

25 **Abstract**

26 Ripples and small-scale bedforms are ubiquitous in shallow water environments under the combined action
27 of currents and waves. Small scale processes linked to their formation and migration are interconnected
28 with sediment transport at larger scales (e.g. tens of metres to kilometres), both resulting in and being
29 affected by large scale sediment transport and geomorphological evolution. The lower shoreface provides
30 a key link between coasts and continental shelves, but the contribution of ripples and small-scale bedforms
31 to sediment transport in this region has yet to be fully addressed. This work presents a study of sediment
32 dynamic processes on the lower shoreface in the presence of small-scale bedforms. Observations were
33 made during the winter of 2017 on the lower shoreface of Perranporth Beach, which is in the south west
34 of the UK and exposed to Atlantic waves. The analysis of morphological expressions and the variability
35 of ripples under waves, currents and wave-current conditions are assessed. Ripple morphology and
36 associated dynamics are analysed for their potential contribution to the exchange of sediment between the
37 lower and the upper shoreface. In the present study it was observed that even though ripples were evolving
38 depending on the wave-current forcing, little ripple migration was observed due to low wave skewness.
39 The implication is that ripple migration and bedload transport are only a small contribution to onshore
40 sediment transport under low to moderate energy conditions. However, during more energetic conditions,
41 ripples were washed out and the wave skewness increased, resulting in onshore sediment transport under
42 a sheet flow regime. This suggests that ripple formation and migration can have little impact on the cross-
43 shore supply of sediment from the lower shoreface to the upper shoreface and that more energetic wave
44 conditions are required to significantly transport sediment towards the beach.

45 **Keywords:** time-series, vortex ripples, sediment exchanges, ripple thresholds, lower shoreface

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50 **Highlights:**

- 51 • High-resolution observations on the seabed reveal 2D and 3D wave vortex ripples in a macrotidal
52 sandy lower shoreface, oriented almost parallel to the coastline.
- 53 • The morphological ripple transitions provide assessment of sediment transport regime thresholds.
- 54 • The hypothesis of cross-shore sediment supplied from the lower to the upper shoreface through
55 ripple migration is not supported in the present study.

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71 **1. Introduction**

72 Ripples are the most common and smallest bedform type on sandy seabeds, under low to intermediate flow
73 conditions, between the thresholds for grain movement and sheet flow (Dalrymple and Rhodes, 1995).
74 They are essential to bottom boundary layer processes through the interacting triad of hydrodynamics,
75 mobile seabed, and transport of sediment particles (Nielsen, 1981; Davies and Thorne, 2008). Bedload
76 sediment transport is partially attributed to ripples transport by the growth, morphological change,
77 dynamism and migration, while the uneven bed alters boundary layer dynamics and the resulting suspended
78 sediment dynamics and fluxes. Ripples also act as a key control on the bed shear stress by influencing the
79 partition between skin friction and form drag, effective bed roughness, and near-bed velocity structure
80 (Glenn and Grant, 1987; Grant and Madsen, 1979; Wiberg and Nelson, 1992; Li et al., 1996; Li and Amos,
81 1998, Hurther and Thorne, 2011).

82 Several ripple classification schemes exist. Ripples are morphologically classified based on their crest
83 planform into straight-crested (two-dimensional) ripples, or sinuous and linguoid (three-dimensional)
84 ripples (Allen 1968, Baas et al., 2016). Clifton and Dinger (1984) classified ripples as orbital, anorbital or
85 suborbital when ripple wavelength respectively scales with the wave orbital diameter, the sediment grain
86 size or both. Ripples are also classified based on the processes controlling sediment grain motion into
87 rolling-grain, vortex, and post-vortex ripples. Rolling-grain ripples form on flat beds under oscillatory
88 flows just above the threshold for grain motion. They typically remain small with low ripple steepness
89 (η/λ with η the ripple height and λ the ripple length) values less than 0.1 (Bagnold, 1946; Rousseaux,
90 2006) and are the precursor of vortex ripples. As flow forcing (i.e. velocities) increases, ripples become
91 steeper, and with steepness values in the range of 0.1-0.2 a lee side eddy may form, trapping sediment
92 eroded from the ripple surface, and forming vortex ripples (Bagnold, 1946; Traykovski et al., 1999; Thorne
93 et al., 2009, Hurther and Thorne 2011; Nelson et al., 2013). Vortex ripples are generally triangular, symmetric
94 and ripple steepness ratio is $\sim 0.1-0.25$. Their formation is related to waves when the ratio between the
95 orbital diameter (d_0) and the median sediment grain size (d_{50}) is less than 5000 and they reach equilibrium
96 rapidly. The presence of lee side eddies ejects sediment higher into the water column at flow reversal
97 (Bagnold, 1946; Clifton and Dinger, 1984, Thorne et al., 2003, Davies and Thorne, 2005), thus

98 contributing to increased sediment resuspension. As velocities increase further, orbital diameters become
99 larger and when $d_0/d_{50} > 5000$, ripple height decreases but ripple wavelength remains unchanged, resulting
100 in decreasing steepness (< 0.15) and so-called post-vortex ripples, and eventually further progression to
101 sheet flow (Clifton and Dingler, 1984). Similarly, under wave conditions, Thorne et al. (2009)
102 distinguished between 2D steep ripples ($\frac{\eta}{\lambda} \geq 0.12$), 2-3D transitional ripples ($0.08 \leq \frac{\eta}{\lambda} \leq 0.12$) and
103 dynamically plane bed ($\frac{\eta}{\lambda} \leq 0.08$), observing different boundary layer flow characteristics for each one
104 and roughly similar to the vortex, post-vortex and wash-out ripples respectively.

105 The transitional region between the breaker zone and the continental shelf, where changes on the beach
106 profile are no longer discernible but seabed agitation by waves is still significant, is commonly referred to
107 as the lower shoreface. The boundary between upper and lower shoreface is a very variable range and is
108 approximately located at 6-10 m water depth. We refer the interested reader to the recent reviews of
109 Anthony and Aagaard (2020) and Hamon-Kerivel et al. (2020) for detailed discussions of this zone. The
110 lower shoreface is an essential element of coastal geomorphology as it potentially is a vast source of
111 sediment for coastal landforms and accurate coastal sediment budgets would then need to consider
112 exchanges with the lower shoreface (e.g. Valiente et al., 2019b). However, high-resolution observational
113 studies of sediment transport, and in particular of bedload transport, are still rare (Anthony and Aagaard,
114 2020) due to a range of technical and logistical difficulties. Ripple migration, wash-out or sheet flow can
115 be mechanisms of net bedload transport (Traykovski et al., 1999; Camenen and Larson, 2006; van Rijn,
116 2007a). One implication is that bedload transport may be inferred from observations of ripples and their
117 migrations.

118 Cross-shore sediment exchange between the upper and the lower shoreface is mainly wave-driven, related
119 to wave asymmetry and wave induced currents (as undertow), although coastal ocean currents (due to tides,
120 winds, and other processes) can also transport sediment (Wright et al., 1991; Styles and Glenn, 2005;
121 Ruessink et al., 2011). In the absence of currents, wave asymmetry is the primary mechanism for ripple
122 migration. Asymmetries are required as linear, monochromatic waves will have equal velocities on each
123 half wave cycle and thus no net sediment is transported (i.e. bedform migration) (Traykovski et al., 1999).

