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Infrared spectroscopy and chemometric modelling of organic carbon measured by Rock-Eval pyrolysis of UK shale rock

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Abstract

Shale rock core from the Bowland Shale Formation, UK was analysed in the laboratory using Rock-Eval(6) pyrolysis and Fourier Transform Infrared Spectroscopy (FTIR). These methods are used to characterise the organic constituents of soil and rock. This research is a proof-of-concept study to investigate whether regression models developed using FTIR and Rock-Eval data for the same length of core can be used to estimate selected Rock-Eval parameters. The accuracy of the regression models was assessed using statistical methods, the results of which were used to choose preferred models for each Rock-Eval parameter. Models produced were shown to have an acceptable level of uncertainty for Total Organic Carbon, S1, S2 and S3 outputs which led us to conclude these are potentially suitable for estimating unknown down-core Rock-Eval parameter values. Conversely, the T_{\max} model had a higher variability in the cross-validation data above the acceptable level of uncertainty which could lead to erroneous estimates. Down-core interpolations of selected Rock-Eval parameters could be practically achieved by modelling FTIR data by maintaining standard sample frequencies for Rock-Eval while supplementing with higher frequencies for FTIR and chemometric analysis.

1. Introduction

Unconventional shale gas systems comprise black shale mudrocks that are self-contained hydrocarbon source and reservoir because they potentially support large quantities of methane that can be recovered at surface using hydraulic fracturing. Alongside inorganic mineral content and physical properties, the hydrocarbon generation capacity, organic matter type and thermal maturity are the determining factors used to estimate gas-in-place and producible gas resource (Jarvie, 2012, Andrews, 2013, Scotchman, 2015, Whitelaw et al., 2019, Li et al., 2021). During hydrocarbon exploration, understanding of the main organic geochemical factors is usually elicited from the interpretation of Rock-Eval pyrolysis and total organic carbon (TOC %) analyses, validated using optical methods such as vitrinite reflection (Whitelaw et al., 2019). However, new approaches to analysis and data interrogation such as infrared spectroscopy and chemometrics have been recently shown to provide additional utility (Chen et al., 2014a, Fletcher et al., 2014, Leach et al., 2008).

Rock-Eval is routinely employed during the appraisal of shales, coals and other sediments because it yields key information on kerogen type and maturity (Table 1), requires minimal sample preparation and uses just 10–60 mg of rock (Behar et al., 2001, Marshall et al., 2015, Newell et al., 2016, Waters et al., 2020). This traditional geochemical screening approach is valuable to the exploration community because of the large body of literature, including: 1) data from basins in North and South America, Europe (UK, France, Poland), Africa and Australia; 2) published information on the technical limitations of the analyses (e.g. mineral matrix effects, T_{max} suppression); and 3) shale gas assessment specific methodologies and unified data processing/presentation approaches (Cornford et al., 1998; Dembicki, 2009; Espitalie & Joubert, 1987; Jarvie et al., 2007; Romero-Samiente, 2016). However, recent studies of the main unconventional hydrocarbon play in the UK, namely the Carboniferous Bowland Shale Formation, has shown fairly thin organic rich intervals interbedded with calcareous mudstones and turbidites (Hennissen et al., 2017, Andrews, 2013, Słowakiewicz et al., 2015, Könitzer et al., 2016, Waters et al., 2020, Emmings et al., 2019). Given this cyclical and laterally variable pattern of organic matter quantity and type there is a need for cost effective high-resolution geochemical screening method.

A complementary approach to evaluate the hydrocarbon generation capacity and characterise organic matter type in shale mudrocks is infrared spectroscopy, coupled with statistical methods collectively referred to as chemometrics. Chemometrics can establish whether relationships exist between properties e.g. using FTIR and organic matter data e.g. lignin, organic carbon, polycyclic aromatic hydrocarbons and selected physico-chemical properties (Leach et al., 2008, Mas et al., 2010, Mostert et al., 2010, Tinti et al., 2015, Vane et al., 2003, Washburn and Birdwell, 2013, Craddock et al., 2017, El-Rub et al., 2019, Varma et al., 2018).

IR spectroscopy quantifies the transitions between energy states after molecules that possess dipole moments are excited (Chen et al., 2015). The advantage of the technique over Rock-Eval is that it is non-destructive, it can be run expediently in the laboratory or field and has a low cost per sample (Washburn and Birdwell, 2013). The IR causes the molecules to vibrate – the movements include stretching, bending, twisting, rocking, wagging, and out-of-plane deformation. Each vibration type relates to the corresponding molecular bonds e.g. C-H, O-H and C=O. The intensity of the response is proportional to the abundance of the functional groups present in the sample (Chen et al., 2014a), although quantification in geological samples is difficult because of

intrinsic sample heterogeneity. Characteristics of hydrocarbon source rocks including the amount and type of organic carbon and mineral composition have been evaluated by IR spectroscopy (Chen et al., 2014a, Fletcher et al., 2014, Leach et al., 2008). Mid-IR (MIR) spectroscopy quantifies the molecular response of a sample to infrared radiation, typically from Wavenumbers 4000 to 400 cm^{-1} (a wavenumber is a measure of the spatial frequency of waves per cm). The response provides information on the functional group chemistry of samples, which in this research is being used to supplement analysis by Rock-Eval.

This study investigates whether the application of FTIR chemometrics to Carboniferous Shales from the Edale Formation, UK (lateral equivalent of Bowland Shale Formation) can estimate Rock-Eval parameter values. Where the latter form the traditional basis of characterising hydrocarbon generation capacity, organic matter type and thermal maturity. The approach may therefore provide a useful supplement to Rock-Eval pyrolysis where high-resolution stratigraphic control is needed on organic carbon type, but economics preclude substantial analytical programs.

2. Materials and methods

2.1 *Karenight core from the Bowland Shale Formation*

The Karenight-1 (SK36NWB13) borehole used for this study was drilled for mineral exploration by Drilling and Prospecting International in 1973 and stored in temperature and moisture-controlled conditions at the UK Research and Innovation National Geological Repository hosted at British Geological Survey. Karenight is located 5 km northeast of Matlock, Derbyshire (1.53°W; 53.18°N) and is situated on the boundary of the southern extent of the Derbyshire structural High and northern extent of the Edale Gulf (Figure 1: (Waters et al., 2009)). The rock core was taken from the Edale Shales Group from the Carboniferous period (Pendleian Substage and the *Eumorphoceras* zone) (Wilson and Stevenson, 1973). The core interval analysed spans 17 m and was located between 235 m to 252 m below ground level (m bgl). The stratigraphy comprises grey coloured dark mudstone with carbonaceous layers with thin laminar siltstone between 235 and 245 m bgl and limestone between 245 and 250 m bgl (Figure 2) (Hennissen et al., 2017). Seventy-two samples were extracted from the core to reflect the main lithological units. Each sample was freeze dried and ground to a fine powder.

2.1.1 *Rock-Eval*

Each sample was analysed using a Rock-Eval(6) pyrolyzer, configured in standard mode (pyrolysis and oxidation as a serial process). Each sample (~60 mg /dry wt) was heated isothermally at 300°C for 3 mins and then from 300 to 650°C at 25°C/min in an inert atmosphere of N₂. The residual carbon was oxidised at 300°C (isothermal 1 min) and then from 300 to 850°C at 20°C/min (hold 5 min). The performance of the instrument was checked every 10 samples against the accepted values of the Institut Français du Pétrole (IFP) standard (IFP 160 000, S/N15-081840). Rock-Eval parameters were calculated by integration of the amounts of HC (thermally-vaporized free hydrocarbons) expressed in mgHC/g rock (S1) and hydrocarbons released from cracking of bound OM expressed in mgHC/g rock (S2) (Engelhart et al., 2013). The Hydrogen Index (HI) was calculated from $S2 \times 100 / \text{TOC}$ and the Oxygen Index (OI) from $S3 \times 100 / \text{TOC}$.

2.1.2 *Fourier Transform Infrared Spectroscopy*

Each sample was subject to mid-infrared spectroscopy (MIR) using Fourier Transform Infrared (FTIR) (Wavenumbers: 4000 to 400 cm^{-1}). A Bio-Rad FTS 3000 FTIR instrument was operated in diffuse

reflectance mode using Resolutions Pro software (Version 5.1). Approximately 300 mg of freeze dried and milled sample was transferred to a stainless-steel cup and gently tamped and levelled using a stainless-steel spatula and rod. The cup and sample were subsequently placed into Pike AutoDiff autosampler. Prior to analysis the alignment of the interferometer was checked and adjusted to optimise the signal reaching the detector. Background FTIR measurements were made using finely ground potassium bromide (KBr) prior to each run. Each sample, including background, was analysed in replicate. The first analysis was made in the position the sample was placed in the AutoDiff, the second following a 90° rotation of the cup and sample. Samples were scanned 40 times at 4 cm⁻¹ resolution.

2.2 Data evaluation and predictive modelling

Data evaluation and predictive modelling was conducted using the R programming language (R Development Core Team, 2016). Down-core profiles of the Rock-Eval data were produced to visualise geochemical variations and allow a qualitative interpretation of the parameters measured.

FTIR spectra were visually assessed for any obvious differences between 'a' and 'b' duplicate samples. If there were no differences, mean spectra were calculated and baseline corrected using asymmetric least squares trend estimation function in the 'ptw' R package (Gerretzen et al., 2014) followed by smoothing using a 5-point running mean.

Principal components analysis (PCA) was conducted using a centred and scaled co-variance matrix of all FTIR wavenumbers and samples. These data were used to produce a number of uncorrelated vectors (loadings). The linear equation for the loadings data produces coefficients called principal component scores for each sample. The scores were plotted to assess whether there was any visual association with Rock-Eval data. The PC loadings and coefficients were plotted to characterise the influence wavenumber.

Partial least squares regression (PLSR) modelling of the of the baseline corrected mean smoothed FTIR data and selected Rock-Eval parameters (T_{max} , S1, S2 and S3) was completed using the orthogonal scores algorithm in the 'R caret' Package (Kuhn et al., 2015). HI and OI were calculated using the equations in Table 1. Three models were produced: i) all data (wavenumber 4000 to 570 cm⁻¹); ii) fingerprint region (wavenumber 570 to 2400 cm⁻¹); and iii) non-fingerprint region (wavenumber 2400 to 4000 cm⁻¹). Selected dependent Rock-Eval parameters included: i) T_{max} ; ii) HI; iii) S1; iv) S2; and v) S3. Multiple PLSR model runs were completed, each used a different number of PCs as an input parameter, ranging from 1-15 PCs. The optimum PC number was selected using 100-fold cross validation and the minimum root mean square error of predictions using the train function in the R caret package. The models developed using the optimised PC value were subject to 10-fold cross-validation to train and test the models by a leave-one-out (LOO) method using the `mvr_dcv` function in the R Chemometrics package. Each model was subject to detailed evaluation using the multiple acceptance criteria (Table 1). Beriro et al. (2013) reported that the multiple selection criteria approach to model evaluation is a valid approach to select best performance models from a number of potentially preferred models.

