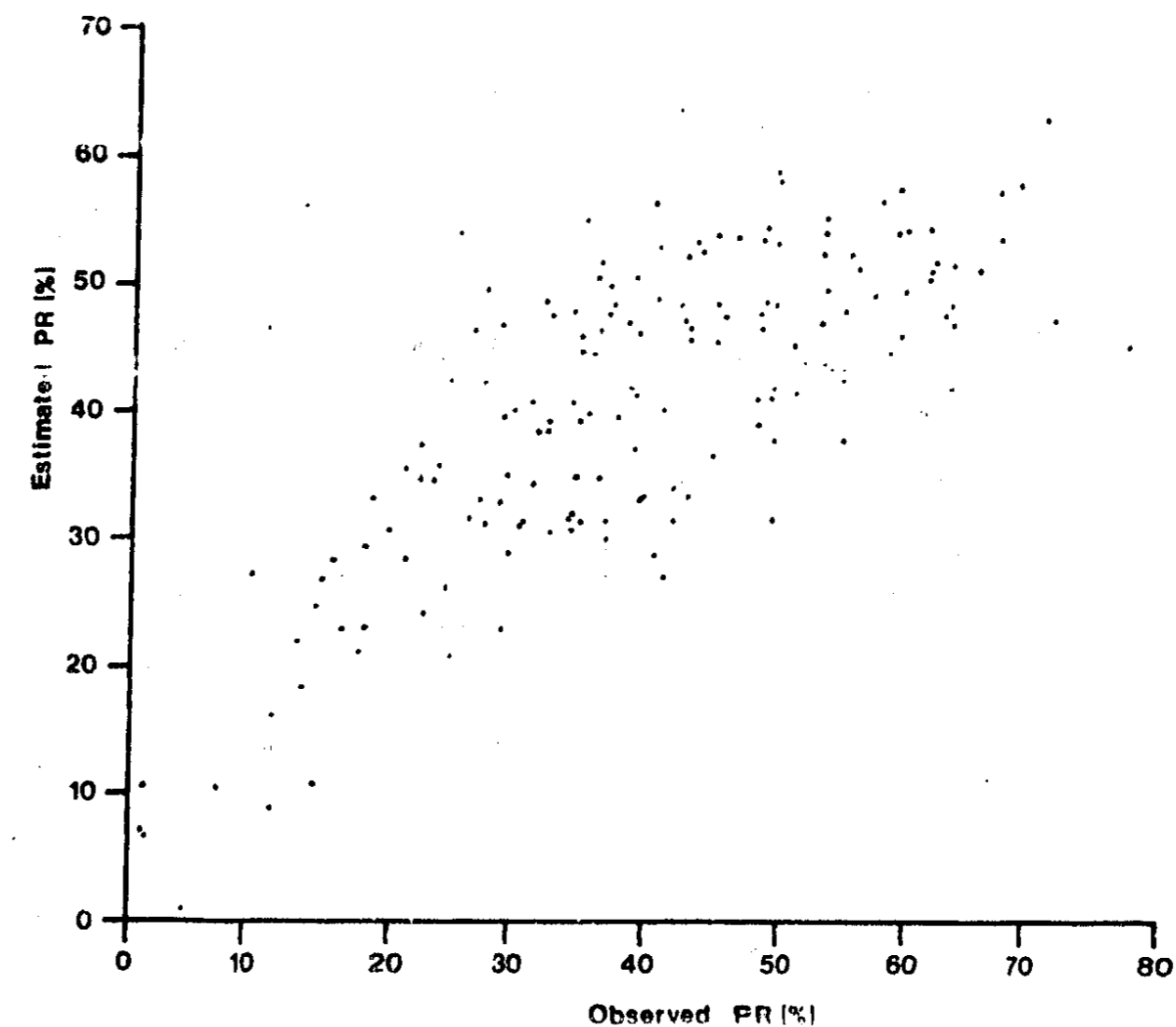


FIGURE 4.1 Catchment average values of estimated PR plotted against observed PR

It is possible to revise the estimates of percentage runoff obtained from the above equations by using data available at the site of interest.

If event data (ie flow and rainfall data at a short time period) are available in sufficient quantity then it may be possible to derive a relationship based on these data alone. More normally though it is only possible to replace the value of SPR obtained from the WRAP map. To do this requires the careful abstraction of the flow hydrograph and corresponding rainfall for at least five big flood events. The hydrograph should be separated as described in FSR 1.6.4.3 and the volume of quick response runoff calculated. PR is the ratio of quick response runoff to total rainfall expressed as a percentage. If the catchment contains an urban fraction, adjust PR to give PR_{rural} using equation 4.11 (otherwise PR_{rural} = PR). The dynamic adjustments are given by equations 4.13 and 4.14 and once calculated should be subtracted from PR_{rural} to give SPR. SPR's calculated from several events should be averaged and the resulting value becomes the new estimate of SPR for use in design flood estimation.

Many sites however may just have daily mean flow data; this can be used to refine a SPR estimate by using the base flow index (BFI) derived from these daily flows. The BFI is the ratio of base flow to total flow using a particular form of flow separation (Low Flow Studies, NERC) and is well correlated with SPR. Table 4.3 details a regression analysis which gives the equation

$$SPR = 72.0 - 66.5 BFI \quad 4.15$$

TABLE 4.3 SPR - BFI REGRESSIONS

Dependent variable : SPR						
Independent variable	Estimate	se	t	R ²	see	observations
1. All catchments						
BFI	- 64.24	4.47	14.36	0.56	9.4	166
Constant	71.03	2.18	32.54	-	-	-
2. All catchments weighted by number of available events						
BFI	- 66.49	4.28	15.55	0.59	8.97	166
Constant	72.05	2.10	34.38	-	-	-

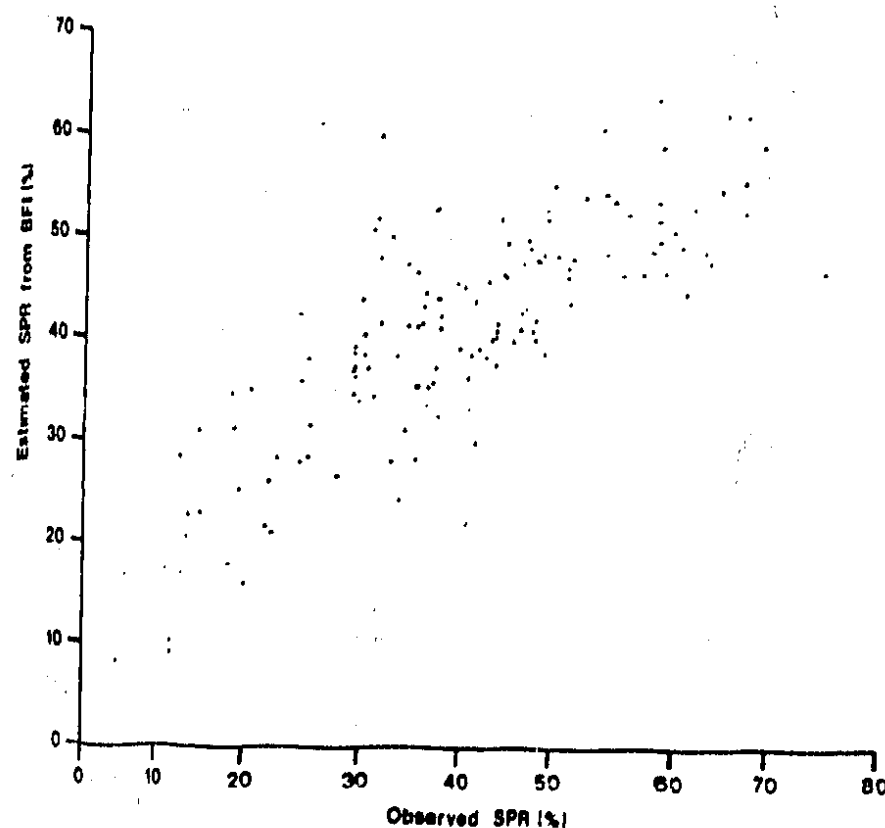


FIGURE 4.2
SPR estimated from BFI plotted against catchment average values calculated from event data

This equation should be used in preference to the soil equation (equation 4.9) as it is based on hydrological data at the site of interest but will yield inferior estimates to those obtained from event analysis. Figure 4.2 shows SPR's estimated using equation 4.15 plotted against observed values.

5 BASE FLOW ESTIMATION

The equations given in the previous two sections allow the response hydrograph to be estimated. The final step in the formulation of the design flood hydrograph is the addition of a certain flow to represent the flow in the river before the event started and to a lesser extent the start of slow response runoff from the event itself. This flow was labelled average non-separated flow (ANSF) by the FSR, a term that serves as a reminder that the hydrograph was separated as an expedient for analysis and does not represent a separation of flow generated by different runoff processes.

Regression analysis yields an equation for ANSF in terms of the variables CWI and SAAR

$$ANSF = (33(CWI-125) + 3.0 SAAR + 5.5) \times 10^{-5} \quad 5.1$$

where ANSF is the additional flow in cumecs/km² that should be added to each ordinate in the design flood. Details of the equation can be found in Table 5.1.

TABLE 5.1 THE ANSF REGRESSION

Dependent variable : ANSF						
Independent variable	Estimate	se	T	R ²	see	observations
CWI	0.000328	0.0000216	15.63	0.420	0.025	1851
SAAR	0.0000298	0.0000011	28.10	-	-	-
Constant	- 0.04059	0.002598	15.20	-	-	-

In the design situation CWI is determined directly from SAAR using Figure FSR 1.6.62. ANSF is therefore solely dependent on SAAR and the value obtained from the equation can be checked against the graphed relationship given in Fig. 5.1 which shows ANSF against SAAR.

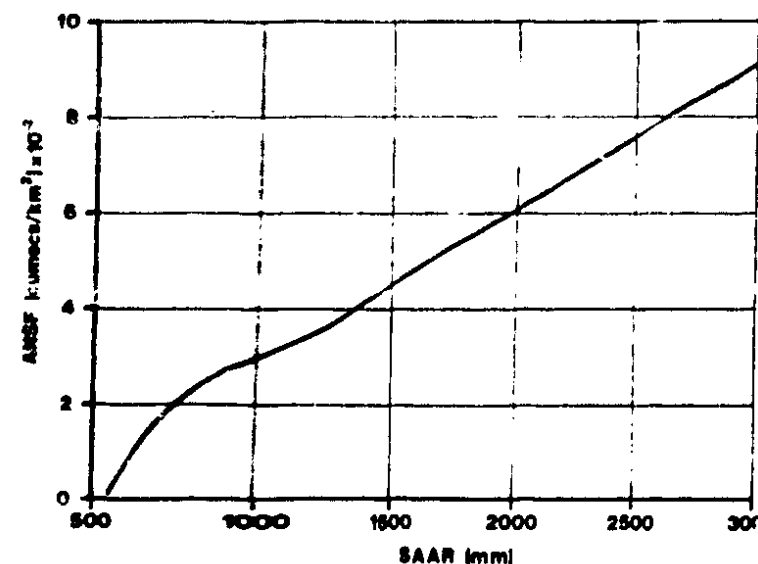


FIGURE 5.1
Graphical representation of ANSF-SAAR relationship for design use

6 ASSESSMENT OF PROCEDURES

Although a comparison of observed and estimated parameter values for catchments used in the regression studies is not a particularly rigorous assessment for the equations given in sections 3, 4 and 5, a list of observed average, maximum and minimum values together with their estimates is contained in Table 6.1. An asterisk in the table indicates that some events on the catchment have been used for volume analysis only.

TABLE 6.1 OBSERVED AND ESTIMATED PARAMETER VALUES

CATCHMENT	PERCENTAGE RUNOFF				TIME TO PEAK (H)			
	MEAN	OBSERVED MAX	MIN	ESTIMATED MEAN (FROM SOIL)	MEAN	OBSERVED MAX	MIN	ESTIMATED MEAN
19002	38.47	44.44	34.44	47.44	7.21	7.60	5.10	6.94
19003	71.72	44.53	49.20	30.01	5.13	6.50	4.00	6.89
21001	40.39	18.39	19.27	31.65	9.98	12.00	7.00	9.72
21030	46.58	26.64	35.30	35.52				
23002	50.15	20.35	50.45	42.45	5.25	6.40	6.00	6.82
23005	69.07	45.27	52.40	53.55	6.60	7.90	5.50	8.65
23006	40.74	40.74	54.97	52.49				
23010	55.12	31.37	53.15	54.98				
24003	50.58	42.19	54.46	50.31				
24005	44.01	15.36	46.71	37.39	7.16	9.80	4.70	8.93
24007	57.93	25.10	46.32	39.91	5.64	8.20	4.00	6.18
25003	51.47	25.00	51.35	35.99	3.99	4.00	2.00	2.67
25034	40.35	17.26	49.45	34.35	10.95	11.50	10.40	14.45
25026	53.91	40.34	53.59	55.29				
25011	46.77	46.77	52.77	57.74				
25012	65.00	59.63	51.22	56.99				
25810	55.20	43.02	47.05	48.34	2.20	2.65	1.75	3.25
27001	64.12	21.70	48.34	38.36	2.18	2.45	1.55	1.31
27010	34.18	34.18	32.38	21.26	9.53	10.20	8.20	13.81
27026	53.94	21.82	39.80	43.16				
27027	90.99	29.01	59.16	49.27	0.60	13.50	5.70	5.50
27031	59.40	25.47	41.85	47.34	7.90	10.20	6.50	9.25
27034	61.11	45.14	51.72	47.34	4.95	5.00	4.90	5.47
27035	55.30	23.30	44.48	51.07	7.70	7.70	7.70	9.10
27051	51.75	19.77	47.46	50.19	7.01	8.20	5.20	8.04
28016	27.11	22.03	17.21	26.61	3.44	3.80	3.10	3.09
28023	17.31	9.02	21.10	25.46	21.30	30.00	16.61	14.23
28026	59.05	41.48	46.49	39.04	0.71	12.50	7.50	6.34
28033	41.53	10.82	53.93	43.21	24.94	30.00	13.40	14.96
28041	45.14	29.07	53.79	46.92	2.56	2.95	1.85	2.94
28070	40.14	20.55	44.81	43.71				
29004	36.61	11.63	20.43	34.80	2.65	3.55	1.55	3.43
30001	37.64	17.07	31.14	28.69	8.12	10.20	5.80	12.84
30004	20.12	9.60	33.40	19.40	19.94	24.00	16.00	16.31
31005	54.17	27.66	43.40	40.14	9.34	11.60	5.00	11.13
31010	38.10	23.14	41.91	36.08	34.25	42.00	26.50	19.32
31021	14.61	7.04	30.59	26.14	14.10	14.10	14.10	10.54
31023	25.15	25.15	39.23	53.25				
32801	46.16	15.98	46.16	4.30	4.30	4.30	4.30	5.07
33014	13.20	7.27	22.11	4.53	4.53	6.35	2.75	6.02
33015	34.50	18.38	29.19	24.60	23.90	22.40	14.56	14.56
33029	11.11	1.11	10.54	19.31	33.20	13.00	18.13	13.00
33045	18.50	3.09	33.34	22.19	10.46	14.80	6.50	12.05
33809	54.17	30.61	37.71	51.33	18.45	22.80	15.20	9.82
34003	16.35	6.17	5.91	15.78	13.32	26.80	16.00	16.00
34005	23.00	18.44	35.90	29.17	23.90	18.50	9.90	13.78
34007	30.60	27.07	33.09	35.90				
34011	12.00	9.58	16.19	18.08				
35005	65.15	27.66	35.97	43.86	10.80	13.20	9.00	14.66
36008	43.01	21.92	33.36	44.27	11.14	16.20	7.00	10.92
37001	61.86	10.94	36.42	45.97	23.27	31.00	12.60	17.16
37003	33.00	3.24	21.67	34.24	33.13	39.00	26.50	17.56
37007	36.44	10.00	44.86	44.00				
37008	25.61	24.34	31.99	31.51	13.38	17.00	10.40	12.19

TABLE 6.1 OBSERVED AND ESTIMATED PARAMETER VALUES - Contd

CATCHMENT	PERCENTAGE RUNOFF				TIME TO PEAK (H)			
	MEAN	OBSERVED MAX	MIN	ESTIMATED MEAN (FROM SOIL)	MEAN	OBSERVED MAX	MIN	ESTIMATED MEAN
37331	23.92	33.96	12.31	44.12				
38003	1.10	1.53	0.87	7.25	-1.69	4.45	4.90	4.80
38007	37.57	65.23	9.58	30.46	39.97	3.67	5.75	2.25
39004	1.74	2.82	0.75	1.27	11.29	1.91	3.25	1.25
39005	19.34	33.91	12.90	30.73	19.55	3.21	5.85	1.95
39007	23.15	34.56	12.07	34.63	30.83	12.60	16.00	10.10
39017	53.66	80.96	0.32	43.29	59.64	9.31	11.30	6.50
39022	39.45	55.07	25.28	33.39	21.63	20.54	13.50	13.51
39025	24.50	50.38	7.96	42.57	37.30	15.00	17.90	10.78
39026	34.81	60.02	20.36	44.71	46.64	20.34	28.60	14.10
39036	3.37	3.37	3.37	9.61				
39052	27.46	39.68	6.49	42.12	43.10	5.53	8.60	3.90
39813	47.94	65.55	14.26	47.64	6.39	8.50	4.70	4.19
39814	39.96	58.01	21.14	41.33	1.89	2.35	1.25	2.31
39820	48.55	71.24	32.66	48.69	6.55	7.10	6.00	3.61
39830	13.89	19.57	8.73	18.40	3.21	4.05	2.35	2.45
39831	14.97	27.25	8.83	10.70	1.48	1.90	1.10	2.65
40004	66.15	68.44	63.87	47.79	19.15	19.20	19.10	12.21
40006	22.43	36.06	7.22	24.39	27.63	7.19	8.60	8.95
40007	45.16	62.75	25.43	42.56	42.54			
40008	36.52	54.98	25.64	31.51	36.76			
40009	43.09	61.01	14.90	45.59	41.18	8.77	14.20	5.10
40010	40.03	70.56	19.92	41.18	52.44	15.64	22.90	11.60
4005	45.69	64.55	25.11	47.45	40.59	17.32	21.40	14.10
4006	59.32	80.93	15.15	45.97	43.76	12.85	16.50	10.50
4007	77.20	84.70	44.24	44.31	14.20	14.50	14.50	12.21
4015	1.17	2.75	0.59	4.80	4.10	5.30	2.70	7.28
4021	53.13	67.43	39.18	43.72	60.05			
4022	49.30	63.57	42.74	37.79	47.78	7.24	12.00	4.00
4025	55.43	66.19	43.94	44.71	59.63			
4025	49.39	58.76	35.36	48.37	49.04	8.53	11.30	6.30
41801	36.05	76.64	14.47	40.65	41.18	3.73	5.60	2.20
43002	34.56	61.13	8.58	34.90	39.65	7.49	8.00	7.00
43003	41.17	59.15	17.49	27.05	35.14	11.65	15.20	9.50
43804	37.47	61.83	9.34	39.53	4.69	6.10	3.00	6.77
43805	21.94	40.32	7.78	34.59	5.59	7.10	4.40	6.67
43805	31.22	42.33	14.27	34.51	19.17	4.50	2.10	4.77
43805	39.53	55.34	21.82	54.22	47.62	3.72	5.60	3.37
43802	17.30	76.44	55.17	57.17	51.70	2.64	3.95	2.64
46805	49.42	53.92	44.83	58.00	2.08	2.45	1.65	1.87
47007	31.69	57.95	17.54	38.43	5.25	6.20	4.20	4.60
47028	29.34	59.12	5.92	40.08	46.55			
47011	28.99	54.17	10.95	39.48	38.86	5.75	7.90	3.90
48004	34.08	51.12	15.31	47.85	24.72	7.39	9.80	4.06
48005	10.25	20.00	3.77	27.25	26.00	4.37	5.10	4.25
48005	37.09	50.66	27.20	48.29	32.32	10.24	11.30	9.50
48005	48.07	74.84	16.01	53.47	40.22	5.61	7.70	3.50
51002	15.22	13.85	9.12	26.81	29.96	4.56	6.00	3.52
52004	38.89	50.80	15.57	36.44	37.19	6.69	9.00	7.89
52005	34.80	56.66	14.30	31.28	32.90	9.73	11.00	8.30
52006	34.17	49.69	18.65	31.73	47.97	11.36	14.00	7.77
52010	48.11	70.73	35.14	38.97	41.41	10.73	11.40	10.00
52016	8.30	14.45	1.86	33.92	16.99	4.31	6.50	4.23
52020	47.40	82.22	59.82	42.38	56.97	3.97	3.70	3.20
53005	18.00	28.57	3.54	23.14	30.78	9.88	16.10	9.37
53007	28.82	49.07	19.04	32.91	36.28	10.58	14.00	11.20
53008	30.49	58.25	19.51	31.18	36.10			
53009	16.51	24.17	7.49	23.06	32.77	7.80	9.50	5.98
54004	42.68	55.85	17.52	47.07	36.32	12.42	15.00	9.25
54006	20.74	29.15	15.79	28.50	21.23	23.97	26.20	21.00
54010	41.07	44.80	38.61	40.15	37.01	21.30	21.30	17.84
54011	34.22	65.12	12.24	30.76	27.73	12.92	16.50	10.34
54019	40.44	51.65	22.10	28.79	38.59	42.75	46.50	17.93
54020	21.99	28.83	16.64	37.40	25.36			
54022	40.04	57.87	10.51	56.35	54.06	2.35	3.95	1.75
54034	26.47	46.07	6.56	35.44	35.18			
54090	53.76	77.68	13.69	54.11	54.49	1.39	2.03	0.88
55008	49.25	61.70	33.89	58.52	57.04	2.18	2.75	1.65
55012	54.62	59.59	48.27	42.43	49.09	4.12	9.00	4.43
55041	16.09	15.94	15.84	28.87	24.98	22.40	30.50	8.00
55022	49.15	58.18	43.08	31.58	43.26	12.80	15.00	7.00
55025	30.63	39.90	24.37	31.32	35.15	5.87	6.70	5.10
55026	49.24	62.43	33.65	41.78	52.11	5.80	6.50	5.10
55034	58.82	72.68	41.65	57.39	57.77	1.54	2.13	1.08
56002	24.02	28.94	18.15	46.05	46.05	6.00	6.00	6.00
56003	26.23	40.65	9.83	31.49	34.72	3.53	4.20	3.00
56004	7.99	30.54	12.45	41.06	42.26	7.70	7.60	5.23

TABLE 6.1 OBSERVED AND ESTIMATED PARAMETER VALUES - Contd

CATCHMENT	PERCENTAGE RUNOFF				TIME TO PEAK (H)			
	MEAN	OBSERVED MAX	MIN	ESTIMATED MEAN (FROM SOIL)	MEAN	OBSERVED MAX	MIN	ESTIMATED MEAN
56005	34.77	49.80	22.02	45.96	5.25	7.30	4.10	4.04
56006	50.84	73.89	19.16	45.11	47.04	4.56	6.00	3.50
56011	30.28	40.20	23.92	42.72	33.25	6.58	10.50	4.00
57004	40.56	59.34	25.40	52.92	48.42	6.32	9.40	4.60
57005	46.51	52.32	29.56	53.60	46.80	6.13	5.20	4.50
57006	43.70	68.71	16.44	53.35	51.48	4.75	4.40	1.70
58001	36.87	46.26	20.59	49.87	47.75	4.43	6.50	3.30
58002	36.58	51.30	25.78	57.47	56.77	4.87	7.40	3.40
58003	36.64	51.77	26.49	29.99	34.28	6.51	9.00	3.80
58006	44.06	62.10	27.61	52.58	48.83	3.82	5.20	2.80
58005	55.82	71.96	34.21	51.17	46.70	4.57	4.50	3.44
58009	72.11	80.00	40.00	49.00	36.64	3.32	6.40	4.50
60002	51.56	60.56	39.09	43.87	47.84	6.95	9.00	4.40
60003	44.51	60.45	32.97	32.97	33.31	6.30	14.00	14.00
60006	29.19	40.19	29.19	33.70	44.34	3.05	3.50	2.60
61001	56.29	60.74	49.55	57.77	51.39	9.80	9.80	4.30
61003	27.13	33.05	12.61	33.07	30.23	7.09	9.80	9.20
62002	41.96	53.64	26.48	31.44	34.54	5.45	6.30	4.00
64001	59.35	60.37	54.70	42.09	47.52	4.86	4.00	3.67
65001	41.84	50.85	47.51	47.87	54.50	4.26	5.35	4.00
65801	59.05	60.03	30.17	63.64	62.68	4.19	6.20	2.40
66002	15.86	19.75	45.06	60.11	3.73	6.70	2.70	1.69
66004	4.35	10.58	10.47	27.24	36.76	4.57	7.40	1.80
66006	41.80	49.46	2.74	1.14	0.48	3.85	5.10	2.60
67011	63.40	60.28	23.59	32.19	38.43	6.73	9.30	4.40
67005	63.17	60.03	26.99	41.00	57.22	4.22	5.20	2.70
67008	28.40	40.12	41.00	41.91	39.51	5.28	6.80	4.38
68006	18.00	40.47	25.51	46.59	44.56	5.40	5.80	5.00
68010	45.18	50.37	19.84	29.42	34.37	7.06	9.80	6.00
68010	51.17	50.17	31.98	51.17	45.49	5.63	6.20	4.80
68008	43.05	40.76	24.93	48.80	42.36	4.00	4.00	7.07
69004	26.18	30.22	4.67	45.59	4.67	4.00	6.15	4.16
69011	32.13	30.04	29.21	23.04	23.04	9.00	10.00	6.54
69012	53.84	40.07	41.22	46.55	46.55	4.75	4.90	6.36
69013	14.83	10.02	27.17	27.17	4.80	4.80	4.60	4.56
69018	52.51	40.00	24.00	24.00	3.50	3.50	4.10	5.47
69019	14.00	10.00	25.00	25.00	4.00	4.00	4.00	4.00
69027	31.04	20.23	40.68	40.68	2.40	2.90	1.70	3.37
69031	46.55	33.43	44.05	44.05	7.44	9.00	5.90	5.84
69034	36.07	7.13	51.81	51.81	5.19	6.10	4.10	5.54
69802	56.47	46.58	53.79	53.79	1.84	4.13	1.17	2.07
70006	29.44	10.16	35.03	35.03	3.80	4.60	3.00	3.00
71003	57.47	26.72	56.41	51.61	3.86	4.60	2.00	5.73
71004	33.21	21.39	46.96	44.44	2.97	3.75	1.65	2.66
71802	38.84	14.35	50.50	46.96	5.16	6.40	4.40	7.23
71904	69.02	57.20	57.20	57.20	4.74	5.30	3.90	5.35
72002	34.95	19.53	55.03	59.24	7.22	8.60	6.20	7.53
72006	61.52	44.15	51.02	51.02	2.07	2.55	1.75	3.02
72518	61.45	47.59	54.46	54.46	5.69	7.00	4.40	7.23
72820	26.52	18.52	46.39	46.39	6.44	7.90	5.30	8.65
73005	32.10	6.51	48.61	48.19	2.23	8.80	4.40	6.74
73007	42.85	10.09	47.65	43.21	6.19	4.65	0.95	1.35
73008	31.39	26.60	52.17	47.65	6.19	7.20	4.00	5.34
73803	65.25	21.59	34.31	41.55	3.88	4.30	3.60	3.28
73804	71.15	51.22	37.73	37.73	4.80	5.80	4.20	6.33
74001	65.56	57.62	62.84	62.84	9.90	9.90	9.90	4.40
75006	71.84	43.08	51.14	51.14	7.44	9.60	5.50	4.21
75007	51.23	54.43	47.17	47.17	3.80	3.80	2.90	3.09
76005	65.87	39.79	41.49	55.16	3.93	5.00	2.90	3.86
76008	58.62	65.87	52.13	46.87	3.86	4.60	3.00	3.86
76011	67.42	52.45	50.42	54.31	6.25	7.00	5.50	9.81
76014	63.21	13.93	53.52	62.21	2.59	4.75	1.45	3.14
76805	53.10	32.97	49.43	51.64	3.84	5.10	2.90	4.75
77002	55.11	4.45	53.97	54.82	1.87	4.05	0.85	3.48
83002	58.48	31.14	52.13	51.94	5.40	6.30	4.60	9.19
84002	63.57	58.63	55.09	61.16	4.00	4.00	4.00	4.00
84009	59.47	56.71	56.07	56.07	2.93	3.40	2.50	2.74
84012	61.30	33.63	49.36	55.45	1.87	4.45	3.25	3.62
84022	33.03	42.19	30.44	35.70	6.08	7.30	5.20	5.38
		16.15	47.15	43.91	3.38	4.35	2.75	7.36

A more meaningful assessment is summarised in Table 6.2 which gives observed and estimated Tp's and PR's on an event basis for the test data set. This table also lists estimated and observed peak flows for each event and a volume ratio expressing the volume of the estimated hydrograph as a percentage of the observed volume over the duration of the estimated response hydrograph. For one event on each catchment the observed and estimated hydrographs are plotted in Figures 6.1(a)-(f).