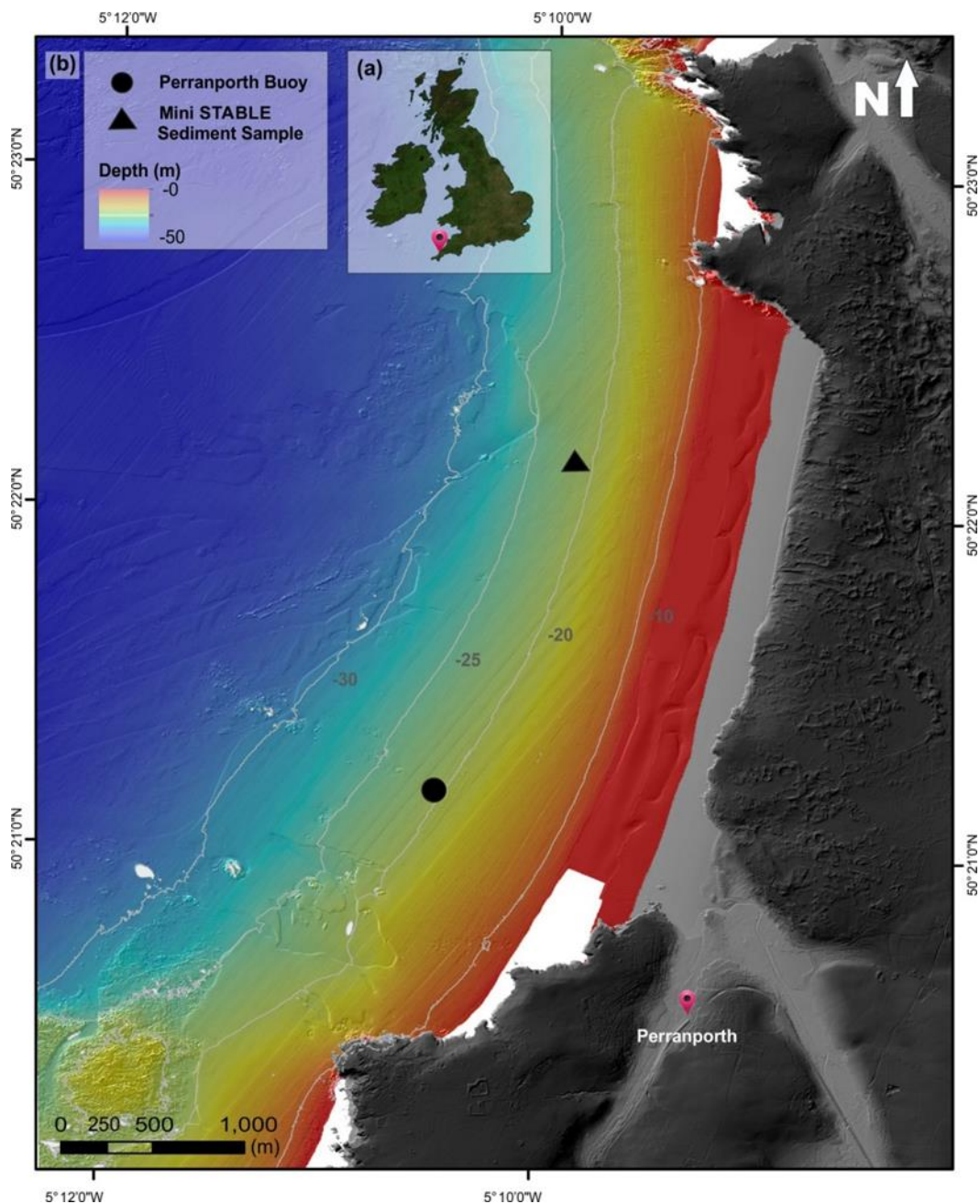
124 The general and theoretical understanding of bedform contribution to sediment transport is that the
125 bedform migration component is onshore and large compared with the suspended component in relatively
126 deep water and becomes progressively smaller with respect to the suspended transport towards the shore,
127 through the shoaling and surf zone (Miles and Thorpe, 2015). However, Crawford and Hay (2001)
128 observed offshore ripple migration during storm growth and onshore migration during storm decay, with
129 the bedform migration highly correlated with the near-bed wave orbital velocity skewness in both cross-
130 shore directions. Therefore, the relative contribution of bedform migration to sediment exchanges in the
131 lower shoreface remains an open question.

132 The current study presents high-resolution observations of near-bed hydrodynamics and ripples on a
133 macrotidal lower shoreface during winter (January-February) 2017 and evaluates the potential contribution
134 of these bedforms to sediment exchanges between the lower and upper shoreface. The study was conducted
135 in an embayed beach system at an intermediate point between the depth of closure based on the
136 morphological change and the depth of transport considered as the boundary of intense sediment transport
137 (upper-plane bed transition) (Valiente et al., 2019a). These observations provide new direct observations
138 of small-scale dynamics and resulting sediment fluxes and transport on the lower shoreface of such an
139 embayed system. These can provide new insights into the potential return of sediment from the lower
140 shoreface to the beach and the potential role of small-scale bedforms in onshore sediment transport outside
141 the breaking zone during calm and mild energy conditions. We introduce and describe the study site in
142 section 2 and the observational methods in section 3. Results are presented in section 4 and discussed in
143 section 5.

144 **2. Study area**

145 The study area is located offshore of Perranporth Beach (PB), in the southwest of England (Fig. 1a). The
146 coastline of the southwest of England typically consists of hard rock cliffs interspaced by embayed sandy
147 beaches. It is exposed to macro- to hyper-tidal ranges (mean spring tide range (MSR) from 4 to 12 m) and
148 medium- to high-energy waves from the Atlantic Ocean (Scott et al., 2016). Located on the northwest coast
149 of Cornwall, Perranporth Beach is a predominantly sandy beach with a semi-diurnal macro-tidal regime

150 (mean neap and spring tidal ranges of 3.1 m and 6.1 m) (Austin et al., 2010; Inch et al., 2017). The beach
151 is 3.5 km long and has an intertidal area ~200-300 m wide, which widens at the southern end to ~400 m
152 (Fig. 1 b). PB is backed by an eroding sand dune system with steep vegetated dunes reaching nearly a mile
153 inland, and by Devonian hard rock cliffs at the north and south ends of the beach (Fig. 1 b) (Poate et al.,
154 2014; Scott et al., 2016).



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156 Figure 1.- Study area. (a) Location of Perranporth study area and (b) shaded-relief of Composite Digital
157 Terrain Model (DTM) at 1 m resolution from LIDAR data available at <http://environment.data.gov.uk> and

158 bathymetry at 2 m resolution from UKHO INSPIRE Portal & Bathymetry DAC referenced to the Ordnance
159 Datum Newlyn (ODN). The bathymetric contours are displayed every 5 m. The Mini-STABLE rig location
160 is indicated with a black triangle and the offshore Buoy of Perranporth location is indicated with a black
161 circle. The detailed geo-referenced shaded-relief images had sun-illumination with an azimuth of 315° and
162 an elevation of 20° and two times vertical exaggeration of bathymetry dataset to highlight the
163 morphological details of the seabed.

164

165 PB is relatively straight, facing the west-northwest towards the Atlantic (shoreline 11° from North) so it is
166 fully exposed to the dominant westerly waves approach, receiving both Atlantic swell and locally generated
167 wind waves (Austin et al., 2010; Inch et al., 2017). The mean annual significant wave height (H_s) and mean
168 peak period (T_p), measured by the coastal Perranporth wave buoy during the period 2006- 2019, were 1.58
169 m and of 10.6 s, respectively, and significant wave height with an annual return period is 6.28 m (Channel
170 Coastal Observatory, 2020). High atmospheric pressure and northerly wind are also observed to cause
171 northerly waves, which are small but energetically significant (Poate et al., 2014). The wave climate has a
172 marked seasonality, with wave height and wave periods increasing during winter months. The monthly
173 averaged H_s and T_p values from the coastal Perranporth wave buoy (from the same 2006 to 2019 record)
174 range from 1.12 m and 9.0 s in June to 2.24 m and 12.4 s in January (Channel Coastal Observatory, 2020).
175 For the period of this study, January to March 2017, the monthly averaged H_s values were 1.57, 2.10 and
176 2.04 m and the corresponding T_p values 11.0, 12.7 and 12.2 s (Channel Coastal Observatory, 2020). The
177 shoreline location also displays high variability as a consequence of this weather seasonality (Davidson et
178 al., 2017). From November to February shoreline retreat occurs in response to a succession of erosive
179 storms, while beach recovery begins in late March, at slower rate ($\sim 1/4$) than the retreat, often persisting
180 until October (Davidson et al., 2017).