3. Results and discussion

3.1 *Rock-Eval*

The Rock-Eval pyrolysis data ($n=72$) for S1, S2, S3, HI and T_{\max} values are summarised by down-core plots (Figure 2) and descriptive statistics (Table 2). The down-core profiles of the Rock-Eval parameters show broadly parallel trends for hydrocarbon composition indicated by TOC, S1 and S2 and HI. Conversely, the amount of oxygen and thermal maturity determined by S3 and T_{\max} follow independent trends.

Weight percentage TOC provides a general indication of organic richness and is indirectly related to the hydrocarbon generation potential of a source rock. Proceeding down-core through the Karenight succession, three TOC depth interval zones are clear 235 to 242 m bgl characterised by low but variable TOC ranging from 2.54 to 7.08 % with a mean of 4.02 % ($n=31$), a second transitional zone between 242 to 243 m bgl with TOC of 4.74 to 8.18 and a mean of 6.69 wt % ($n=6$) and a higher and less variable TOC interval from 244 to and including 252 m bgl ranging from 0.36 to 8.20 with a mean of 6.4 % ($n=35$).

The Rock-Eval data presented in the down-core plots show that organic matter corresponds with the stratigraphic and lithological profile of the core. The organic matter content is generally higher in the mudstone bands between 245 and 250 m bgl than the thin laminar siltstone between 235 and 245 m bgl (Figure 2) (Hennissen et al., 2017). The changes in lithology in each part of the core clearly affect the Rock-Eval parameter values. The organic matter in the limestones is low, whereas the siltstone presents higher values. The Rock-Eval HI also corresponds with the same change in lithology where the values are higher in the mudstone and interbedded limestone. Further comparison of the TOC content suggests the highest values correspond to nine carbonaceous units, whereas the TOC content in siltstone, silty mudstone and finer grained clay-dominated mudstone varies independently of lithology (Figure 2). In contrast, to the siltstones, the limestones at 247, 249, 251 m have low TOC in the range of 0.36 to 1.09 %. Taken individually, the TOC suggests the source rock potential of Karenight is good to very good (Peters et al., 2005). The TOC data presented here are higher than those reported for drill-core of Namurian, Arnsbergian age from Widmerpool Gulf (range 0.4-7.3%, mean TOC 3%, $n=32$), those for the Namurian upper Bowland-Hodder unit from the Cleveland Basin (range 0.37-2.45%, mean 1.9, $n=6$) and the Craven Basin (range 1.76-3.72%, mean 2.3% ($n=36$)) (Könitzer et al., 20015, Hough et al., 2014, Słowakiewicz et al., 2015). However, it should be borne in mind that not all organic matter has equal hydrocarbon generative potential.

3.2 *Fourier transform infrared spectroscopy*

The FTIR analysis of the Karenight samples is summarised by a mean spectrum for all samples (Figure 3). The plot shows distinct peaks in the aliphatic ($\sim 2750-3000\text{ cm}^{-1}$), carbonyl ($\sim 1700\text{ cm}^{-1}$), CH_3 & CH_4 ($\sim 1400-1550\text{ cm}^{-1}$) and aromatic deformation ($\sim 800\text{ cm}^{-1}$). These wavenumber assignments are tentative and based on values published by Lis et al. (2005) and Chen et al. (2015). The data from these studies derived for samples contained in a pressed potassium bromide (KBr) disc, whereas our FTIR data are produced using diffuse reflectance using the pure milled samples. The two approaches can produce slightly different peak assignments; for this reason, all assignments referred to herein are tentative.

The aliphatic region ($\sim 2750\text{-}3000\text{ cm}^{-1}$) peaks produced for the Karenight core are similar to those produced for U.S shale samples originating from Anvil Pots mine and Garden Gulch Member (Washburn and Birdwell, 2013). Again, the method, Attenuated Total Reflectance-FTIR is different to our study as it measure one specific sample point rather than a diffuse reading, so direct comparison is subject to instrumental uncertainties. Further discussion of the Karenight core FTIR mean spectrum, especially in the fingerprint region ($400\text{-}2000\text{ cm}^{-1}$), is not possible due to the background noise caused by its inorganic (mineral) constituents. For example, $1400\text{-}1500\text{ cm}^{-1}$ could be CH_2 , CH_3 -bending or CH_3 absorption (Chen et al., 2014b) or be due to the presence of carbonates (Calderón et al., 2011). Further discrimination of the importance of this noise may be possible using complementary techniques such as x-ray diffraction or potentially pre-treatment of the sample to remove the inorganic constituents.

Baseline corrected and mean-smoothed FTIR spectra for all samples were reviewed in depth order (Figure 4). There is no obvious depth-based trend in the spectra, although there are differences in the size of the aliphatic peaks ($\sim 2750\text{-}3000\text{ cm}^{-1}$). Plots ordered on increasing Rock-Eval parameter values (S_1 , S_2 , S_3 and T_{max}) show that for S_1 and S_2 there is an increase in the aliphatic region and a reduction in the aromatic and oxygenated functional group region ($1850\text{-}1600\text{ cm}^{-1}$). Peaks present in from Wavenumber $950\text{-}1050\text{ cm}^{-1}$ show an increase in area and a peak at Wavenumber $\sim 1400\text{ cm}^{-1}$ an increase in relative height (CH_2 and CH_3). Reliable interpretation of these features is difficult because of the presence of the mineral component and the complexity of the organic matter.

There are a number of ways to overcome the issue of converging IR signals including sample clean-up to isolate the organic constituents (Calderón et al., 2011, Fletcher et al., 2014), micro-FTIR (Chen et al., 2014b) and pyrolysis gas FTIR (Fletcher et al., 2014). Any additional sample preparation or analytical work on shale samples is likely to provide valuable information about their hydrocarbon characteristics. However, these approaches are time consuming and expensive, rendering them beyond the scope of this paper. This is because this study is designed to demonstrate the value of FTIR in rapid low-cost evaluation of shales to supplement hydrocarbon industry standard screening analysis, namely, Rock-Eval.

3.3 Chemometric modelling

Principal components analysis (PCA) was undertaken using different parts of the FTIR data. The results were evaluated in the context of selected Rock-Eval trends and interpretation. T_{max} is defined as the temperature of the maximum rate of hydrocarbon generation measured on the S_2 peak and is derived during the pyrolysis of non-volatile hydrocarbons contained within the sample (Behar et al., 2001). The oil-gas window of a shale is typically define by an approximate cut-off point 435°C , below which the kerogen is considered immature and commercially unproductive (Słowakiewicz et al., 2015). The HI is also affected by thermal maturity and tends to decrease with maturity. An indicative HI cut-off point for a change in residual kerogen type (Type II/III oil prone to Type III to gas prone) is 200 mg HC/g TOC . T_{max} and HI values do not lend themselves to direct identification using conventional FTIR data analysis because they are derived from either thermal cracking of bound hydrocarbons in the case of T_{max} or calculated parameters in the case of HI. However, they are important indicators of thermal maturity and kerogen type that correspond with the organic composition of the shale rock, which for this reason mean they were chosen to aid with PCA interpretation.

A PCA bi-plot of the PC1 and PC2 scores with data points colour coded using the T_{\max} and HI cut-off points (435 °C and 200 mg HC/g TOC respectively) shows two tentative clusters of samples and a limited number of outliers (Figure 5).

The bottom right-hand cluster in Figure 5 (red data points: $T_{\max} < 435$ °C and HI < 200 mg HC/g TOC) comprises samples that are generally greater than 244 m bgl and correspond to mudstone with limestones lithology (Figure 2). The top left-hand cluster (blue data points: $T_{\max} > 435$ °C and HI > 200 mg HC/g TOC) are shallower and match to the mudstone with thin laminar siltstone (Figure 2). The outliers are indicated on Figure 5 and apart from one or two unexplained examples, relate to anomalies that appear to be associated with the core lithology and stratigraphy. These results show that the PCA is able to distinguish characteristics related to the organic matter present in the mudstone not visible purely using the FTIR spectra. These characteristics correspond to the stratigraphy of the core rather than to the thermal maturity of the organic matter.

The relative contribution to the loadings and coefficients for PC1 to PC4 made by each wavenumber was calculated and visualised (Figure 6). The results suggest both the loadings and regression coefficients are strongly influenced by wavenumbers 3800-3400, 3300-2800, 2700-2400 and 2000-500 cm^{-1} . These wavenumbers reflect the trends in the mean spectrum discussed earlier (Figure 3). The contributions of the wavenumbers to the loadings and coefficients are higher when the PCA is restricted to fingerprint and non-fingerprint region data. This suggests that the PLSR modelling might provide better predictive models for the truncated datasets because of the stronger signals represented by the loadings and coefficients derived from the respective wavenumbers.

Partial least squares regression models using all data, fingerprint and non-fingerprint region as independent variables were created using Rock-Eval parameters S1, S2, S3, T_{\max} and TOC as dependent variables. HI and OI were calculated from modelled S2, S3 and TOC respectively using the equations shown in Table 1. Each of the PLSR models was evaluated using four goodness-of-fit statistics for the median cross-validation predicted values (Table 3). The most accurate models, defined using set criteria (Table 1), are: i) S3 using all data; ii) T_{\max} , S1 and S2 using the non-fingerprint region; and iii) TOC using the fingerprint region. The fact that different sections of the FTIR spectra were used to produce the preferred models supports the assertion that that specific wavenumber regions reflect distinct organic characteristics of the Karenicht core measured using Rock-Eval.

FTIR fingerprint region principal components produced the best model for predicting TOC (Table 3). The median cross-validation values conform well to the one-to-one line with minimal variation and extreme values (Figure 7). Lines of best fit for 10th and 90th percentile fall within a small range but converge slightly at higher TOC, suggesting some heteroscedasticity (Figure 7a). Analysis of the residuals shows that the model accounts for the variation in the data with no apparent systematic trend and low R-squared (Figure 7b). Percentage error is quite high for low TOC values (Figure 7c).

Non-FTIR fingerprint principal components produced the best model for predicting T_{\max} (Table 3). The median cross-validation values broadly conformed to the one-to-one line, notwithstanding a limited number of extreme values (Figure 8a). The model tends to under predict low T_{\max} values and over predict high values (Figure 8a and Figure 8d). Lines of best fit for 10th and 90th percentile fall within a small range but converge slightly at higher T_{\max} , suggesting some heteroscedasticity (Figure 8a). Repeated cross-validation data ranges presented in the same plot varied widely. Analysis of the

residuals shows that the model accounts for the variation in the data with no apparent systematic pattern and low R-squared (Figure 8b). Percentage error is generally high (Figure 8c).