It is difficult to give a concise and meaningful summary of the results presented in Table 6.2. Of the 42 peaks from events classified as good quality, 16 (38%) are estimated to within 25% and 27 (64%) to within 50%; of these peaks 18 are underestimated and 24 overestimated. These overall figures hide systematic variations that exist on individual catchments which are worth looking at in more detail.

TABLE 6.2 COMPARISON OF OBSERVED AND ESTIMATED FEATURES ON SIX TEST CATCHMENTS

All estimates are based solely on catchment characteristics

Event	Unit hydrograph, Tp		% runoff		Peak flow		% vol
	Obs	Est	Obs	Est	Obs	Est	
19001							
7	7.8	7.99	56.5	50.34	149.4	152.2	102.7
8	6.0		45.3	48.92	106.3	108.7	117.0
9	7.1		54.8	49.98	113.9	76.1	103.6
10	5.6		51.7	52.59	130.3	146.8	103.4
11	8.3		58.7	48.98	169.8	145.8	100.8
29001							
2	5.6	11.56	2.7	17.28	1.25	7.23	676.5
4	11.6		2.5	4.75	1.47	2.91	183.0
5	5.7		3.3	18.32	2.51	12.61	507.4
6	5.1		1.7	14.90	0.81	6.77	914.8
7	12.0		2.4	17.50	1.13	6.78	605.7
8	-		1.0	3.76	1.09	3.69	296.6
9	5.0		3.3	21.40	3.70	20.53	484.1
10	5.2		1.9	11.59	3.96	12.54	610.8
11	-		1.8	0.23	1.28	0.15	11.0
39012							
1	3.0	4.62	15.7	19.78	15.81	17.91	112.2
3	-		23.4	40.52	14.66	18.60	145.8
4	4.2		14.7	38.07	11.3	23.39	234.9
5	-		8.7	27.01	10.13	19.35	230.5
6	-		11.7	21.86	13.11	17.79	136.8
7	4.0		24.2	39.56	12.23	23.45	168.2
8	3.9		9.7	24.62	11.18	17.80	186.7
9	-		21.5	38.02	14.07	21.25	167.7
10	5.3		20.5	333.27	22.70	52.21	151.3
11	4.5		9.8	12.44	9.5	9.42	117.5
12	-		12.3	22.51	11.98	14.55	150.3
45004							
1	9.7	10.24	34.3	29.18	62.95	53.09	94.3
2	10.3		17.3	19.25	42.02	45.54	135.2
3	12.2		43.4	20.23	60.66	30.90	52.8
4	6.8		42.4	27.96	59.60	49.16	87.8

5	10.4		50.6	20.75	71.61	37.01	56.3
6	10.0		34.9	25.45	44.22	32.82	116.7
7	9.0		39.2	27.76	47.58	35.43	106.4
8	8.0		45.7	29.81	64.65	44.52	80.6
9	-		67.2	32.88	73.00	38.05	63.0
10	5.3		45.8	29.14	71.02	45.44	75.1
11	10.8		42.1	29.34	60.59	41.67	81.3
12	7.0		44.1	30.46	78.35	49.66	75.8
13	-		14.4	3.54	73.34	11.18	23.5
14	-		37.9	20.20	217.91	52.01	61.2
15	-		51.8	33.91	89.32	59.56	72.6
54016							
1	22.5	19.97	25.2	28.58	10.16	15.52	158.4
2	-		25.2	27.51	7.42	13.97	198.6
3	30.5		24.6	16.52	11.32	12.42	94.2
5	23.5		13.6	17.82	6.98	12.93	169.9
8	-		27.8	27.24	10.02	16.42	153.8
9	24.5		19.1	17.91	10.27	16.20	119.1
12	-		23.8	30.28	11.31	19.08	152.9
67010							
1	3.3	3.53	63.7	53.44	11.46	10.65	99.7
2	2.8		46.3	54.83	12.61	16.96	122.6
3	4.4		46.9	53.75	11.87	11.63	123.8
4	3.8		46.1	56.42	11.16	14.44	137.8
5	1.7		45.7	57.77	18.02	17.24	129.6
6	3.8		60.0	58.06	11.74	9.40	106.9
7	2.7		46.8	56.71	13.60	17.47	125.0
8	-		62.6	61.28	12.30	17.34	105.5
9	2.7		59.5	58.30	14.52	15.27	100.4
11	-		58.7	59.24	15.01	14.15	120.8
13	-		45.4	55.96	10.53	12.97	154.5
14	2.6		64.5	55.83	11.29	11.20	87.0

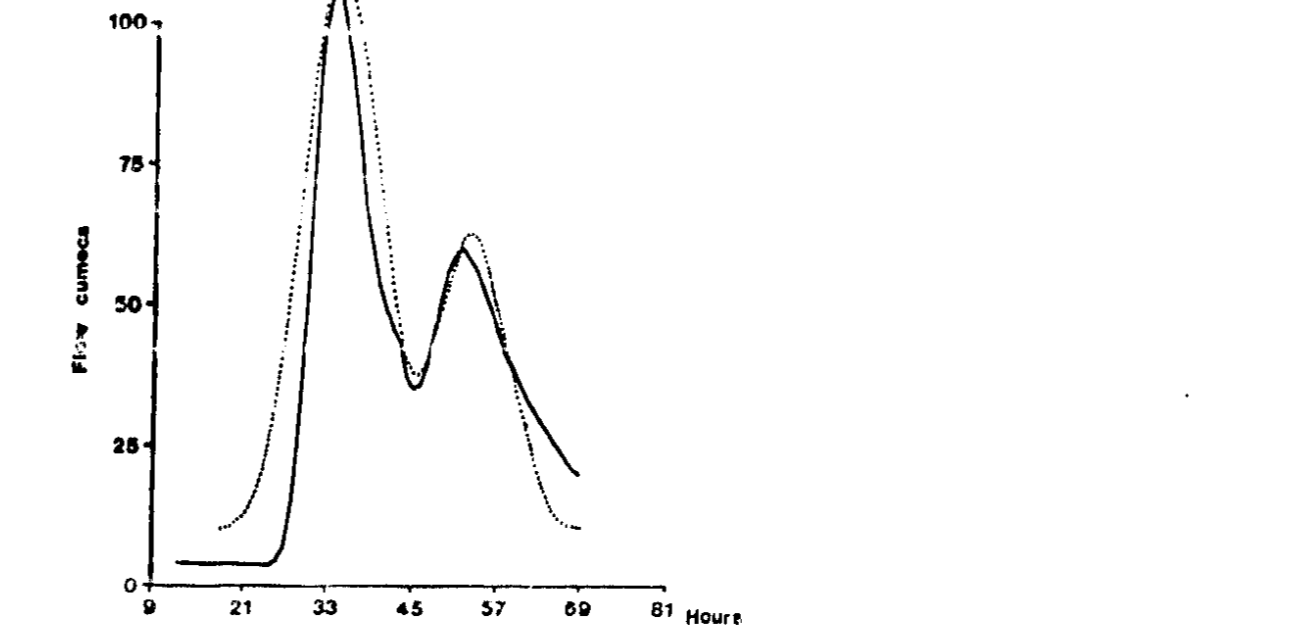
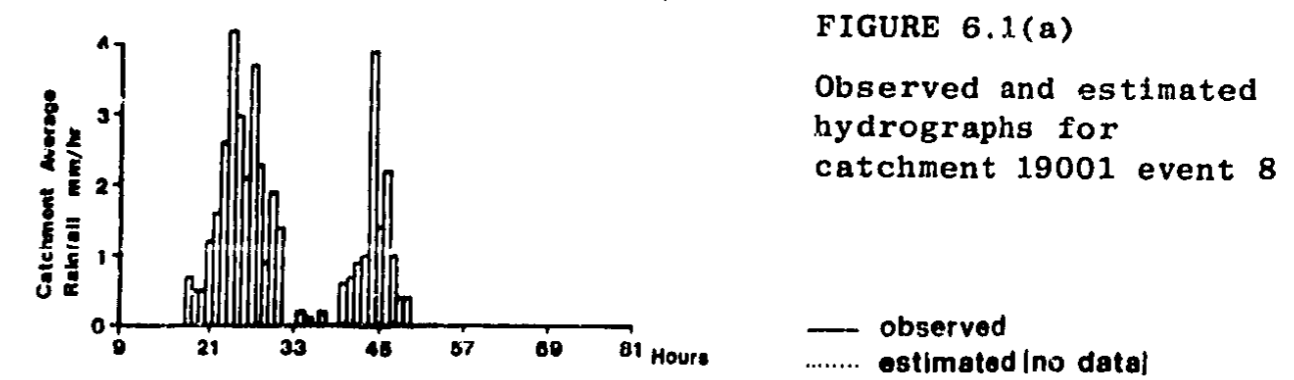
19001 Almond at Craigie Hall

The model equations have performed remarkably well on this catchment. The event plotted in Figure 6.1(a) illustrates an event where the peak has been estimated very closely although there is an overestimation of runoff volume by 17%, an error partly explained by the shorter duration of the estimated response hydrograph and an overestimate of ANSF.

29001 Waithe Beck at Brigsley

With the exception of just one event all peaks have been grossly overestimated. Observed percentage runoffs are in the range 1.0 to 3.3% yet the catchment located mainly on type 1 soils is assigned a modelled SPR of 19%. Observed values of T_p are from 5.1 to 12.0 hours with the estimated value at the top of this range. Event 2 in Figure 6.1(b) shows the overestimation typical of events on this catchment. In trying to improve the estimate by using all the other events (ie 8 events) as available data an 'observed' value of SPR can

values. A similar procedure could be applied to the estimation of ANSF. Figure 6.1(b) illustrates the estimated hydrographs when these expedients have been adopted.



39012 Hogsmill at Kington-upon-Thames

On this catchment, with an urban fraction of about 0.5, peak flows are again overestimated. The illustrated event (Figure 6.1(c)) is one of the worst on the catchment. Refining the estimate of SPR using the other event data gives 19%, considerably less than the 34% from the soil map, and in good agreement with the value obtained from using BFI of 17%. The timing of the peak and duration of the response flow are good. Although catchments with a larger urban fraction are included in the calibration data set, the method is not recommended for application in such conditions.

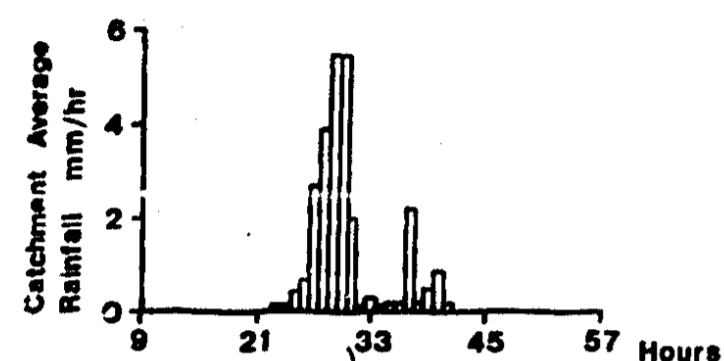
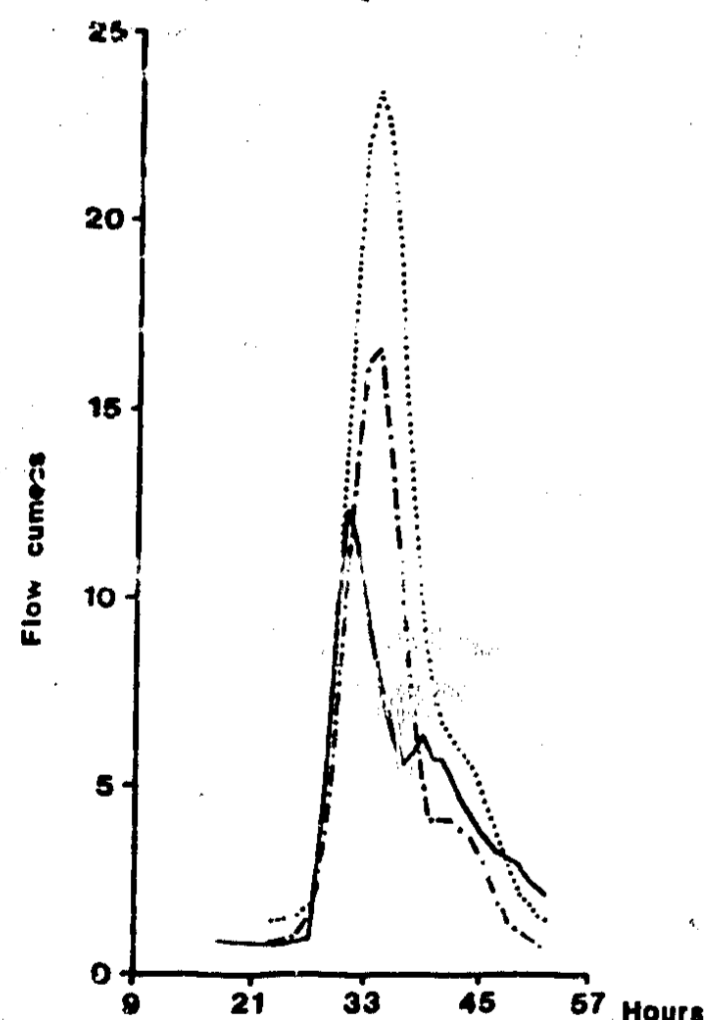


FIGURE 6.1(c)

Observed and estimated hydrographs for catchment 39012 event 7

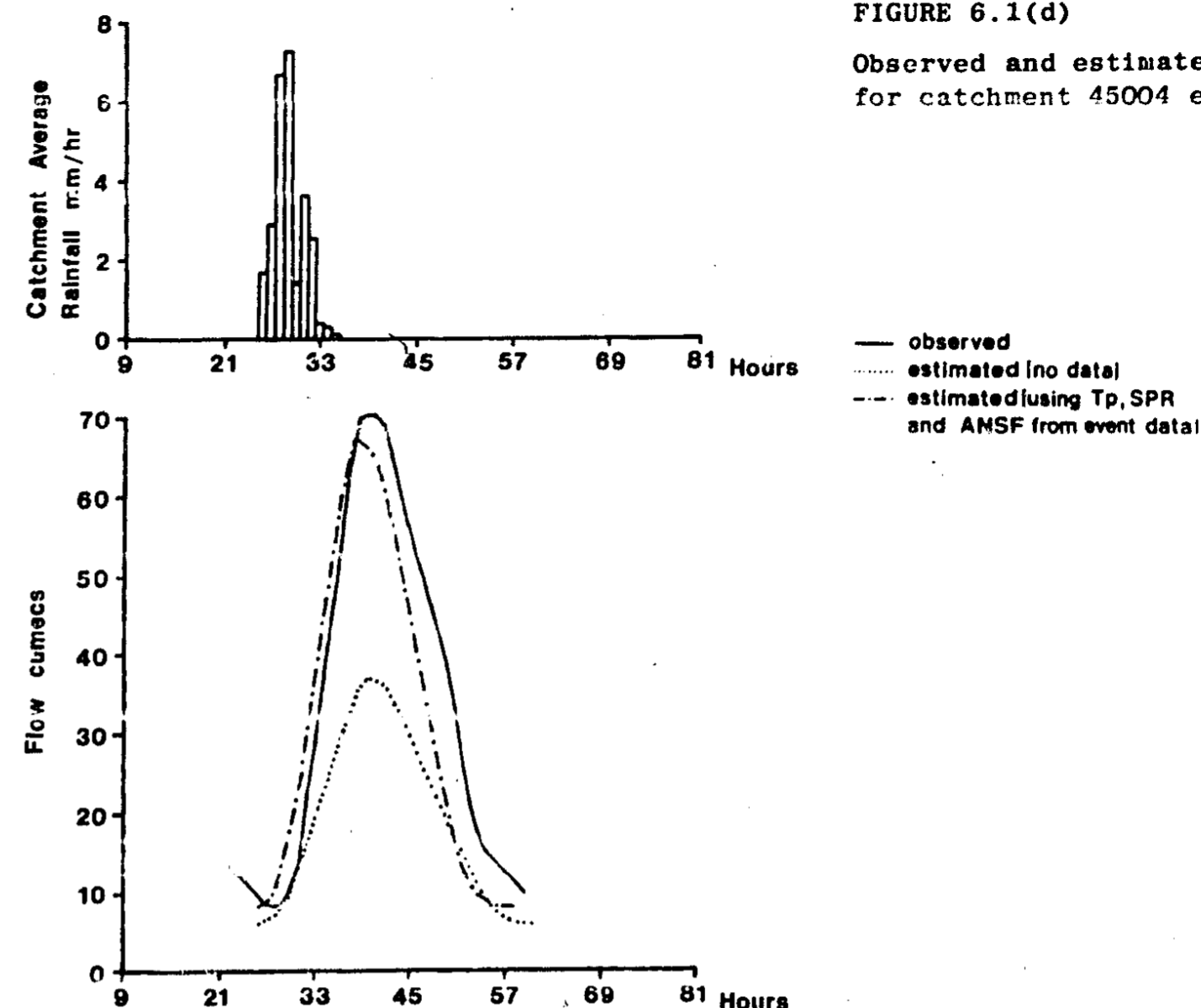
— observed
 estimated (no data)
 - - - estimated (using T_p , SPR and ANSF from event data)

45004 Axe at Whitford

This is the only catchment in the test data set on which peaks are consistently underestimated, Figure 6.1(d) showing one of the poorer examples. Again, using local data, the SPR from soil of 27% can be replaced by 41% from event data or 39% using BFI and a dramatic improvement in the example event is seen.

FIGURE 6.1(d)

Observed and estimated hydrographs for catchment 45004 event 5



— observed
 estimated (no data)
 - - - estimated (using T_p , SPR and ANSF from event data)

54016 Roden at Kodington

The event shown in Figure 6.1(e) shows that the problems encountered on this catchment are rather different. Percentage runoff is estimated quite well (SPR 28% from soil, 31% from BFI and 27% using event data) but there is a considerable baseflow error and the response hydrograph shape is rather symmetrical and hence of shorter duration than that observed. With only three other events for which a unit hydrograph was derivable it is not possible in this case to replace the triangular unit hydrograph with one derived from local data. Boorman and Reed (1981) assess methods of deriving an average unit hydrograph suitable for use in this context. The observed ANSF's can be averaged to give a value to replace the one obtained from the equation. The effect this has on event 2 is shown in the figure.

67010 Gelyn at Cynefall

On this catchment the 'no data' equations have performed reasonably well with an equal number of events over and under estimated. In the example of Figure 6.1(f) the response flow is seen to start too early, to be too great early in the event, and to end more quickly than is observed. On this event the constant proportional loss model is not working well although the main peak is estimated reasonably.

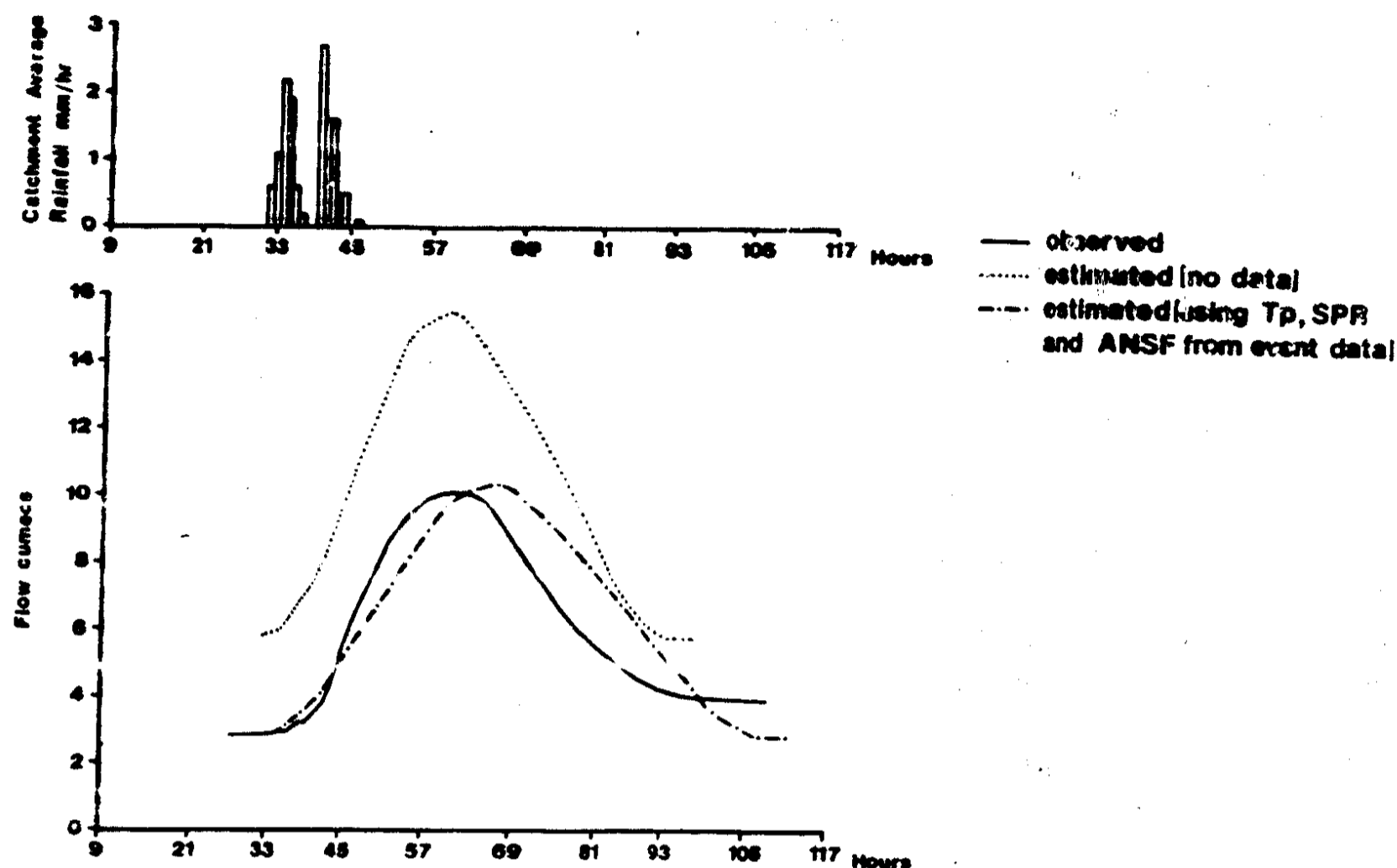


FIGURE 6.1(c) Observed and estimated hydrographs for catchment 54016 event 1

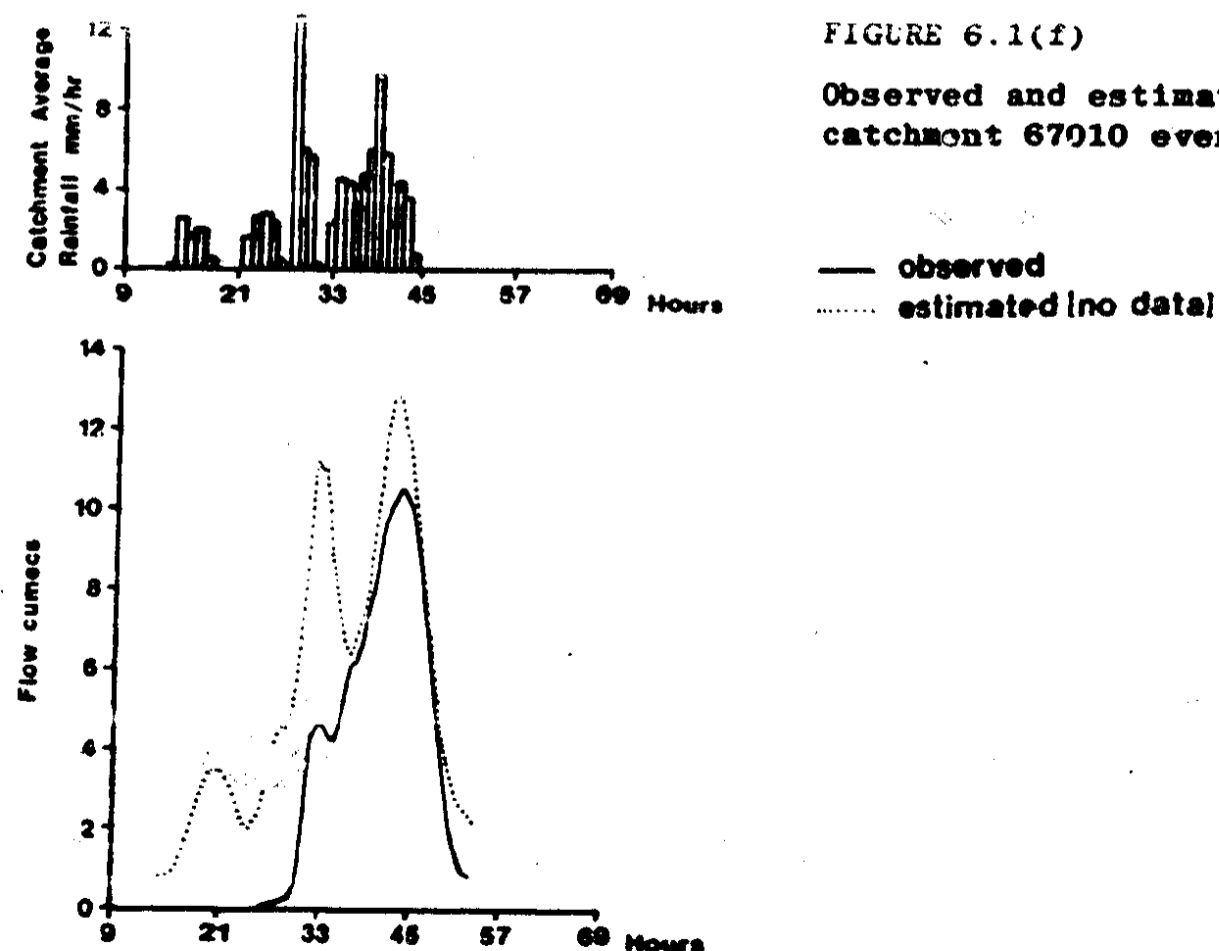


FIGURE 6.1(f)
Observed and estimated hydrographs for catchment 67010 event 13

Summary

The results presented in Table 6.2 represent a severe test of the flood estimation procedure as they are based solely on catchment characteristics. The use of local data to replace regression equation estimates of model parameters has been demonstrated to give a great improvement in the accuracy of the estimations on the six test catchments. A typical application in the United Kingdom will be able to draw on some local data either at the site of interest or from a nearby gauging station. Several types of data can prove beneficial in reducing errors; event data of the type collected for this study are obviously of most use as they can yield both timing and volume of runoff information. Daily mean flows assist in estimating response volumes. The applications given for the test data have revealed many of the problems that may be expected in genuine applications. However, while these problems are revealed in the examples, they will normally remain hidden. The hydrologist or engineer making a flood estimate must remember the uncertainties involved and take steps appropriate to the application to improve the estimate. Applications where errors are likely to be greater include catchments containing significant urbanisation or a large proportion of highly permeable soils.

7 CONCLUSION AND SUMMARY OF RECOMMENDED EQUATIONS

Since the publication of the FSR a considerable amount of new event data has been collected and analysed in line with the procedures of the FSR. The whole data set has been reviewed applying criteria that were more rigorous than those used originally. In addition to the event data review, catchment characteristics were also checked and updated where new maps defining relevant variables had been produced. With the aid of a new computer database system, the Flood Event Data Archive, these data, and key parameters derived from event analyses, are stored in a well organised and easily accessible form. The data set is generally larger than the one available to the Flood Studies team containing many more events from more catchments; it does however have slightly fewer events for which unit hydrographs could be derived.