181 Following Wright and Short (1984), PB is a low-tide bar and rip with typically single or double subtidal
182 bars located around the seaward limit of the surf zone (Scott et al. 2016). Winter periods are often typified
183 by highly dissipative beach states (Austin et al., 2010; Poate et al., 2014; Scott et al., 2016; Davidson et

184 al., 2017). The low tide beach gradient is such that $\tan\beta = 0.012$, where β is the beach profile slope, and
185 the intertidal beach is relatively flat ($\tan\beta = 0.015-0.025$) with a concave-shaped profile. PB sediment is
186 composed of medium quartz sand ($d_{50} = 0.35$ mm) with a relatively high carbonate content (~50 %) which
187 suggests the influence of offshore sediments (Austin et al., 2010; Poate et al., 2014; Inch et al., 2017) and
188 supply of sediment from the lower shoreface to the beach. PB has a bar system with some rip channels
189 exposed during spring tide low water but is relatively homogenous alongshore and featureless on the upper
190 intertidal (Austin et al., 2010, 2013; Poate et al., 2014; Inch et al., 2017).

191 The beach system is dominated by cross-shore surf zone driven sediment transport and shore-normal waves
192 (Scott et al., 2016) and the embayment presents important rip circulation. At locations where rip circulation
193 is not active, longshore currents dominate (Austin et al., 2010). Offshore sediment transport has been
194 shown to be dominated by bed return flow currents aided by rip currents during shore-normal storms,
195 which advect sediments from the intertidal upper beach, depositing it in the subtidal sand bars (Scott et al.,
196 2016). Wave-ripples have been shown to develop on the upper shoreface of PB (between 1-6 m depth)
197 under low-energy conditions (orbital velocities < 0.65 m/s) and have been observed to migrate onshore,
198 with a maximum migration rate just onshore of the wave breakpoint (Miles et al., 2014). Onshore ripple
199 migration was shown to correlate with positive (onshore) wave skewness while its direction was dependent
200 on the surf position-controlled velocity skewness, orbital velocity, and mean flow (Miles et al., 2014).
201 Sediment transport rates associated with these bedforms were also onshore directed and increased
202 shoreward which contributed up to the 15% of the total sediment transport (Miles and Thorpe, 2015).

203 Exchange of sediment between the beach and the lower shoreface occurred at PB during the 2013-2014
204 winter, the stormiest on record for the Ireland-UK domain over the past 60-years (Masselink et al., 2016;
205 Scott et al., 2016). The sediment eroded from the beach was mainly deposited in large subtidal bar systems,
206 while some were transported offshore (Scott et al., 2016). After the period of storms, beach recovery
207 occurred by migration of bars and nearshore sediment transport onshore (Masselink et al., 2016; Scott et
208 al., 2016). However, part of the sediment eroded from the beach during storms was still retained in the
209 subtidal bar system and remained inactive on the lower shoreface (Scott et al., 2016). Multiannual sediment

210 budgets (Valiente et al.,2019b; 2020) highlighted the importance of lower shoreface sediment transport to
211 sediment budgets of the PB embayment, both in cross-shore and along-shore directions.

212 **3. Methodology**

213 Observations reported here were collected with an instrumented benthic tripod, mini-STABLE
214 (Sediment Transport And Boundary Layer Equipment) deployed at approximately 20 m depth
215 referenced to Ordnance Datum Newlyn (ODN) and about 1.5 km offshore of Perranporth Beach (PB) at
216 5.1646° W 50.3690° N (Fig. 1) from the 18 January to 12 March 2017.

217 **3.1. Study-site geomorphology**

218 The geomorphological setting of the study site was put in context by a Digital Elevation Model (DEM)
219 constructed by combining LIDAR data at 1 m of resolution and multi-beam bathymetry data at 2 m
220 resolution. The DEM was corrected and referenced to Ordnance Datum Newlyn (ODN) using the
221 Vertical Offshore Reference Frame model (VORF) facilitated by the United Kingdom Hydrographic
222 Office and it was imported into a Geographic Information System (ESRI's ArcGIS© desktop v. 10.3).
223 The bathymetry and the topography were displayed using a Universal Transverse Mercator (UTM 30N
224 zone) projection in World Geodetic System (WGS-84) geographic coordinate system and Datum (Fig.
225 1 b).

226 **3.2. Observational campaign**

227 **3.2.1. Bottom sediment samples**

228 Two sediment samples were recovered at the location of the Mini-STABLE deployment site using a Van
229 Veen Grab, during the tripod recovery on the 12 March 2017 (Fig. 1 b). The grabs were subsampled and
230 analysed at Marine Sciences Institute facilities of the Scientific Research Council (CSIC) in Barcelona
231 (Spain). They were first dried in an oven at 80°C for 24 hours. The sediment fraction finer than 2000 µm
232 was examined using an LA-950V2 laser scattering particle size distribution analyser. From the data the
233 grain size distribution and the median grain size, d_{50} , were derived.

234 **3.2.2. Winds and waves**

235 The wave field information was obtained from the Directional Waverider Buoy off Perranporth (Datawell;
236 Directional Waverider MkIII) available online via the Channel Coastal Observatory

237 (www.channelcoast.org). The buoy was located at a water depth of ~20 m referenced to Ordnance Datum
238 Newlyn (Fig. 1 b). Since both the wave buoy and the benthic tripod are deployed in similar depths and
239 close location, it is reasonable to expect that the wave buoy spectra are representative of the benthic tripod
240 location (see location in Fig. 1 b).

241 3.2.3. Mini-STABLE tripod instrumentation

242 While the deployed benthic tripod hosted a large number of acoustic and optical instruments, we will focus
243 on data collected by a three-dimensional Acoustic Ripple Profiler 3D-ARP, ([http://www.marine-](http://www.marine-electronics.co.uk/)
244 [electronics.co.uk/](http://www.marine-electronics.co.uk/)) (Bell and Thorne, 2007; Marine Electronics, 2009; Thorne et al., 2013; Moate et al.,
245 2016; Kramer and Winter, 2016; Thorne et al., 2018), and an Acoustic Doppler Velocimetry (ADV, Nortek
246 Vector).

247 The 3D-ARP is a dual axis, mechanically rotated, pencil beam scanning sonar operating at 1.1 MHz used
248 to determine how the seabed micro-morphology (< 1 m length scale) evolves with time. Regular scans of
249 a circular area of the seabed allow the relationship between the bed morphology and the changing
250 hydrodynamic conditions to be examined (Thorne and Hanes, 2002; Lichtman et al 2018). The 3D-ARP
251 was clamped to the underside of the frame at a nominal height of 1.2 m above the bottom of the frame. A
252 full bathymetry scan was recorded every 2 hours. With the sensor at ~1.2 metres above the bed, the
253 circular area covered by the scans was ~4 m in diameter. The vertical resolution was 2 mm directly below
254 the transducer (nadir) (Thorne et al., 2018). The bed surface acoustic backscattered data points were
255 gridded into a horizontal resolution of $\Delta x = \Delta y = 5$ mm resulting in a digital elevation map with consistent
256 grid cells.