Non-fingerprint FTIR principal components produced the best model for predicting S1 (Table 3). The median cross-validation values conformed well to the one-to-one line at the high and low S1 values, (Figure 9a). There were also a limited number of extreme values. As with TOC, lines of best fit for 10th and 90th percentile data show that most of the cross-validation data fall within a small range. The 10th and 90th percentile lines of best fit converge slightly at higher S1 values, indicating possible heteroscedasticity. Repeated cross-validation of the S1 data presented in the same plot showed more variation for low and high values of the data rather than the mid-range. Analysis of the residuals suggests that the model accounts for the variation in the data with no apparent systematic pattern, confirmed by a low R-squared value for the linear model line of best fit (Figure 9b). Percentage error is well constrained throughout the data (Figure 9c).

Non-fingerprint FTIR principal components produced the best model for predicting S2 (Table 3). The median cross-validation values conformed very well to the one-to-one line (Figure 10a). the cross-validation data for S2 has a very small range in comparison to other parameters. The 10th and 90th percentile lines of best fit also converge at higher S2 values, indicating likely heteroscedasticity. These lines are slightly below the one-to-one line at higher S2 values. Repeated cross-validation data revealed minimal variation, suggesting repeatability good throughout the S2 range. Analysis of the residuals suggests that the model accounts for the variation in the data with no apparent systematic pattern and low R-squared (Figure 10b). Percentage error was high (Figure 10c).

All data FTIR principal components produced the best model for predicting S3 (Table 3). The median cross-validation values conformed well to the one-to-one line, although a possible sigmoidal shape is present. The model over predicts in the mid to upper range of the data (Figure 11a). As with other Rock-Eval parameters, lines of best fit for 10th and 90th percentile data show that most of the data falls within a small but diverge slightly at higher S3 values, indicating possible heteroscedasticity. Repeated cross-validation data present low variation in comparison of other Rock-Eval parameters, suggesting repeatability is moderate. Analysis of the residuals suggests that the model accounts for the variation in the data but with a slight systematic pattern show also by the R-squared (Figure 11b). Percentage error was high (Figure 11c).

Overall, the most accurate models with the lowest cross-validation goodness-of-fit statistics are for S1, S2, S3 and TOC. Percentage error results are all higher than T_{Max} despite lower MAE, RMSE and higher R-squared. The residuals plots for all Rock-Eval parameters suggest none of the models are over-fitted although there is an indication of heteroscedasticity in 10th and 90th percentile best fit lines. The absolute error plots show that S1, S2, S3, TOC and HI models conform well to the measured data trend line in comparison to T_{max} .

For this study we created a new goodness-of-fit metric called mean percentage range standardised error (MPRSE) to describe the model residuals as a percentage of the range. We did this because it was difficult to distinguish between goodness-of-fit statistics using MAE, RMSE, R-squared and MPAAE. Low MPRSE indicates the modelled values are closer to the measured values than high MPRSE. Using multiple acceptance criteria in environmental modelling is well-documented (Bennett et al., 2012, Jakeman et al., 2006) but it is rarely applied rigorously (Beriro et al., 2013). For example, (Washburn and Birdwell, 2013) report 'excellent models' based on R-squared being >0.9. We argue

that although the published models produce high R-squared (Washburn and Birdwell, 2013), such a definitive conclusion should be supported using congruent model acceptance criteria. Washburn and Birdwell (2013) show similar percentage error values as this research (~20%), which we would argue is not as excellent as a high R-square might suggest. However, the authors acknowledge their sample set is small and not fully representative of the variation of shales present in the UK (Washburn and Birdwell, 2013).

MPRSE for the PLSR models show that: i) T_{max} , has the highest values (>10%); and ii) S1, S2, S3 and TOC MPRSE lowest (<10%) (Table 3). These findings are important because Rock-Eval pyrolysis is used as screening tool with selected parameter cut-off points or thresholds are often being applied to the data e.g. T_{max} of $\geq 435^{\circ}\text{C}$ is indicative of an oil prone shale rock based on its thermal maturity. In practice, it is important to ensure that any decisions made using modelled values minimise uncertainties, especially false positives i.e. a modelled T_{max} value of 440°C which is actually 410°C given that this scenario may lead to the assumption that the shale is of sufficient thermal maturity to generate oil and/or oil and gas when it is not. This situation could occur if MPRSE was not used to evaluate the T_{max} or S1 models. Where T_{max} MPAE is 0.75% and MPESR is 15.51%, MPAE appears low but is caused by high absolute values $>400^{\circ}\text{C}$ in comparison to a small range $\sim 50^{\circ}\text{C}$ (Figure 15); conversely, S1 has a high MPAE of 35.57% and a low MPRSE 9.2% (Table 3). When modelling is undertaken to predict one variable only, MPAE can be used to discuss the predictions relative to the magnitude of the parameter unit and its range but when multiple units are being modelled than MPRSE is more appropriate. We suggest that the models presenting MPRSE $\sim 10\%$ have an acceptable level of uncertainty in the context of the Rock-Eval ranges measured for the Karenight core (Table 3). However, this assumption needs to be considered in the context of the other of lines-of-evidence including the measured-modelled scatters plots. We suggest that the S1, S2, S3 and TOC models are potentially suitable for predicting down-core values. Modelled T_{max} has a low MPRSE the cross-validation data in the scatter plots is widely spread and therefore may not be suitable for making reliable predictions. The relative ranges used to draw these conclusions are for the Karenight borehole only. Using a larger dataset with ranges that are geographically/geologically constrained to the wider basin(s) may be more useful. Such data were unfortunately not available for this research and may help establish if this technique is useful to quantify geochemical parameters on a more basin-wide scale.

HI and OI were calculated using modelled TOC, S2 and S3 and compared to calculations made using measured values (Figure 12 and Figure 13). HI correlations do not appear particularly strong whereas OI look reasonable. Further analysis was conducted by incorporating the data into the Van-Krevelen diagrams.

Van-Krevelen diagrams and S2 to TOC bi-plots are used as an indication of the maturity of the shale and are also known to be used as crude estimate of kerogen type as well as generative-potential (Słowakiewicz et al., 2015, Könitzer et al., 2016, Waters et al., 2020, Monaghan et al., 2017). Comparison of the measured and modelled values suggest a good correspondence and similar clustering (Figure 14). For example, the majority of modelled values fall within the expected HI range of $\sim 150\text{-}300$ and OI $\sim 2\text{-}7$ mg/g TOC which in turn elicits a similar kerogen classification to that using measured values. Inspection of the modelled values on the van-Krevelen diagram confirms that the modelled HI values are conservative. However, three limestone samples with low measured HI values appear to be under-estimated by the FTIR modelling approach. Nevertheless, when both bi-

plots are considered together as would be standard procedure during a prospect appraisal it is clear the modelled values provide a similar indication of kerogen type and generative potential to that from the actual Rock-Eval(6) pyrolysis derived HI, OI and TOC values.

The shales examined in this current study pose a similar problem in that they are from one core of limited thermal maturity range, kerogen types and palaeogeographic position in the basin. In addition, this research used one chemometric modelling method. There are many contemporary techniques that also produce transparent model outputs, e.g. evolutionary algorithms (Beriro et al., 2014), that could form the basis of a comparative study. Doing so is expected enhance the utility of applied chemometrics in understanding shales in an unconventional hydrocarbon context and move toward optimising both the modelling method and model evaluation steps basin as well as individual core assessments. Overall, this research provides encouraging proof-of-concept results that require developing further using a range of shales that cover a range of burial conditions and maturity.

4. Conclusions

This study shows that FTIR analysis of UK shale from the Bowland Shale Formation can be used in conjunction with principal components analysis and partial least squares regression modelling to estimate selected organic characteristics derived using Rock-Eval pyrolysis. PCA explains more about the organic signature of the rock than spectral analysis alone. This is because the FTIR peak resolution is complicated by the presence of the inorganic (mineral) constituents of the rock. More detailed quantification and characterisation of the organic fraction of the rock would be informative but moves the scope of the research away from a rapid low-cost technique for increasing the resolution of down-core organic matter characterisations. However, in order to provide greater confidence in the conclusions drawn here, it may be required in future studies. The PLSR models showing MPESR ~10% and a small range associated with the cross-validation data present an acceptable level of uncertainty (TOC, S1, S2, S3, HI, and OI) and are suitable interpolating down-core Rock-Eval parameter values. Conversely, FTIR modelled T_{max} has an MPESR >10% and a high cross-validation data range is above the acceptable level of uncertainty. Down-core interpolations of selected Rock-Eval parameters could be practically achieved by modelling FTIR data by maintaining standard sample frequencies for Rock-Eval samples while supplementing with higher frequencies for FTIR and chemometric analysis. The approach has the potential to provide greater spatial characterisation of the shale rock where high-resolution stratigraphic control is needed on organic carbon type, but economics preclude substantial analytical programs. The application of the techniques shown here may also have wider value to other geological research pertaining to mudrock successions including radioactive waste disposal.

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ACCEPTED MANUSCRIPT

Figure Captions

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Figure 2 Karenight lithology and Rock-Eval(6) down-core plots. Based on Hennissen et al. (2017) © 2017 BGS (NERC), available under CC BY 4.0

Figure 3 FTIR mean data spectrum

Figure 4 FTIR all depth sample data

Figure 5 FTIR principal components analysis bi-plot for PC1 and PC2

Figure 6 PC loadings, regression coefficients and median spectra for PC1 to PC4 using all data (A) all wavenumbers (4000-400 cm^{-1}) (B) the non-fingerprint (4000-2500 cm^{-1}) and (C) the fingerprint region (2500-500 cm^{-1})

Figure 7 Preferred Tmax PLSR model derived from non-fingerprint data showing (A) repeated LOO PLSR (B) absolute residuals (C) percentage residuals (D) absolute error

Figure 8 Preferred HI PLSR model derived from non-fingerprint data showing (A) repeated LOO PLSR (B) absolute residuals (C) percentage residuals (D) absolute error

Figure 9 Preferred S1 PLSR model derived from all data showing (A) repeated LOO PLSR (B) absolute residuals (C) percentage residuals (D) absolute error

Figure 10 Preferred S2 PLSR model derived from non-fingerprint data showing (A) repeated LOO PLSR (B) absolute residuals (C) percentage residuals (D) absolute error

Figure 11 Preferred S3 PLSR model derived from fingerprint data showing (A) repeated LOO PLSR (B) absolute residuals (C) percentage residuals (D) absolute error

Figure 12 Comparison between HI calculated using measured and modelled values

Figure 13 Comparison between OI calculated using measured and modelled values

Figure 14 Van-Krevelen diagrams and S2 to TOC cross-plots for measured and modelled values

Table Captions

Table 1. Acceptance criteria used for model evaluation

Table 2. Descriptive statistics for Rock-Eval data (n=72)

Table 3. PLSR goodness-of-fit statistics calculated for median cross-validation data

Method	Description	Acceptance criteria
Scatter plot	Scatter plot comparing observed Rock-Eval and modelled data	Conformity to one-to-one line
Goodness-of-fit statistics	MAE RMSE R-squared MPAE	MAE: low RMSE: low R-squared: high MPAE: low
Residuals analysis	Scatter plot of the residual difference between measured and modelled data	Absence of pattern in the scatter of the residual points on plot and very low R-squared
Absolute error analysis	Line plot comparing measured observed modelled data	Broad congruence and trend of peaks
Percentage error analysis	Plot showing percentage error	Low

Notes: MAE = Mean Absolute Error; RMSE = Root Mean Squared Error; MPAE = Mean Percentage Absolute Error.