In the derivation of new model parameter estimation equations consideration has been given to easing problems encountered in characteristic abstraction and application under extreme conditions. The new equations, presented in summary form in the following section, do not represent a major improvement in the standard of flood estimation procedures for ungauged sites. They do however offer a consolidated set of guidelines based on material previously published in a variety of sources (eg FSR, FSSR's). The relatively minor changes that have been introduced are recommended on the basis of an enhanced (and better validated) data set and because of the reviewed choice of dependent and independent variables to assist application. That the FSR parameter estimation equations are not found seriously deficient is a particularly pleasing, and, for all FSR users, a reassuring aspect of this review.

Looking to the future, the most needed enhancement in rainfall-runoff modelling for flood estimation is better definition of runoff volumes. A new soil map containing more classes and at a larger scale is on the horizon and promises the most significant improvement within the framework of the current design package.

SUMMARY OF RECOMMENDED MODEL PARAMETER ESTIMATION EQUATIONS

Summary of Recommended Model Parameter Estimation Equations

Unit Hydrograph Parameters

$$T_p(o) = 283 S^{1085^{-0.33}} (1+URBAN)^{-2.2} SAAR^{-0.54} MSL^{0.23} \text{ (hours)}$$

$$T_p(T) = T_p(o) + T/2 \text{ (hours)}$$

$$Q_p = 220/T_p \text{ (cumecs per 100 sq km)}$$

Percentage Runoff

$$PR_{rural} = SPR + DPR_{CWI} + DPR_{RAIN}(\%)$$

where

$$SPR = 10S_1 + 30S_2 + 37S_3 + 47S_4 + 53S_5 \text{ (\%)}$$

$$DPR_{CWI} = 0.25 (CWI-125) \text{ (\%)}$$

$$DPR_{RAIN} = 0.45 (P-40)^{0.7} \text{ (\%)} \text{ for } P > 40 \text{ mm}$$

$$= 0 \text{ for } P < 40 \text{ mm}$$

$$PR = PR_{rural} (1.0 - 0.3 URBAN) + 21.0 URBAN \text{ (\%)}$$

If mean daily flow data available to calculate BFI

$$SPR = 72.0 - 66.5 BFI \text{ (\%)}$$

Base Flow

$$ANSF = (33(CWI - 125) + 3.0 SAAR + 5.5) \times 10^{-5} \text{ (cumecs/sq km)}$$

Acknowledgement

This work was carried out as part of a research project funded by the River Flood Protection Commission of the Ministry of Agriculture, Fisheries and Food.

The collection, analysis and validation of the data were carried out by a great many members, both past and present, of the catchment response group of the Applied Hydrology section of the Institute of Hydrology. Dr M J Lowing and Dr D W Reed have provided invaluable assistance in the interpretation of analyses and preparation of the report.

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APPENDIX A

CATCHMENT AND EVENT DATA

TABLE A.1 CATCHMENT CHARACTERISTICS FOR BASINS USED IN THE STUDY

NUMBER	NAME	AREA	MSL	ST025	S442	SOIL1	SOIL2	SOIL3	SOIL4	SOIL5	UPSWN	LAKE	RFI
19001	ALMOND AT CRAIGIE HALL	369.00	42.00	S 11	914	0.	0.	0.	0.80	0.20	0.11	0.04	0.384
19002	ALMOND AT ALMOND WEIR	43.90	17.00	S 11	1052	0.	0.	0.	1.00	0.	0.07	0.	0.344
19005	ALMOND AT ALMONDELL	229.00	25.20	S 11	768	0.	0.	0.	0.64	0.36	0.10	0.07	0.343
20001	TYNE AT EAST LINTON	307.00	31.90	S 11	759	0.05	0.	0.22	0.72	0.02	0.12	0.02	0.543
21030	MEGGET AT HENDERLAND	56.20	12.40	T 11	1524	0.	0.	0.51	0.	0.49	0.	0.	0.405
23002	DERWENT AT EDDY'S BRIDGE	119.00	21.40	T 11	932	0.	0.	0.	0.20	0.80	0.	0.	0.428
23005	NORTH TYNE AT FARTSET	285.00	36.30	T 11	1255	0.	0.	0.	0.	1.00	0.	0.	0.228
23006	SOUTH TYNE AT FEATHERSTONE	321.90	32.70	T 11	1357	0.	0.	0.	0.	1.00	0.	0.07	0.321
23010	TARSET BURN AT GREENHAUGH	96.00	15.25	T 11	1035	0.	0.	0.	0.	1.00	0.	0.	0.258
24003	WEAR AT STANHOPE	171.90	21.81	T 11	1318	0.	0.	0.	0.02	0.98	0.	0.10	0.350
24005	BROWNEY AT BURN HALL	178.45	31.71	T 11	770	0.	0.	0.	0.99	0.01	0.05	0.	0.535
24007	BROWNEY AT LANCHESTER	44.50	11.90	T 11	768	0.	0.	0.	0.93	0.07	0.	0.	0.448
25003	TROUTBECK AT MOOR HOUSE	11.40	3.07	T 11	2182	0.	0.	0.	0.	1.00	0.	0.	0.152
25004	SKERNE AT SOUTH PARK	250.19	44.20	T 11	671	0.	0.	0.	1.00	0.	0.08	0.	0.533
25006	GRETA AT RUTHERFORD BRIDGE	86.10	17.89	T 11	1179	0.	0.	0.	0.	1.00	0.	0.	0.215
25011	LANGDON BECK AT LANGDON	13.00	5.21	T 11	1621	0.	0.	0.	0.	1.00	0.	0.	0.211
25012	MARWOOD BECK AT MARWOOD	26.10	6.28	T 11	1440	0.	0.	0.	0.	1.00	0.	0.	0.211
25019	STAE WEIR AT MOOR HOUSE	0.04	0.16	T 11	2182	0.	0.	0.	0.	1.00	0.	0.	0.152
27001	MIDD AT MUNSINGORE WEIR	484.30	34.64	T 11	993	0.01	0.	0.	0.69	0.30	0.02	0.25	0.506
27010	MOGGE BECK AT BRANSDALE WEIR	19.90	8.41	T 11	1057	0.	0.	0.	0.40	0.60	0.	0.	0.489
27026	ROTHER AT WHITTINGTON	165.00	15.33	T 11	900	0.03	0.	0.70	0.15	0.86	0.07	0.07	0.454
27027	WARPE AT ILKLEY	443.00	55.10	T 11	1382	0.	0.	0.	0.13	0.88	0.	0.09	0.378
27031	COLNE AT COLNE BRIDGE	245.00	23.65	T 11	1107	0.	0.46	0.	0.22	0.31	0.11	0.20	0.397
27034	URE AT KILGRAM BRIDGE	510.20	30.10	T 11	1429	0.	0.01	0.	0.42	0.55	0.01	0.01	0.345
27035	AIRE AT KILDWICK BRIDGE	282.30	11.70	T 11	1100	0.	0.	0.	0.53	0.47	0.02	0.13	0.422
27051	CRIMPLE BECK AT BURN BRIDGE	3.10	3.75	T 11	331	0.	0.	0.	1.00	0.	0.	0.	0.335
28016	RYTON AT SERLEY PARK	237.11	35.60	T 11	631	0.84	0.	0.	0.16	0.	0.04	0.	0.492
28023	WYE AT ASHFORD	154.00	26.41	T 11	1200	0.20	0.	0.	0.	0.20	0.02	0.	0.735
28026	ANKER AT POLESWORTH	368.00	34.10	T 11	697	0.	0.	0.02	0.98	0.	0.07	0.	0.495
28033	DOVE AT HOLLINSCLOUGH	8.05	3.90	T 11	1392	0.	0.	0.	0.	1.00	0.	0.	0.447
28041	HAMPS AT WATERHOUSES	35.13	14.42	T 11	1064	0.	0.	0.	0.	1.00	0.	0.	0.389
28070	SURPAGE BROOK AT SURPAGE	7.10	1.24	T 11	965	0.	0.10	0.	0.	0.90	0.	0.	0.397
29001	WATHE BECK AT BRIGGSLEY	108.30	20.17	T 11	698	0.81	0.	0.01	0.19	0.	0.	0.	0.864
29004	ANCHOLME AT BISHOPSBRIDGE	54.65	12.11	T 11	630	0.51	0.08	0.	0.42	0.	0.	0.	0.650
30001	JITHAM AT CLAYPOLE HILL	298.00	46.92	T 11	625	0.41	0.04	0.	0.55	0.	0.02	0.	0.650
30004	PARTNEY LYNN AT PARTNEY HILL	61.64	15.14	T 11	673	0.	0.	1.00	0.	0.	0.	0.	0.770
31005	HELLAND AT TIKOVER	417.00	55.36	T 11	643	0.02	0.	0.	0.98	0.	0.01	0.15	0.497
31010	CHATER AT POSTERS BRIDGE	68.90	21.46	T 11	641	0.06	0.	0.	0.94	0.	0.	0.02	0.497
31021	JELLAND AT ASHLEY	250.70	28.98	T 11	653	0.	0.	0.	1.00	0.	0.02	0.04	0.443
31023	WEST GLEN AT EASTON WOOD	4.40	2.80	T 11	527	0.	0.	0.	1.00	0.	0.	0.	0.165
32801	FLORE EXPERIMENTAL STATION	5.81	3.28	T 11	654	0.	0.	0.	1.00	0.	0.	0.	0.492
33014	LARK AT TEMPLE WEIR	272.00	20.87	T 11	422	0.55	0.	0.45	0.	0.	0.02	0.	0.771
33015	QUICK AT WILKIN WEIR	372.00	16.10	T 11	555	0.10	0.	0.01	0.85	0.	0.00	0.	0.547
33029	STRINGSIDE AT WHITE BRIDGE	95.80	7.04	T 11	437	0.75	0.25	0.	0.	0.	0.	0.	0.931
33045	WHITTLE AT QUIDENHAM	28.30	7.52	T 11	648	0.	0.	1.00	0.	0.	0.	0.	0.694
33809	BURY BROOK AT BURY WEIR	65.30	10.00	T 11	554	0.	0.	0.85	0.15	0.	0.	0.	0.299
34003	BURE AT INGMORTH	165.00	22.36	T 11	699	1.00	0.	0.	0.	0.	0.	0.03	0.529
34005	TUD AT COSTESSEY PARK	73.30	22.70	T 11	680	0.08	0.	0.92	0.	0.	0.	0.	0.663
34007	DOVE AT OAKLEY PARK	134.00	16.53	T 11	600	0.	0.	1.00	0.	0.	0.	0.	0.484
34011	HENSUM AT PARENHAM	127.10	17.69	T 11	706	0.20	0.	0.20	0.	0.	0.01	0.	0.821
35006	GIPPING AT STOWMARKET	129.00	14.51	T 11	518	0.	0.10	0.90	0.	0.	0.02	0.	0.359
36008	STOUR AT WEST HILL	224.00	37.90	T 11	617	0.	0.07	0.93	0.	0.	0.01	0.	0.370
37001	RODDING AT REDBRIDGE	303.00	62.60	T 11	635	0.	0.	0.80	0.20	0.	0.10	0.	0.358
37003	TER AT CRABBS BRIDGE	77.80	24.83	T 11	587	0.	0.36	0.64	0.	0.	0.	0.	0.526
37007	WID AT WHITTLE	136.00	26.90	T 11	620	0.	0.03	0.90	0.07	0.	0.13	0.	0.386
37008	CHELMER AT SPRINGFIELD	100.00	43.53	T 11	596	0.	0.10	0.90	0.	0.	0.03	0.	0.542
37331	CROUCH AT WICKFORD	71.80	12.40	T 11	571	0.	0.	0.10	0.90	0.	0.05	0.	0.244
38003	MIRAM AT PANSHANGER	133.90	17.30	T 11	665	0.60	0.40	0.	0.	0.	0.01	0.	0.412
38007	CANDON BROOK AT ELIZABETH WAY MARLOW	21.37	5.60	T 11	640	0.	0.30	0.70	0.	0.	0.29	0.	0.737
38006	HANDLE AT BEDDINGTON PARK	122.00	2.40	T 11	800	0.90	0.10	0.	0.	0.	0.39	0.	0.623
39005	BEVERLEY BROOK AT WIMBLEDON COMMON	43.50	7.40	T 11	440	0.05	0.70	0.	0.25	0.	0.51	0.	0.633
39007	BLACKWATER AT SWALLOWFIELD	350.30	22.34	T 11	719	0.25	0.14	0.35	0.26	0.	0.33	0.	0.789
39012	HOGSMILL AT KINGSTON UPON THAMES	69.10	11.47	T 11	691	0.25	0.01	0.01	0.55	0.	0.46	0.	0.130
39017	PAT AT GRENON UNDERWOOD	11.40	2.05	T 11	660	0.	0.	0.	1.00	0.	0.	0.	0.130
39022	LODDON AT SHEEPBRIDGE	164.11	32.07	T 11	328	0.35	0.	0.	0.45	0.	0.02	0.	0.746
39025	ENBORNE AT BRINTON	147.60	23.10	T 11	334	0.	0.	0.	0.85	0.	0.01	0.	0.512
39026	CHEWELL AT SANBURY	191.60	27.91	T 11	26	0.06	0.	0.	0.94	0.	0.02	0.09	0.352
39036	LAW BROOK AT ALBURY	16.20	7.66	T 11	350	1.00	0.	0.	0.	0.	0.	0.06	0.403
39052	THE CUTT AT PITTS WEIR, BINFIELD	50.20	11.01	T 11	697	0.	0.	0.20	0.80	0.	0.18	0.	0.419
39812	MOLE AT MORLEY	89.90	14.64	T 11	825	0.	0.	0.	1.00	0.	0.09	0.19	0.403
39814	MOLE AT IPFIELD WEIR	12.67	4.06	T 11	839	0.	0.	0.	1.00	0.	0.19	0.28	0.419
39816	CRAWTERS BROOK AT HAZELWICK	4.50	3.46	T 11	825	0.	0.	0.	1.00	0.	0.77	0.	0.419
39820	DOLLIS BROOK AT HENDON LANE BRIDGE	25.10	10.80	T 11	688	0.	0.	0.	1.00	0.	0.60	0.	0.419
39830	BECK AT RECTORY ROAD	10.00	5.30	T 11	665	0.77	0.	0.	0.23	0.	0.44	0.	0.419
39831	CHAFFINCH BROOK AT BECKENHAM	7.00	4.01	T 11	683	0.65	0.	0.	0.15	0.	0.41	0.	0.419
40004	ROTHER AT UJIAN	205.70	28.10	T 11	851	0.	0.	0.02	0.98	0.	0.01	0.05	0.380
40006	BOURNE AT MADLOW	50.30	13.51	T 11	724	0.53	0.06	0.	0.38	0.	0.03	0.	0.656
40007	MEDWAY AT CHARFORD	255.10	25.04	T 11	874	0.	0.	0.02	0.98	0.	0.02	0.19	0.471
40008	GREAT STOUR AT WYE	230.00	29.80	T 11	749	0.32	0.30	0.	0.38	0.	0.03	0.05	0.561
40010	EDEN AT STONE BRIDGE	138.20	19.40	T 11	797	0.	0.	0.	1.00	0.	0.01	0.02	0.458
41005	OUSE AT GOLDMIDGE	224.29	30.92	T 11	775	0.14	0.	0.11	0.75	0.	0.03	0.04	0.304
41006	UCK AT ISFIELD	180.90	26.70	T 11	359	0.	0.	0.	1.00	0.	0.04	0.12	0.432
41007	ARUN AT PARK HOUND	87.80	16.35	T 11	550	0.	0.	0.	1.00	0.	0.02	0.	0.411
41015	EHS AT WESTOURNE	403.30	44.77	T 11	755	0.04	0.	0.	0.96	0.	0.01	0.06	0.411
41021	CLAYHILL STREAM AT OLD SHIP	52.30	7.27	T 11	907	0.54	0.10	0.	0.06	0.	0.	0.05	0.458
41022	LOD AT HALFWAY BRIDGE	7.12	5.70	T 11	240	0.	0.	0.29	0.71	0.	0.	0.	0.174
41025	LOXWOOD STREAM AT DRUNGEWICK	51.98	16.50	T 11	665	0.24	0.	0.	0.76	0.	0.01	0.	0.360
41028	CHESS STREAM AT DRUNGEWICK	91.54	25.65	T 11	503	0.06	0.	0.	0.92	0.	0.02	0.	0.179
41801	HOLLINGTON ST AT HOLLINGTON	21.91	9.96	T 11	842	0.	0.	0.	1.00	0.	0.31	0.	0.367
45002	EKE AT STOODLEIGH	422.00	48.10	T 11	762	0.	0.	0.	1.00	0.	0.40	0.	0.509
45003	CULM AT WOODMILL	226.10	26.45	T 11	965	0.47	0.02	0.	0.02	0.12	0.	0.	0.521

NUMBER	NAME	AREA	MSL	STORS	SAAR	SOIL1	SOIL2	SOIL3	SOIL4	SOIL5	URBAN	LAKE	RFI
45004	AKE AT WHITFORD	289.50	33.60	3.55	1209	0.50	0.	0.15	0.35	0.	0.01	0.	0.492
45804	BARLE AT BUSHFORTH	129.00	35.20	5.90	1655	0.	0.55	0.	0.	0.35	0.	0.	0.
45805	EKE AT PAXTON	147.59	33.76	9.30	1467	0.	0.90	0.	0.	0.10	0.	0.	0.
46003	DART AT AUSTINS BRIDGE	248.00	35.20	16.50	1921	0.26	0.24	0.	0.	0.50	0.	0.	0.527
46005	EAST DART AT BELLEVER BRIDGE	21.50	11.90	22.60	2103	0.	0.	0.	0.	1.00	0.	0.	0.385
46802	SWINCOMBE AT SWINCOMBE BRIDGE	14.20	3.62	26.90	1966	0.	0.	0.	0.	1.00	0.	0.	0.368
46805	BALA BROOK AT BALA RES INTAKE	5.90	2.83	75.90	2146	0.	0.	0.	0.	1.00	0.	0.	0.
47007	YEALM AT PUSLINCIA	54.90	16.60	17.80	1442	0.14	0.50	0.	0.	0.36	0.	0.	0.531
47008	THRUSHEL AT TINIA	112.70	19.60	6.81	1259	0.	0.33	0.	0.67	0.	0.	0.	0.363
47011	PLYM AT CARN WOOD	79.20	18.30	19.30	1644	0.10	0.40	0.	0.	0.50	0.03	0.22	0.499
47004	WARLEGGAN AT TRENKOFFE	25.30	10.00	17.43	1533	0.	0.25	0.	0.	0.75	0.	0.	0.720
48005	KENNYH AT TRURO	19.10	7.18	13.10	1121	0.	1.00	0.	0.	0.	0.06	0.	0.646
48009	ST VEOT AT CRAIGS HILL WOOD	22.70	12.17	17.97	1939	0.	0.20	0.	0.	0.80	0.	0.02	0.595
49003	DE LANK AT DE LANK	21.70	6.70	12.80	1681	0.	0.	0.	0.	1.00	0.	0.	0.445
51002	MORNER WATER AT WEST LUCCONEE	20.80	10.73	34.96	1400	0.	0.90	0.	0.10	0.	0.	0.25	0.559
52004	ISLE AT ASHFORD	90.10	14.30	5.10	904	0.09	0.	0.20	0.71	0.	0.02	0.	0.448
52005	TONE AT BISHOPS HILL	202.00	37.30	5.60	993	0.18	0.47	0.	0.35	0.	0.06	0.	0.466
52006	TEO AT PEN HILL	213.10	10.70	5.50	846	0.30	0.	0.45	0.25	0.	0.05	0.03	0.358
52010	BRUE AT LOVINGT	135.20	20.35	4.68	909	0.07	0.02	0.63	0.29	0.	0.	0.	0.471
52016	CURRY POOL AT CLU	15.70	7.15	20.75	918	0.	0.44	0.	0.56	0.	0.	0.	0.743
52020	GALLICA BROOK AT BRYNE INTRINSICA	16.40	6.04	13.58	980	0.	0.	0.40	0.40	0.	0.01	0.11	0.248
53005	MIDFORD BROOK AT MIDFORD	147.40	24.90	3.00	998	0.60	0.	0.10	0.30	0.	0.05	0.	0.606
53007	FROME AT TELLES AT MIDFORD	261.60	27.70	2.30	933	0.27	0.03	0.35	0.35	0.	0.02	0.	0.536
53008	AVON AT ST SOMERS	303.00	29.70	2.56	838	0.37	0.	0.38	0.25	0.	0.	0.	0.565
53009	MELLOW BROOK AT MELLOW	72.60	16.13	4.15	1025	0.57	0.	0.43	0.	0.	0.07	0.	0.606
54004	SOME AT STONELEY	242.00	28.80	1.00	707	0.	0.	0.	0.	0.	0.	0.	0.111
54006	STOUR AT RIDGEMAN	124.00	35.55	3.07	721	0.38	0.14	0.08	0.40	0.	0.14	0.	0.730
54010	STOUR AT ASCOT	119.00	38.95	2.90	711	0.10	0.	0.40	0.50	0.	0.	0.	0.539
54011	SALWARPE AT HARRINGTON HILL	134.00	26.91	4.95	691	0.42	0.	0.01	0.57	0.	0.03	0.	0.655
54016	RODEN AT RODINGTON	259.00	40.20	0.92	721	0.50	0.03	0.	0.47	0.	0.	0.	0.607
54019	AVON AT STARETON	347.00	56.70	1.40	676	0.30	0.	0.70	0.	0.	0.04	0.	0.500
54020	PERRY AT YEATON	180.90	31.57	2.56	772	0.14	0.10	0.	0.76	0.	0.02	0.04	0.660
54022	SEVERN AT BILLY JEY	6.90	6.90	17.70	1249	0.	0.	0.	1.00	0.	0.	0.	0.490
54034	DOULES BROOK AT DOULES	40.20	1.30	2.78	751	0.	0.00	0.50	0.	0.	0.	0.	0.431
54040	FANLHYTH AT FANLHYTH	0.92	1.45	124.07	2350	0.	0.	0.	1.00	0.	0.	0.	0.220
55008	WYE AT CERN BRMYN	10.40	5.36	47.44	2532	0.	0.	0.	1.00	0.	0.	0.	0.305
55012	TRFON AT CILBERY	244.20	35.97	7.98	1661	0.	0.63	0.	0.37	0.	0.	0.	0.590
55021	LUGG AT BUTTS BRIDGE	371.00	48.51	4.04	918	0.	0.90	0.03	0.	0.07	0.01	0.	0.662
55022	TROTHY AT MITCHEL TROT	142.00	23.76	3.00	913	1.00	0.	0.	0.	0.	0.	0.	0.456
55025	LLYNY AT THREE COCKS	132.00	18.69	4.03	994	1.00	0.	0.	0.	0.	0.	0.17	0.574
55029	WYE AT DOOLE FARM	174.00	35.30	3.50	1654	0.	0.50	0.	0.40	0.	0.	0.	0.333
55034	CYFF AT PLYMNING	3.10	3.01	46.68	2455	0.	0.	0.	1.00	0.	0.	0.	0.290
56002	EBBW AT RHIDDERYD	217.00	38.21	9.74	1491	0.	0.05	0.55	0.	0.40	0.10	0.06	0.
56003	HONDDU AT THE FORGE SPECON	62.20	20.20	9.02	1260	0.	0.78	0.	0.	0.22	0.	0.	0.507
56004	USK AT LLANDETTY	544.00	43.70	4.58	1498	0.	0.60	0.	0.	0.40	0.02	0.08	0.467
56005	LLYD AT PONTNIP	99.10	25.37	14.23	1425	0.	0.25	0.30	0.	0.45	0.16	0.	0.542
56006	USK AT TRELONG	183.90	22.37	8.87	1702	0.	0.53	0.	0.	0.47	0.	0.11	0.440
56011	SIRHOWY AT WATTSVILLE	76.10	31.33	11.13	1547	0.	0.	0.65	0.	0.35	0.09	0.12	0.514
57004	CYNOV AT ABERCYNON	106.00	25.80	7.30	1801	0.	0.	0.30	0.	0.70	0.04	0.	0.430
57005	TAF AT PONTYPRIDD	454.80	42.26	9.23	1863	0.	0.	0.40	0.	0.60	0.05	0.15	0.489
57006	RHONDDA AT TREMADOC	100.50	22.89	7.48	2187	0.	0.	0.48	0.	0.52	0.17	0.04	0.467
58001	NEATH AT RESOLVEN	190.90	28.30	13.50	1897	0.	0.	0.10	0.	0.90	0.01	0.	0.322
58005	EHENNY AT EHENNY	62.90	13.67	7.19	1350	0.30	0.30	0.36	0.	1.00	0.05	0.	0.609
58006	MELLYE AT PONT NEAR VAUGHAN	65.80	14.71	25.93	2021	0.	0.	0.	0.	1.00	0.	0.12	0.342
58008	DULATS AT CILFRYD	43.00	14.04	14.94	1665	0.	0.	0.15	0.	0.85	0.	0.	0.339
58009	EHENNY AT KEEPERS LODGE	62.50	13.05	7.67	1350	0.30	0.30	0.38	0.	0.92	0.05	0.	0.629
60002	COTHE AT FELIN HYNACHODY	297.90	50.02	4.56	1646	0.	0.43	0.	0.	0.37	0.	0.	0.444
60003	TAF AT CLOGFYRAN	217.30	33.60	4.21	1411	0.	0.97	0.	0.	0.03	0.	0.	0.616
60006	GWILT AT GLANGWIL	129.50	24.05	5.92	1600	0.	0.70	0.	0.	0.10	0.	0.	0.437
60007	TONY AT DOLAU MIREN	231.00	36.20	10.15	1749	0.	0.07	0.	0.	0.93	0.	0.	0.406
61001	WESTERN CLEDDAU AT BRENDERGAST HILL	197.60	27.60	3.24	1266	0.	0.95	0.	0.	0.05	0.	0.	0.637
61003	GWAUN AT CILRHEDYN BRIDGE	31.30	9.38	25.47	1474	0.	1.00	0.	0.	0.	0.	0.	0.585
62002	TEIFI AT LLANFAIRYLLAN DYSSAL	510.00	70.65	1.53	1479	0.	0.65	0.	0.11	0.24	0.	0.	0.517
64001	DOVEY AT DOVEY SPYLLAN	471.30	37.47	5.22	1863	0.	0.50	0.	0.	0.50	0.	0.	0.359
65001	GLASLYN AT BEODGELERT	65.60	15.20	33.55	3279	0.	0.02	0.	0.	0.98	0.	0.26	0.307
65801	NANT PERIS AT TAN-YR-ALT	11.40	4.50	54.22	4128	0.	0.	0.	0.	1.00	0.	0.	0.
66002	ELWY AT PANT-YR-ORION	220.00	37.66	6.77	1175	0.01	0.85	0.	0.13	0.	0.06	0.	0.444
66004	WHEELER NEAR BODAFON	52.90	11.32	11.96	856	0.67	0.33	0.	0.	0.	0.	0.	0.843
66006	ELWY AT BONT-Y-SSWYDD	194.00	27.50	5.40	1200	0.	0.83	0.	0.	0.17	0.	0.06	0.479
66011	CONWAY AT CWM LLAYDDEL	344.00	29.04	17.20	2234	0.	0.51	0.	0.	0.49	0.	0.02	0.305
67003	BRENIG AT PONT-Y-RHODD	20.20	7.09	13.80	1308	0.	0.	0.	0.	1.00	0.	0.	0.382
67005	CEIRIOG AT BRYKINALLT WEIR	113.70	27.87	11.93	1257	0.	0.43	0.	0.	0.57	0.	0.	0.465
67008	ALYD AT PONT Y CAPEL	227.00	45.80	4.97	910	0.15	0.70	0.	0.10	0.05	0.04	0.01	0.558
67010	GELTH AT CYNEFELL	13.10	5.67	10.58	2220	0.	0.15	0.	0.	0.85	0.	0.06	0.256
68006	DANE AT HULME WALKER	150.00	30.94	10.03	1034	0.11	0.09	0.	0.49	0.32	0.02	0.04	0.477
68010	PENDER AT FORD LANEWEN	18.40	6.28	8.18	790	0.	0.	0.	1.00	0.	0.	0.	0.24
68002	SANDERSONS BROOK AT SANDSACH	4.40	3.24	5.18	749	0.	0.17	0.	0.83	0.	0.	0.	0.
69008	DEAF AT STANVEYLAN	51.80	20.95	12.02	931	0.24	0.47	0.	0.25	0.24	0.03	0.02	0.
69011	MICKER BROOK AT CHUJ	67.30	17.77	7.66	373	0.04	0.17	0.	0.80	0.	0.30	0.	0.
69012	BOLLIN AT WILMSLOW	72.50	20.07	9.43	939	0.47	0.33	0.	0.12	0.08	0.07	0.11	0.
69013	SINDORLAND BROOK AT PARTINGTON	44.80	13.75	2.92	330	0.	0.84	0.	0.	0.16	0.	0.49	0.
69018	NEWTON BROOK AT NEWTON-LE-WILLOWS	32.80	14.37	5.40	885	0.	0.	0.	1.00	0.	0.09	0.	0.
69019	WASSLEY BROOK AT WASSLEY	24.70	11.15	10.94	330	0.10	0.	0.	0.90	0.	0.34	0.	0.
69027	TAF AT PORTWOOD	150.00	41.40	5.62	1179	0.	0.	0.	0.41	0.59	0.22	0.17	0.
69031	NETHERLEY BROOK AT GREEN'S BRIDGE	47.90	9.79	5.46	857	0.	0.07	0.	0.93	0.	0.17	0.	0.
69034	MUSBURY BROOK AT HELMESHORE INTAKE	3.10	2.60	86.53	1466	0.	0.	0.	0.	1.00	0.	0.	0.
69002	ETHEROUD AT WOODHEAD	13.00	5.91	35.71	1530	0.	0.	0.	0.	1.00	0.	0.	0.
70008	TAF AT NEWBURGH	28.90	11.33	8.09	965	0.	0.35	0.	0.65	0.	0.07	0.	0.
70013	CROSSDALE BECK AT CROSSDALE FLUME	10.36	5.24	37.80	1539	0.	0.	0.	1.00	0.	0.	0.	0.353
70004	CALDER AT WHALLEY ABBEY	314.00	37.12	5.02	1227	0.	0.	0.	0.71	0.29	0.09	0.02	0.304
70008	HODDER AT HODDER PLACES	261.00	37.99	4.93	1480	0.	0.	0.	0.38	0.61	0.	0.13	0.
71802	RIBBLE AT HALTON WEST	204.70	40.06	5.88	1529	0.	0.	0.	0.17	0.85	0.	0.	0.263
71804	DUNSOPT AT FOOTOLME	24.90	7.24	33.46	1409	0.	0.	0.	0.	1.00	0.	0.	0.
72002	WYRE AT ST. MICHAEL'S-ON-WYRE	275.00	34.17	7.74	1257	0.	0.07	0.	0.46	0.47	0.01	0.	0.323
72006	LUNE AT KIRKBY LONSDALE	507.20	49.60	4.77	1437	0.	0.	0.	0.01	0.99	0.	0.	0.
72018	NEW HILL BROOK AT CARVERS BRIDGE	64.50	16.77	7.77	1024	0.	0.10	0.	0.87	0.03	0.02	0.	0.166
72820	BURNES GILL AT TEBAY (MS)	0.72	0.80	179.74									