257 The ADV was configured into the XYZ coordinate system. A rotation of the axis to earth coordinates was
258 applied using the mean heading angle recorded by the ADV's compass during the first 400 bursts (period
259 of the study). Velocity components were then referenced to the shoreline (11° with respect to the north).
260 The ADV was configured to a sampling rate of 16 Hz and nominal velocity range of 1 m/s. The ADV
261 sampled 12.5 minute bursts every hour. The ADV transducer was located at 1.19 m above the bottom of
262 the frame (see Table I). ADV measurements were verified, tested and processed by applying a quality data
263 control procedure and a despiking method based on Goring and Nikora (2002). A concurrently deployed

264 Acoustic Doppler Current Profiler (Nortek Signature 1000 AD2CP) is used here to provide the water depth
 265 time series at 4 Hz continuously during the whole period of the Mini-STABLE frame deployment (see
 266 Table I).

267 Table 1.- Details of the relevant instruments deployed on the Mini-STABLE frame and of the Perranporth
 268 WaveRider buoy. The period analysed was from the 18 January to the 3 February 2017.

Instrument	Measurement used	Sampling interval	Location
ADV	Velocity, intensity and direction	1 h	1.19 mab (Mini-STABLE)
3D-ARP	Seabed micro-bathymetry	2 h	1.2 mab (Mini-STABLE)
AD2CP	Water depth	0.25 s	1.82 mab (Mini-STABLE)
Directional Waverider Buoy	H_s, T_z, T_p	30 min	20 m of water depth (ODN)

269

270 3.3. Data Analyses

271 3.3.1. Seabed detection

272 The 3D-ARP can be used to record the range at which a threshold backscatter level is encountered for each
 273 head position. The data were processed using the bed recognition algorithm suggested by (Bell and Thorne
 274 (1997a) which extracts the precise position of the bed echo and obtains the coordinates (x,y,z) of the sea
 275 bed for each scan. The method compares the signal with an expected pattern and selects the best match
 276 between both (Bell and Thorne, 1997b, Thorne et al 2018). A program was designed to keep running orders
 277 applied to detect anomalous points and replace them with estimates based on values from the adjacent
 278 space and time bins. In addition, with increasing range from the transducer, the backscattered echo level
 279 declines due to signal spherical spreading and scattering in the water column. To reduce noise, the echo
 280 signals were smoothed by a five-point window moving average at the bed profile stage after the bed
 281 detection. Finally, the seabed topographic variation at the study site was calculated by averaging the z-

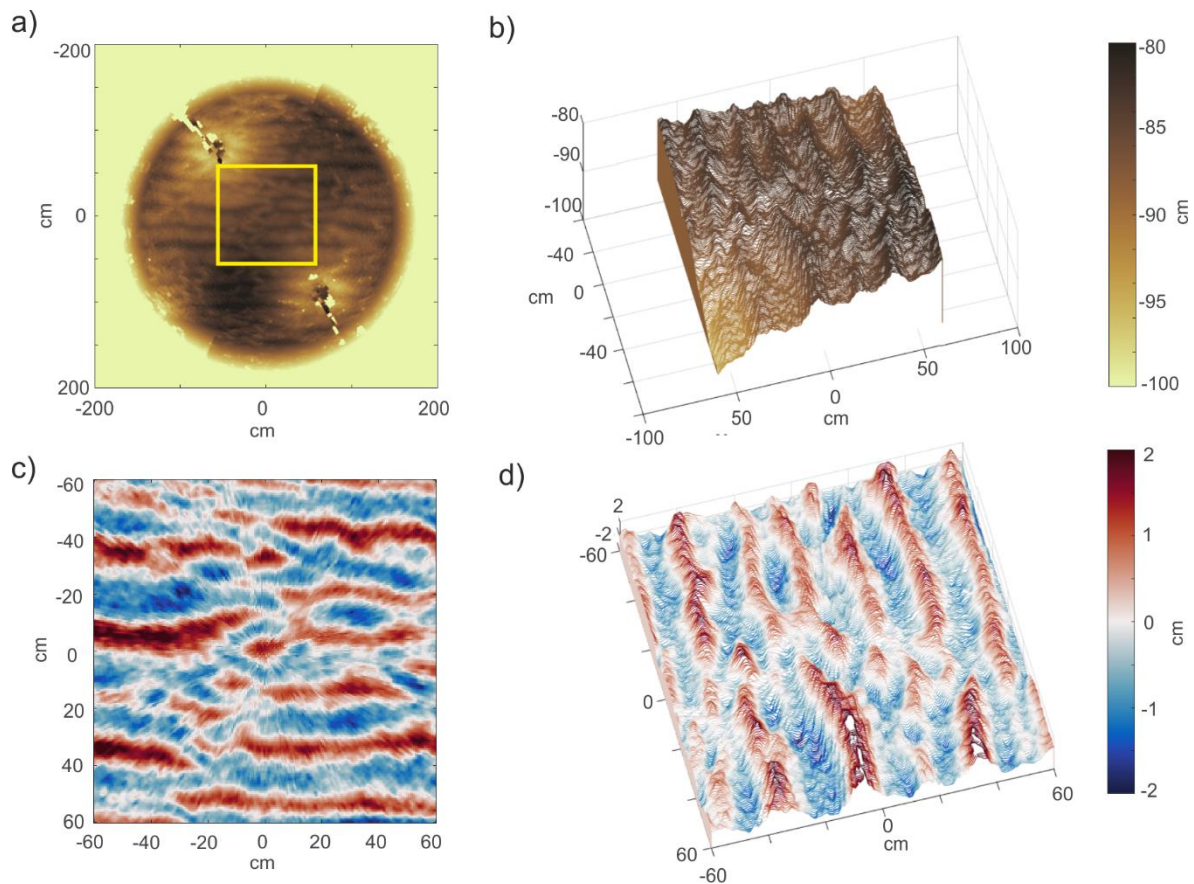
282 coordinate of each scan from the 3D-ARP data during the whole period studied (including the periods with
283 the scour formation around the frame legs).

284 *Ripple observations*

285 Ripple geometry and dimensions are here described as the orientation of the crestlines, and the cross-
286 sectional ripple height and wavelength (η and λ , respectively). To determine the spatial variability and the
287 geometric properties of ripples, a method that determined the locations of the crests and troughs in a
288 measured bed elevation profile was needed and then, the geometric properties of individual ripples were
289 determined. The ripple dimensions were estimated from the small-scale gridded bathymetry dataset from
290 the 3D-ARP as follow: (i) the central area of the scans was cropped considering only a square of 0.6 x 0.6
291 m (the points directly below the transducer or nadir angle are where scans provide the best resolution) and
292 also to remove or minimise scour (Fig. 2 a and b). (ii) The global trend was subtracted from the bathymetry
293 in order to focus only on the fluctuations of the seabed elevations around a horizontal reference level
294 ignoring other morphologies not related to the ripples (Fig. 2 c and d). A fifth order polynomial based on
295 least squares was removed profile by profile (swath by swath) at each scan. The resulting residual
296 bathymetry is a zero-mean bathymetry. (iii) The crest orientation of the ripples was considered by selecting
297 the direction which ripples crests were closer (the smallest wavelength). Therefore, a first approximation
298 for ripple wavelengths was estimated by using the transect method which evaluates for the local extrema
299 (crest or trough) between zero down-crossings and the measured distance between them. (iv) The scans
300 were rotated perpendicular to the ripple crests-lines. Ripple crests were detected for each profile or transect.
301 (v) The ripple height was estimated statistically using the standard deviation of the elevation multiplied by
302 a factor equal to $2\sqrt{2}$ (Traykovski et al., 1999, Thorne et al 2009). (vi) Ripple wavelength was estimated
303 again by using the same transect method but now considering transects perpendicular to the ripple crests.
304 A smooth window was applied to each transect and wavelengths larger than 40 cm were removed as these
305 were considered larger seabed undulations or irregularities and not related to ripples. Finally, the mean
306 wavelengths for each transect and for each scan, were calculated.