Table 1

	TOC (%)	S1 (mg HC/g)	S2 (mgHC/g)	S3 (mg CO ₂ /g)	Tmax (°C)	HI mg HC/g TOC
Mean	5.43	1.07	11.4	6.48	435	201
Maximum	9.29	2.22	26.5	23.4	445	298
Minimum	0.36	0.09	0.62	1.60	424	82.0
Standard deviation	2.17	0.54	6.02	4.06	5.94	52.6
Relative standard deviation	40.0	50.3	52.8	62.6	1.37	26.2

Notes: TOC = Total Organic Carbon; HI = Hydrogen Index; HC = hydrocarbons

Table 2

Dependent variable	Independent variables	MAE	RMSE	R-squared	MPAE	MPRSE
All FTIR data	Tmax	2.98	4.52	0.45	0.68	14.20
	S1	0.22	0.28	0.72	31.37	10.22
	S2	2.53	3.45	0.67	41.94	10.16
	S3	0.06	0.07	0.65	42.64	9.77
	TOC	0.78	0.96	0.8	22.59	8.78
Non-Fingerprint region FTIR data	Tmax	3.26	4.45	0.45	0.75	15.51
	S1	0.20	0.26	0.77	35.57	9.20
	S2	1.80	2.34	0.85	39.85	6.94
	S3	11.17	12.67	0.02	96.83	43.11
	TOC	0.85	1.06	0.76	30.43	9.53
Fingerprint FTIR data	Tmax	3.18	4.8	0.4	0.73	15.12
	S1	0.3	0.4	0.43	42.97	14.29
	S2	2.57	3.43	0.68	43.09	9.91
	S3	0.09	0.12	0.12	53.54	15.39
	TOC	0.71	0.96	0.81	23.10	7.98

Notes: Models meeting goodness-of-fit acceptance criteria shown in bold red text. MAE = Mean Absolute Error; RMSE = Relative Mean Squared Error; MPAE = Mean Percentage Absolute Error; MPRSE = Mean Percentage Range Standardised Error.