CATCH NO	EV NO	DATE OF STORM	RAINFALL TOTAL DURN (MM) (H)	PEAK FLOW (CUFECS)	LAG (H)	ANSP (CUFECS)	SMD (MM)	APIS (MM)	CWI (MM)	RUNOFF X	1-HOUR UNIT HYDROGRAPH				
											UM PEAK (CUFECS)	TIME TO PEAK (H)	WIDTH AT 0.5 PEAK (H)	UM TIME BASE (H)	
24003	1	9 11 63	26.9 16	70.89	4.2	4.80	0.	3.3	128	13.9	31.8
24003	8	25 9 65	42.9 15	72.81	7.6	2.06	1.7	1.0	124	18.1	42.2
24003	11	2 10 66	48.4 34	121.03	5.6	1.85	3.7	3.3	124	20.7	42.8
24003	16	4 9 67	34.9 35	64.67	5.1	3.86	0.	14.1	139	15.7	45.1
24003	17	6 10 67	25.5 18	76.80	6.2	3.30	0.6	4.1	128	15.4	60.6
24005	1	8 12 54	33.6 11	34.99	3.0	4.24	3.2	0.3	122	9.8	29.2	21.0	7.5	10.7	31.6
24005	2	27 8 56	27.7 10	31.02	10.0	1.87	0.8	1.8	125	7.3	26.4	23.1	9.8	9.7	28.7
24005	5	13 3 64	36.5 31	27.30	3.5	2.82	0.	3.4	128	8.0	21.9	23.0	5.0	9.5	29.3
24005	7	23 3 64	30.1 30	44.48	9.1	4.73	0.5	1.6	126	11.0	36.6	29.0	7.5	8.2	21.9
24005	8	28 9 65	14.9 8	18.80	8.6	1.80	25.3	3.3	103	3.3	21.9	27.0	8.5	8.5	24.2
24005	9	30 9 65	14.9 8	20.44	2.7	4.26	0.	10.5	135	3.4	22.5	26.1	9.0	8.0	23.6
24005	10	17 11 65	43.0 46	48.39	6.5	11.43	0.	10.0	134	15.8	36.7
24005	12	9 4 66	21.4 12	42.39	7.7	5.10	1.0	7.7	131	9.5	44.0	31.0	6.0	7.1	21.7
24005	13	12 8 66	35.4 33	29.74	11.0	1.34	38.8	5.4	91	8.2	23.0	23.0	7.0	8.5	31.3
24005	14	2 10 66	39.7 37	21.81	13.5	1.18	17.4	2.9	110	8.6	21.5
24005	15	8 8 67	42.8 21	28.38	10.1	0.96	62.0	1.5	64	5.7	13.4	35.6	4.7	5.9	19.4
24005	16	16 10 67	42.5 16	40.67	9.1	1.54	0.6	1.7	126	11.8	27.7
24005	17	1 11 67	16.0 9	19.10	9.5	1.99	1.2	0.7	124	3.8	23.9	30.0	8.5	8.5	20.1
24005	18	4 11 67	56.2 22	58.48	9.0	4.29	0.	2.5	127	23.1	41.1	21.0	7.0	10.0	31.0
24005	19	10 10 67	21.2 11	22.24	11.1	2.49	0.2	0.9	125	5.7	30.7	25.0	6.5	8.8	26.9
24005	21	11 1 69	18.4 17	22.74	7.7	2.29	8.1	2.4	119	4.3	22.2	32.1	7.7	6.9	20.8
24005	22	2 5 69	19.4 18	26.49	7.7	2.29	0.6	5.4	129	5.3	34.0	32.8	6.5	6.9	20.1
24005	23	6 5 69	15.5 12	30.78	5.5	4.98	0.6	5.4	129	5.3	34.0	32.8	6.5	6.9	20.1
24007	2	30 10 68	73.5 94	12.46	11.1	0.80	0.	2.1	127	42.6	57.9
24007	5	11 1 69	18.0 17	8.03	7.3	1.25	0.2	1.0	125	7.0	44.0	32.2	5.7	7.7	10.9
24007	7	5 5 69	16.2 17	8.27	5.7	0.71	3.8	2.2	121	4.3	26.2	41.0	4.8	5.5	16.1
24007	8	23 6 69	21.0 21	8.86	8.7	1.88	4.3	9.2	129	5.9	39.5	35.3	4.6	6.7	18.1
24007	9	17 9 69	20.2 21	8.36	5.0	0.89	11.8	3.5	116	5.7	26.3	35.0	4.0	6.3	19.2
24007	11	20 1 71	16.7 12	7.24	5.8	0.70	42.0	2.0	85	5.1	25.3	3.0	4.9	6.0	17.6
24007	13	22 4 71	51.9 33	13.66	12.0	0.66	2.7	1.3	123	5.7	33.9	33.0	7.3	7.5	18.7
25003	2	21 11 63	38.9 18	12.29	3.0	0.33	0.	11.0	135	18.5	30.7	47.7	5.0	4.4	14.5
25003	3	8 8 64	36.5 8	14.33	2.8	0.46	83.3	12.1	53	18.3	50.1	49.4	4.0	5.0	12.5
25003	5	15 9 65	38.6 14	13.52	2.4	0.27	3.3	0.7	122	23.0	39.7	47.2	4.0	5.0	13.6
25003	11	2 7 68	29.7 8	24.11	2.5	0.92	0.	11.6	136	21.9	73.6	64.7	4.0	3.8	9.6
25003	13	20 9 68	40.5 11	13.74	3.5	0.67	0.	21.3	146	32.6	80.5	49.6	2.9	5.4	11.6
25004	3	21 1 59	28.5 32	26.85	4.1	10.28	0.	9.3	134	4.9	17.0
25004	5	14 3 64	26.7 28	24.07	6.2	3.91	2.0	4.2	127	6.9	25.7
25004	8	9 4 66	23.8 13	29.67	12.0	6.86	0.4	7.7	132	7.0	29.6	13.9	10.4	16.8	46.4
25004	9	16 10 67	43.5 18	32.23	11.1	3.86	1.0	5.3	129	10.9	23.0
25004	10	4 11 67	50.1 23	35.50	16.2	3.88	0.2	2.9	127	20.3	40.6
25006	2	20 4 71	30.1 30	30.13	1.9	0.94	41.6	0.8	104	43.2	53.9
25006	4	20 11 71	24.3 9	29.11	5.4	1.63	0.2	1.9	126	9.8	40.3
25011	3	16 3 72	35.4 5	15.16	1.5	0.66	1.2	0.2	124	16.6	46.8
25012	3	16 3 72	31.5 15	36.06	1.3	0.86	2.8	0.4	122	22.7	72.2	75.4	1.8	2.6	9.5
25012	4	17 6 72	16.8 14	11.59	3.1	0.34	12.0	0.2	113	10.0	59.6	48.9	2.7	4.6	13.5
25810	3	13 7 61	81.2 33	0.05	2.0	0.00	53.9	11.0	82	34.9	43.0
25810	4	3 8 61	58.7 19	0.09	0.8	0.00	50.4	0.7	75	26.6	45.3	83.9	1.5	2.1	9.1
25810	5	16 10 61	69.3 30	0.09	3.5	0.00	4.1	1.2	122	45.6	65.2	97.0	2.4	2.5	6.5
25810	6	17 8 61	25.5 30	0.02	6.4	0.00	50.7	1.2	75	14.0	49.0	57.5	2.4	3.0	13.3
25810	7	21 8 61	17.3 16	0.03	2.8	0.00	45.7	13.9	93	10.8	62.3	85.3	2.3	2.5	8.0
27001	6	9 11 63	29.9 15	76.62	5.5	11.99	36.8	3.9	92	6.5	21.7
27001	7	20 11 63	34.3 23	148.95	10.8	18.55	0.	5.5	130	14.1	41.2
27001	8	13 3 64	42.0 24	84.21	5.9	8.46	0.	4.1	129	12.2	29.1	16.7	10.2	14.5	17.6
27001	9	25 3 64	29.3 26	89.53	12.4	15.54	0.5	1.9	126	13.3	44.5	18.0	10.0	12.7	36.4
27001	15	22 2 67	23.7 12	93.14	8.1	13.87	0.	4.9	129	7.7	32.4	24.0	8.2	3.7	28.9
27001	16	27 2 67	35.9 26	138.30	14.8	14.87	0.	3.6	128	14.9	41.6
27001	17	8 6 67	34.3 34	133.17	15.0	9.83	27.6	7.0	104	14.5	41.5
27001	18	17 8 67	51.3 29	274.18	15.5	19.32	1.4	6.7	130	32.9	64.1
27001	19	16 10 67	51.3 29	186.69	6.1	19.93	5.0	19.3	136	9.5	51.5
27001	20	2 7 68	18.5 10	166.69	6.1	19.93	5.0	19.3	136	9.5	51.5
27001	21	11 9 68	66.8 31	303.85	13.8	10.74	51.6	7.4	80	34.7	51.9
27001	22	30 10 68	38.9 36	87.37	5.9	21.48	0.	2.4	127	9.8	23.1	18.5	9.7	10.8	38.5
27001	23	1 11 68	37.7 26	227.90	13.3	29.99	0.	18.3	143	23.4	62.1
27010	22	19 9 68	60.1 42	9.34	7.9	0.26	99.0	0.4	37	20.5	34.2
27026	1	24 11 63	28.5 31	29.36	9.1	1.85	0.	1.3	126	9.7	34.1
27026	3	8 9 65	30.0 13	34.73	5.6	1.87	0.2	11.1	135	8.8	29.4
27026	4	8 12 65	44.2 40	54.91	10.1	3.20	0.1	2.4	127	23.8	53.0
27026	5	5 4 66	21.1 12	42.04	4.7	3.70	0.	2.7	127	9.0	42.9
27026	6	8 3 67	34.6 29	26.09	7.7	1.30	4.0	1.1	122	7.6	21.8	24.7	5.7	7.3	30.4
27026	7	13 5 67	37.6 31	44.19	10.6	1.78	0.1	6.7	131	15.8	42.0
27026	8	14 7 68	38.2 17	35.28	10.4	0.62	17.8	5.1	112	10.4	27.1	22.5	13.5	10.3	28.8
27026	9	1 11 68	33.3 19	31.09	5.4	2.05	0.	3.1	128	10.6	31.8
27027	1	7 1 65	15.0 14	129.37	6.1	15.36	0.	4.3	129	9.3	62.1	30.7	6.5	8.1	20.0
27027	4	16 4 65	12.4 15	71.29	3.4	15.85	0.	2.4	127	4.2	35.7
27027	5	2 8 65	18.9 12	78.50	4.3	10.98	0.	6.1	131	5.5	29.0
27027	6	3 8 65	17.6 14	87.25	4.7	12.97	3.5	15.4	136	6.0	34.4
27027	7	9 9 65	11.7 9	79.22	6.1	10.94	0.	5.5	130	6.8	41.4
27027	8	25 9 65	42.9 23	153.60	6.0	10.91	0.2	3.7	128	20.2	47.1	19.6	8.0	13.5	29.7
27027	9	29 10 65	14.1 13	90.93	3.8	9.98	0.	3.3	128	5.1	36.5
27027	10	30 10 65	45.8 45	195.90	9.6	13.01	0.	10.0	135	37.1	81.0
27027	11	16 12 65	32.1 36	278.68	9.4	26.94	0.	5.8	130	28.5	88.7
27027	12	4 2 66	18.6 15	163.84	5.7	24.43	0.	3.1	128	16.9	91.0
27027	13	7 2 66	49.7 30	165.25	9.8	22.47	0.	9.2	134	22.5	45.3
27027	14	26 6 66	21.3 21	80.56	5.1	11.35	3.6	4.8	126	7.9	37.2
27027	15	14 11 66	26.7 37	144.45	5.5	21.59	0.	9.1	134	13.1	49.0
27027	18	17 12 66	37.3 23	194.38	9.3	19.26	0.1	1.0	125	28.8	77.2
27027	19	18 12 66	29.9 20	173.58	9.4	30.26	0.	18.0	143	16.0	53.7	23.9	7.6	10.2	26

CATCH NO	EV NO	DATE OF STORM	RAINFALL TOTAL DURN (MM) (H)	PEAK FLOW (CUMEC)	LAG (H)	ANSE (CUMEC)	SMD		AP15		CWI		1-HOUR UNIT HYDROGRAPH		UM TIME BASE (H)
							(MM)	(MM)	(MM)	(MM)	UH PEAK (CUMEC)	TIME TO AT 0.5 (H)	WIDTH (H)	PER 100 SQ KMS	
29001	11	6 10 74	53.1 35	1.28	12.3	0.14	84.4	4.3	4.5	4.5	0.0	1.8			
29004	2	2 6 69	26.9 16	5.38	7.5	0.68	9.4	2.2	117	4.6	17.1	20.2	5.8	12.6	29.8
29004	3	27 7 69	50.8 11	7.40	9.7	0.06	94.0	1.1	32	5.9	11.7	22.9	8.0	10.9	26.8
29004	4	16 11 69	31.6 11	8.42	9.9	0.89	42.2	2.1	84	8.2	25.8	18.9	9.3	11.3	35.2
29004	5	12 4 70	33.1 17	7.43	11.2	0.45	0.7	0.4	124	8.9	26.9	17.1	10.2	11.6	41.8
29004	6	8 3 72	11.2 12	6.05	8.7	1.74	0.1	8.9	133	4.1	36.6	14.1	9.4	15.8	47.3
29004	7	15 7 73	58.6 20	9.23	13.7	0.60	45.0	1.4	81	12.6	21.4	14.1	9.4	15.8	47.3
29004	8	10 7 74	53.1 23	8.72	13.6	0.69	79.0	4.9	50	16.9	31.8	14.1	9.4	15.8	47.3
29004	11	18 4 75	19.4 14	6.66	7.2	0.95	0.1	3.2	128	5.3	27.1	22.0	6.0	10.9	28.7
30001	1	29 10 60	17.6 14	16.82	22.7	4.78	0.1	2.9	127	5.3	30.1	9.0	21.2	24.3	75.0
30001	2	3 12 60	35.2 20	27.12	32.9	4.99	0.1	0.2	125	13.2	37.4	9.0	19.7	25.5	72.6
30001	3	18 12 60	35.9 47	23.87	18.0	4.57	0.1	0.1	125	9.8	27.2	10.0	18.8	24.8	61.6
30001	4	28 11 65	25.9 14	17.27	20.8	3.41	0.1	2.2	127	5.9	22.8	10.0	19.0	19.6	72.0
30001	5	10 12 65	20.2 18	18.70	22.1	4.93	0.1	4.2	128	6.5	32.0	9.2	19.0	24.6	71.7
30001	6	18 12 65	16.7 18	16.80	19.4	7.90	0.1	4.1	126	7.0	31.1	9.2	19.0	24.6	71.7
30001	7	13 1 67	47.1 41	23.38	33.7	2.08	3.6	5.4	126	15.3	32.0	9.0	20.5	26.5	70.6
30001	8	1 11 68	36.5 19	26.35	26.9	2.90	0.1	5.5	130	11.7	32.2	9.0	20.5	26.5	70.6
30001	9	5 5 69	27.7 10	19.29	22.4	2.26	15.0	0.8	110	6.0	21.8	10.6	21.0	19.7	65.5
30001	10	22 1 71	24.0 23	13.90	17.3	2.57	29.0	1.8	97	4.6	19.1	10.0	24.0	26.0	59.2
30001	13	8 3 75	35.8 18	33.34	19.2	3.28	0.1	2.0	127	11.1	30.9	11.0	16.0	21.0	59.1
30004	1	19 12 62	15.5 10	11.09	0.8	0.52	0.1	0.6	125	2.3	14.7	18.5	8.2	12.9	34.4
30004	3	28 11 65	18.9 16	11.05	12.0	0.38	0.1	3.1	128	10.1	27.4	19.0	11.5	11.8	35.0
30004	4	17 12 65	18.9 19	5.45	13.4	1.25	0.1	3.4	133	5.1	27.2	18.2	11.1	12.5	36.1
30004	5	5 11 67	15.2 16	3.72	10.1	0.86	9.9	6.6	121	3.3	21.9	18.2	11.1	12.5	36.1
30004	6	10 7 68	105.5 24	13.34	12.2	0.36	37.2	3.1	70	13.1	15.3	19.0	6.0	9.0	20.3
30004	7	7 8 68	33.8 7	5.09	5.7	0.67	32.3	2.3	94	2.9	8.6	29.0	6.0	9.0	20.3
30004	8	15 9 68	30.1 29	6.59	6.9	0.74	2.8	1.9	124	6.6	22.0	22.2	10.0	13.5	23.1
30004	9	1 11 68	48.7 26	10.17	10.9	0.92	0.1	6.4	131	12.2	25.0	18.5	10.7	12.5	35.1
30004	10	11 11 68	11.9 3	7.33	7.0	0.32	0.1	5.2	130	4.4	20.1	23.0	10.0	10.0	28.2
30004	11	6 10 74	27.7 8	7.89	10.7	0.90	50.4	5.4	79	6.7	24.3	20.0	11.6	12.0	31.6
30004	12	18 4 75	22.0 10	3.64	5.5	1.12	0.1	6.3	131	6.9	22.4	27.5	5.0	8.6	23.2
31005	1	27 2 67	17.3 18	22.98	52.0	2.90	0.1	1.0	126	7.6	44.1	10.0	11.0	11.0	59.1
31005	2	25 11 68	16.5 22	20.33	49.3	2.28	0.1	0.8	125	9.2	56.5	10.0	11.0	11.0	59.1
31005	3	11 3 69	27.8 42	39.51	44.3	3.89	4.3	0.5	121	16.2	58.2	5.7	42.0	46.4	103.3
31005	6	9 1 70	9.4 24	16.03	44.3	1.85	40.0	4.1	89	8.5	90.8	10.0	11.0	11.0	59.1
31005	7	22 1 71	26.3 22	33.46	37.9	4.47	24.2	2.1	102	11.2	42.4	10.0	11.0	11.0	59.1
31005	8	5 12 72	20.3 14	22.93	25.9	3.29	47.7	5.0	82	5.6	27.7	8.2	26.5	26.5	83.4
31005	9	19 11 74	22.0 26	32.33	41.1	6.46	1.7	7.0	130	9.2	47.0	10.0	11.0	11.0	59.1
31005	10	5 5 75	19.7 12	10.27	31.7	2.43	0.1	2.4	127	7.0	70.0	10.0	11.0	11.0	59.1
31010	1	10 7 63	72.8 22	20.93	14.3	0.55	60.0	2.4	67	16.8	23.1	10.0	11.0	11.0	59.1
31010	2	1 11 68	28.0 15	12.39	15.7	1.07	0.1	5.7	130	10.6	40.9	10.0	11.0	11.0	59.1
31010	3	5 5 69	38.9 11	16.26	12.8	0.77	27.7	0.3	97	12.4	32.1	10.0	11.0	11.0	59.1
31010	5	12 7 72	16.3 7	5.61	18.7	0.67	38.5	6.7	93	5.7	35.2	10.0	11.0	11.0	59.1
31010	6	20 11 74	19.9 24	7.60	17.3	1.13	2.6	4.6	127	8.8	44.3	14.2	14.1	13.4	51.5
31010	7	8 3 75	32.8 23	15.63	12.6	0.79	0.1	3.0	127	14.2	43.1	10.0	11.0	11.0	59.1
31010	8	18 4 75	22.2 15	15.02	11.9	1.73	0.1	5.0	129	11.3	51.1	10.0	11.0	11.0	59.1
31021	4	1 12 72	27.0 21	13.20	16.0	1.01	59.8	3.1	68	6.1	22.6	10.0	11.0	11.0	59.1
31021	6	19 6 73	52.0 21	13.88	13.2	0.49	86.8	0.1	38	3.7	7.0	10.0	11.0	11.0	59.1
31023	2	21 7 73	20.3 14	1.17	3.5	0.06	35.9	4.8	93	5.1	25.2	39.5	4.3	5.9	16.3
32801	1	13 10 66	19.4 9	1.60	5.4	0.19	4.8	5.5	125	6.0	30.7	35.7	4.4	5.5	20.2
32801	2	1 12 66	9.2 12	1.14	2.6	0.28	0.1	4.8	129	3.9	42.9	40.3	5.4	6.8	14.0
32801	3	9 12 66	21.5 16	2.31	5.5	0.19	0.1	3.7	128	14.5	66.6	28.6	5.6	7.7	23.3
32801	5	9 7 68	71.9 26	2.92	5.3	0.08	28.8	1.2	97	19.3	26.8	25.9	6.4	9.1	24.8
32801	6	1 11 68	29.2 16	3.06	5.2	0.16	0.1	3.3	128	13.1	44.9	36.1	4.3	5.3	20.1
32801	7	15 1 69	9.7 7	1.21	2.1	0.24	0.1	1.9	126	3.2	32.8	64.7	2.8	3.3	10.6
32801	9	5 5 69	30.4 13	1.25	5.0	0.09	33.7	0.1	91	4.9	16.0	36.5	3.8	5.8	18.9
32801	10	30 5 69	26.7 13	4.27	6.8	0.16	3.2	2.7	124	13.7	51.3	46.0	3.6	4.5	15.1
33014	1	27 2 61	17.0 31	7.21	23.0	2.21	0.4	1.4	125	3.0	17.7	7.8	22.4	28.8	94.2
33014	3	20 1 62	13.4 34	6.16	22.4	2.30	0.1	1.0	125	1.5	11.0	10.0	11.0	11.0	59.1
33014	5	8 12 65	18.5 25	7.10	28.0	1.14	0.1	1.9	126	2.9	15.8	10.0	11.0	11.0	59.1
33014	6	30 12 66	11.8 11	6.05	24.4	2.24	0.1	3.6	126	1.3	11.2	10.0	11.0	11.0	59.1
33014	7	5 11 67	18.8 14	6.11	25.0	2.17	23.2	9.1	110	1.6	7.3	11.0	25.9	21.5	58.1
33014	8	4 1 68	10.2 12	5.17	23.3	1.39	0.1	0.9	125	1.7	16.8	8.5	25.5	26.5	77.8
33014	11	17 12 68	14.8 12	6.78	22.8	1.15	0.1	1.8	126	2.5	16.6	10.0	11.0	11.0	59.1
33014	12	22 1 69	11.9 8	8.95	23.2	2.96	0.1	1.9	126	2.2	18.2	10.0	11.0	11.0	59.1
33014	15	5 5 69	35.4 10	8.74	20.4	1.95	10.1	0.0	114	2.9	8.3	10.0	11.0	11.0	59.1
33015	7	17 11 63	46.9 53	16.16	20.8	1.03	46.7	0.6	78	11.4	24.3	7.0	23.5	41.0	75.9
33015	8	23 11 63	18.6 21	12.14	17.8	1.96	9.2	0.9	116	5.8	31.1	8.7	14.2	27.0	93.8
33015	11	24 9 65	41.0 43	11.24	30.6	0.65	48.2	0.3	77	7.5	18.4	6.7	33.2	37.5	91.0
33015	13	22 12 65	15.9 18	14.42	16.6	3.15	0.1	1.1	126	6.0	37.8	10.0	11.0	11.0	59.1
33015	15	18 4 66	17.4 38	14.10	21.5	2.90	1.4	2.8	126	7.9	45.5	7.4	21.8	28.9	92.5
33015	16	1 10 66	28.8 54	14.77	27.3	3.40	12.0	12.8	125	10.3	35.8	10.0	11.0	11.0	59.1
33015	17	13 10 66													