307 Ripple migration was analysed by using 2D cross-correlation method, which accounts for tidal rotation
308 and wave forcing at different angles (Lichtman et al., 2018). The migration distances were calculated from

309 spatial difference between successive (2-hourly) 3D-ARP bed scans, determined by 2D cross-correlation.
 310 The distance of migration between two scans divided by the 120 minutes gave the migration rate. The area
 311 used for the 2D cross-correlation was the same square of 0.6 x 0.6 m as used for ripple morphology analysis
 312 (Fig. 2).



313
 314 Figure 2.- Example of the pre-processing applied automatically to each scan before ripple dimensions
 315 analysis using cmocean colormaps (Thyng et al., 2016): (a) complete scan measured with the 3D-ARP on
 316 the 31st of January at 0 h, the yellow square at the centre is the cropped area of 0.6 x 0.6 m. The two black
 317 lines are two of the tripod legs (some scour around them is visible); (b) three-dimensional view of the
 318 cropped area; (c) zero-mean residual bathymetry after subtract the global trend; (d) three-dimensional view
 319 of c). Note that a) and b) scale are distance from 3D-ARP to seabed and c) and d) scale are seabed
 320 topography variations.

321

323 Over the time the frame was deployed, the benthic tripod did induce scour around the legs (Fig. 2). Since
324 the alteration by the frame of the near-bottom hydrodynamics as well as the seabed morphology can modify
325 the processes related to ripple formation and dynamism, the ripple analysis was focused only on the early
326 part of the record prior to significant scouring to retain the integrity of the data analysis. The period
327 analysed was from the 18 January to the 3 February 2017, when scour was either not present or was
328 considered to have limited impact on the hydrodynamics and the processes related to ripple formation and
329 evolution.

330 3.3.2. Hydrodynamic data analysis

331 The parameters of orbital velocity, wave skewness, seabed roughness, bottom shear stress, Shields
332 parameter and other relationships derived from them, such as ripple predictions and sediment transport
333 rates were estimated from hydrodynamic measurements. Since the methods utilized here are approaches
334 frequently used and well described in the literature, only a short description is presented in this section and
335 the original works are referred for a detailed description of each method.

336 *Wave parameters*

337 Wave spectrum parameters were directly obtained from the directional wave buoy data (Table I) and
338 provided half-hourly time series for the significant wave height (H_s), the zero up-crossing wave period
339 (T_z) defined spectrally, the peak period (T_p); and the peak wave direction (direction of the waves with the
340 highest energy) during the study period. The near-bottom wave orbital velocity, U_w , was then calculated
341 following small-amplitude linear wave theory considering regular waves (Soulsby, 2006; Wiberg and
342 Sherwood, 2008). This approach is sufficient when the wave height is small compared to the waves
343 wavelength and the water depth and the water is shallow with respect to the wavelength (Wiberg and
344 Sherwood, 2008; Xiong et al., 2018) as was the case at our study site. The Newton-Raphson iteration
345 method was used to determine the wave number k from the dispersion equation following the Fenton and
346 McKee (1990) algorithm.

347 *Wave skewness*

348 The normalized velocity skewness was calculated from ADV measurements. It is defined as (Elgar, 1987):

349
$$U_{sk} = \frac{\overline{(u(z,t) - \bar{u})^3}}{u_{rms}(z)^3} \quad (\text{eq. 1})$$

350 Where $u(z, t)$ is the instantaneous cross-shore horizontal velocity, the overbar denotes time-averaging over
 351 a 12.5 minute burst of the ADV data (sampling at 16 Hz), and z is at the depth of measurements.

352
$$u_{rms}(z) = \overline{(u(z, t) - \bar{u})^2}^{1/2} \quad (\text{eq. 2})$$

353 *Seabed roughness*

354 The total roughness length (z_0) is the sum of the roughness due to grain size (z_{0s}), the form-drag roughness
 355 (z_{0f}) and the sediment transport component of roughness (z_{0t}) (Soulsby 1997):

356
$$z_{0s} = 2.5d_{50}/30 = d_{50}/12 \quad (\text{eq. 3})$$

357
$$z_{0f} = a_r \frac{\eta^2}{\lambda} \quad (\text{eq. 4})$$

358
$$z_{0tc} = \frac{5\tau_{0s}}{30g(\rho_s - \rho)} \quad \text{for currents} \quad (\text{eq. 5})$$

359
$$z_{0tw} = 0.00533 \cdot U_w^{2.25} \quad \text{for waves} \quad (\text{eq. 6})$$

360 Where τ_{0s} is the skin-friction shear stress according to Soulsby (1997) (see eq. 10 below), and a_r is an
 361 empirical coefficient $a_r = 0.533$ according to Raudkivi (1988), η and λ are the ripple height and
 362 wavelength, respectively; U_w is the wave orbital velocity; d_{50} is the median sediment grain size; g is the
 363 acceleration due to gravity; ρ is the water density; and ρ_s is the sediment density.

364 Because ripples were arranged parallel to the near-bottom currents at our study site (see results), the form-
 365 drag roughness effect was considered negligible for the currents parameters analysis resulting in a total
 366 roughness length as follows:

367
$$z_{0c} = z_{0s} + z_{0tc} \quad \text{for currents} \quad (\text{eq. 7})$$

368
$$z_{0w} = z_{0s} + z_{0f} + z_{0tw} \quad \text{for waves} \quad (\text{eq. 8})$$

369 *Bed shear stress*

370 Bed shear stresses are calculated using the model for combined waves and currents proposed by Soulsby
 371 and Clarke (2005), and modified by Malarkey and Davies (2012). This model includes a representation of
 372 non-linear wave-current interactions and is applicable to hydrodynamically rough beds under the
 373 approximation of $z_0 \ll BL \ll h$ where z_0 is the bed roughness length, h is the water depth, and BL is the
 374 wave boundary layer thickness calculated as $BL = \max(a_r \sqrt{0.5 f_w} a_w, z_{0w})$. The wave orbital amplitude,
 375 a_w , and wave-only friction factor, f_w , are given by the formulations: $a_w = \frac{U_w T}{2\pi}$ and $f_w =$
 376 $1.39(a_w/z_{0w})^{-0.52}$. The mean bed shear stress due to combined flow (τ_m), including wave-current
 377 interaction, over hydrodynamic rough beds (sand and gravel beds) is:

$$378 \quad \tau_m = \rho u_{*m}^2 \quad (\text{eq. 9})$$

379 where, $u_{*m} = \sqrt{\left[\frac{b u_{*e}}{2a}\right]^2 + \frac{\bar{U} u_{*e}}{a} - \frac{b u_{*e}}{2a}}$; \bar{U} is the depth averaged current speed, calculated from the burst-
 380 averaged ADV-measured velocities following Malarkey and Davies (2012); $a = \kappa^{-1} \log(\delta/z_0)$, δ is the
 381 bottom boundary layer thickness, $b = \kappa^{-1} \log(h/e\delta)$, $\kappa = 0.4$ the von Kármán constant and $u_{*e} = \left(\frac{\tau_e}{\rho}\right)^{1/2}$
 382 is the effective friction velocity where $\tau_e = \sqrt{\tau_c^2 + 2\tau_c\tau_w|\cos\phi| + \tau_w^2}$. Where ϕ is the angle between
 383 the current direction and the wave propagation direction, and τ_c and τ_w are the bed shear stress considering
 384 currents alone and waves alone, respectively, estimated as:

$$385 \quad \tau_c = \rho C_D \bar{U}^2 \quad (\text{eq. 10})$$

386 where C_D is the drag coefficient defined as:

$$387 \quad C_D = \left[\frac{0.40}{\ln\left(\frac{h}{z_{0c}}\right) - 1} \right]^2 \quad (\text{eq. 11})$$

388 For a sinusoidal wave of period T , and orbital velocity U_w , the amplitude of the bed shear stress is given
 389 by:

$$390 \quad \tau_w = \frac{1}{2} \rho f_w U_w^2 \quad (\text{eq. 12})$$

391 The maximum bed shear stress due to combined flow, including wave-current interaction, (Soulsby, 1997)
 392 is:

$$393 \quad \tau_{max} = [\tau_m^2(1 + \varepsilon_1 + \varepsilon_2) + \tau_p^2 + 2\tau_m\tau_p\sqrt{1 + \varepsilon_1 + \varepsilon_2}|\cos\phi|]^{1/2} \quad (\text{eq. 13})$$

394 Where $\tau_p = \rho u_* e u_{*w}$, see (Soulsby 1983), $\varepsilon_1 = \tau_c \tau_w |\cos\phi| / (\tau_c + \tau_w)^2$ and $\varepsilon_2 = \tau_w^2 / 4(\tau_c + \tau_w)^2$ and
 395 $\tau_w = \rho u_{*w}^2$.