Table 3

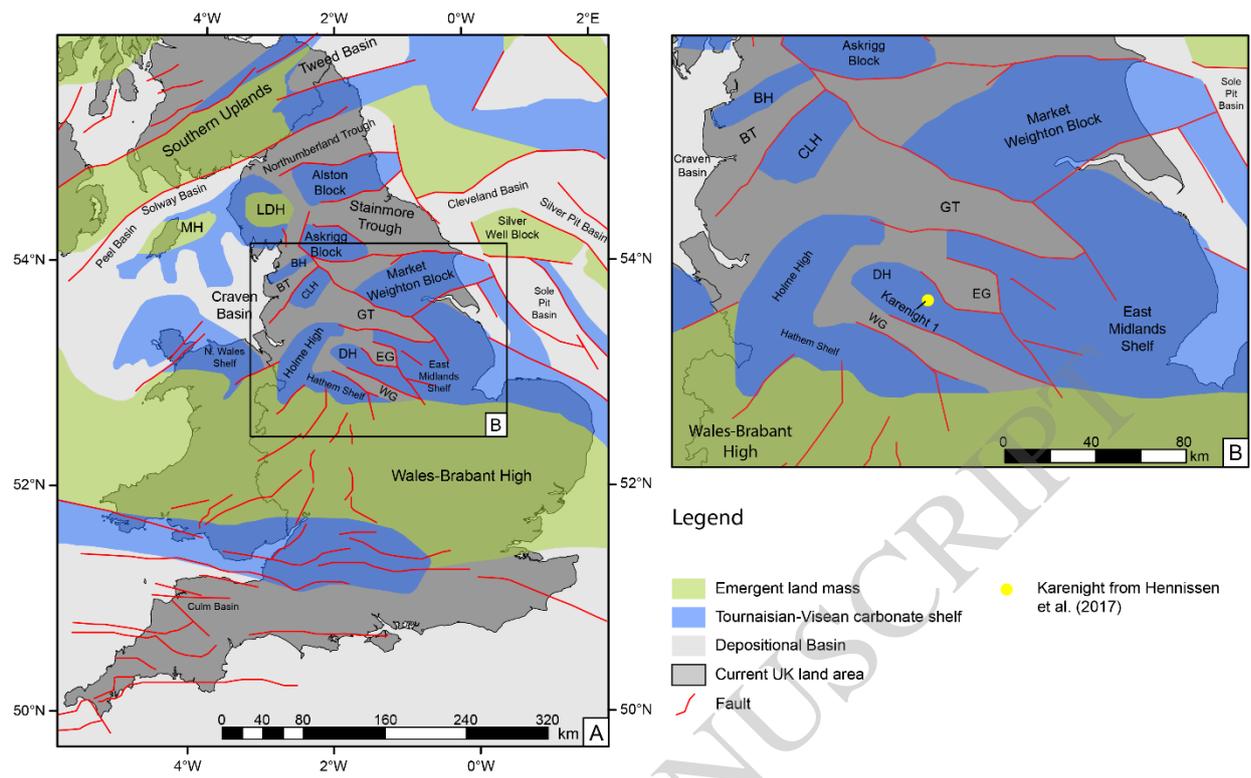


Figure 1

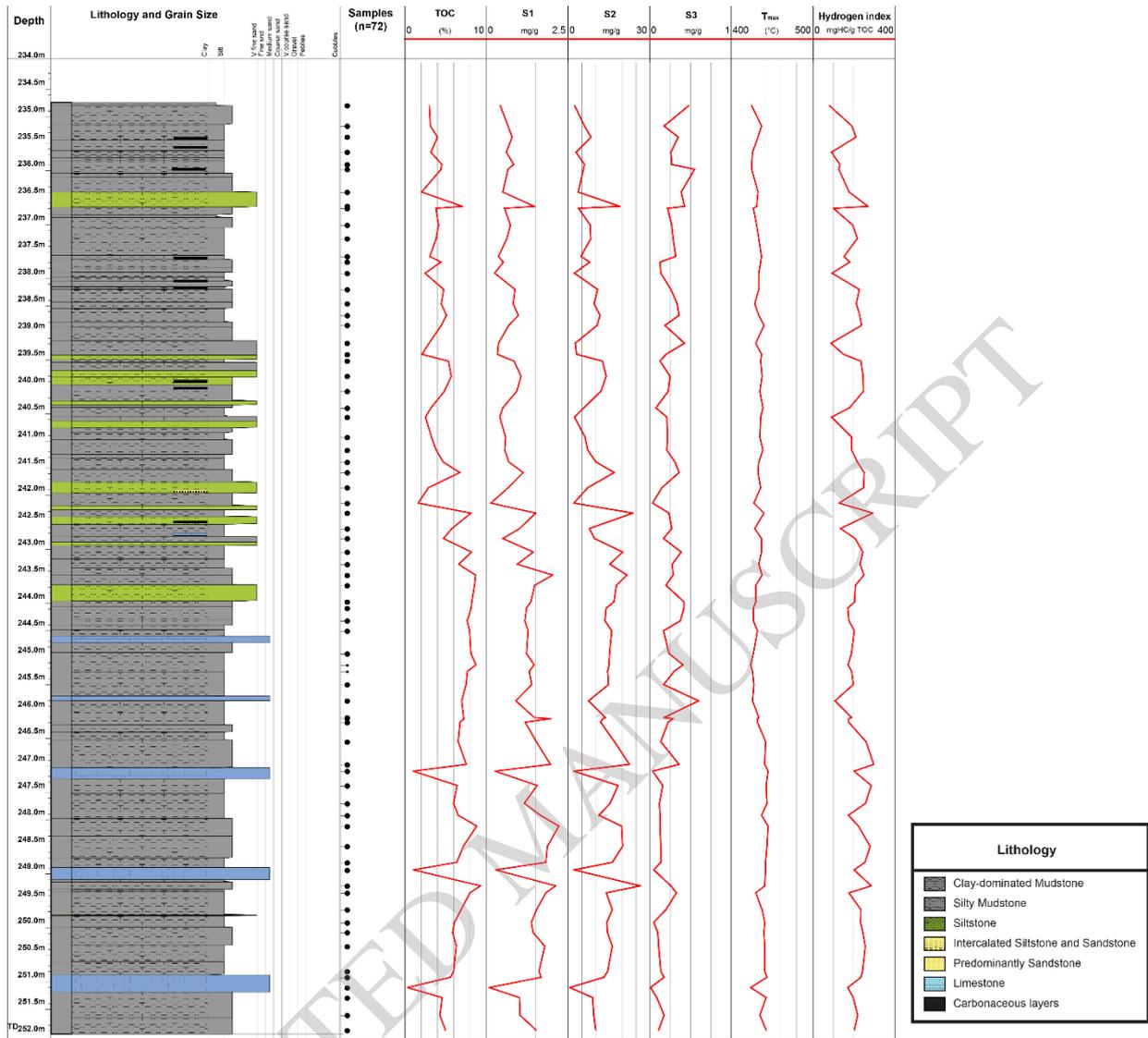


Figure 2

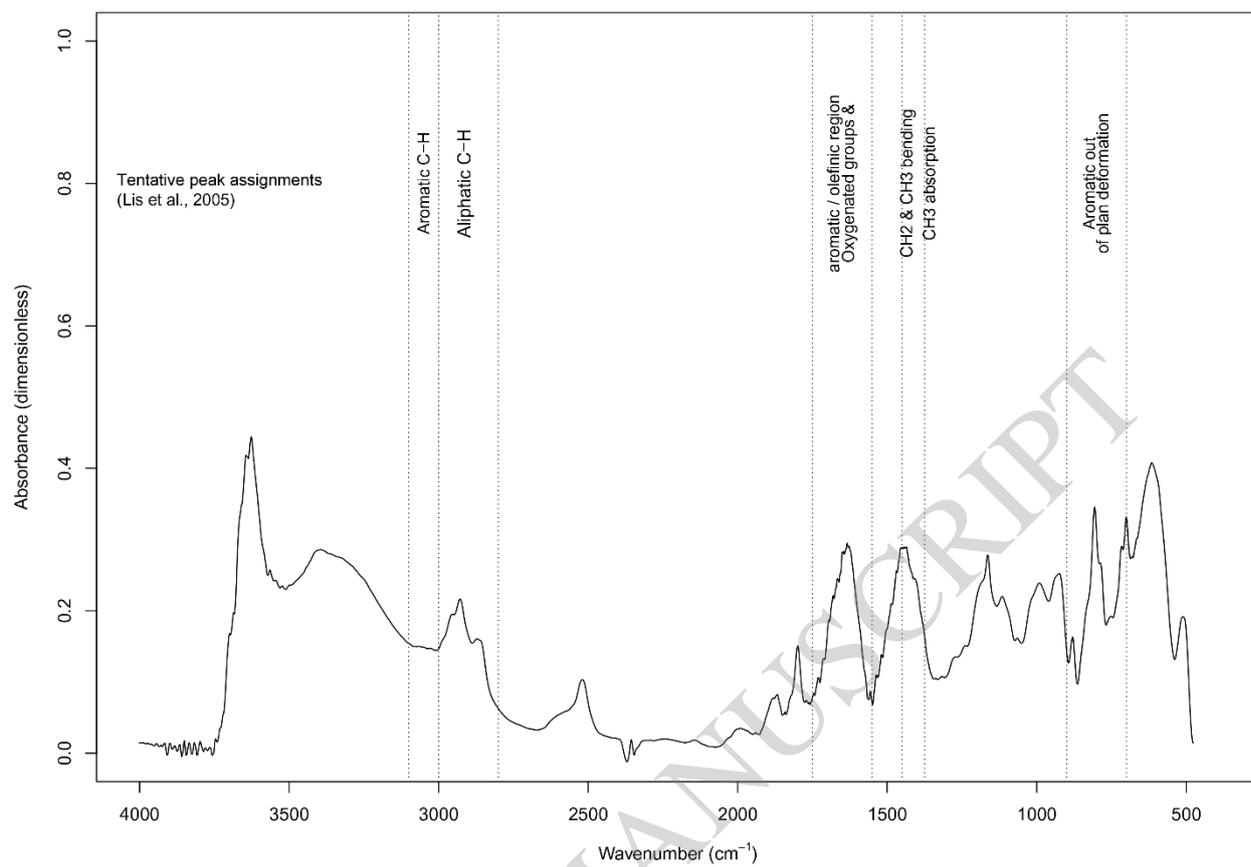


Figure 3