CATCH NO	EV NO	DATE OF STORM	TOTAL RAINFALL (MM)	DURN (H)	PEAK FLOW (CUMEC)	LAG (H)	ANSF (CUMEC)	SMD (MM)	APIS (MM)	CWI (MM)	1-HOUR UNIT HYDROGRAPH		UM TIME BASE (H)
											UM PEAK (CUMEC)	TIME WIDTH TO AT 0.5 (H)	
37331	1	23 2 67	10.2	12	6.43	4.3	0.56	0.	2.6	127	2.8	27.1	
37331	7	27 2 67	12.5	17	8.16	5.8	0.61	0.	3.4	128	4.1	33.0	
37331	8	27 4 67	18.9	10	5.84	6.3	0.23	14.5	1.0	111	2.5	12.3	
37331	11	18 12 67	18.4	13	7.49	7.1	0.29	9.6	0.3	115	4.4	23.9	
37331	13	8 9 68	13.0	9	4.76	7.6	0.20	81.1	7.0	50	2.6	19.6	
38003	1	2 5 61	8.4	6	1.64	4.3	0.98	4.7	1.3	121	0.1	1.4	
38003	2	12 6 61	27.6	19	1.65	5.9	0.79	81.3	0.	43	0.2	0.9	
38003	3	6 7 61	25.7	10	1.49	5.9	0.52	34.1	1.9	92	0.3	1.0	
38003	4	25 6 67	30.0	5	2.54	3.5	0.72	51.3	8.1	81	0.3	1.0	
38003	7	22 7 67	25.3	9	2.18	4.0	0.63	88.4	0.7	37	0.2	0.9	
38003	9	15 9 68	67.6	18	3.61	3.1	0.48	37.0	5.8	93	1.0	1.5	
38007	1	26 6 58	39.1	24	13.27	5.5	0.32	14.2	5.6	116	18.7	47.7	32.3
38007	2	1 7 58	36.1	30	14.04	5.6	0.26	6.3	2.0	120	20.5	56.7	35.0
38007	3	19 9 60	21.4	13	8.37	3.0	0.25	44.4	4.4	85	11.7	34.8	44.2
38007	4	8 10 60	18.6	11	6.88	4.4	0.50	9.6	4.3	119	10.2	54.9	35.5
38007	5	30 10 60	14.2	8	7.61	3.7	0.76	0.	10.3	135	7.3	52.5	47.8
38007	6	25 11 60	15.9	5	7.17	4.1	0.67	0.	5.2	130	10.5	66.2	39.5
38007	9	13 7 62	13.3	6	2.19	4.4	0.09	106.3	2.3	21	1.4	10.4	
38007	11	31 8 63	15.1	9	2.60	1.8	0.04	62.9	1.4	63	1.3	8.6	67.0
38007	12	17 11 63	13.3	7	2.00	3.5	0.21	0.	1.0	126	3.4	25.3	37.6
38007	14	21 7 64	39.4	4	8.46	3.3	0.27	66.8	1.3	59	7.0	17.7	
38007	15	19 7 65	22.6	8	5.89	2.5	0.21	82.1	0.5	43	2.3	10.3	
38007	16	17 11 65	11.3	7	3.84	2.9	0.37	23.4	3.4	105	2.9	25.9	55.2
38007	18	22 9 66	33.5	6	4.08	2.4	0.34	75.5	0.5	50	4.4	13.3	37.0
38007	19	27 2 67	14.4	12	4.34	4.8	0.46	0.	3.7	128	6.0	55.3	28.7
38007	20	25 6 67	25.6	5	4.37	1.7	0.20	58.5	2.3	68	2.7	10.4	70.0
38007	22	15 7 68	25.8	7	7.60	2.1	0.31	68.4	1.8	58	4.8	18.7	59.9
38007	23	7 10 68	21.1	8	6.27	3.0	0.19	15.9	0.1	117	7.7	36.4	34.6
38007	24	28 10 68	15.1	2	4.85	2.6	0.35	15.9	0.7	109	3.1	20.9	54.9
39004	6	16 6 65	12.8	9	1.53	1.6	0.07	71.4	1.2	54	0.1	0.8	145.7
39004	7	7 7 65	10.1	11	1.89	4.1	0.01	0.	0.	11	0.	0.	0.
39004	8	22 7 65	15.2	12	1.73	2.2	0.09	88.1	6.3	43	0.2	1.0	82.2
39004	9	2 9 65	18.0	10	2.37	1.9	0.07	95.5	1.7	31	0.2	1.0	82.2
39004	10	3 9 65	58.4	14	3.72	2.3	0.08	82.7	14.2	56	0.8	1.3	56.6
39004	11	19 11 65	19.0	13	2.02	2.2	0.07	4.9	2.7	126	0.2	1.1	100.3
39004	12	28 11 65	27.3	18	2.47	3.8	0.05	0.	1.7	126	0.4	1.4	77.9
39004	13	22 6 66	29.1	6	3.07	1.8	0.13	82.7	4.7	43	0.3	1.1	77.9
39004	14	25 6 67	28.1	7	3.84	1.1	0.20	50.6	9.1	62	0.4	1.3	91.3
39004	15	22 7 67	20.4	7	2.96	2.2	0.19	91.2	0.6	34	0.3	1.3	91.3
39004	16	1 11 67	20.7	7	2.34	1.7	0.17	0.8	9.1	133	0.4	1.7	75.1
39004	17	17 4 68	9.3	2	3.06	0.8	0.25	8.0	2.4	119	0.1	1.1	
39004	18	4 5 68	13.9	9	2.65	2.2	0.18	7.5	0.4	117	0.2	1.3	102.9
39004	19	18 5 68	16.3	14	2.86	0.5	0.19	7.3	3.9	121	0.3	1.7	
39004	20	13 7 68	17.6	6	3.32	2.3	0.15	35.3	2.2	91	0.2	1.3	95.9
39004	21	28 8 68	16.4	4	3.94	1.3	0.23	56.4	2.2	70	0.2	1.1	138.6
39004	22	7 9 68	12.7	12	2.75	2.5	0.25	58.8	2.4	88	2.1	1.7	
39004	24	8 7 69	30.0	20	3.92	0.13	0.13	101.0	0.4	24	0.7	1.5	
39004	25	28 7 69	39.6	15	3.92	0.13	0.13	108.3	0.1	16	0.5	1.2	108.8
39004	26	2 8 69	27.4	9	4.33	1.1	0.14	81.2	4.3	48	0.3	1.1	
39004	27	5 8 70	15.9	3	5.53	2.5	0.13	144.2	1.3	17	0.4	2.3	
39004	28	13 11 70	30.6	10	4.30	2.5	0.04	79.8	3.4	48	0.5	1.7	64.6
39005	2	25 7 62	28.3	12	12.97	3.9	0.34	107.3	2.7	20	3.9	13.7	39.1
39005	3	5 8 63	15.3	16	3.95	4.7	0.35	8.5	3.0	119	2.5	16.1	48.7
39005	4	5 9 63	13.3	6	4.28	4.9	0.35	76.2	7.4	56	1.9	14.3	63.9
39005	5	10 6 63	10.6	6	6.44	2.5	0.29	92.0	0.9	33	1.3	12.9	66.6
39005	6	17 11 63	11.7	7	5.14	2.1	0.22	100.4	1.1	72	2.7	22.8	33.2
39005	7	16 4 64	12.4	7	6.24	2.4	0.62	9.4	2.6	118	2.2	17.6	90.9
39005	8	20 4 64	15.4	10	11.82	3.3	0.78	0.	6.6	131	5.2	35.9	48.8
39005	9	1 6 64	23.0	8	12.13	2.7	0.80	13.6	12.0	123	5.4	23.3	51.7
39005	10	13 6 64	9.5	2	9.98	1.8	0.91	3.1	6.5	128	2.5	26.3	
39005	11	21 7 64	23.2	2	14.53	4.1	0.50	97.2	0.2	28	4.1	17.6	
39005	14	22 6 64	26.3	8	9.72	3.7	0.80	82.6	0.6	43	3.7	14.2	73.7
39005	15	19 7 66	19.8	10	12.32	3.9	0.98	124.8	5.2	5	4.6	23.0	53.8
39005	16	29 8 66	26.5	10	14.33	2.9	1.10	89.5	5.7	42	6.3	23.9	43.3
39005	17	23 6 67	27.3	3	12.97	1.9	0.86	51.0	5.8	81	4.6	18.8	68.7
39005	18	8 6 67	21.3	10	9.22	2.0	0.46	101.3	1.9	25	3.6	18.6	68.7
39005	21	4 7 69	41.1	23	10.85	5.7	0.29	100.3	0.1	24	8.2	19.8	46.1
39005	22	28 7 69	36.2	16	9.32	4.3	0.09	108.4	0.1	16	5.7	15.7	35.3
39007	1	22 1 71	14.2	25	21.38	15.1	8.71	0.	8.6	133	2.7	19.1	
39007	2	14 3 71	19.2	13	13.95	11.9	3.04	4.8	0.4	120	2.4	13.0	15.8
39007	3	17 3 71	23.3	23	20.32	12.6	3.96	0.6	3.8	128	5.3	22.6	11.6
39007	4	22 4 71	31.4	31	21.85	21.2	3.00	27.1	0.2	98	5.6	18.0	14.7
39007	5	25 4 71	16.2	13	20.13	13.5	5.44	8.5	9.6	126	3.6	22.3	
39007	6	10 6 71	47.7	20	26.23	26.6	2.02	41.4	7.4	91	9.2	19.2	
39007	7	13 6 71	31.4	29	23.83	22.7	4.26	13.8	8.2	119	7.4	23.6	
39007	8	18 6 71	35.3	40	25.41	24.0	3.52	6.3	2.3	120	9.2	25.7	9.3
39007	9	15 11 74	33.8	24	27.47	24.4	1.86	37.3	5.3	92	12.4	36.6	8.3
39007	10	20 11 74	41.5	37	31.46	21.6	9.74	0.	5.1	133	9.9	23.8	7.2
39007	11	18 1 75	20.9	9	25.46	15.8	4.89	0.	3.8	128	5.7	28.3	13.0
39007	12	19 1 75	21.3	18	25.77	16.8	6.28	0.	12.3	137	6.1	28.5	11.3
39007	13	18 4 75	18.6	10	24.31	13.5	4.99	1.3	2.7	126	3.8	20.3	16.0
39012	1	7 8 60	31.7	4	15.81	3.2	0.78	90.8	0.1	34	5.0	15.7	46.3
39012	3	20 4 64	23.4	18	14.66	2.0	1.87	0.	5.5	130	3.7	23.4	
39012	4	31 5 64	23.4	9	11.31	3.1	1.25	12.8	6.9	119	3.4	14.7	43.5
39012	5	21 7 64	26.6	4	10.13	3.0	1.70	37.5	0.1	67	2.1	8.7	
39012	6	3 9 65	39.8	12	12.11	3.0	1.67	93.0	11.9	43	4.7	11.7	
39012	7	28 11 65	25.9	19	12.23	4.8	(0.93)	0.	1.7	126			

CATCH NO	EV NO	DATE OF STORM	RAINFALL TOTAL (MM)	DURN (H)	PEAK FLOW (CCUMCS)	LAG (H)	ANSF (CCUMCS)	SMD (MM)	APIS (MM)	CMI (MM)	1-HOUR UNIT HYDROGRAPH		UM TIME BASE (H)			
											UM PEAK PER 100 SQ KMS	TIME TO AT 0.5 PEAK (H)				
39814	18	19 8 70	12.7	9	0.84	1.2	0.04	138.3	8.8	4	5.4	44.2	122.1	1.5	2.0	5.1
39820	2	23 9 55	40.8	14	11.55	6.0	0.27	48.0	9.2	86	16.9	41.5				
39820	3	21 1 52	22.3	20	7.88	4.4	0.76	0	6.8	131	11.7	53.1				
39820	4	7 6 63	18.2	5	15.81	3.8	0.35	50.1	3.0	77	13.0	71.2				
39820	5	9 12 66	16.6	14	5.84	6.7	0.29	0.1	2.1	127	8.4	50.8	32.5	6.0	7.3	19.6
39820	6	5 9 68	38.8	22	6.33	10.4	0.37	38.3	15.5	102	21.1	54.4				
39820	8	7 10 68	22.1	22	5.07	5.1	0.19	4.9	0	120	7.2	32.7				
39820	9	1 11 68	15.1	19	5.58	6.5	0.36	0	4.7	129	6.6	43.5				
39820	11	16 12 68	33.1	17	6.35	6.5	0.34	0	2.8	127	14.0	41.4	27.6	7.1	8.8	22.7
39830	1	6 7 63	23.1	11	1.23	2.9	0.01	77.3	1.1	49	2.3	10.0	52.0	2.9	4.8	11.8
39830	2	1 6 64	25.4	8	2.03	2.0	0.10	24.5	16.8	117	4.4	17.3	50.7	3.1	4.8	12.4
39830	3	18 8 64	18.7	11	1.30	3.2	0.04	88.9	6.2	42	1.7	9.0	59.5	2.3	4.1	10.4
39830	5	22 6 66	27.0	7	1.64	3.1	0.03	81.3	1.4	45	3.3	12.2	57.2	3.3	4.0	11.4
39830	6	29 8 66	51.5	16	1.28	2.0	0.07	101.7	0.0	23	2.8	8.7				
39830	7	2 10 66	10.6	10	1.42	1.9	0.12	73.3	4.3	55	2.4	12.4	59.4	3.2	4.3	10.0
39830	8	29 5 67	9.7	10	1.18	2.8	0.13	14.5	1.6	112	1.6	16.2	66.5	3.3	3.7	9.4
39830	9	23 6 67	26.2	8	1.62	2.6	0.05	60.5	0	64	3.4	13.0	54.7	2.8	4.8	10.7
39830	11	1 11 67	19.9	9	1.95	3.1	0.19	22.0	5.8	108	3.9	19.6	47.6	3.9	4.9	13.5
39830	12	16 12 67	26.2	14	1.73	3.6	0.18	0	5.2	130	5.1	19.5	38.0	4.1	5.5	16.2
39830	13	25 4 67	25.9	5	2.21	2.5	0.11	51.4	6.7	82	4.0	15.0	57.5	3.3	4.3	10.7
39831	1	6 7 63	23.8	11	1.25	1.7	0.03	77.3	0.8	48	2.3	9.8				
39831	2	16 4 64	11.9	9	1.45	1.1	0.04	8.5	4.2	120	4.4	15.7	136.9	1.6	1.6	5.0
39831	3	1 6 67	23.6	8	1.70	2.2	0.07	25.6	14.1	113	4.8	18.0				
39831	4	12 6 64	14.5	8	1.29	1.4	0.02	18.0	0.2	107	7.7	9.7	95.1	1.2	2.2	6.9
39831	5	7 7 65	20.7	10	1.32	1.2	0.02	114.8	0.7	91	1.8	10.4	128.5	1.4	1.8	5.0
39831	6	2 9 65	15.3	5	1.65	1.4	0.03	120.0	1.9	6	1.4	9.8	136.4	1.6	1.6	5.1
39831	7	2 9 65	36.4	16	2.34	4.1	0.13	14.0	94		17.1	25.4				
39831	10	2 10 66	19.7	10	2.06	1.2	0.07	73.2	3.8	55	2.9	14.4				
39831	11	18 10 66	5.4	7	1.52	1.1	0.11	41.1	5.2	89	1.2	22.2	131.1	1.9	1.6	5.3
39831	12	18 10 66	10.3	4	2.18	1.1	0.21	35.6	6.7	96	7.3	22.2	128.6	1.6	1.7	3.3
39831	13	29 5 67	11.4	10	1.99	0.9	0.08	14.6	1.7	110	9.5	13.9				
39831	15	25 6 67	28.9	3	2.12	0.7	0.15	31.4	9.9	82	4.9	17.0				
39831	16	7 9 67	16.4	3	1.89	1.9	0.03	104.2	0.8	31	1.9	11.4	197.2	1.7	1.1	1.2
39831	17	1 11 67	19.3	7	1.84	1.0	0.11	22.0	6.2	109	3.9	20.3				
39831	18	12 7 68	14.4	4	1.37	1.0	0.04	40.0	6.1	41	1.4	9.5				
39831	19	12 7 68	14.7	1	1.97	1.8	0.06	61.7	2.5	65	2.0	13.5				
39831	20	16 12 68	19.1	1	2.62	3.3	0.12	0	3.2	130	7.9	27.3				
39831	22	20 3 71	16.0	3	2.67	1.8	0.10	74.2	5.9	62	2.5	15.8	138.8	1.9	1.3	4.0
39831	23	20 3 67	26.2	8	1.69	1.9	0.04	60.9	0	84	2.8	10.6				
40004	8	21 1 70	36.1	14	7.11	15.1	1.12	1.1	127		22.1	15.7	7.5	19.1	27.3	91.3
40004	8	22 1 71	30.6	12	48.00	20.7	3.80	0.1	5.2	730	20.9	68.4	11.0	19.2	22.3	37.0
40004	10	7 9 65	24.2	8	2.21	7.0	0.25	30.4	2.8	97	1.7	7.2	27.2	6.4	9.3	21.9
40004	11	8 12 65	19.2	25	5.24	14.3	0.35	0.2	1.0	125	6.7	23.0	23.2	0.4	9.2	29.5
40004	12	24 2 66	20.0	22	5.07	11.6	0.24	0	0		6.7	25.0	23.2	0.4	9.2	29.5
40004	13	17 6 66	16.4	17	5.91	7.0	0.54	0.8	4.2	128	5.3	26.5				
40004	14	29 11 66	17.6	6	3.81	8.1	0.50	0	3.1	128	3.9	19.0	26.2	6.9	7.2	27.9
40004	15	9 12 66	26.7	25	4.07	11.1	0.60	0	2.5	127	3.7	22.0	25.0	8.8	9.3	25.5
40004	16	25 1 67	1.8	7	4.83	3.2	0.84	0	4.0	128	3.2	25.2	26.5	7.8	10.7	29.5
40004	17	20 2 67	16.7	15	3.37	7.3	0.53	0	6.6	131	3.4	25.1	21.5	6.9	8.7	22.5
40004	18	2 2 67	17.3	15	3.51	7.3	0.51	0	2.2	127	3.3	22.0	21.5	7.0	10.1	30.9
40004	19	6 6 67	16.1	14	4.09	5.1	0.57	3.5	1.0	122	3.5	17.0	25.6	6.5	9.0	25.1
40004	20	2 6 67	33.3	3	4.70	7.0	0.41	44.2	8.6	69	2.9	8.5	32.5	7.0	7.0	20.2
40004	21	17 6 67	33.0	20	7.23	13.4	0.37	33.0	6.3	115	10.5	30.1				
40004	22	18 12 67	9.3	13	3.60	6.9	0.42	9.6	0.2	115	3.4	17.5	25.0	7.5	8.7	17.1
40004	24	21 12 66	7.7	8	4.17	6.1	0.90	0	6.1	131	3.0	30.5	23.0	7.4	9.4	26.3
40004	26	11 3 69	31.3	14	6.52	10.8	0.73	0	8.6	133	9.7	31.8	21.5	6.5	8.5	34.7
40004	27	14 9 69	24.3	16	34.86	7.1	0.72	41.0	1.5	85	42.3	36.7	27.4	7.0	9.0	22.0
40007	1	8 10 60	12.0	26	31.89	14.0	3.24	4.3	3.2	124	12.2	38.1				
40007	2	25 10 60	30.8	17	62.08	14.5	4.23	0	2.5	127	16.5	53.4				
40007	3	18 10 60	15.4	20	57.08	19.2	7.70	0	11.6	136	12.4	47.0				
40007	4	31 10 60	27.5	28	48.63	12.2	12.53	0	18.0	142	13.5	46.9				
40007	5	25 12 60	23.4	14	42.97	14.4	7.84	0	5.6	137	14.5	62.5				
40007	6	2 12 60	5	31	100.30	9.3	7.81	0	2.6	127	23.8	39.4				
40007	7	7 9 61	33.0	24	40.42	18.7	4.85	0.2	4.2	128	19.4	62.8				
40007	8	21 6 61	12.9	21	65.24	15.9	8.90	0	6.6	133	17.6	53.6				
40007	9	27 7 61	19.3	10	36.40	11.3	5.98	0	6.6	133	8.3	42.1				
40007	10	10 1 62	20.6	14	40.81	13.9	4.62	0	7.5	132	9.8	52.6				
40007	11	1 1 62	20.9	19	35.06	10.8	10.68	0	6.9	131	9.6	42.7				
40007	12	10 3 63	23.2	24	35.14	12.0	5.04	0	7.5	132	9.2	34.6				
40007	13	10 11 63	27.6	13	41.25	12.0	4.99	0	4.3	139	7.8	36.7				
40007	14	17 11 63	80.6	33	57.01	14.1	6.11	0	4.6	129	42.6	27.1				
40007	15	24 11 63	32.3	30	28.85	16.9	4.80	0	1.7	138	5.2	43.7				
40007	16	7 6 64	42.0	22	43.84	17.6	2.67	8.1	1.7	118	12.1	28.8				
40007	17	28 11 65	28.4	20	43.84	11.0	3.11	0	3.2	128	10.8	38.0				
40007	18	2 10 66	39.1	21	43.94	15.4	3.47	7.3	3.6	121	13.0	37.1				
40007	22	23 2 67	28.8	18	45.40	15.1										

CATCH NO	EV NO	DATE OF STORM	RAINFALL TOTAL (MM)	DURN (H)	PEAK FLOW (CUMEC)	LAG (H)	INSP (CUMEC)	SND (MM)	AP25 (MM)	CWT (MM)	1-HOUR UNIT HYDROGRAPH					
											UM PER 100 SQ KMS	TIME TO PEAK (H)	WIDTH AT 0.5 PEAK (H)	UM TIME BASE (H)		
41022	1	28 11 70	25.5	19	9.99	9.5	0.62	0.	1.0	125	13.3	52.0	19.0	12.0	11.5	35.5
41022	4	5 3 72	11.9	3	6.79	3.4	1.28	0.	12.1	137	6.0	30.2	22.5	7.5	11.5	26.4
41022	5	12 12 72	14.7	1	3.64	3.6	2.16	9.8	5.0	120	6.3	43.0	21.0	9.8	13.0	27.0
41022	7	21 11 74	23.0	14	27.45	7.8	9.29	0.	13.2	138	11.7	46.6	34.0	7.6	8.0	16.7
41022	8	19 1 75	34.3	18	29.84	7.2	1.62	35.6	5.1	94	21.8	63.6	33.0	7.6	8.0	17.7
41022	10	8 4 75	14.3	10	10.09	5.2	1.64	0.4	5.6	130	6.6	46.5	25.0	4.8	10.5	23.5
41022	11	18 4 75	20.7	15	10.38	7.9	0.77	3.5	2.9	124	10.3	49.8	19.0	4.0	14.0	30.5
41022	12	1 12 75	32.7	18	16.49	6.4	0.69	12.5	3.3	115	14.0	42.7	25.0	4.6	9.5	25.5
41025	2	10 2 72	14.6	33	3.62	17.9	1.19	0.2	1.9	126	7.9	53.9
41025	3	4 3 72	20.6	19	17.50	22.8	1.12	0.	3.1	130	13.1	63.6
41025	5	12 12 72	13.5	17	11.99	21.9	3.86	0.	7.2	132	5.9	43.9
41025	7	14 2 74	23.6	30	23.68	15.1	2.30	0.2	5.0	129	16.9	66.2
41025	10	24 12 74	23.4	26	20.14	23.5	1.94	0.	4.1	129	14.5	61.9
41025	12	1 12 75	26.8	17	21.90	19.2	0.91	14.1	3.8	114	16.5	61.4
41028	1	13 1 65	20.1	13	5.39	10.2	0.47	2.9	3.0	125	10.6	52.8	21.0	9.5	11.4	30.2
41028	2	19 11 65	43.6	16	3.93	7.1	0.55	0.	3.3	128	17.6	40.4	22.5	6.8	11.5	26.4
41028	3	29 11 65	27.4	21	5.79	5.0	7.45	0.	3.0	127	13.1	47.8	21.5	7.6	10.7	30.3
41028	4	8 12 65	35.3	26	10.40	11.1	0.39	0.2	1.4	126	20.1	56.8
41028	5	22 12 65	23.8	14	7.50	6.8	0.82	0.	2.1	127	12.8	53.7	27.0	7.6	9.0	23.2
41028	6	19 2 66	33.3	35	6.19	11.9	0.65	0.	4.7	129	19.6	58.8	24.0	6.5	9.5	27.3
41028	7	20 2 67	16.0	9	6.17	3.0	0.50	0.	8.4	133	8.7	54.4	29.3	8.5	8.2	21.6
41028	8	27 2 67	26.8	17	5.63	7.4	0.37	0.	2.4	127	13.7	51.2	20.8	8.7	12.0	29.5
41028	9	7 11 67	45.5	24	7.70	12.0	0.72	1.4	12.1	135	21.6	47.4	19.4	10.0	15.0	27.3
41028	10	3 2 68	19.1	11	6.29	5.6	0.97	0.	8.4	133	10.2	53.5	24.5	9.0	9.5	26.4
41028	11	10 10 68	26.2	13	6.79	6.8	0.84	0.6	7.0	131	12.5	47.9	21.2	9.0	10.5	19.1
41028	12	15 10 68	19.4	20	3.69	9.0	0.18	26.2	5.9	104	9.9	30.8	29.0	9.1	8.4	21.5
41028	13	22 1 71	29.3	18	6.11	5.2	0.75	0.2	3.9	130	14.0	47.6	21.5	10.4	12.6	32.8
41028	14	10 1 72	31.2	13	4.27	11.8	0.16	0.	2.5	127	11.6	37.3	18.8	11.3	12.0	35.1
41028	15	24 2 74	42.9	19	8.48	9.1	0.69	0.	3.9	130	23.1	33.9	21.4	10.1	12.7	26.6
41028	16	21 11 74	40.9	18	13.62	5.5	3.08	0.	10.9	133	14.5	35.4	27.3	6.3	8.6	23.5
41028	19	1 1 75	31.7	26	8.27	8.5	0.66	0.	10.0	134	14.3	31.5	27.0	9.0	10.1	25.1
41801	3	12 2 69	19.7	25	3.31	5.2	0.32	0.	7.0	124	12.4	52.4
41801	4	12 3 69	18.2	17	0.94	3.3	0.97	0.	6.5	131	7.0	38.3	43.5	5.6	6.0	13.6
41801	5	31 3 69	19.7	5	1.62	2.9	0.33	41.8	1.2	94	3.5	18.0
41801	6	4 7 69	43.4	19	1.74	4.3	0.01	94.6	0.	30	7.1	16.3	55.8	4.0	4.1	11.7
41801	7	28 7 69	31.2	13	0.75	3.4	0.01	104.5	0.	18	4.5	14.5	51.6	2.2	4.2	15.2
41801	8	1 8 69	15.3	5	1.31	1.9	0.02	92.1	1.6	34	2.7	17.6	64.6	3.2	3.8	9.6
41801	9	2 8 69	19.8	9	3.77	4.7	0.07	97.3	0.4	54	3.0	17.5	50.2	3.6	4.4	11.0
41801	10	13 11 70	33.6	30	2.76	5.6	0.06	52.5	3.0	75	42.8	76.6
41801	11	13 6 71	50.8	34	2.93	9.8	0.02	39.0	4.7	70	19.8	33.2	38.5	4.1	4.5	19.9
41801	12	18 6 71	30.8	12	1.48	4.1	0.05	15.1	6.6	116	12.9	41.8	39.2	3.1	6.5	15.4
41801	13	8 11 69	23.3	7	1.24	3.1	0.00	98.6	4.9	31	4.0	17.3	66.0	4.3	4.1	8.6
41801	14	6 12 72	12.5	9	2.48	4.1	0.06	44.3	8.8	89	5.2	41.9	65.0	4.1	3.8	9.3
41801	15	21 5 73	24.1	6	2.44	2.3	0.03	23.1	1.2	103	9.9	20.3
41801	16	21 11 74	30.2	17	3.02	3.8	0.15	0.	11.6	136	17.3	37.2	66.4	3.3	3.3	10.7
41801	20	28 11 75	26.5	8	2.84	3.5	0.14	14.4	8.7	119	10.7	36.2	53.0	3.5	4.3	12.4
45002	1	24 8 63	23.3	16	37.80	10.2	10.14	2.9	3.9	124	4.6	19.8
45002	2	18 11 63	50.7	15	14.50	2.2	22.30	0.	17.4	142	24.6	47.7
45002	3	12 11 64	30.8	24	69.96	7.4	6.04	20.9	1.9	96	4.5	14.7	28.1	8.0	7.3	23.0
45002	4	15 11 65	29.0	17	167.45	8.1	41.80	0.	7.5	132	13.6	47.0
45002	5	23 11 65	51.2	44	155.58	11.8	45.47	0.	13.1	138	27.6	54.0
45002	6	20 1 66	20.9	6	70.71	6.7	13.97	0.2	0.5	125	3.4	16.2
45002	7	28 11 65	26.0	21	102.94	5.9	31.17	0.	6.1	131	6.5	25.0	27.6	7.0	7.2	35.0
45002	8	8 12 65	68.5	43	188.51	14.7	32.22	0.1	3.7	128	37.1	56.1
45002	9	14 10 66	25.5	13	61.53	7.8	11.03	1.0	8.7	132	4.7	18.3	25.2	8.0	7.0	28.3
45002	10	9 12 66	34.3	26	109.80	5.9	23.14	0.	3.6	128	11.6	33.3	24.2	7.6	8.0	30.0
45002	11	12 12 66	47.5	44	133.76	12.2	40.20	0.	6.9	131	18.5	38.9
45002	12	30 12 66	28.9	18	147.19	8.8	41.89	0.	10.2	133	11.2	38.9
45002	13	20 2 67	32.6	21	149.83	9.9	39.45	0.	21.6	146	17.3	52.6
45002	14	27 2 67	34.5	21	154.66	6.4	28.51	0.	3.2	128	10.2	29.3	29.5	7.8	6.5	24.7
45002	15	4 3 68	13.6	6	135.16	13.5	29.95	0.	5.2	130	27.3	33.6
45002	16	7 1 68	55.1	20	169.32	13.8	16.44	10.5	3.4	117	15.7	28.5	27.4	7.0	6.6	27.4
45002	17	27 7 69	100.3	29	74.02	13.4	3.74	88.6	0.0	36	8.6	8.6	28.0	7.0	7.4	24.9
45002	18	18 9 69	36.9	10	90.39	5.8	6.83	15.8	5.4	114	4.6	12.4
45002	19	16 12 65	14.5	54	22.34	9.9	36.42	0.	8.1	133	63.3	61.1
45002	22	1 11 70	47.2	16	171.42	13.0	36.49	0.	3.8	128	24.1	51.1
45003	2	10 11 63	23.2	19	26.62	13.4	6.19	30.1	3.0	99	7.0	30.2	14.2	13.3	18.3	41.7
45003	3	15 11 63	24.2	31	31.35	9.1	7.81	0.	9.0	134	7.9	32.7	18.0	12.6	13.3	35.2
45003	4	19 11 65	25.3	23	63.94	9.7	5.03	0.	4.2	129	11.7	46.1
45003	5	29 11 65	25.3	19	62.01	5.2	6.05	2.4	4.9	127	11.2	44.3	22.8	10.5	11.0	26.8
45003	6	8 12 65	29.7	44	39.12	14.3	5.97	0.1	2.6	127	11.8	39.1	17.6	11.4	11.0	41.2
45003	7	1 1 66	21.2	25	30.24	5.4	9.27	0.	8.1	133	8.7	40.9	22.3	10.5	10.7	28.5
45003	8	22 12 66	25.8	8	47.48	12.2	3.54	46.8	1.4	79	10.5	36.4	20.0	12.4	11.0	33.6
45003	9	28 12 66	24.4	36	34.20	13.1	4.71	0.	3.1	128	8.9	36.4	20.0	11.6	10.2	33.2
45003	10	16 2 67	25.6	17	65.01	10.0	3.27	0.	16.0	140	15.1	59.2	25.0	11.0	10.7	24.3
45003	11	19 2 67	21.3	25	53.63	11.6	9.21	0.	11.2	136	9.0	42.0	23.4	10.2	11.0	25.3
45003	12	30 10 67	29.4	16	48.43	13.2	5.07	22.1	6.9	109	12.1	41.1	17.7	13.2	14.0	33.6
45003	13	8 1 68	31.7	24	71.59	11.0	4.86	0.	4.1	129	15.0	50.4	19.8	12.0	12.0	32.2
45003	14	10 7 68	57.2	18	201.66	6.4	3.06	42.0	4.2	87	30.3	58.6
45003	16	23 12 68	28.9	39	37.77	16.9	6.07	0.	4.9	129	12.3	42.6	16.5	9.5	14.0	39.4
45003	18	27 7 69	110.8	30	115.51	14.7	1.43	120.3	0.1	4	19.4	17.5	27.0	11.6	8.9	23.4
45004	1	16 2 67	35.6	30	62.95	9.3	7.75	0.	8.2	133	12.2	34.3	23.7	9.7	10.1	24.7
45004	2	3 3 67	48.4	32	42.07</											