396 *Shields parameter and its thresholds*

397 The Shields parameter, θ , is a non-dimensional bed-shear stress variable used to identify or determine when
 398 seabed states typically reach the initiation of sediment motion in a fluid flow. The Shields parameter also
 399 gives an approximation of the limits of seabed morpho-states in relation to the incident hydrodynamic
 400 conditions, in our case for a constant sediment size throughout the study period and evaluated during waves
 401 and currents separately (Soulsby et al., 2012).

$$402 \quad \theta = \frac{\tau}{g(\rho_s - \rho)d_{50}} \quad (\text{eq. 14})$$

403 Where the Shields parameter due to waves (θ_w) and currents (θ_c) are calculated using the equations of τ_w
 404 and τ_c defined in eq. 12 and eq.10, respectively.

405 Shields parameters provide criteria for the definition of thresholds of initiation of movement, wash out and
 406 sheet flow regime. The critical Shields parameter for initiation of motion, θ_{cr} is given as (Soulsby 1997)

$$407 \quad \theta_{cr} = \frac{\tau_{cr}}{g(\rho_s - \rho)d_{50}} = \frac{0.3}{(1 + 1.2D^*)} + 0.055[1 - \exp(-0.02D^*)] \quad (\text{eq. 15})$$

408 where τ_{cr} is the critical threshold for the bed shear stress; $D^* = d_{50}[(s - 1)g/v^2]^{1/3}$ is the dimensionless
 409 sediment grain size, with $D^* = 6.64$ at our Perranporth lower shoreface site; $v = 10^{-6}$ (m²/s) is the
 410 kinematic viscosity coefficient; and $g = 9.81$ (m/s²) is the gravity acceleration.

411 According to Soulsby et al. (2012), the limit of wash-out (θ_{wo}) and skin-friction sheet flow threshold (θ_{sf})
 412 can be inferred using a criterion given in terms of skin friction Shields parameters as a function of D^* :

$$413 \quad \theta_{wo} = 1.66D_*^{-1.3} \quad \text{when } D^* > 1.58 \quad (\text{eq. 16})$$

414 $\theta_{sf} = 2.26D_*^{-1.3}$ when $D^* > 1.58$ (eq. 17)

415 *Ripple prediction*

416 Ripple characteristics are predicted following the equilibrium dimensions of Soulsby et al. (2012), which
 417 are based on extensive field and laboratory data sets. This simpler approach is preferred to the non-
 418 equilibrium procedure because in the field it is difficult to know the history of development or even a
 419 starting point of ripples, so equilibrium can be useful with the proviso that relict ripples can be retained for
 420 certain conditions. Following this method, different morpho-states are expected to develop under different
 421 hydrodynamic forcing regime, and the method estimates wavelength, λ , and ripple height, η , (from the
 422 slope, η/λ) as a function of the hydrodynamic forcing regime and the dominance of waves or currents. The
 423 hydrodynamic forcing regimes are here determined by thresholds on the Shields parameter. Ripples only
 424 start to evolve above the threshold of initiation of sediment motion (θ_{cr}), which is evaluated as a function
 425 of sediment size. Above this limit, ripples grow towards morphologies in equilibrium with the
 426 hydrodynamic forcing (Soulsby et al., 2012). For increasing hydrodynamic forcing, ripple dimensions
 427 reduce above a wash-out threshold ($\theta > \theta_{wo}$), and disappear above a sheet flow threshold ($\theta > \theta_{sf}$) since
 428 θ_{sf} borders the limit of ripple existence (Carmenen, 2009)

429 Dominance of waves or currents is assessed from the values of θ_w and θ_c . When waves dominate ($\theta_w >$
 430 θ_c), estimated ripple dimensions increase (decrease) with increasing (decreasing) energy due to their
 431 functional relationship with the wave orbital velocity. When $\theta_w > \theta_{cr}$ ripples heights, η , and wavelengths,
 432 λ , are defined as (Soulsby et al., 2012):

433 $\frac{\lambda}{a_w} = [1 + 1.87 \times 10^{-3} \Delta (1 - \exp\{-(2 \times 10^{-4} \Delta)^{1.5}\})]^{-1}$ (eq. 18)

434 $\frac{\eta}{\lambda} = 0.15 [1 - \exp\{-(5000/\Delta)^{3.5}\}]$ (eq. 19)

435 where $\Delta = a_w/d_{50}$

436 Otherwise, λ and η are taken as the pre-existing values (relict ripples).

437 When currents dominate ($\theta_c > \theta_w$) and $\theta_c > \theta_{cr}$ current ripples can develop. For a given grain size, ripples
 438 of constant height and wavelength develop if the current speed is maintained for a sufficient period of time,
 439 then:

$$440 \quad \eta_{max} = d_{50} 202 D^{*-0.554} \quad \text{for } 1.2 < D^* < 16 \quad (\text{eq. 20})$$

$$441 \quad \lambda_{max} = d_{50} (500 + 1881 D^{*-1.5}) \quad \text{for } 1.2 < D^* < 16 \quad (\text{eq. 21})$$

442 Soulsby et al. (2012) defined a reduction in ripple height between θ_{wo} and θ_{sf} assuming that the wavelength
 443 is unaffected by wash-out and is equivalent to the maximum value indicated above. Then, the equilibrium
 444 ripple height including wash-out is:

$$445 \quad \begin{cases} \eta_{eq} = \text{pre-existing value (relict or frozen ripples)} & 0 < \theta_c < \theta_{cr} \\ \eta_{eq} = \eta_{max} & \theta_{cr} < \theta_c < \theta_{wo} \\ \eta_{eq} = \eta_{max} \left(\frac{\theta_{sf} - \theta_c}{\theta_{sf} - \theta_{wo}} \right) & \theta_{wo} < \theta_c < \theta_{sf} \\ \eta_{eq} = 0 & \theta_c > \theta_{sf} \end{cases} \quad (\text{eq. 22})$$

446 One implication of the method as described above is that the reduction of ripple dimensions for large
 447 hydrodynamic forcing is only ensured for current-dominated conditions. Under wave dominance, no
 448 reduction is applied to ripple dimensions: ripple wash-out and disappearance under wave sheet flow are
 449 therefore not considered (Camenen, 2009; Soulsby et al., 2012). Finally, for waves and currents acting
 450 together, this ripple prediction model assumes that only the dominant ripple forcing of the two is present
 451 at any time (Li and Amos, 1998).