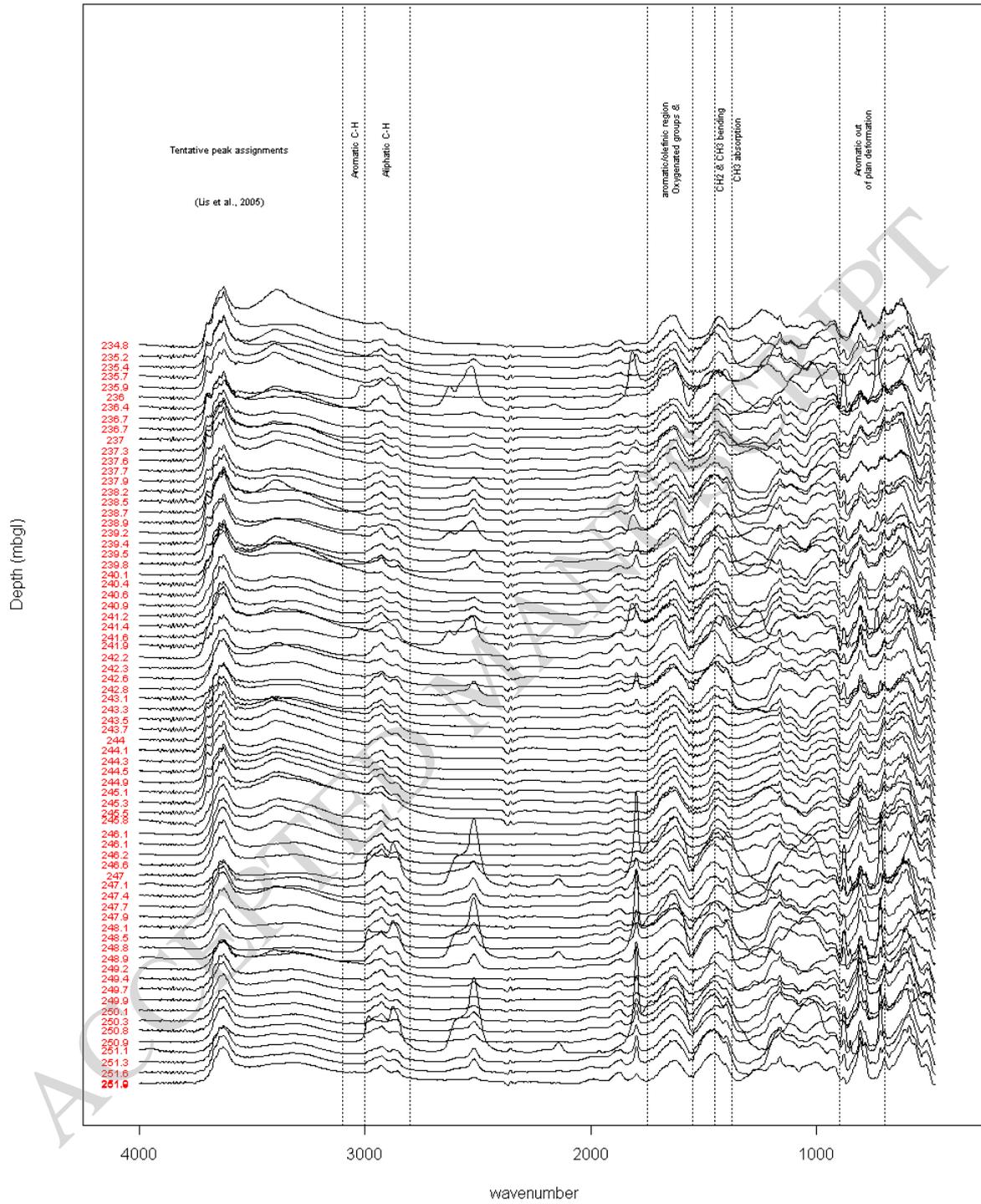


Figure 4

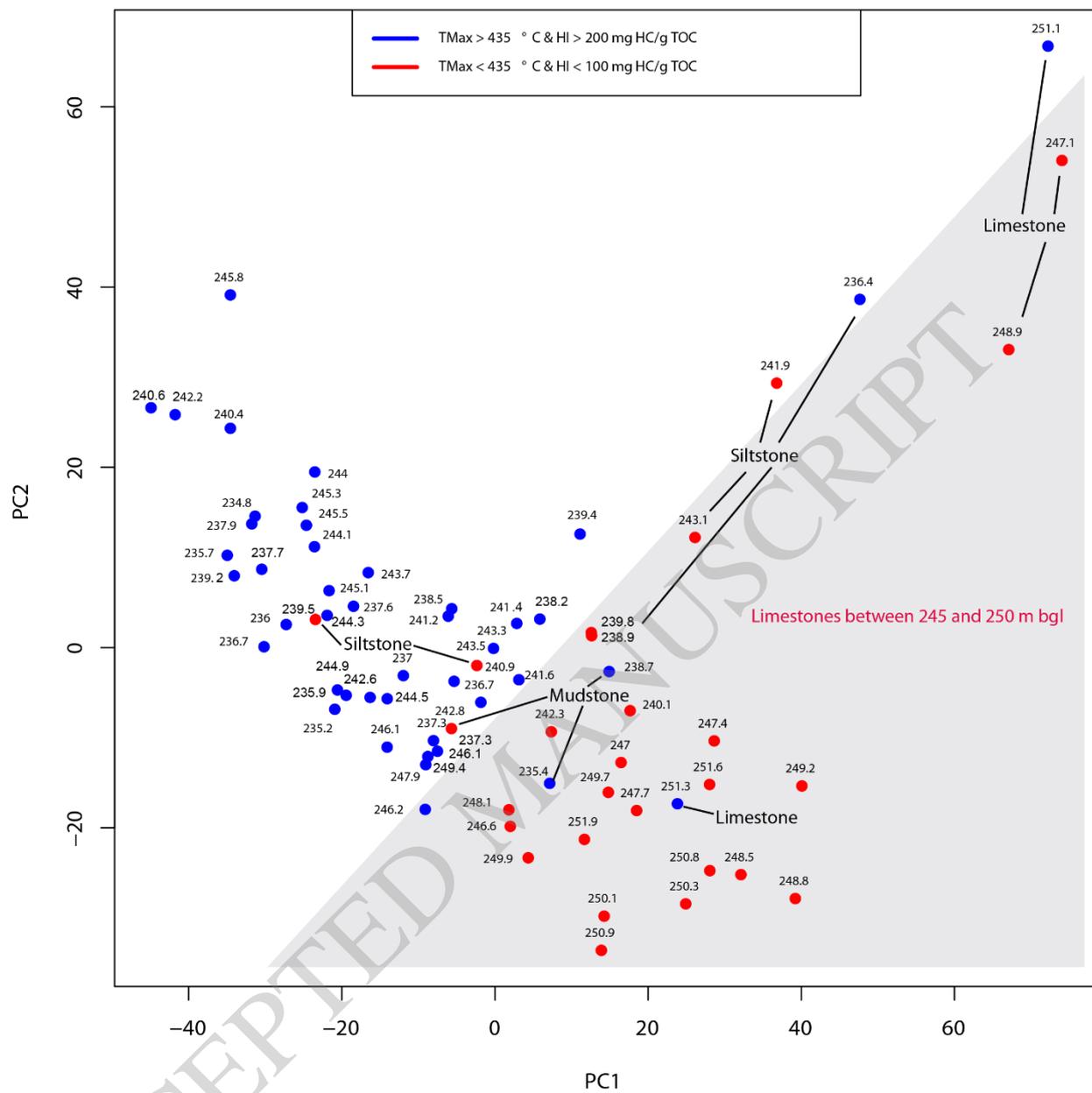


Figure 5

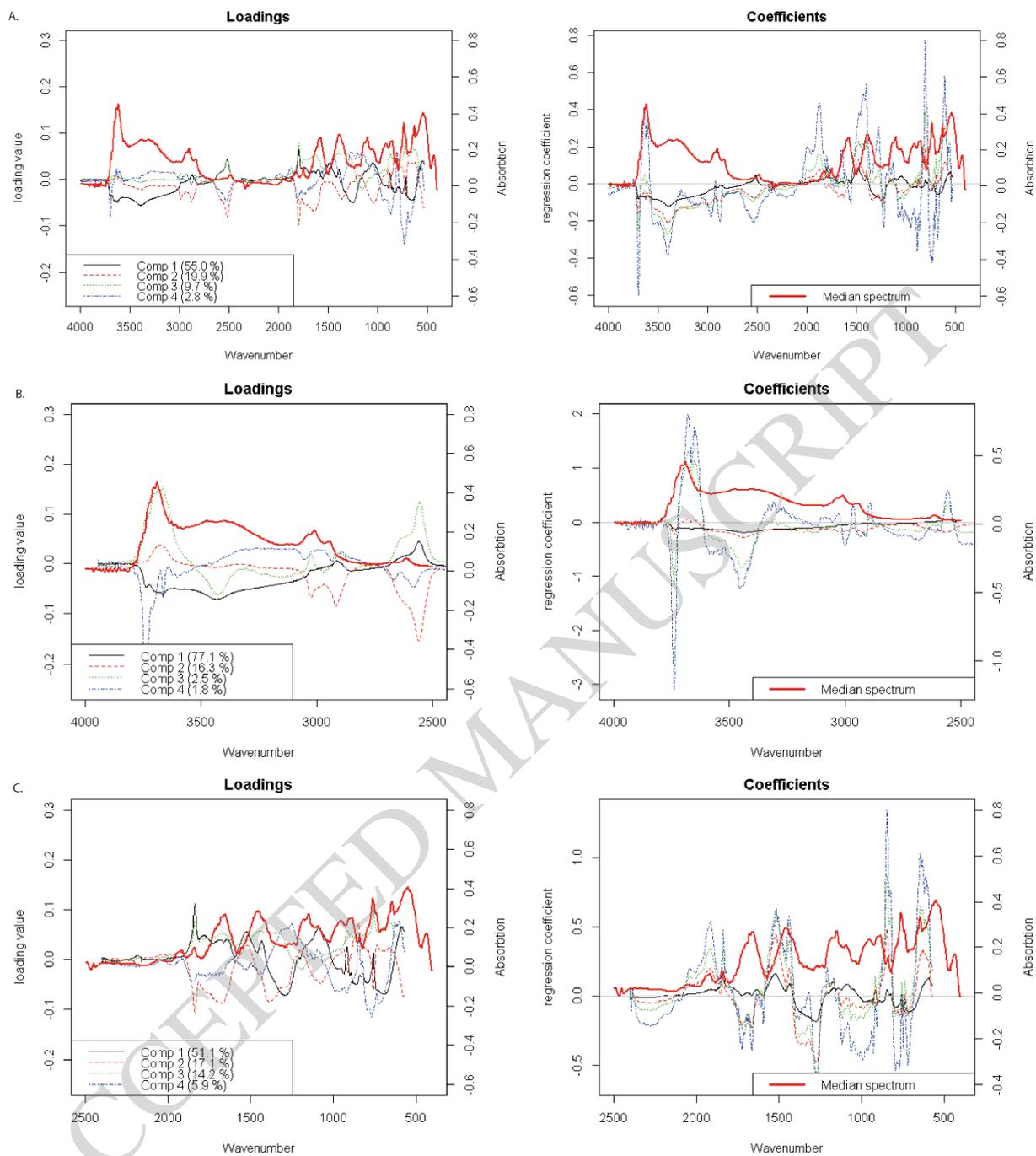


Figure 6

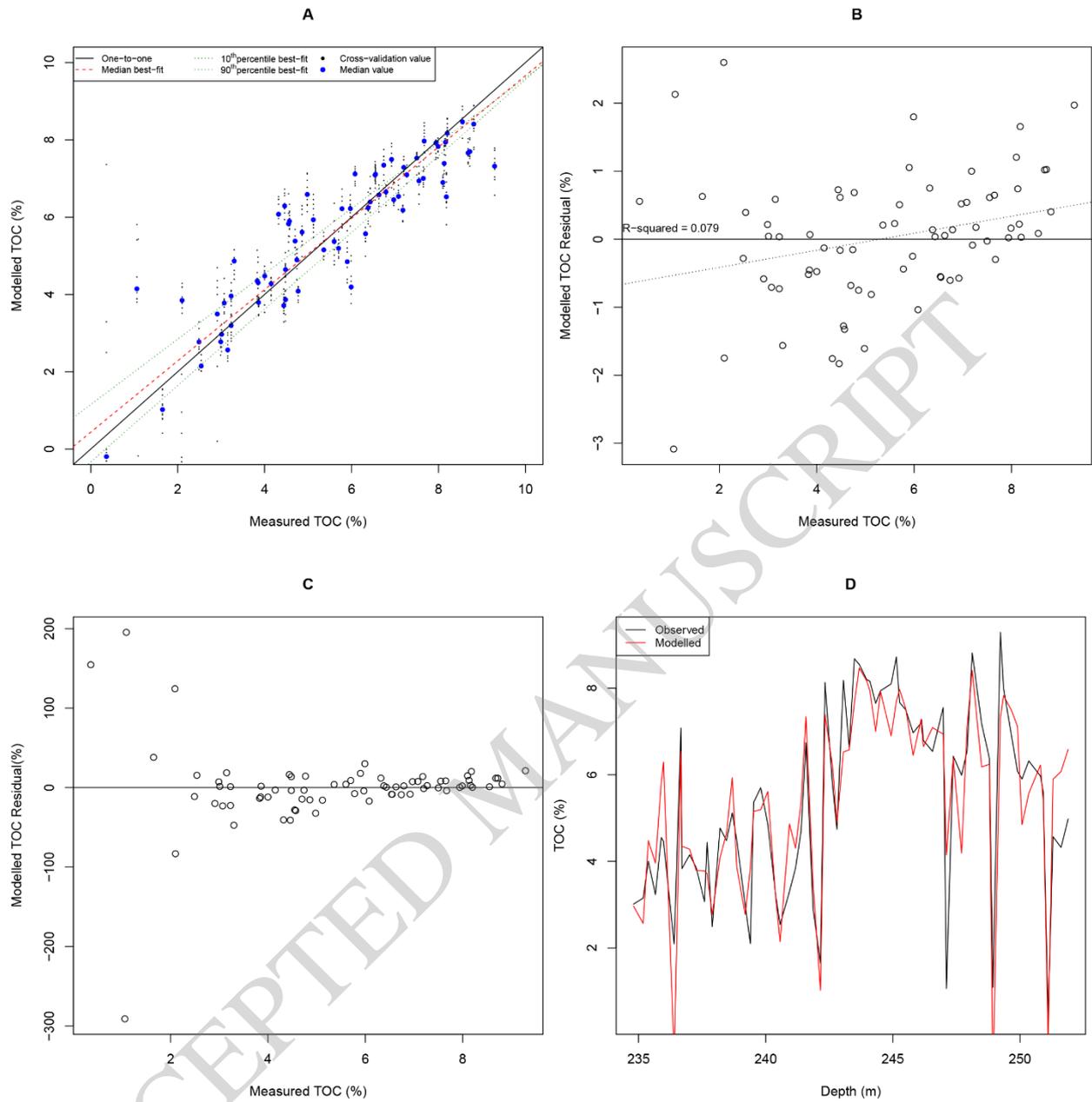


Figure 7