CATCH NO	EV NO	DATE OF STORM	RAINFALL		PEAK FLOW (CUMEC/S)	LAG (H)	ANSF (CUMEC/S)	SMD (MM)	APIS (MM)	CWI (MM)	1-HOUR UNIT HYDROGRAPH		UH PEAK (CUMEC/S)	UH TIME WIDTH (H)	UH AT 0.5 (H)	UH BASE (H)
			TOTAL (MM)	DURN (H)							PER 100 SQ KMS	TO AT 0.5				
47007	5	17 1	65	10.1	20.81	7.6	5.80	0.	16.6	141	27.8	57.8	27.7	4.5	7.0	26.1
47007	6	22 1	65	10.1	21.58	6.1	5.03	0.	9.0	133	9.9	32.1	36.5	5.5	6.1	18.4
47007	7	28 1	65	10.1	21.78	5.7	3.12	0.	0.8	125	11.1	33.4	36.7	5.6	6.1	18.1
47007	8	24 2	66	10.1	21.88	5.3	2.01	0.	1.9	126	8.4	23.1	43.5	4.2	5.0	15.6
47007	10	2 2	66	10.1	21.98	5.0	3.80	0.	9.4	134	10.4	39.0	41.5	4.8	5.3	16.3
47007	11	5 2	66	10.1	22.00	4.7	0.91	2.6	4.8	127	9.4	17.5	41.1	6.0	5.8	15.6
47007	12	22 2	66	10.1	22.08	4.3	2.57	0.	3.0	127	10.0	22.7	38.0	6.0	5.1	17.2
47007	13	20 2	67	10.1	22.04	6.9	1.83	0.	15.3	144	8.4	34.4	36.0	5.4	6.7	18.3
47007	14	27 2	68	10.1	23.31	7.1	1.88	0.4	10.2	144	17.6	35.3	28.2	4.2	8.6	22.3
47008	2	12 1	72	10.1	30.42	5.1	4.17	0.	16.6	141	9.4	40.0				
47008	4	30 1	72	10.1	30.70	14.1	3.41	0.	5.6	130	20.6	59.1				
47008	6	22 1	73	10.1	31.32	7.6	0.85	0.	1.3	116	4.1	21.2				
47008	7	15 1	73	10.1	31.07	5.0	2.78	0.	2.6	127	2.7	20.0				
47008	8	29 1	73	10.1	31.04			0.	1.1	124	1.5	16.0				
47008	10	25 1	74	10.1	31.01		1.15	0.	4.2	129	12.0	40.8				
47008	14	13 1	75	10.1	31.21	3.9		5.5	7.4	66	1.9	5.0				
47011	1	1 1	101	10.1	16.33	3.7		1.5	1.1		3.8	11.6	50.5	4.2	4.7	12.6
47011	2	15 1	101	10.1	16.94	6.7	0.67	33.0	7.1	78	7.2	19.8	28.3	7.9	8.8	21.7
47011	3	1 1	101	10.1	18.46	4.9	1.46	0.	0.2	125	6.1	15.9				
47011	5	23 1	101	10.1	31.73	3.1	3.40	1.1	3.7	129	8.1	30.8	43.0	3.9	6.0	15.9
47011	6	1 1	101	10.1	32.39	7.1	2.48	1.7	3.6	126	8.3	27.3				
47011	8	1 1	101	10.1	33.01											
47011	9	4 1	101	10.1	33.63	6.5	1.20	2.9	1.5	123	5.2	17.0	39.7	7.5	5.9	16.2
47011	12	3 1	101	10.1	34.25	10.1	0.99	27.9	2.3	99	21.4	30.4				
47011	14	26 1	101	10.1	34.87	3.2	4.69	0.	5.1	117	23.3	54.2				
47011	15	10 1	101	10.1	35.49	4.7	3.24	0.	1.1							
47011	16	12 1	101	10.1	36.11	6.8	2.78	0.	2.3	121	7.7	26.5				
47011	17	21 1	101	10.1	36.73	6.8	4.09	0.	9.0	134	14.7	29.7	31.1	6.4	7.9	20.2
47011	17	21 1	101	10.1	37.35	5.3	3.64	0.	3.1	130	9.4	45.2				
48004	1	17 1	101	10.1	14.00	8.2	2.03	0.	13.2	138	17.1	47.0	34.4	4.0	5.7	20.0
48004	2	11 2	101	10.1	14.62	6.9	1.48	0.	3.2	129	11.6	40.1	30.6	6.8	7.4	21.5
48004	3	20 2	101	10.1	15.24	13.8	0.54	0.	12.1	101	12.3	26.6	27.2	8.5	8.0	24.9
48004	4	6 11	101	10.1	15.86	10.3	0.52	35.6	5.7	103	7.3	21.4	22.5	9.4	9.4	26.6
48004	5	17 6	101	10.1	16.48	5.2	0.29	28.6	7.1	90	6.4	15.3	20.0	7.0	7.0	17.6
48004	7	11 6	101	10.1	17.10	13.6	0.69	1.4	1.1	120	10.4	27.9	27.2	8.0	5.0	24.0
48004	9	17 11	101	10.1	17.72	7.7	1.05	0.	5.2	130	10.3	29.3	28.0	6.0	9.0	28.5
48004	10	26 9	101	10.1	18.34	11.0	0.59	0.	1.9	126	21.0	34.0	32.0	6.3	6.3	21.8
48004	11	17 11	101	10.1	18.96	10.2	1.33	0.7	11.1	135	14.4	47.5	35.6	7.5	5.9	19.4
48004	12	12 11	101	10.1	19.58	6.9	1.01	0.	3.2	128	13.1	32.3	25.3	6.2	9.4	25.4
48004	12	12 11	101	10.1	20.20	6.4	1.47	0.	0.5	134	15.4	51.1	37.0	7.7	6.5	17.1
48005	2	25 4	101	10.1	20.82	6.2	0.17	0.	3.0	128	2.2	9.5	41.3	4.0	3.5	16.7
48005	3	28 7	101	10.1	21.44	7.5	0.11	3.6	0.1	124	5.1	5.9	33.0	8.1	7.9	17.9
48005	6	18 8	101	10.1	22.06	5.1	0.31	0.	1.1	124	1.1	6.4	48.6	4.4	4.8	13.3
48005	9	1 11	101	10.1	22.68	2.0	0.15	44.6	6.3	86	0.9	3.8	53.2	3.0	4.4	19.1
48005	11	1 11	101	10.1	23.30	1.7	0.15	1.7	2.2	127	6.4	20.0	40.4	4.4	4.4	17.7
48005	13	30 11	101	10.1	23.92	4.3	1.17	0.	2.5	127	2.1	12.0	50.5	4.0	4.5	12.4
48005	13	30 11	101	10.1	24.54	4.3	1.17	0.	7.0	131	2.4	19.1	59.6	4.1	4.1	10.5
48005	15	16 6	101	10.1	25.16	1.6	0.27	0.	2.9	127	1.8	11.1	60.0	3.1	4.2	10.1
48005	16	13 6	101	10.1	25.78	4.0	0.15	96.2	10.1	124	1.3	4.4	39.8	4.4	3.8	14.3
48005	16	13 6	101	10.1	26.40	3.2	0.15	76.8	4.4	124	4.4	8.3	43.1	3.3	4.3	17.2
48009	2	29 11	101	10.1	27.02	7.9	1.79	0.	9.8	134	24.9	49.2				
48009	4	25 11	101	10.1	27.64	6.3	1.39	0.	6.4	131	14.3	34.6	21.5	10.8	10.4	30.9
48009	5	31 11	101	10.1	28.26	7.9	0.2	0.2	0.6	121	1.4	32.2				
48009	6	11 11	101	10.1	28.88	13.8	0.75	5.5	3.5	122	1.1	37.9	15.0	9.8	13.4	47.3
48009	8	4 11	101	10.1	29.50	19.0	0.27	81.6	7.3	90		27.2				
48009	9	17 10	101	10.1	30.12	3.4	0.97	0.	3.5	128	3.6	21.0		9.5	11.0	31.0
48009	10	12 11	101	10.1	30.74	3.4	1.68	6.	10.3	125	16.4	50.7	31.0	11.3	8.0	19.9
49003	1	20 12	66	10.1	14.10	5.9	1.56	0.	14.4	139	1.8	52.4	37.0	4.2	6.0	18.1
49003	2	22 1	67	10.1	14.72	5.0	1.01	0.	0.7	134	1.8	53.6	38.1	3.3	6.2	16.8
49003	3	27 1	67	10.1	15.34	1.0	0.15	0.	0.5	129	25.1	94.9	38.5	6.3	5.3	18.1
49003	4	15 1	67	10.1	15.96	5.8	1.50	0.	14.3	139	36.9	74.8				
49003	6	17 12	67	10.1	16.58	8.5	0.81	0.	1.4	136	30.9	90.1				
49003	7	21 12	68	10.1	17.20	5.6	0.78	0.	9.1	129	13.5	48.6	30.0	7.7	7.2	22.7
49003	8	23 12	68	10.1	17.82	13.9	0.56	0.	9.1	134	18.2	88.5	35.0	6.6	5.5	18.8
49003	9	27 7	70	10.1	18.44	9.0	0.87	95.0	0.1	51	24.7	88.0	31.7	6.7	6.9	21.3
49003	10	16 1	70	10.1	19.06	0.1	0.17	0.	12.8	137	24.7	51.9	37.0	5.0	5.6	18.9
49003	11	1 11	70	10.1	19.68	5.6	0.47	0.	7.2	132	23.7	50.3	33.0	4.2	6.1	21.5
49003	12	29 11	71	10.1	20.30	3.6	4.79	0.	9.8	134	10.5	16.3	34.0	7.7	6.3	20.1
49003	13	23 1	72	10.1	20.92	5.9	0.59	0.	5.6	131	18.9	52.0	34.0	6.8	8.1	14.7
49003	14	14 1	72	10.1	21.54	6.0	0.39	0.	10.0	135	17.2	64.0	34.8	5.8	5.0	20.2
49003	15	11 11	72	10.1	22.16	5.9	0.32	0.	6.1	131	16.4	47.1	32.0	4.2	6.7	21.6
49003	16	1 11	73	10.1	22.78	7.9	0.08	11.9	2.3	115	9.3	25.9	38.1	6.2	6.6	16.9
49003	17	1 11	73	10.1	23.40	7.1	0.52	43.3	17.4	99	17.7	57.9	32.5	3.6	7.0	20.2
49003	18	13 10	74	10.1	24.02	6.7	0.11	90.2	6.9	41	10.7	20.1	39.3	5.4	3.5	17.5
49003	19	17 10	74	10.1	24.64	5.8	0.32	0.	2.3	127	27.3	60.7	37.5	4.0	6.0	15.0
51002	1	4 9	74	10.1	25.26	5.0	0.92	67.3	22.3	80	3.7	14.6	32.0	5.5	7.0	20.8
51002	2	22 9	74	10.1	25.88	3.5	0.54	90.5	6.3	40	5.8	13.4	32.4	4.0	6.5	21.3
51002	3	26 9	74	10.1	26.50	4.1	0.22	0.6	12.5	136	10.9	18.9	29.5	3.0	3.5	26.7
51002	4	10 11	74	10.1	27.12	6.1	0.84	6.2	6.2	124	2.8	16.5	31.7	6.0	8.0	19.6
51002	5	19 11	74	10.1	27.74	6.1	0.46	0.	3.5	128	4.8	15.9	31.5	4.4	6.5	22.3
51002	11	30 1	75	10.1	28.36	3.1	1.70	0.	11.7	136	7.9	16.7	42.5	3.5	5.6	15.0
51002	13	30 11	75	10.1	28.98	3.6	0.10	23.0	0.6	57	1.5	9.1	29.2	3.9	8.0	23.4
51002	13	30 11	75	10.1	29.60	3.6	1.19	15.7	6.1	115	8.9	17.3				
52004	1	22 10	66	10.1	10.4	1.98	46.8	5.7	7.9	7.9	11.1	33.7	25.0	7.4	10.2	24.1

CATCH NO	EV NO	DATE OF STORM	RAINFALL		LAG (H)	ANSF (CUMEC)	1-HOUR UNIT HYDROGRAPH			UM PEAK (CUMEC)	TIME TO PEAK (H)	UM WIDTH AT 0.5 PEAK (H)	UM BASE (H)
			(MM)	(H)			(MM)	(MM)	(MM)				
54004	8	22 7 22	65	20.1	20	32.0	10.0	49.6	9.3	13.0	22.0	75.6	
54004	9	22 7 22	68	20.5	20	32.0	10.0	49.6	9.3	13.0	22.0	75.6	
54004	10	22 7 22	68	20.5	20	32.0	10.0	49.6	9.3	13.0	22.0	75.6	
54004	11	22 7 22	68	20.5	20	32.0	10.0	49.6	9.3	13.0	22.0	75.6	
54004	12	22 7 22	68	20.5	20	32.0	10.0	49.6	9.3	13.0	22.0	75.6	
54004	13	22 7 22	68	20.5	20	32.0	10.0	49.6	9.3	13.0	22.0	75.6	
54004	14	22 7 22	68	20.5	20	32.0	10.0	49.6	9.3	13.0	22.0	75.6	
54006	9	10 12 68	68	36.4	21	20.0	10.0	5.8	120	5.7	15.8	57.0	
54006	10	10 12 68	69	28.3	25	19.0	10.0	5.8	120	5.7	15.8	57.0	
54006	11	10 12 68	69	35.7	13	21.0	10.0	5.8	120	5.7	15.8	57.0	
54006	12	10 12 68	69	28.7	22	18.0	10.0	5.8	120	5.7	15.8	57.0	
54006	14	10 12 68	69	44.9	25	20.0	10.0	5.8	120	5.7	15.8	57.0	

CATCH NO	EV NO	DATE OF STORM	RAINFALL		LAG (H)	ANSF (CUMEC)	1-HOUR UNIT HYDROGRAPH			UM PEAK (CUMEC)	TIME TO PEAK (H)	UM WIDTH AT 0.5 PEAK (H)	UM BASE (H)				
			(MM)	(H)			(MM)	(MM)	(MM)					(MM)	(MM)		
54090	8	24 9 75	34	60.2	67.0	91.2	1.3	1.6	9.0								
54090	9	30 11 75	31	116.6	31	1.94	1.7	0.07	4.4	7.2	127	88.5	75.9	98.9	1.5	2.1	7.0
54090	10	30 12 75	29	95.9	29	1.73	5.2	0.04	0.2	1.3	126	59.5	66.9	107.5	1.9	1.7	7.0
54090	11	11 2 76	25	86.4	25	1.75	2.1	0.06	0.1	5.3	130	54.0	75.9	71.1	1.2	2.3	10.9
54090	12	5 7 76	27	97.3	27	1.18	0.8	0.01	97.1	2.8	30	4.2	13.7	141.4	1.4	1.6	4.8
54090	13	15 8 77	27	97.6	27	1.18	0.8	0.01	80.1	4.9	49	33.6	34.4	129.4	1.9	1.7	5.1
54090	14	9 9 77	17	73.6	17	1.50	2.8	0.07	0.1	4.1	120	47.1	64.0	91.6	1.7	1.9	8.4
54090	16	1 11 77	23	76.9	23	2.51	3.1	0.12	0.3	27.4	152	52.0	67.5	92.5	1.1	1.5	9.0
54090	17	22 11 77	19	48.7	19	1.68	3.2	0.07	0.1	10.1	135	23.1	47.5	92.5	1.1	1.5	9.0

CATCH NO	EV NO	DATE OF STORM	RAINFALL		PEAK FLOW (CUMEC)	LAG (H)	ANSF (CUMEC)	SMD (MM)	APIS (MM)	CWI (MM)	1-HOUR UNIT HYDROGRAPH					
			TOTAL (MM)	DURN (H)							UH PEAK (CUMEC)	UH TIME (H)	UH WIDTH (H)	UH TIME BASE (H)		
56005	12	6 11 70	57.3	20	31.32	4.8	5.43	1.2	1.8	125	15.0	26.1	22.7	6.2	11.2	26.6
56005	14	24 1 75	31.7	11	34.86	5.8	6.97	0.	10.8	135	9.6	30.3	37.5	4.1	1.4	18.9
56005	15	14 2 74	42.5	14	36.35	4.8	6.44	0.	10.3	135	11.9	28.0	30.7	5.0	8.6	19.0
56005	16	10 10 76	30.6	11	46.84	4.1	7.78	14.3	6.3	117	12.5	40.7	*	*	*	*
56005	17	13 10 76	30.9	14	40.33	6.0	8.10	6.4	7.1	125	15.4	49.8	*	*	*	*
56005	18	17 10 76	41.7	17	49.59	6.8	9.93	2.9	5.8	127	18.9	45.4	*	*	*	*
56006	1	11 12 64	81.7	39	193.65	5.2	12.40	0.	9.1	134	52.6	64.4	*	*	*	*
56006	2	12 1 65	44.8	16	226.53	2.8	18.70	0.	13.7	138	23.6	63.9	67.6	4.5	3.8	8.8
56006	3	8 12 65	59.1	48	148.38	4.8	8.76	0.	3.2	128	33.1	50.8	*	*	*	*
56006	4	16 12 65	144.6	52	223.56	5.5	11.02	0.	2.2	134	104.8	73.9	*	*	*	*
56006	5	24 2 66	53.0	15	193.12	3.3	16.18	0.	8.1	133	30.5	57.5	60.0	3.5	4.0	10.5
56006	6	27 2 67	64.0	18	239.32	5.3	13.57	0.	8.2	133	42.0	65.6	38.5	6.0	5.3	18.3
56006	7	16 10 67	81.0	18	242.66	3.6	17.05	0.	14.2	139	48.0	59.3	44.0	5.8	5.6	14.1
56006	12	10 2 74	57.8	25	142.40	3.5	33.30	0.	19.7	144	27.2	47.1	50.0	3.5	4.6	13.0
56006	14	12 11 74	98.9	29	160.68	6.5	14.95	0.	16.7	141	33.9	49.2	38.0	3.7	6.0	17.3
56006	16	24 9 75	74.9	32	78.31	2.8	6.22	105.7	2.0	21	14.4	19.2	29.5	3.6	7.2	23.3
56006	17	11 2 76	41.1	21	76.95	6.7	6.53	0.	2.6	127	19.9	38.7	*	*	*	*
56006	18	2 2 77	40.3	20	89.41	3.7	14.38	0.	3.6	128	11.8	29.2	36.5	5.8	4.0	19.4
56006	19	11 12 77	50.2	22	100.01	3.1	14.77	0.	14.0	139	12.9	42.2	40.0	4.6	5.8	16.2
56011	3	30 11 73	47.8	26	26.33	9.4	1.14	0.	2.4	127	19.2	40.2	22.3	4.0	8.2	33.5
56011	4	11 2 76	24.8	18	10.94	9.9	1.50	0.	3.8	128	7.7	31.0	18.3	10.5	12.5	35.8
56011	5	24 9 76	57.7	22	42.95	6.2	2.79	62.2	17.4	80	13.0	26.0	33.7	7.6	6.8	19.4
56011	7	14 3 77	40.3	31	25.03	2.8	3.14	0.	7.8	132	9.6	23.9	38.4	4.2	6.0	17.0
57004	1	10 10 68	43.7	12	65.38	4.4	10.67	0.	11.6	136	17.6	40.3	45.0	1.8	4.8	15.1
57004	2	22 4 70	40.2	18	61.30	4.6	12.57	0.6	16.0	140	15.5	38.4	42.3	1.7	3.4	19.4
57004	3	1 11 70	63.8	15	93.74	3.7	18.50	0.	28.4	133	35.1	55.1	43.5	2.7	3.8	18.0
57004	4	6 1 71	71.5	23	89.19	5.1	4.01	0.	2.7	127	23.4	32.7	69.0	2.1	2.5	11.1
57004	5	17 10 71	97.0	39	82.37	6.5	5.64	0.	10.2	137	47.4	48.8	33.5	3.7	4.7	23.8
57004	6	14 2 72	95.6	31	73.51	5.4	6.21	0.	2.3	127	42.4	44.4	38.0	3.0	4.5	20.3
57004	7	7 9 72	68.2	22	61.93	6.0	5.63	33.7	5.7	95	11.2	16.4	70.0	2.0	2.6	10.7
57004	8	12 11 72	64.8	18	97.35	2.8	9.62	0.	8.3	133	27.0	41.7	47.5	2.0	4.0	15.4
57004	9	30 11 72	68.3	30	74.46	5.3	9.32	0.	17.8	142	40.0	58.6	32.5	2.0	5.0	24.2
57004	10	3 12 72	48.4	19	62.46	3.8	14.44	0.	24.5	149	19.2	39.6	33.5	2.0	5.1	23.0
57004	11	4 12 72	75.0	21	91.75	4.0	22.98	0.	32.4	157	37.4	49.9	38.5	2.0	5.3	18.3
57004	12	12 12 72	57.1	12	94.37	3.9	19.11	0.	22.7	147	26.2	46.9	45.0	2.4	4.5	15.7
57004	13	1 4 73	66.7	19	60.08	6.1	2.91	0.6	1.2	125	19.0	28.5	48.0	2.9	4.6	14.8
57004	14	4 8 73	83.1	26	79.11	4.3	6.28	0.	16.8	141	24.5	29.5	47.0	3.4	4.2	14.8
57004	15	9 1 74	40.9	9	76.32	3.4	10.98	0.	12.4	137	15.3	37.4	45.0	2.9	4.5	14.7
57004	16	10 11 74	42.4	17	64.47	2.8	10.28	0.	15.9	140	14.2	33.4	70.0	2.0	2.3	11.3
57004	17	12 11 74	61.7	24	87.94	2.0	15.26	0.	22.3	147	27.6	44.7	*	*	*	*
57004	18	19 1 75	57.2	21	98.89	4.6	9.43	0.	6.7	131	26.3	46.0	66.0	3.0	2.8	11.8
57004	19	24 1 75	75.2	20	108.52	6.5	14.21	0.	25.0	150	45.5	60.6	50.0	3.0	3.7	14.8
57004	20	30 11 75	51.6	13	91.33	3.9	14.1	0.	25.6	150	22.7	44.0	58.0	2.0	2.9	13.4
57004	22	3 10 76	91.4	21	113.07	3.5	10.1	0.	4.7	129	47.1	51.5	45.0	2.0	3.5	17.7
57004	23	4 10 76	64.3	26	69.27	7.4	8.1	0.	16.1	141	36.8	57.2	27.5	4.6	5.0	28.6
57004	24	15 2 77	42.0	13	62.04	3.7	7.1	0.4	15.1	139	16.8	40.0	*	*	*	*
57004	25	10 10 77	59.9	24	64.26	4.9	5.46	0.1	3.2	128	23.1	39.2	42.3	2.1	4.4	17.4
57004	26	31 10 77	94.0	23	146.06	7.6	12.48	0.	26.1	151	64.6	68.7	45.3	2.7	3.7	17.0
58001	1	26 1 61	31.6	14	59.43	3.8	8.44	0.5	0.1	124	6.7	21.3	*	*	*	*
58001	2	10 9 62	66.7	29	114.88	5.3	6.53	0.	2.8	127	18.6	27.8	*	*	*	*
58001	3	16 11 63	55.4	16	107.34	4.9	16.31	0.	15.4	140	11.4	20.6	40.8	6.5	4.9	17.5
58001	4	15 11 63	48.5	29	127.72	5.3	39.52	0.	53.3	178	13.1	27.0	41.0	4.0	4.8	17.3
58001	5	13 7 64	56.8	27	48.84	3.8	8.28	5.5	33.3	134	12.4	21.8	*	*	*	*
58001	9	15 1 65	50.6	25	43.51	5.4	17.80	0.	17.0	142	19.5	38.5	20.4	4.0	11.0	32.5
58001	11	11 7 65	74.1	48	45.54	5.7	6.88	31.8	19.5	112	24.1	32.6	23.0	4.0	7.0	34.3
58001	12	7 12 65	82.5	36	99.57	6.4	15.27	0.	3.5	128	33.8	40.9	35.0	4.2	5.1	21.6
58001	15	30 12 66	46.0	17	119.87	4.1	23.17	0.	21.5	146	20.7	45.1	34.0	4.3	7.0	18.7
58001	17	28 7 67	78.6	29	112.62	8.6	5.73	19.5	19.7	125	39.7	45.5	26.3	4.2	4.4	33.5
58001	18	15 10 67	61.8	20	115.92	6.1	17.61	0.	16.5	141	32.7	53.0	33.8	5.4	4.7	23.5
58001	19	26 6 68	40.9	10	110.87	5.1	14.91	1.7	25.2	148	13.1	32.1	43.0	3.3	3.8	18.3
58001	20	27 10 68	49.8	29	69.68	5.1	14.73	0.	15.8	140	24.2	38.7	*	*	*	*
58001	21	1 11 70	64.7	15	143.82	5.6	27.62	0.	30.8	133	36.0	11.3	*	*	*	*
58002	10	1 11 70	52.8	17	154.68	4.6	2.51	0.	20.3	145	26.1	49.3	36.9	7.4	8.4	13.3
58002	11	6 1 71	69.7	24	141.22	7.6	0.52	0.	1.1	126	18.0	25.8	45.3	4.6	4.6	15.3
58002	12	9 8 71	67.2	18	128.04	6.9	4.96	4.6	2.0	122	24.6	36.6	38.0	3.4	7.2	14.9
58002	13	18 10 71	71.7	33	141.13	4.7	11.78	0.	14.5	139	28.2	39.4	36.0	3.4	6.0	18.9
58002	14	11 11 72	50.3	26	130.97	3.1	9.77	0.	8.3	133	16.3	32.4	35.5	4.8	6.4	18.5
58002	15	5 8 73	73.1	24	156.82	5.4	7.79	10.6	22.1	127	28.1	14.0	46.0	4.0	6.7	15.2