452 *Sediment transport rate*

453 A semi-quantitative approach to calculate the sediment transport intensity under varying hydrodynamic
 454 conditions is applied using rate estimates of van Rijn (2007a, 2007b). This estimation for bedload and
 455 suspended sediment load transport uses hydrodynamic conditions (depth, current velocity, wave height,
 456 wave period, etc.) as well as sediment size (d_{50}). This method represents a strong simplification of sediment
 457 transport processes, although it has shown reasonable veracity for steady and oscillatory flow outside the
 458 surf zone with medium-coarse sands (> 200 microns).

459 To calculate the net sediment transport rates (over a wave period), the sum of the bedload (q_b) and
460 suspended load (q_s) transport rates is given by:

$$461 \quad q_{total} = q_b + q_s \quad (\text{eq. 23})$$

462 For coastal flow (steady flow with or without waves) the bedload transport according to van Rijn (2007a)
463 is defined as:

$$464 \quad q_b = \alpha_b \rho_s U h (d_{50}/h)^{1.2} M_e^{1.5} \quad (\text{eq. 24})$$

465 Where q_b is the bedload transport rate (in kg/s/m); $\alpha_b = 0.015$; $M_e = (U_e - U_{cr}) / [(s - 1)g d_{50}]^{0.5}$ is the
466 non-dimensional mobility parameter; $U_e = U + \gamma U_w$ the effective velocity (in m/s) with $\gamma = 0.4$ for
467 irregular waves; U is the depth averaged flow velocity (m/s); U_w is the orbital velocity (m/s); $U_{cr} =$
468 $\beta u_{cr,c} + (1 - \beta) u_{cr,w}$ is the critical velocity (m/s) with $\beta = U / (U + U_w)$; $u_{cr,c}$ is the critical velocity
469 (m/s) for currents based on Shields; $u_{cr,w}$ is the critical velocity (m/s) for waves, which for the case when
470 $0.00005 < d_{50} < 0.0005$ m, are:

$$471 \quad u_{cr,c} = 0.19 d_{50}^{0.1} \log(12h/3d_{90}) \quad (\text{eq. 25})$$

$$472 \quad u_{cr,w} = 0.24 [(s - 1)g]^{0.66} d_{50}^{0.33} T_p^{0.33} \quad (\text{eq. 26})$$

473 d_{90} is the particle size such that 90% are less or equal (m), and $s = \rho_s / \rho_w$ is the relative density.

474 The suspended load transport rate is defined as transport of sediment by the mean current while including
475 the effects of wave stirring on the suspended load (van Rijn, 2007b):

$$476 \quad q_s = 0.012 \rho_s U d_{50} M_e^{2.4} D^{*-0.6} \quad (\text{eq. 27})$$

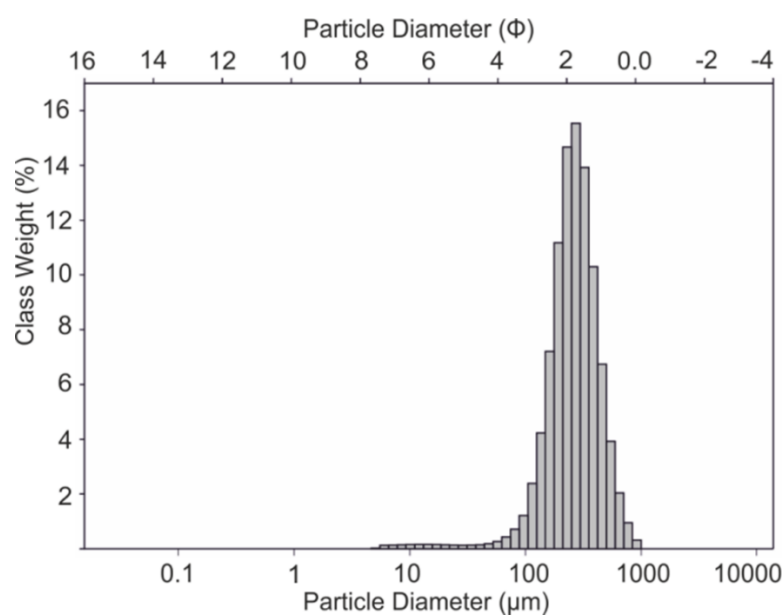
477 **4. Results**

478 **4.1. Shoreface morphology and sediment characteristics**

479 Perranporth shoreface displays a cross-shore profile with slopes of $\tan\beta \sim 0.004$ and concave-shaped until
480 ~ 30 m depth (ODN) (Fig. 1 b). Over this area, the seafloor morphology is uniform and homogeneous,

481 limited by rocky outcrops at the north and south ends of the embayment following the emerged cliffs of
482 Devonian rocks (Fig. 1 b). Just at the south of the northern outcrops, at approximately 25 m depth, six
483 subaqueous dunes lie with ~0.5 m high and ~110 m of wavelength, they display asymmetries with the lee
484 side facing to the south, suggesting a dominant southward residual current. At approximately 30 m depth
485 contour (ODN) an abrupt edge 1 m high appears breaking the seafloor homogeneity. It is arranged mainly
486 parallel to the shoreline except at the southern area where the edge appears shallower without apparently
487 any alignment. Offshore of this edge the seafloor changes to more complex morphologies exhibiting tidal
488 channels aligned northeast-southwest, 0.3-0.5 m deep (maximum ~1 m) and widths ranging from tens to
489 hundreds of meters. The head of these channels are located near the rocky outcrops at the north area of the
490 continental shelf, becoming wider towards the southwest. Thus, the study site is in the transitional zone
491 between the tidal morphologies (less than 30 m depth) and the nearshore bars (greater than 6 m depth) on
492 the upper shoreface.

493 The grain size analyses of the surficial sediment showed a moderately sorted medium sand composition
494 with d_{50} of 266 μm at the Mini-STABLE frame location. 97% of the sediment was sand with 7.6% coarse
495 sand ($2\text{ mm} > d_{50} > 0.5\text{ mm}$), 48.1% medium sand ($0.5 > d_{50} > 0.25\text{ mm}$), 36.5% fine sand ($0.25 > d_{50} >$
496 0.125 mm), and 4.8% very fine sand ($0.125 > d_{50} > 0.063\text{ mm}$), and the remaining 3% was silt ($d_{50} < 0.63$
497 mm) fraction (Fig. 3).



498

499 Figure 3.- Grain size distribution of the bottom sediment sample recovered at the Mini-STABLE frame
500 location deployment using the Van Veen Grab during the tripod recovery.

501

502 **4.2. Time series**

503 4.2.1. Wave conditions

504 The wave time series shows the root mean square wave height, $H_{rms}(H_{rms} = H_s/\sqrt{2})$ ranging from 0.5
505 m to 2 m and mean wave periods (T_z) from 5 to 10 s (Fig. 4 a). The highest waves ($H_{rms} \sim 3$ m) took place
506 on 3 February when T_z was between 8-10 s. Wave directions were unidirectional coming from the west-
507 northwest with a mean wave direction of $\sim 280^\circ$ (data not shown).

508 The near-bottom wave orbital velocities (U_w) ranged between 0.1 and 0.4 m/s displaying peaks following
509 a similar form to the wave heights time series (Fig. 4b). The highest waves occurred at the end of the period
510 on the 3 February, with orbital velocities increasing to 0.6 m/s.