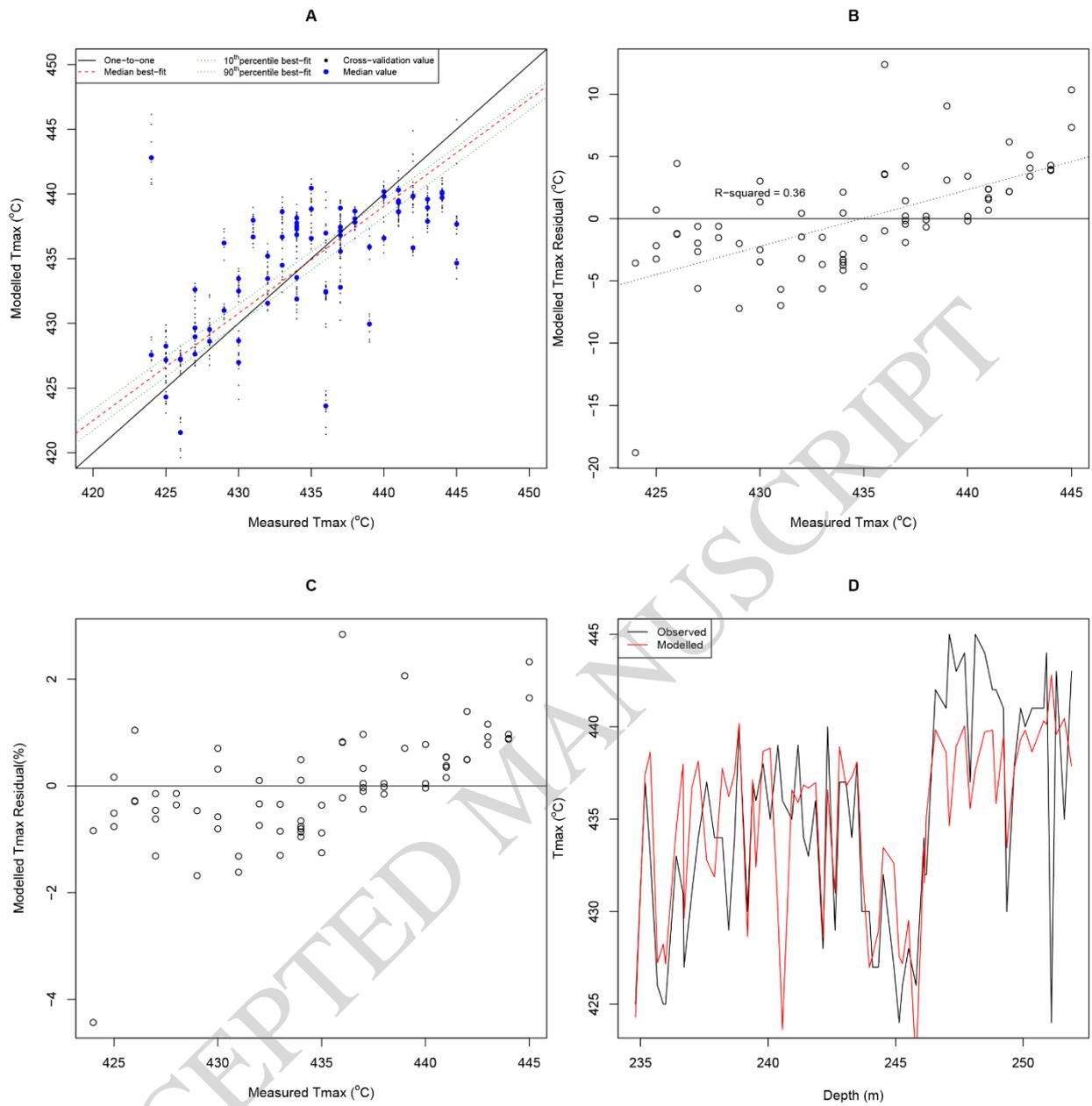


Figure 8

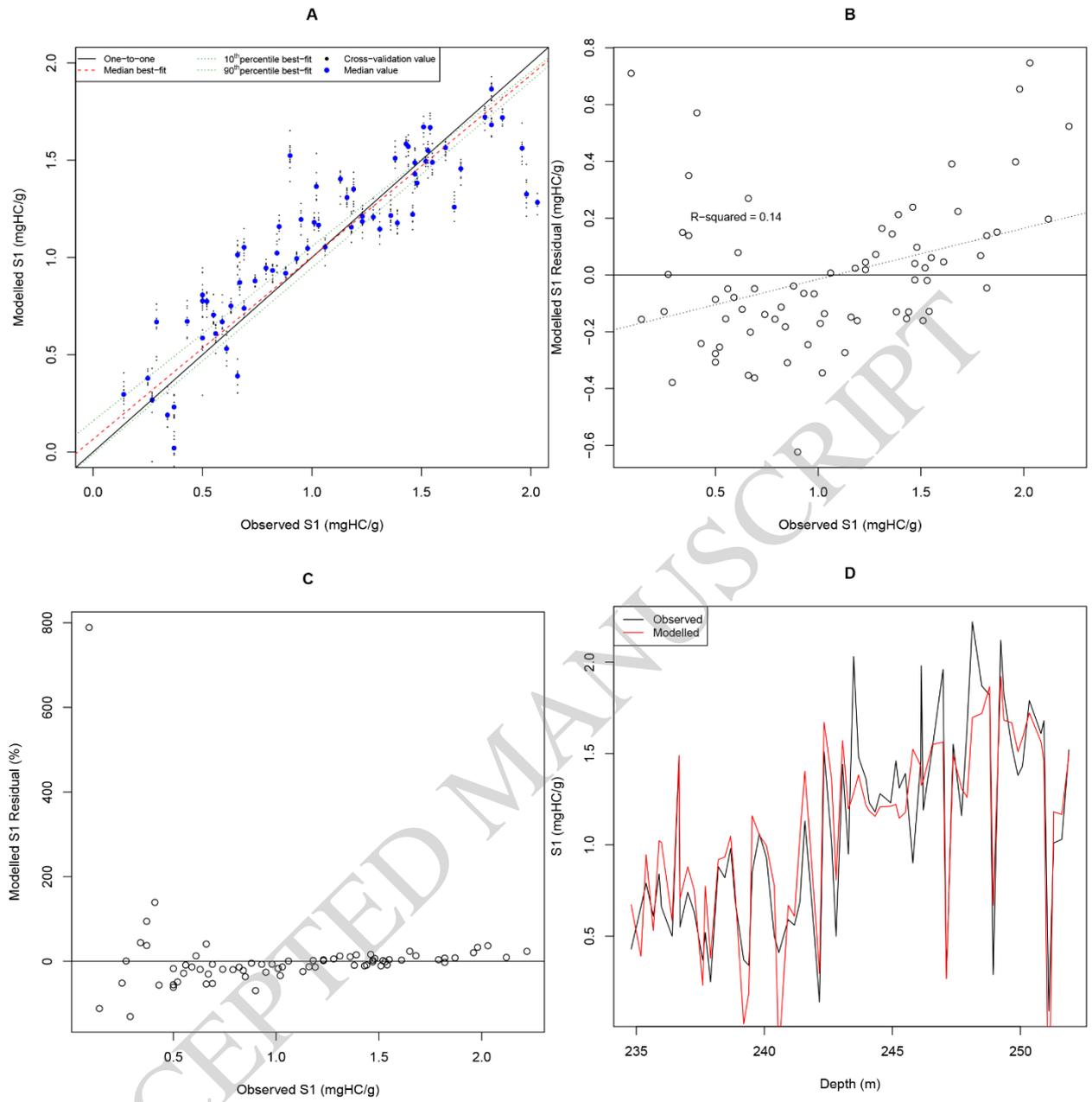


Figure 9

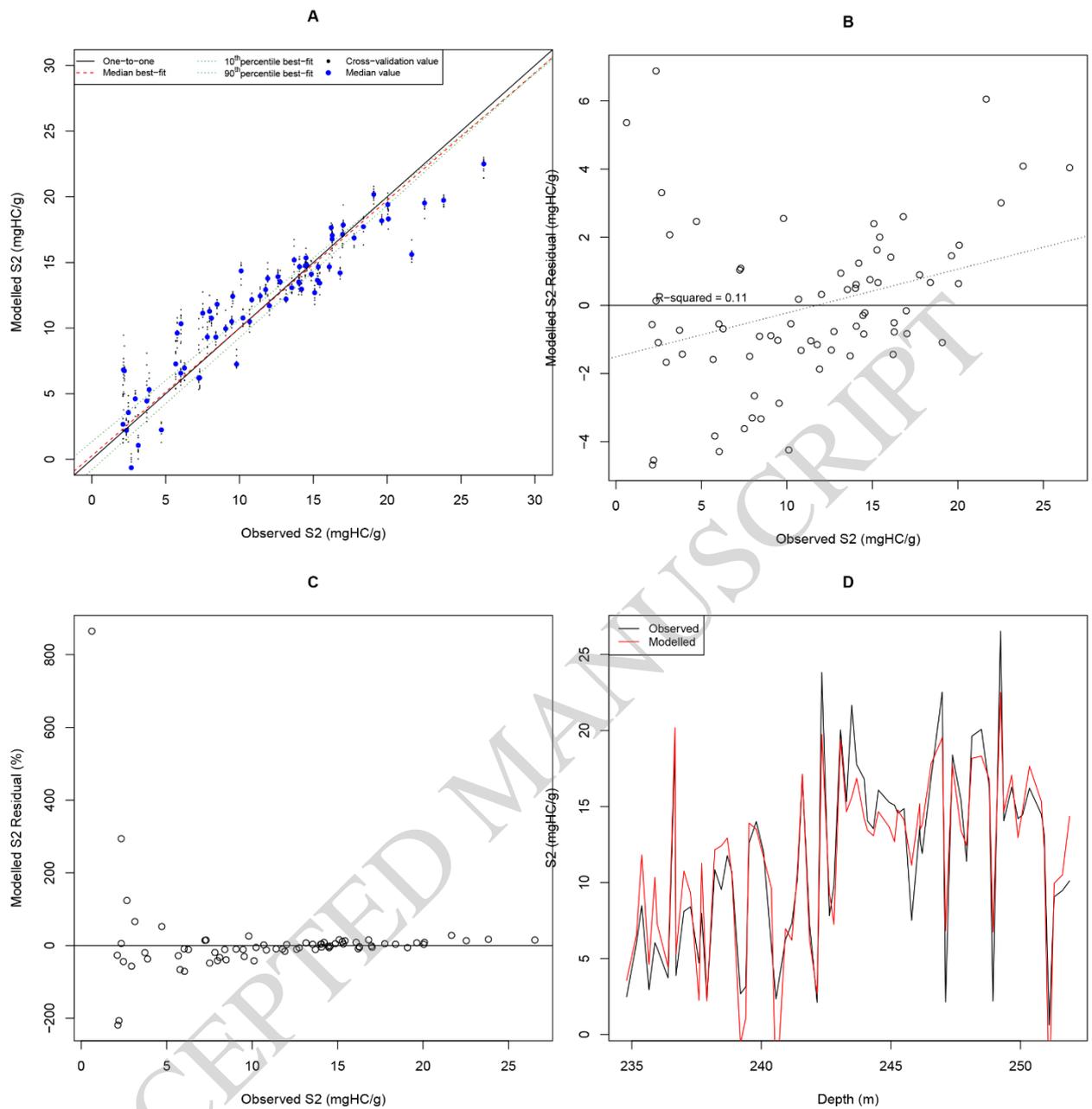


Figure 10

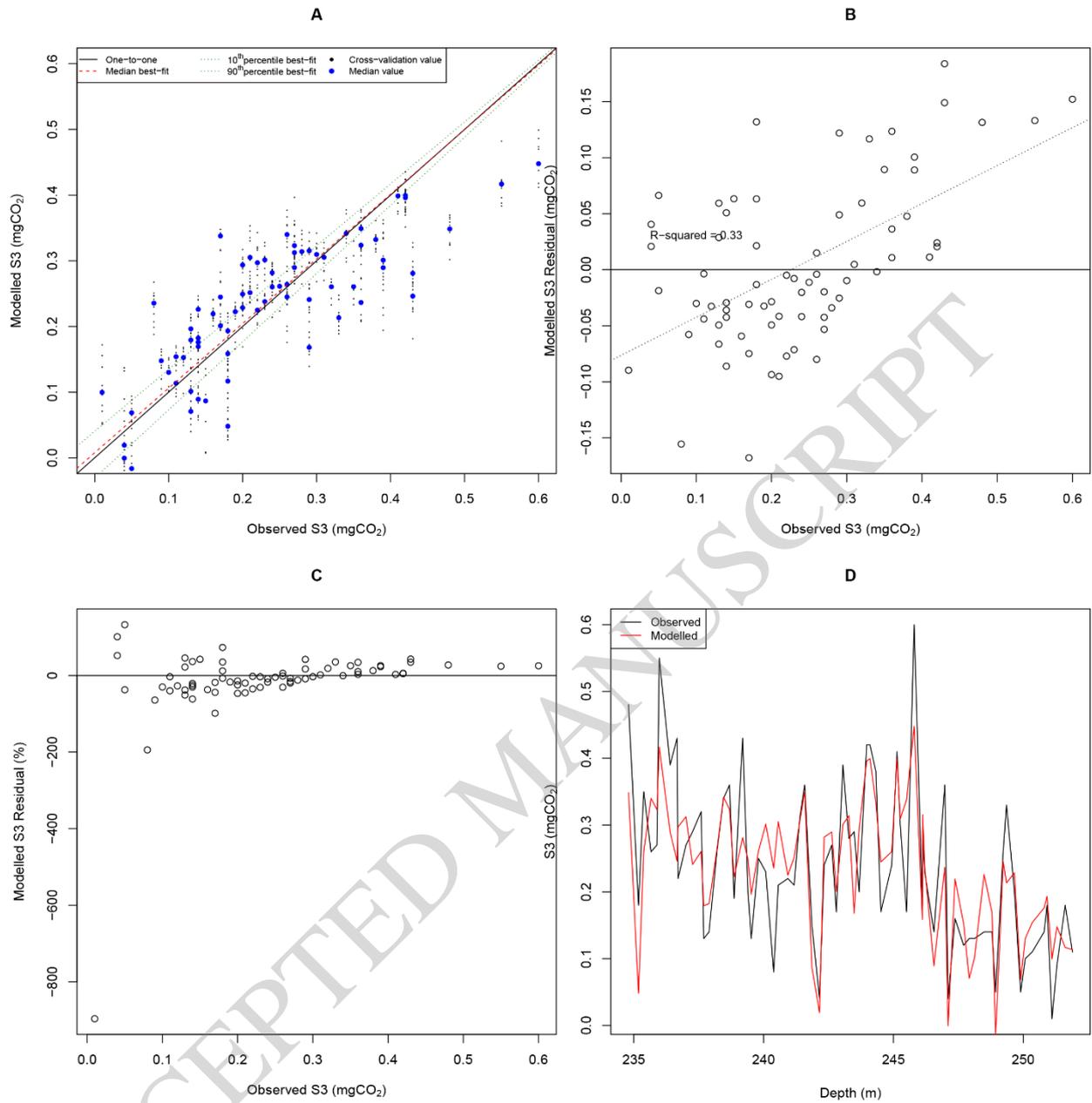