CATCH NO	EV NO	DATE OF STORM	RAINFALL		PEAK FLOW (CUMEC)	LAG (H)	ANSF (CUMEC)	SMD (MM)	APIS (MM)	CWI (MM)	1-HOUR UNIT HYDROGRAPH					
			TOTAL (MM)	DURN (H)							UH PEAK (CUMEC)	UH TIME (H)	UH WIDTH (H)	UH TIME BASE (H)		
58003	1	15 1 65	40.5	26	18.16	10.0	3.10	0.	10.9	135	18.2	44.9	23.2	7.7	9.6	24.9
58003	2	1 12 65	17.4	10	18.09	6.2	3.59	0.	7.2	132	7.1	40.7	34.7	6.7	7.0	

1-HOUR UNIT HYDROGRAPH

CATCH NO	EV NO	DATE OF STORM	RAINFALL TOTAL DURN (MM)	PEAK FLOW (CUMEC)	LAG (H)	ANSF (CUMEC)	SMD (MM)	APIS (MM)	CWI (MM)	RUNOFF (MM)	1-HOUR UNIT HYDROGRAPH			UM TIME BASE (H)		
											UM PEAK (CUMEC)	TIME TO AT 0.5 PEAK (H)	WIDTH PEAK (H)			
65001	13	14 9 65	123.3	28	52.78	9.1	0.35	3.2	4.5	126	52.9	42.7	25.5	3.4	9.8	24.0
65001	14	28 12 65	71.6	17	43.81	5.0	1.32	0.	0.7	125	25.3	35.3	31.3	3.7	7.0	21.5
65001	15	26 6 66	106.8	24	51.09	8.2	0.80	2.4	7.7	130	45.2	42.3	22.0	3.9	10.1	30.5
65001	21	22 3 68	117.2	34	56.63	11.0	1.52	0.	17.5	137	65.7	56.0	22.0	3.9	10.1	30.5
65801	2	28 4 72	86.3	17	17.00	4.0	0.44	20.0	1.0	105	38.9	45.1	45.0	2.1	5.1	14.5
65801	8	11 11 72	45.0	25	23.50	5.9	0.86	0.	11.9	136	53.5	82.8	49.2	6.7	5.1	12.4
65801	16	12 12 72	55.8	10	28.00	3.1	1.99	0.	36.5	161	44.3	79.3	69.0	2.4	3.0	10.1
66002	2	24 5 68	40.5	32	36.44	10.7	3.36	14.0	0.1	111	7.9	19.6	29.0	4.8	5.6	27.1
66002	3	30 6 68	66.3	51	58.51	9.1	3.44	40.0	2.8	87	12.0	18.0	29.0	4.8	5.6	27.1
66002	5	5 5 69	29.9	21	35.71	5.2	4.82	3.6	3.7	125	4.6	15.4	35.1	7.4	5.6	20.5
66002	10	5 7 73	76.8	25	42.74	13.3	0.05	102.7	21.0	43	8.0	10.5	20.6	1.8	9.2	20.5
66004	1	19 8 70	57.7	31	2.54	9.2	0.57	102.7	4.3	26	2.7	4.6	2.7	4.6	2.7	4.6
66004	2	11 6 71	21.5	10	1.38	5.5	0.34	54.4	8.0	78	0.6	2.7	0.6	2.7	0.6	2.7
66004	3	25 7 71	0.6	6	2.64	3.1	0.47	44.4	13.0	94	0.6	2.7	0.6	2.7	0.6	2.7
66004	7	8 11 71	30.7	22	3.83	11.0	0.84	77.6	0.7	48	2.6	4.6	2.6	4.6	2.6	4.6
66004	7	14 7 73	61.2	34	2.37	10.9	0.52	83.3	7.7	49	1.7	2.8	1.7	2.8	1.7	2.8
66906	1	15 7 73	74.4	29	63.92	15.8	3.19	101.9	18.6	41	17.5	23.6	24.3	6.5	6.7	32.4
66906	3	10 11 74	23.4	16	50.97	6.2	6.21	0.3	2.6	127	7.8	33.1	33.1	4.4	7.1	17.5
66906	7	2 7 76	30.4	13	81.79	6.2	16.47	8.3	17.9	134	12.8	42.2	42.2	4.6	7.1	17.5
66906	9	13 10 75	54.6	48	147.17	12.3	8.90	8.7	5.4	121	57.6	66.3	24.2	9.3	8.1	29.8
66011	1	7 7 64	71.6	15	235.74	5.4	6.51	44.4	0.1	80	19.3	27.0	27.0	2.7	4.6	2.7
66011	2	12 11 64	41.2	13	241.45	5.5	10.39	0.	8.1	133	21.4	51.9	36.9	4.3	6.4	17.3
66011	4	11 2 64	191.5	34	535.23	5.9	26.01	0.	22.3	147	147.5	77.0	2.7	4.6	2.7	4.6
66011	9	6 6 65	42.6	10	331.01	4.2	20.64	2.0	9.8	132	22.5	52.7	2.7	4.6	2.7	4.6
66011	10	30 10 66	50.6	17	301.86	5.5	15.83	0.	13.1	138	23.2	57.2	2.7	4.6	2.7	4.6
66011	11	10 10 66	75.4	43	335.68	1.3	27.90	0.	11.0	135	45.0	58.9	45.0	3.5	5.8	11.5
66011	12	26 8 67	71.8	19	379.45	2.7	17.45	0.	1.6	129	38.9	63.0	49.6	5.2	4.8	12.8
66011	13	1 13 67	56.8	14	520.77	4.8	35.88	0.	7.6	132	57.9	80.6	44.0	2.7	5.5	14.3
66011	14	16 10 67	71.4	23	442.82	5.7	25.15	0.3	9.8	134	42.1	74.1	35.7	5.0	7.0	17.1
66011	15	22 12 67	57.9	18	396.79	3.8	43.22	0.2	16.3	147	55.3	77.4	35.0	4.6	7.4	17.0
66011	15	22 12 67	57.9	18	376.91	6.6	19.00	0.	2.8	121	44.9	77.6	2.7	4.6	2.7	4.6
67003	1	22 3 68	50.2	35	13.39	2.8	1.60	0.	10.3	135	38.0	75.7	2.7	4.6	2.7	4.6
67003	3	19 5 70	47.1	30	13.31	3.8	0.54	101.1	1.2	25	31.2	66.2	40.0	6.8	7.0	13.8
67003	4	28 2 71	17.7	19	7.42	7.7	0.52	1.4	2.2	125	11.8	66.5	42.0	4.8	5.0	16.3
67003	5	8 11 71	45.8	24	14.81	10.2	0.27	74.9	1.0	52	24.5	53.5	44.0	4.8	4.6	16.1
67003	6	30 7 72	46.2	27	21.80	7.4	0.17	62.5	0.6	43	35.1	74.1	76.5	7.0	7.0	16.1
67003	7	10 7 73	28.1	6	14.37	1.7	1.10	74.0	0.1	22	11.5	41.0	48.0	2.0	5.5	12.2
67005	7	22 2 67	40.7	21	36.14	6.2	7.73	0.	7.1	132	12.3	30.1	22.5	5.8	8.6	32.2
67005	8	27 2 67	48.2	28	30.85	6.8	7.97	0.	5.4	130	14.5	30.1	20.3	5.0	8.5	37.8
67005	9	15 10 67	53.6	50	27.28	3.7	5.89	0.	9.6	134	15.0	37.9	2.7	4.6	2.7	4.6
67005	10	28 10 67	26.4	13	24.47	3.4	9.20	0.8	13.9	138	6.7	25.3	25.3	5.4	9.2	25.6
67008	13	24 5 68	38.6	30	16.69	8.2	2.06	14.0	0.3	111	6.0	15.5	2.7	4.6	2.7	4.6
67008	15	1 11 68	24.7	20	12.17	12.6	2.20	0.	1.1	128	4.9	19.8	11.5	9.6	24.0	48.7
67008	17	25 4 69	19.4	11	12.13	7.8	2.54	5.7	1.5	120	2.4	12.2	22.0	7.4	9.0	32.5
67008	18	29 5 69	23.3	19	21.23	5.2	6.00	5.6	3.5	122	3.9	16.8	20.0	6.1	13.5	28.6
67008	20	5 4 70	16.7	14	17.59	7.9	4.98	1.4	1.7	125	3.3	15.4	21.2	6.0	9.0	34.5
67008	22	9 8 71	59.0	31	17.44	13.9	1.14	29.3	0.6	96	6.4	10.8	2.7	4.6	2.7	4.6
67008	23	20 11 71	28.5	21	29.84	12.0	2.92	0.1	5.3	130	9.5	33.5	13.0	6.0	19.0	47.5
67010	1	26 6 68	58.4	18	11.46	4.6	0.34	3.6	5.3	126	37.2	63.7	39.7	3.3	6.0	16.1
67010	2	13 9 68	50.7	15	12.61	2.7	0.86	0.	11.6	136	23.5	46.3	51.8	2.8	4.9	11.6
67010	3	29 11 68	52.2	24	11.87	2.3	0.51	0.	6.4	131	24.5	46.9	54.7	4.4	4.8	10.8
67010	4	22 2 67	72.9	21	11.16	5.1	0.32	0.	6.7	131	33.6	46.1	40.2	3.8	5.5	16.7
67010	5	26 2 67	77.9	19	18.02	2.7	0.70	0.	10.0	134	35.6	45.7	57.7	1.7	2.5	14.3
67010	6	4 0 67	67.3	21	11.74	3.2	0.37	0.	15.8	140	40.4	60.0	44.8	3.8	4.3	16.3
67010	7	1 10 67	54.7	13	13.60	2.8	0.73	0.	16.8	141	25.6	66.8	47.1	2.7	4.3	15.0
67010	8	15 10 67	78.6	22	12.30	6.7	0.95	0.	23.7	148	49.2	62.6	2.7	4.3	15.0	
67010	9	22 12 67	75.0	14	14.52	4.5	0.77	0.	6.8	131	44.6	59.5	47.1	2.7	4.1	15.4
67010	11	18 3 68	103.0	29	15.01	7.6	0.36	0.	8.4	131	60.4	58.7	2.7	4.1	15.4	
67010	13	19 0 68	94.5	31	10.53	7.3	(0.23)	4.1	0.1	121	42.9	45.4	2.7	4.1	15.4	
67010	14	2 10 68	31.5	10	11.29	2.4	1.17	0.	25.1	150	20.3	64.5	50.5	2.6	4.1	13.8
68006	2	5 5 65	30.3	12	92.81	9.0	4.89	2.8	3.4	127	13.0	42.8	48.0	3.5	5.2	12.8
68006	3	8 9 65	48.1	19	122.99	4.3	6.81	0.	17.4	135	24.0	40.0	43.1	6.0	4.9	16.0
68006	4	8 12 65	35.1	23	104.94	8.2	4.06	0.	7.5	132	24.3	69.4	2.7	4.6	2.7	4.6
68006	5	14 9 66	25.1	7	70.82	7.2	3.19	0.	6.8	131	10.0	39.8	44.8	6.2	5.6	13.6
68006	6	2 10 67	20.6	10	54.53	4.5	4.35	0.	7.3	132	6.6	32.0	46.5	4.8	5.0	11.9
68006	7	1 7 68	29.2	11	84.43	5.7	1.32	3.4	4.1	125	10.9	37.2	2.7	4.6	2.7	4.6
68010	8	20 11 74	31.4	22	5.45	5.7	0.68	0.	0.6	125	10.1	51.2	24.0	4.0	9.8	11.9
68802	1	11 12 64	87.9	33	1.39	5.5	0.09	4.2	1.3	122	11.9	24.9	2.7	4.6	2.7	4.6
68802	2	8 12 65	31.9	23	1.41	4.3	0.12	0.	2.6	128	10.5	51.3	22.6	2.4	4.6	2.7
68802	4	14 5 67	19.3	13	1.25	4.7	0.17	3.2	8.0	129	9.5	47.7	31.4	2.2	4.6	2.7
68802	5	18 5 67	17.2	15	1.93	5.8	0.2									

CATCH NO	EV NO	DATE OF STORM	TOTAL RAIN (IN)	PEAK FLOW (CUMEC)	LAG (H)	ANSP (CUMEC)	1-HOUR UNIT HYDROGRAPH									
							SND (MM)	APIS (MM)	CMZ (MM)	RUNOFF (MM)	UM PEAK (CUMEC)	TIME TO AT 0.5 (H)	UM TIME BASE (H)			
71802	4	18 3 58	62.0	34	122.02	4.3	12.27	0.	6.4	131	41.7	67.3	23.6	7.4	9.5	28.1
71802	7	30 10 68	54.0	50	133.47	5.8	9.64	1.0	7.9	131	38.7	68.0	32.5	8.6	8.8	16.6
71802	9	30 10 68	52.0	23	162.41	7.9	6.26	0.	5.0	130	29.8	57.3				
71804	1	5 7 60	108.5	39	25.16	1.9	0.53	79.4	7.2	52	64.5	59.4	87.4	2.3	2.6	7.6
71804	2	3 8 61	43.1	18	33.13	2.4	0.43	45.9	1.1	80	21.0	33.3	64.6	1.8	3.1	10.9
71804	3	22 8 62	60.5	23	27.47	0.3	1.08	20.0	9.2	114	18.4	30.4	120.0	1.8	1.8	5.8
71804	4	25 9 63	63.4	25	24.15	2.4	0.37	0.	16.0	141	18.7	29.4	80.2	2.0	2.1	9.7
71804	5	20 11 63	59.3	15	21.84	1.6	0.87	0.	10.6	135	11.5	17.6	85.7	2.1	2.6	7.7
71804	6	8 12 64	73.7	29	22.84	3.3	0.98	0.	32.5	157	27.6	37.4	56.8	2.6	3.0	13.6
72002	2	14 12 62	27.0	24	99.48	6.9	4.69	0.	3.4	128	15.7	58.1	28.5	5.8	8.5	22.0
72002	3	25 9 63	38.2	14	131.13	6.0	8.42	0.	13.5	138	16.9	44.1	29.6	5.8	7.9	21.8
72002	4	2 10 63	31.5	11	138.87	6.1	10.21	0.	6.4	131	17.2	54.5	31.4	5.6	7.6	20.2
72002	5	20 11 63	37.2	13	118.20	5.8	9.83	0.	6.9	131	16.5	52.9	29.9	5.6	8.2	20.8
72002	6	10 5 64	36.8	18	154.79	6.0	5.87	3.6	6.7	128	20.7	56.3	28.0	4.8	8.8	22.1
72002	7	8 12 64	39.8	15	142.71	5.1	13.60	0.	16.8	141	24.5	61.7	26.8	6.3	8.5	26.5
72002	8	8 1 65	67.4	43	120.75	8.7	9.09	0.	11.3	136	41.6	67.8	23.5	7.0	9.0	29.3
72002	9	9 9 65	29.6	18	161.56	6.4	12.33	0.	10.2	135	22.5	73.8	29.5	6.0	7.4	22.9
72002	10	7 12 65	38.0	51	117.3	1.1	6.32	0.	6.6	131	25.0	65.9	28.0	5.8	8.8	21.1
72002	11	16 12 65	41.9	47	121.1	1.9	8.14	0.	3.3	128	27.0	64.5	26.6	6.2	9.7	22.4
72002	12	25 6 66	44.4	22	139.1	1.1	6.81	10.0	6.2	121	25.6	57.7	24.6	4.4	10.5	24.2
72002	20	19 9 68	68.9	41	164.1	1.1	14.45	0.	10.8	135	59.4	86.2	27.0	4.9	6.5	18.2
72002	21	25 1 69	35.1	21	89.74	5.8	7.83	0.	1.8	126	19.5	35.6	27.3	6.4	7.9	24.9
72002	22	2 3 69	44.1	14	160.64	6.6	6.77	5.3	1.1	117	26.5	60.1	26.5	5.0	8.5	22.0
72006	1	16 9 70	37.8	14	280.63	7.3	10.09	20.4	1.9	106	18.9	50.0	43.4	7.0	5.6	14.4
72006	2	31 10 70	15.0	8	259.90	7.8	28.63	0.	24.3	149	11.3	75.3	32.0	7.9	7.6	19.5
72006	3	11 2 71	51.6	26	285.25	11.1	7.62	0.8	0.6	124	32.0	62.0				
72006	4	20 11 71	25.5	16	161.95	5.0	12.04	0.3	2.3	127	12.1	47.4	29.4	7.9	7.2	23.4
72006	5	18 1 72	26.7	17	274.96	6.7	14.29	0.	2.5	127	16.3	61.0	30.8	5.3	8.4	19.3
72006	6	3 7 72	54.2	36	207.83	6.8	13.68	8.6	0.8	117	28.1	51.9				
72006	10	30 4 75	19.9	13	162.83	6.6	14.87	1.0	4.4	128	12.2	61.4				
72006	11	24 9 75	66.6	28	492.98	6.9	28.72	0.7	4.9	129	45.3	87.4				
72818	1	25 1 73	20.8	9	12.94	7.8	0.69	0.	2.6	127	6.0	28.7	30.5	7.8	7.8	20.9
72818	2	3 4 73	23.1	7	17.13	5.3	0.87	0.	9.7	134	6.3	27.3	36.5	5.1	6.7	17.1
72818	3	7 12 73	17.7	10	5.04	8.0	0.49	0.	0.6	125	4.3	24.4	28.2	8.5	9.5	20.8
72818	4	19 12 73	17.6	15	9.58	5.9	1.23	0.	0.6	128	6.1	34.9	28.8	4.4	8.6	24.3
72818	6	24 9 74	17.5	14	7.31	9.6	0.34	0.7	3.8	128	5.4	30.8	23.7	8.8	9.9	27.1
72818	7	6 1 75	17.9	8	6.88	6.9	0.35	0.	0.6	125	3.3	18.5	31.2	8.0	7.9	10.0
72818	8	11 1 75	11.9	6	6.96	6.2	0.75	0.	2.5	127	2.7	22.9	35.0	6.2	7.4	18.9
72818	9	16 2 75	13.4	6	10.83	5.3	0.77	0.	2.2	127	3.8	28.4	37.5	6.2	6.3	17.1
72818	10	18 4 75	11.8	11	6.37	7.3	0.62	1.7	3.9	127	2.7	22.6	36.4	4.9	6.5	19.3
72820	1	3 4 73	68.1	16	0.54	4.9	0.04	0.5	7.7	132	28.6	43.3				
72820	2	4 8 73	16.1	10	0.07	6.0	0.07	54.5	5.2	75	2.3	14.5	46.1	3.8	4.0	16.2
72820	3	8 7 73	49.2	22	0.42	3.1	0.03	28.7	9.6	105	19.9	40.4	40.1	1.8	3.8	20.1
72820	4	11 11 73	33.5	26	0.47	4.5	0.03	22.5	3.5	105	27.0	48.9	33.4	1.0	4.0	21.4
72820	5	11 11 73	33.5	26	0.34	2.7	0.03	10.8	30.8	144	18.9	35.3				
72820	6	15 12 73	28.3	11	0.7	3.2	0.03	0.	4.5	129	5.5	19.0	41.8	4.6	6.0	14.5
72820	8	15 7 74	20.4	13	0.41	1.9	0.04	51.2	2.4	76	7.6	37.5	43.3	1.0	2.9	19.9
72820	9	8 8 74	29.4	5	0.33	1.9	0.04	68.0	0.4	57	1.9	6.5				
72820	10	7 9 74	24.6	12	0.40	1.7	0.11	62.9	17.4	79	10.8	47.7	43.1	1.0	3.8	18.2
73005	1	19 2 70	35.0	18	86.82	4.6	10.23	0.	23.1	148	16.3	48.7	27.9	6.5	7.6	24.7
73005	2	17 6 72	54.8	15	72.00	6.4	3.95	15.4	0.8	110	12.7	23.2	29.5	7.2	7.6	22.5
73005	3	3 7 72	77.1	39	92.13	10.7	7.94	7.4	0.3	117	27.8	34.0	25.5	5.5	8.0	27.6
73005	4	29 11 72	47.2	18	84.02	6.2	9.34	0.	5.0	129	19.1	42.3	28.2	7.0	7.4	24.2
73005	5	6 11 73	50.7	21	58.72	6.9	7.17	0.	1.1	124	15.1	51.1	24.7	7.0	8.0	21.4
73005	6	17 10 74	30.3	17	34.42	5.4	5.46	0.3	1.8	126	5.8	19.1	26.4	7.1	9.0	24.1
73005	7	10 11 74	33.7	14	87.69	11.0	14.29	0.	10.6	135	13.5	40.0				
73005	8	21 1 75	64.9	23	148.25	7.6	18.53	0.	8.2	133	29.8	45.9	28.3	6.9	7.4	24.5
73005	9	16 2 75	30.1	23	52.55	7.2	5.14	0.1	3.6	128	8.4	27.8	30.7	4.7	6.6	23.0
73005	11	21 7 75	82.3	33	74.29	10.9	3.97	73.1	2.9	54	22.7	27.5	21.5	4.0	9.1	33.5
73005	12	24 9 75	64.7	18	118.44	7.1	5.23	1.1	2.6	129	26.5	41.0	25.2	6.0	9.2	25.7
73007	2	30 8 70	38.4	9	13.22	3.5	0.70	8.4	0.0	35	10.2	26.6				
73007	4	18 1 72	53.1	20	23.34	5.3	1.42	11.3	136	19.1	36.0	43.5	4.3	4.8	16.0	
73007	6	8 11 72	89.2	19	38.81	4.9	1.05	1.5	1.7	125	47.6	35.4	48.2	3.6	5.4	13.3
73007	9	28 12 74	44.1	14	30.67	2.4	2.77	0.	14.2	139	25.4	37.5	54.4	4.0	4.0	12.4
73007	10	16 2 75	40.9	24	19.75	7.2	0.59	0.0	2.1	127	18.6	40.7	44.0	3.6	4.5	16.3
73008	1	21 4 70	66.2	30	46.38	10.4	5.79	0.5	3.2	127	32.2	48.6				
73008	2	21 11 70	38.3	23	27.26	7.2	3.00	0.	6.9	131	12.5	32.5				
73008	3	11 11 71	27.8	18	19.90	9.7	2.80	9.3	2.6	127	6.9	24.7				
73008	5	5 11 72	50.8	37	25.54	15.8	3.53	8.3	0.5	117	21.0	41.2				
73008	6	10 11 72	37.4	12	26.12	5.9	8.74	0.	14.0	138	6.2	22.8	24.3	4.6	9.2	27.4
73008	7	12 11 72	48.6	9	26.15	5.8	10.94	0.	14.0	139	4.0	21.6	29.0	5.6	7.7	22.9
73008	8	12 11 72	48.6	9	25.04	5.2	3.79	0.4	8.4	133	7.1	23.9	23.9	4.2	9.5	23.9
73008	9	29 9 75	64.4	30	40.97	5.0	8.80									

CATCH NO	DATE OF STORM	RAINFALL		LTC	ANSP	SNO	APIS	CMI	1-HOUR UNIT HYDROGRAPH		UN	TIME
		TOTAL	DURN						PER 100	PER 100		
84022	8 12	1.72	24.0	4.2	6.52	0.	14.7	129	12.4	47.0	0.	17.4
84022	9 11	3.72	32.9	3.0	3.71	0.	6.7	123	16.2	24.9	0.	17.4
84022	10 23	1.73	16.6	2.9	1.73	0.	6.8	129	2.7	10.5	0.	17.4
84022	11 25	1.74	16.6	3.3	1.75	0.	5.7	130	23.8	34.7	0.	17.4
84022	12 12	5.75	25.05	5.2	1.62	1.2	1.9	125	4.6	20.0	47.3	15.2
85002	8 13	3.68	11.1	4.2	3.68	0.	6.4	131	11.1	29.7	31.9	17.4
85002	9 14	3.68	10.3	7.3	1.10	0.	10.8	135	26.7	65.6	29.0	22.8
85002	10 15	4.0	10.2	5.0	1.79	1.1	1.3	122	16.2	30.4	28.3	7.6
85002	11 16	4.0	11.3	5.6	10.46	0.	10.6	135	17.4	39.7	29.3	21.7
89001	8 14	22.5	18	22.1	18.12	0.	3.1	128	8.8	39.4	9.6	62.0
89001	9 15	39	30	24.2	26.51	0.	3.6	130	30.8	51.3	5.8	130.8
89001	10 16	39	13	20.3	12.44	0.	2.8	127	32.2	51.3	6.5	101.6
89001	11 17	42.0	14	17.6	26.19	1.0	5.1	129	20.0	46.7	5.7	106.2
89001	12 18	42.0	132	17.0	26.19	2.	9.1	134	22.9	43.5	6.0	100.7
89001	1 19	44	116	28.2	8.77	1.0	3.0	126	37.9	30.9	5.5	134.6
89001	2 20	44	78	29.0	17.79	0.	5.8	129	23.3	31.6	5.7	114.0
89001	3 21	48	42	20.9	21.85	0.	12.8	137	14.3	44.7	7.3	79.0
89001	4 22	101.9	240	37.5	16.42	0.	0.4	123	62.6	39.9	4.7	137.2

WHERE THE UNIT HYDROGRAPH DIFFERS FROM ONE HOUR, THE UNIT HYDROGRAPH PARAMETERS HAVE BEEN ADJUSTED TO THE 1-HR UN

APPENDIX B

THE FLOOD EVENT DATA ARCHIVE

The data used for this study are stored on a computer data base called the Flood Event Data Archive. Data held for each event include flow, catchment storage rainfall, raw (collated but not processed) rainfall, antecedent rainfall, soil moisture deficit and text comments. While analysis programmes can access these data directly two standard retrieval options are available to list and plot the data. Examples of these are given in Figures B.1 and B.2. In addition to the event data, information is held that relates directly to catchments. Examples of these are catchment characteristics, digitised data, lists of daily and recording gauges and text comments. The archive contents for a particular catchment are summarised on another standard retrieval as shown in Figure B.3. The lists of daily and recording rainfalls held against each catchment greatly aid the collation of event rainfalls by speeding the interface with peripheral archiver containing data from these gauges.