Figure 11

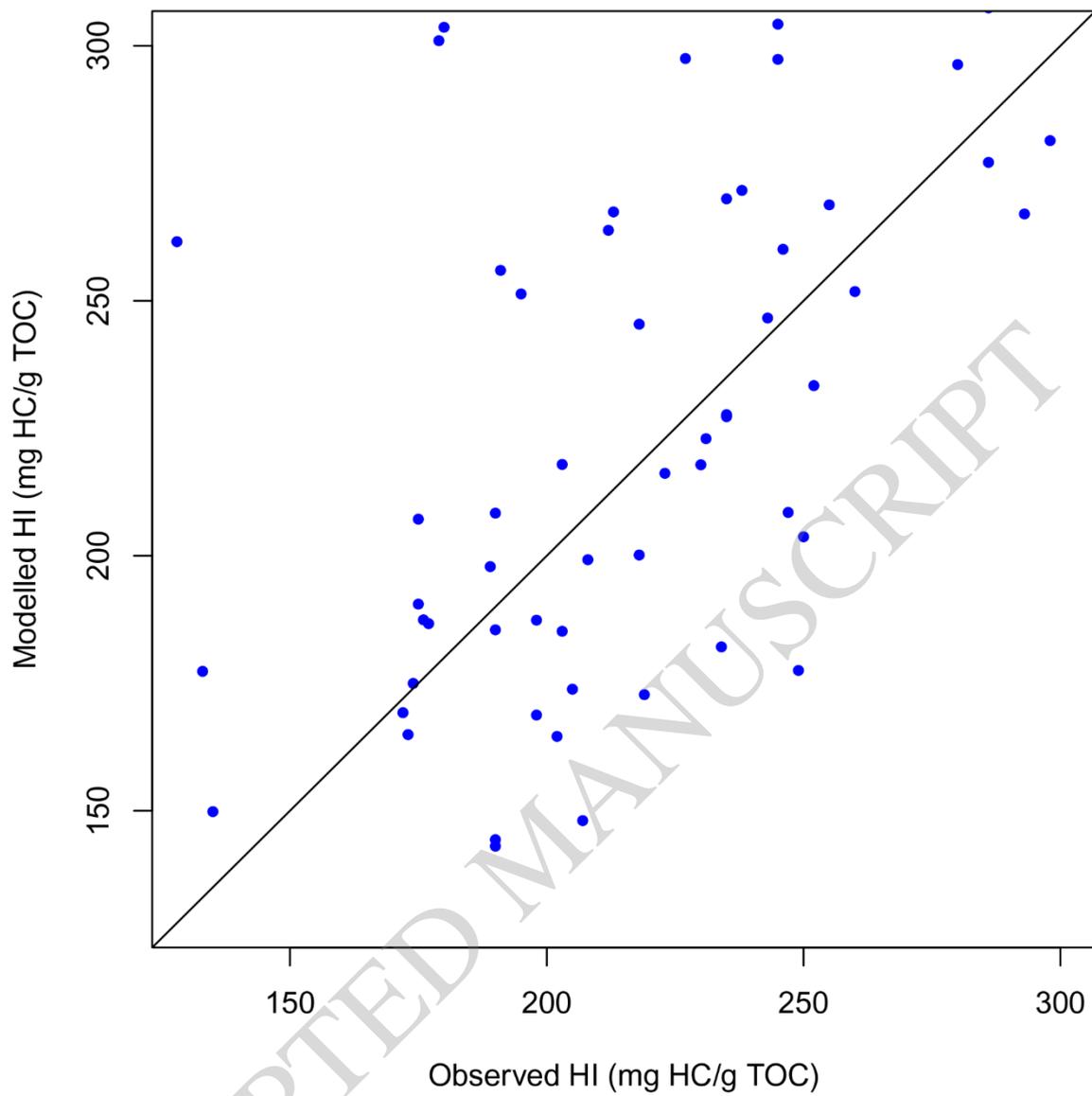


Figure 12

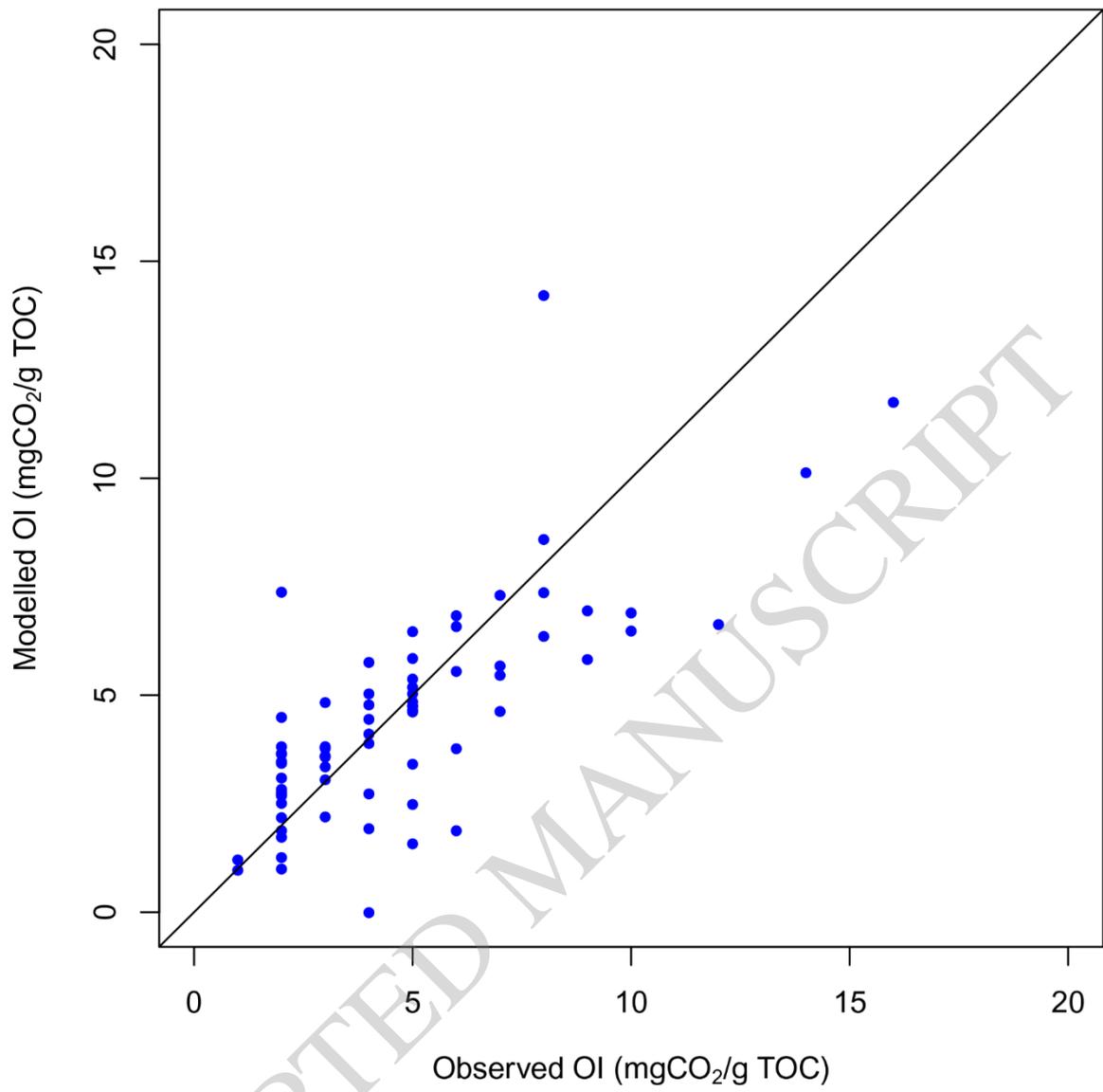


Figure 13

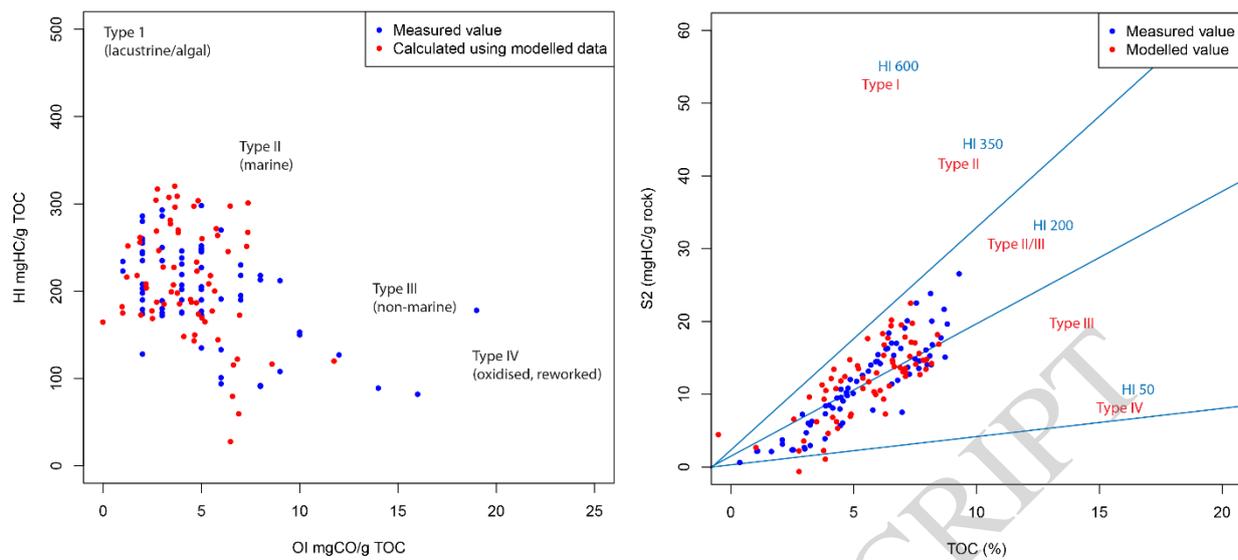


Figure 14