FIGURE B.1

CATCHMENT NUMBER		EVENT NUMBER	
100005	11		
NUMBER OF DATA TIPS	100005	CODE VALUES	0 0 0 0 11 23122
ANTICIPANT RAINFALL	30	5 DAYS PRIOR TO EVENT	7.0 0. 0.30 19.20 0.
RAINFALL AFTER 3.00 BUT BEFORE START OF EVENT	17.40		
END AT 02.00 ON 14/08 13	29.7	FROM STATION(S)	155547
COMMENTS RELATING TO EVENT	PRECIPITATION MODIFIED AT START		
	OVER ESTIMATION OF PEAK DISCHARGE		
DAYS	TIME	FLOW	DISCHARGE
EVENT	AVERAGE	INDIVIDUAL	RAINFALL
14-08	0.00	0.00	0.00
	1.00	10.00	1.27
	2.00	11.00	3.00
	3.00	12.00	0.00
	4.00	13.00	0.00
	5.00	14.00	0.00
	6.00	15.00	0.00
	7.00	16.00	0.00
	8.00	17.00	0.00
	9.00	18.00	0.00
	10.00	19.00	0.00
	11.00	20.00	0.00
	12.00	21.00	0.00
	13.00	22.00	0.00
	14.00	23.00	0.00
	15.00	24.00	0.00
	16.00	25.00	0.00
	17.00	26.00	0.00
	18.00	27.00	0.00
	19.00	28.00	0.00
	20.00	29.00	0.00
	21.00	30.00	0.00
	22.00	31.00	0.00
	23.00	32.00	0.00
	24.00	33.00	0.00
	25.00	34.00	0.00
	26.00	35.00	0.00
	27.00	36.00	0.00
	28.00	37.00	0.00
	29.00	38.00	0.00
	30.00	39.00	0.00
	31.00	40.00	0.00
	32.00	41.00	0.00
	33.00	42.00	0.00
	34.00	43.00	0.00
	35.00	44.00	0.00
	36.00	45.00	0.00
	37.00	46.00	0.00
	38.00	47.00	0.00
	39.00	48.00	0.00
	40.00	49.00	0.00
	41.00	50.00	0.00
	42.00	51.00	0.00
	43.00	52.00	0.00
	44.00	53.00	0.00
	45.00	54.00	0.00
	46.00	55.00	0.00
	47.00	56.00	0.00
	48.00	57.00	0.00
	49.00	58.00	0.00
	50.00	59.00	0.00
	51.00	60.00	0.00
	52.00	61.00	0.00
	53.00	62.00	0.00
	54.00	63.00	0.00
	55.00	64.00	0.00
	56.00	65.00	0.00
	57.00	66.00	0.00
	58.00	67.00	0.00
	59.00	68.00	0.00
	60.00	69.00	0.00
	61.00	70.00	0.00
	62.00	71.00	0.00
	63.00	72.00	0.00
	64.00	73.00	0.00
	65.00	74.00	0.00
	66.00	75.00	0.00
	67.00	76.00	0.00
	68.00	77.00	0.00
	69.00	78.00	0.00
	70.00	79.00	0.00
	71.00	80.00	0.00
	72.00	81.00	0.00
	73.00	82.00	0.00
	74.00	83.00	0.00
	75.00	84.00	0.00
	76.00	85.00	0.00
	77.00	86.00	0.00
	78.00	87.00	0.00
	79.00	88.00	0.00
	80.00	89.00	0.00
	81.00	90.00	0.00
	82.00	91.00	0.00
	83.00	92.00	0.00
	84.00	93.00	0.00
	85.00	94.00	0.00
	86.00	95.00	0.00
	87.00	96.00	0.00
	88.00	97.00	0.00
	89.00	98.00	0.00
	90.00	99.00	0.00
	91.00	100.00	0.00

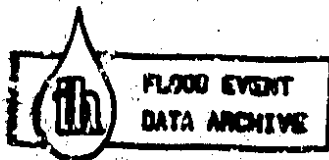
14.00	41.00	74.64	1.00	3.00	3.00
15.00	42.00	75.64	1.00	3.00	3.00
16.00	43.00	76.64	1.00	3.00	3.00
17.00	44.00	77.64	1.00	3.00	3.00
18.00	45.00	78.64	1.00	3.00	3.00
19.00	46.00	79.64	1.00	3.00	3.00
20.00	47.00	80.64	1.00	3.00	3.00
21.00	48.00	81.64	1.00	3.00	3.00
22.00	49.00	82.64	1.00	3.00	3.00
23.00	50.00	83.64	1.00	3.00	3.00
24.00	51.00	84.64	1.00	3.00	3.00
25.00	52.00	85.64	1.00	3.00	3.00
26.00	53.00	86.64	1.00	3.00	3.00
27.00	54.00	87.64	1.00	3.00	3.00
28.00	55.00	88.64	1.00	3.00	3.00
29.00	56.00	89.64	1.00	3.00	3.00
30.00	57.00	90.64	1.00	3.00	3.00
31.00	58.00	91.64	1.00	3.00	3.00
32.00	59.00	92.64	1.00	3.00	3.00
33.00	60.00	93.64	1.00	3.00	3.00
34.00	61.00	94.64	1.00	3.00	3.00
35.00	62.00	95.64	1.00	3.00	3.00
36.00	63.00	96.64	1.00	3.00	3.00
37.00	64.00	97.64	1.00	3.00	3.00
38.00	65.00	98.64	1.00	3.00	3.00
39.00	66.00	99.64	1.00	3.00	3.00
40.00	67.00	100.64	1.00	3.00	3.00
41.00	68.00	101.64	1.00	3.00	3.00
42.00	69.00	102.64	1.00	3.00	3.00
43.00	70.00	103.64	1.00	3.00	3.00
44.00	71.00	104.64	1.00	3.00	3.00
45.00	72.00	105.64	1.00	3.00	3.00
46.00	73.00	106.64	1.00	3.00	3.00
47.00	74.00	107.64	1.00	3.00	3.00
48.00	75.00	108.64	1.00	3.00	3.00
49.00	76.00	109.64	1.00	3.00	3.00
50.00	77.00	110.64	1.00	3.00	3.00
51.00	78.00	111.64	1.00	3.00	3.00
52.00	79.00	112.64	1.00	3.00	3.00
53.00	80.00	113.64	1.00	3.00	3.00
54.00	81.00	114.64	1.00	3.00	3.00
55.00	82.00	115.64	1.00	3.00	3.00
56.00	83.00	116.64	1.00	3.00	3.00
57.00	84.00	117.64	1.00	3.00	3.00
58.00	85.00	118.64	1.00	3.00	3.00
59.00	86.00	119.64	1.00	3.00	3.00
60.00	87.00	120.64	1.00	3.00	3.00
61.00	88.00	121.64	1.00	3.00	3.00
62.00	89.00	122.64	1.00	3.00	3.00
63.00	90.00	123.64	1.00	3.00	3.00
64.00	91.00	124.64	1.00	3.00	3.00
65.00	92.00	125.64	1.00	3.00	3.00
66.00	93.00	126.64	1.00	3.00	3.00
67.00	94.00	127.64	1.00	3.00	3.00
68.00	95.00	128.64	1.00	3.00	3.00
69.00	96.00	129.64	1.00	3.00	3.00
70.00	97.00	130.64	1.00	3.00	3.00
71.00	98.00	131.64	1.00	3.00	3.00
72.00	99.00	132.64	1.00	3.00	3.00
73.00	100.00	133.64	1.00	3.00	3.00
74.00	101.00	134.64	1.00	3.00	3.00
75.00	102.00	135.64	1.00	3.00	3.00
76.00	103.00	136.64	1.00	3.00	3.00
77.00	104.00	137.64	1.00	3.00	3.00
78.00	105.00	138.64	1.00	3.00	3.00
79.00	106.00	139.64	1.00	3.00	3.00
80.00	107.00	140.64	1.00	3.00	3.00
81.00	108.00	141.64	1.00	3.00	3.00
82.00	109.00	142.64	1.00	3.00	3.00
83.00	110.00	143.64	1.00	3.00	3.00
84.00	111.00	144.64	1.00	3.00	3.00
85.00	112.00	145.64	1.00	3.00	3.00
86.00	113.00	146.64	1.00	3.00	3.00
87.00	114.00	147.64	1.00	3.00	3.00
88.00	115.00	148.64	1.00	3.00	3.00
89.00	116.00	149.64	1.00	3.00	3.00
90.00	117.00	150.64	1.00	3.00	3.00
91.00	118.00	151.64	1.00	3.00	3.00
92.00	119.00	152.64	1.00	3.00	3.00
93.00	120.00	153.64	1.00	3.00	3.00
94.00	121.00	154.64	1.00	3.00	3.00
95.00	122.00	155.64	1.00	3.00	3.00
96.00	123.00	156.64	1.00	3.00	3.00
97.00	124.00	157.64	1.00	3.00	3.00
98.00	125.00	158.64	1.00	3.00	3.00
99.00	126.00	159.64	1.00	3.00	3.00
100.00	127.00	160.64	1.00	3.00	3.00

160768

170768

180768

NOTE: ALL FALLS CORRESPOND TO PRICE LIST IN EFFECT AT THE TIME THIS IS PRINTED IN THE OFFICE PRACTICE.



OBSERVED HYDROGRAPH AND RAINFALL

CATCHMENT NO. 11007
EVENT NO. 11
DATE 14/SEP/1988
AREA 403.30 SQ.KM

INDIVIDUAL RAINGAUGE
PROFILE(S)

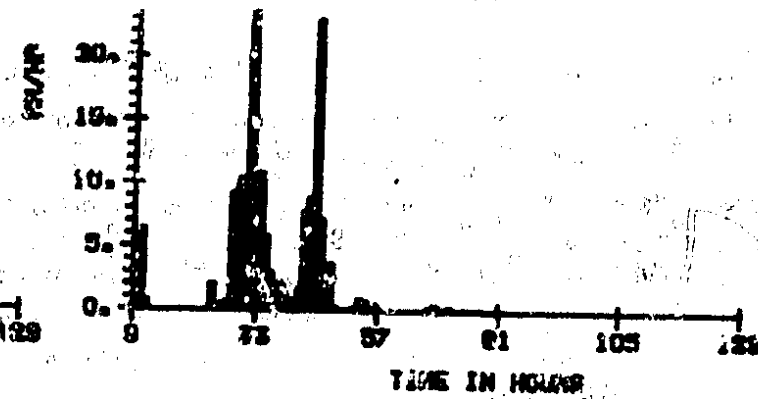
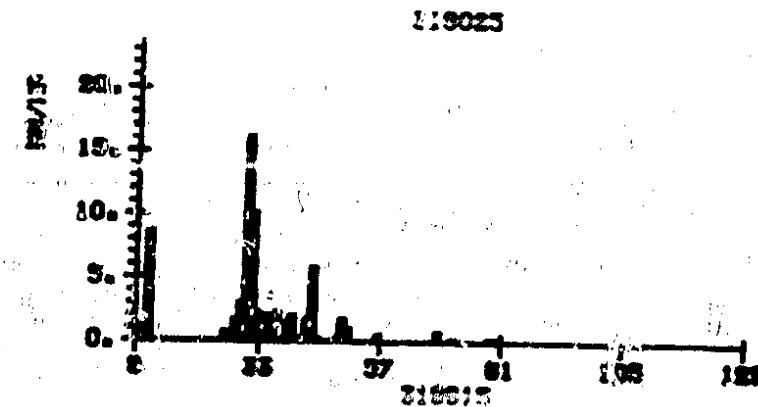
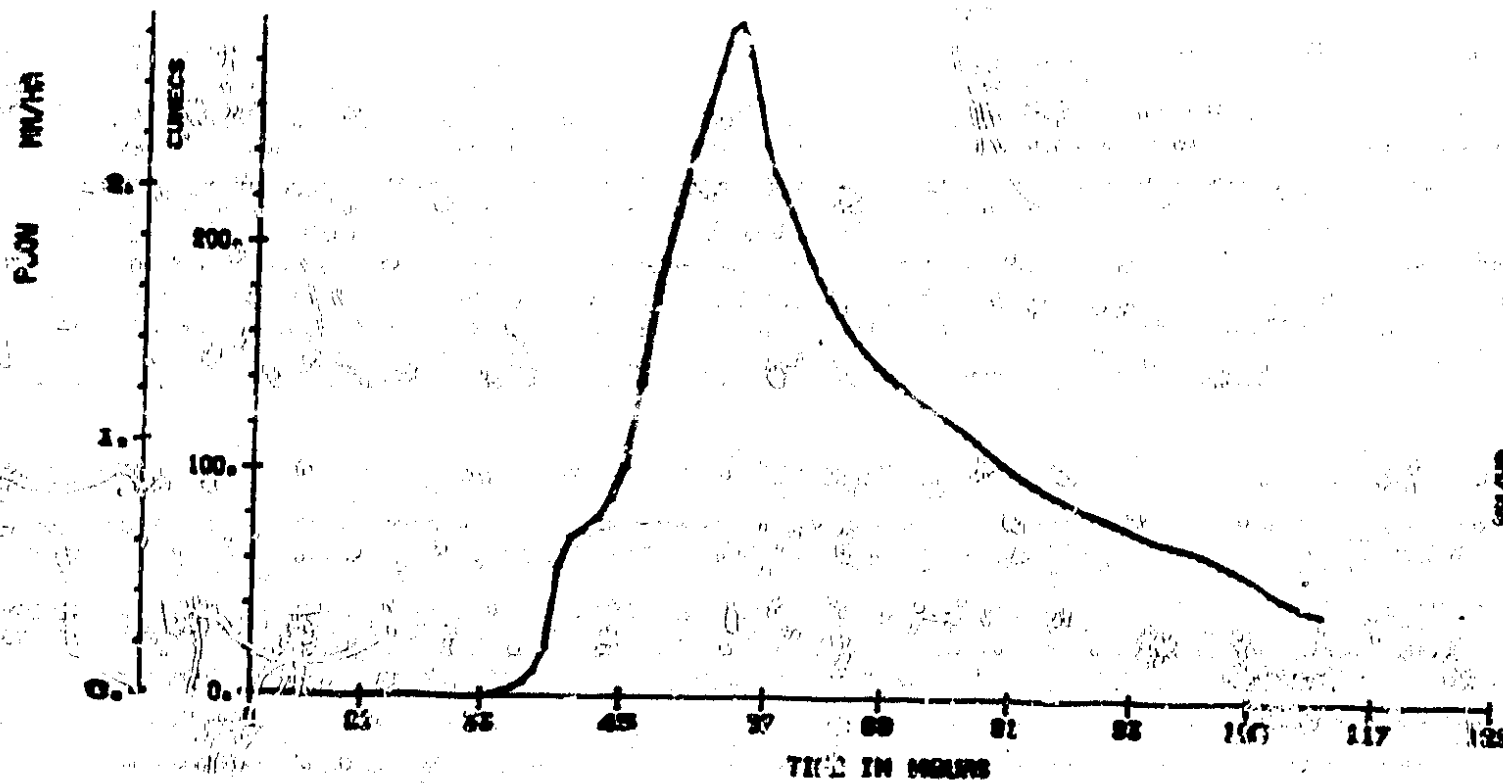
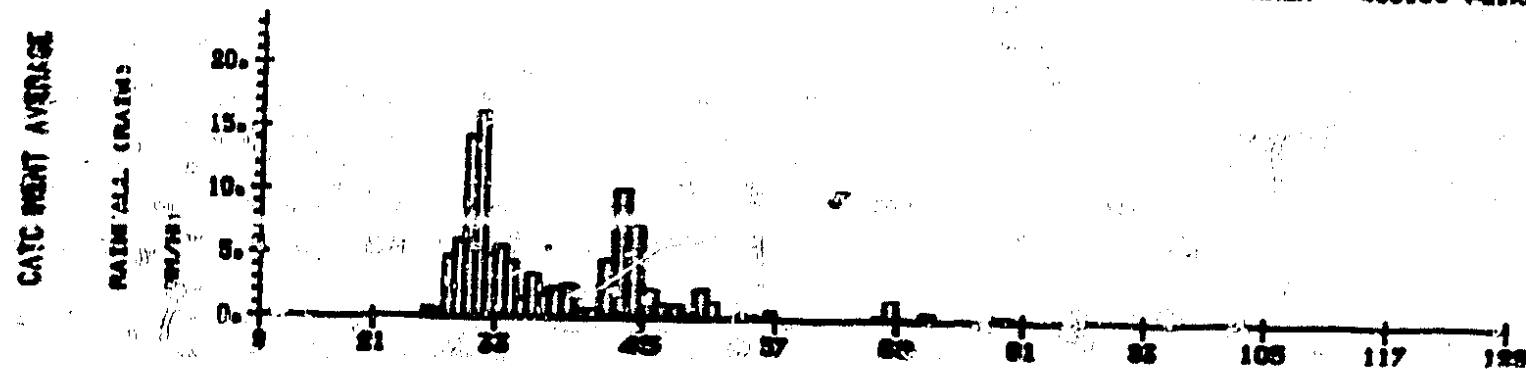


FIGURE D.2

FIGURE B.3

INSTITUTE OF HYDROLOGY FLOOD EVENT DATA ARCHIVE

CATCHMENT NAME: WASH ST PARK
 CATCHMENT NUMBER: 1307
 NUMBER OF EVENTS: 13

DATE OF FORM: 01-11-84
 INDICATE LATEST ENTRY

CATCHMENT DESCRIPTORS FROM FILE CATCHES ENTERED 14-8-84

START OF RECORD NOT KNOWN END OF RECORD CURRENT	FLOW STATISTICS	RAINFALL INDICIES
SPID REF OF GAUGING STATION 5028 7 1 11	AVERAGE DAILY FLOW	CONJECT ANNUAL AVERAGE RAINFALL 755.0 MM
SPID REF OF CATCHMENT CENTROID 5057 7 1 15	MEAN ANNUAL FLOOD (SEEMAP) 22.0 CUMEC	PSND 37.7 MM
CATCHMENT AREA 403.30 SQ KM	MAX FROM ANNUAL MAXING 74.0 CUMEC	5-20 59.0 MM
WATERCOURSE LENGTH 46.77 KM	TEN YEAR FLOOD (RECORDED) 124.2 CUMEC	EST MAX 2HR RAINFALL 173.0 MM
ACTUAL LENGTH 31.14 KM	MAXIMUM RECORDED FLOOD 291.2 CUMEC	EST MAX 24HR RAINFALL 250.0 MM
ALTITUDE OF STATION 1.0 M	YEAR OF BIGGEST FLOOD 1967	JENKINSON R 0.350
ALTITUDE OF WATERSHED 271.0 M	BASE FLOW INDEX	SDBAR 9.20
MAXIMUM ALTITUDE 294.0 M	RESPONSE FLOW INDEX	
USGS SLOPE (S1395) 1.50 W/KM	SOILS	URBAN FRACTION 0.010
TAYLOR-SCHWAB SLOPE 1.45 W/KM	WRAP SOIL INDEX 0.44	LAKE INDEX 0.76
NASH OVERLAND SLOPE W/KM	TYPE 1 FRACTION 0.04	STREAM FREQUENCY 1.55 JUNCTIONS/KM
DRY VALLEY FACTOR 0.013	TYPE 2 FRACTION 0.	SHAPE FACTOR K 1.223
	TYPE 3 FRACTION 0.	
	TYPE 4 FRACTION 0.24	
	TYPE 5 FRACTION 0.	

NUMBER QUAD USED FOR RAINGAUGE SEAS PCHES

5075 1105
5275 1295
5155 1463
5055 1925

ENTERED 23-8-83

LIST OF DAILY RAINGAUGES

RAIN GAUGE NUMBER	GRID REF EAST NORTH	PERCENT OF RECORD START ENDS	ON/OFF CATCHMENT
250957	4879 1325	- 1 0 01	OFF
267429	4840 1350	- 1 0 01	OFF
252265	5076 1307	- 1 0 01	OFF
252259	5041 1392	- 1 0 01	OFF
252432	4995 1405	- 1 0 01	OFF
252535	5113 1441	- 1 0 01	OFF
311053	5253 1296	- 1 0 01	OFF
314200	5124 1265	- 1 0 01	OFF
314435	5213 1271	- 1 0 01	OFF
316065	5250 1319	- 1 0 01	ON
316753	5225 1326	- 1 0 01	ON
316213	5145 1309	- 1 0 01	ON
316225	5157 1334	- 1 0 01	ON
316229	5172 1377	- 1 0 01	ON
316232	5162 1304	- 1 0 01	ON
316233	5160 1302	- 1 0 01	ON
316230	5174 1397	- 1 0 01	ON
316261	5140 1363	- 1 0 01	ON
316343	5180 1321	- 1 0 01	ON
316347	5174 1321	- 1 0 01	ON
316484	5141 1403	- 1 0 01	ON
316524	5146 1397	- 1 0 01	ON
316652	5113 1321	- 1 0 01	ON
316659	5092 1331	- 1 0 01	ON
316833	4942 1361	- 1 0 01	ON
316837	4954 1355	- 1 0 01	ON
316820	4974 1350	- 1 0 01	ON
316944	5028 1371	- 1 0 01	ON
317013	5014 1342	- 1 0 01	ON
317084	5040 1315	- 1 0 01	ON
217105	5007 1265	- 1 0 01	ON
317220	4923 1292	- 1 0 01	ON
317238	4949 1315	- 1 0 01	ON
317241	4927 1296	- 1 0 01	ON
317334	4999 1278	- 1 0 01	ON
317458	5015 1270	- 1 0 01	ON
317543	5007 1222	- 1 0 01	ON
317536	5059 1227	- 1 0 01	ON
315541	4882 1311	- 1 0 01	OFF
316075	4954 1275	- 1 0 01	OFF

ENTERED 23-8-83

LIST OF RECORDING RAINGAUGES

RAIN GAUGE NUMBER	GRID REF EAST NORTH	PERCENT OF RECORD START ENDS	ON/OFF CATCHMENT
250957	4879 1325	- 1 0 01	OFF
252259	5041 1392	- 1 0 01	OFF
316233	5160 1302	SEP 10 10 01	ON
316343	5180 1321	JUL 10 10 01	ON
316484	5141 1403	APR 10 10 01	ON
316524	5146 1397	APR 10 10 01	ON

LIST OF EVENT DATA

EVENT NUMBER	ENTRY CODE	QUALITY CODE	FLOW DATA	RAIN DATA	SHD DATA	APT DATA	COMMENTS	RAWRAIN DATA	NEW PATH DAT	NE. APT DATA	PS RESULT	EVENT DATE
1	11	4312165	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO DATE
2	11	12122	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	3 DEC 1960
3	11	52121	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	27 JAN 1961
4	11	11121	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	27 FEB 1961
5	11	11122	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	3 MAY 1961
6	11	11121	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	16 NOV 1961
7	11	11122	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	13 MAR 1964
8	11	21122	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	31 MAY 1964
9	11	11122	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	23 NOV 1964
10	11	11121	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	22 OCT 1966
11	11	23122	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	14 SEP 1968
12	11	21121	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	15 DEC 1968
13	11	23122	20- 4-82 21- 4-82	21- 4-82 23- 4-82	23- 4-82 23- 4-82	23- 4-82	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	NO ENTRY	11 MAR 1969

EVENT BREAKDOWN IS:

NO ENTRY	7
VARIABLE RAIN	1
UNINTERESTING	1
UNSATISFACTORY	1
SHD	1

APPENDIX C

A LOCALISED REINTERPRETATION OF THE WRAP MAP

During the preliminary analysis of the percentage runoff data a group of catchments stood out as having very much larger percentage runoffs than would be expected from their SOIL classification. One catchment, located entirely on type 1 soil was giving percentage runoffs well over 50% (the highest being 75%). The catchments all fell partly or wholly on a single soil association. While this soil is correctly classed as type 1 by the scheme given in FSR 1.4.2.3 (see also Farquharson et al, 1978), there is evidence from the current study and elsewhere (Gustard, 1981) that its hydrological response is as expected from a type 5 soil. Table C.1 lists the nine catchments occurring on this soil association and gives two measures of their hydrological response; percentage runoff and base flow index. Reinterpreting this soil as type 5 gives a consistent improvement across all the catchments and so it is recommended that the soil map should be amended accordingly. Figure C.1 shows the newly interpreted WRAP map for this area.

TABLE C.1 PERCENTAGE RUNOFF, BFI AND SOIL VALUES FOR ANOMALOUS CATCHMENTS

Catchment	Percentage Runoff	BFI	Soil type 1 (FSR)	SPR from SOIL (FSR)	SPR from soils (now)
76014	30-80	0.25	0.51	29.9	52.0
71802	60-80	0.26	0.09	45.8	53.0
72006	50-80	-	0.21	40.7	53.0
76805	50-70	0.27	1.00	15.0	53.0
27034	50-70	0.34	0.03	45.4	49.8
27027	30-90	0.38	0.16	40.1	52.7
76005	65	0.39	0.48	30.3	51.2
27035	23-50	0.43	0.12	41.5	49.8
73008	20-50	0.50	0.08	27.5	31.8

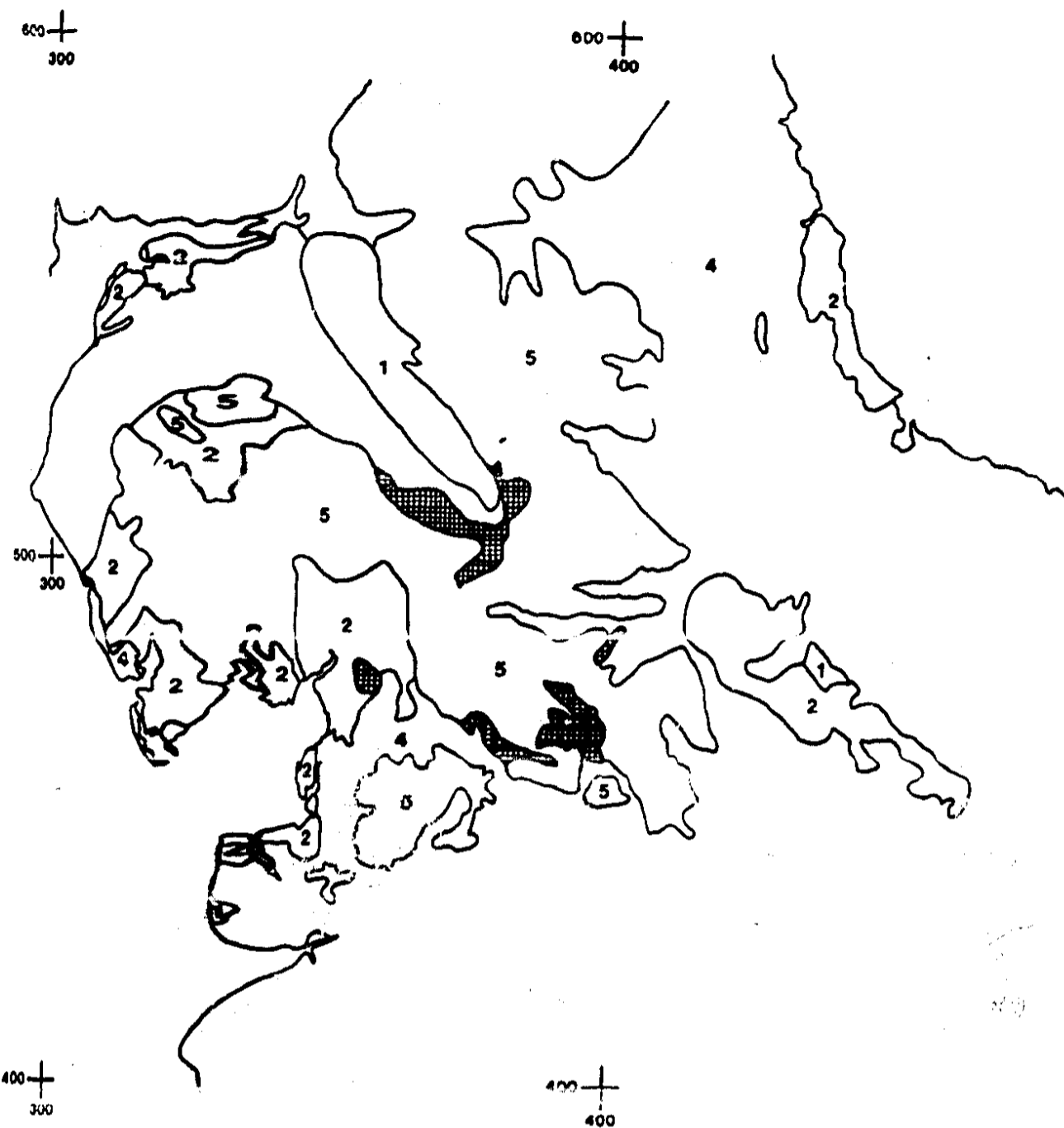


FIGURE C.1 Areas of Soil 1 reinterpreted as Soil 5

It is important to appreciate that such an interpretation of the WRAP map requires careful consideration of the distribution of the soil association under examination, and the veracity and extent of relevant hydrological data. Users of the estimation procedures are advised against making such a reassessment themselves but should use local data to refine FSR estimates as described in Section 4.

References

- Farquharson, F.A.K., Mackney, D., Newson, M.D. and Thomasson, A.J. 1978 'Estimation of runoff potential of river catchments from soil surveys'. Special Survey No. 11. Soil Survey of England & Wales.
- Gustard, A. 1981 'The hydrological response of two upland catchments: implications for flood estimation' PhD Thesis, Lancaster University.