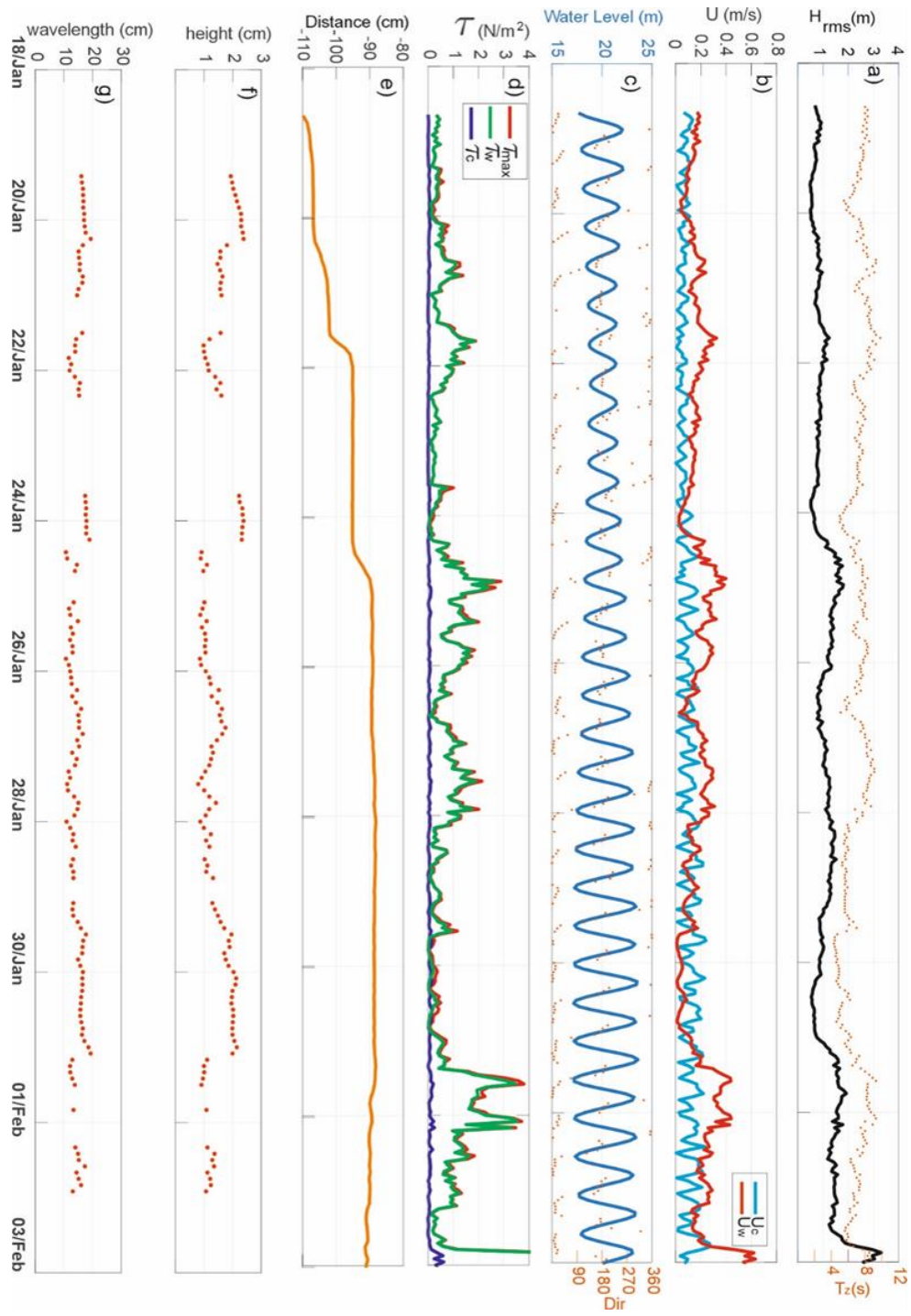
511 4.2.2. Water level and currents

512 Water levels display dominant semi-diurnal tides with strong spring-neap modulation (Fig. 4 c): minimum
513 neap tidal amplitudes were approximately 2.5 m and the maximum spring amplitudes reached
514 approximately 6.3 m. The direction of the near-bed tidal current indicate flood flowing towards north-
515 northeast and ebb towards south (Fig. 4 c). The gradual shift in direction suggests a rotational behaviour
516 and the presence of a near-bed tidal ellipse. The near-bed current magnitude peaked at approximately 0.2
517 m/s during ebbs and floods (Fig. 4b) with slight flood dominance, indicating a probable northward near-
518 bed residual current at this location.

519 4.2.3. Near-bottom shear stress

520 The hydrodynamic forcing acting on the seabed during the study period is characterized by the near-bed
521 shear stress. The stress is presented as the maximum combined wave and current shear stress (τ_{max}), shear
522 stress considering only waves input (τ_w) and shear stress from currents alone (τ_c) (Fig. 4 d). The
523 maximum contributor to the combined wave and currents shear stress was clearly waves, only being

524 reached and seldom exceeded by the current stress during short periods when the orbital velocities were
 525 weak < 0.1 m/s ($H_{rms} \sim 0.5$ m). The combined wave-current shear stress ranged from less than 0.1 to
 526 greater than 3 Nm^{-2} over the studied period, with several peaks of $\tau_{max} > 2 \text{ Nm}^{-2}$ and even $\tau_{max} \sim 4 \text{ Nm}^{-2}$
 527 ² (Fig. 4 d).



529 Figure 4.- Time series from the 18 January to 3 February 2017 of: (a) root mean square wave height (H_{rms})
530 (line) and mean period (T_z) (dots); (b) orbital velocity (red line) and current speed from ADV (blue line);
531 (c) water level depth (line) and direction of near-bed tidal current (dots); (d) maximum combined wave
532 and currents shear stress (red line); wave-alone shear stress (green line), and current-alone mean shear
533 stress (blue line); (e) depth-averaged bed level displaying the relative distance between the 3D-ARP
534 transducer and the seabed level; (f) observed ripple height; (g) observed ripple wavelength.

535

536 4.2.4. Mean bed level variations

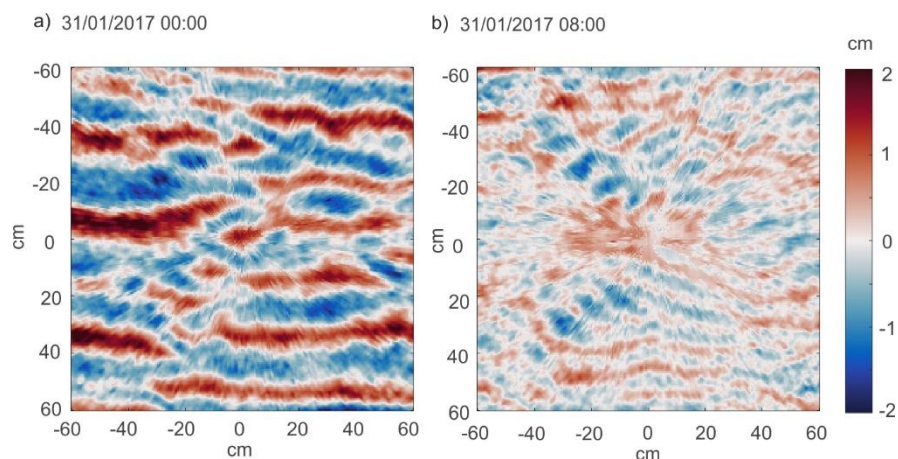
537 The topographic variations of the bed level from the 18 January to 3 February show that the frame
538 experienced four discrete events of rapid settling during the first week of deployment (before
539 approximately 25 January), as evidenced by the steep gradient in the distance between the 3D-ARP
540 transducer and the seabed (Fig. 4e).

541 The first event occurred on the 18 January 2017 with 2.6 cm of sinking and was probably due to initial
542 settling of the frame following deployment. Subsequent settling periods appear to be associated with
543 increased wave activity and occurred 20, 21 and 24 January with settling of 4.2 cm, 7 cm and 5.9 cm
544 respectively. Each of these periods lasted around 16 h and seemed to be a consequence of the frame
545 accommodation and sinking because of its own weight. The association with increased wave activity is
546 likely to result from increased wave-induced pore pressure and resulting liquefaction of the seabed. The
547 overall settling was ~20 cm (Fig. 4 e). After the 25 January, the bed level remained more or less constant
548 without significant changes apart from a small increase of the seabed-to-transducer distance occurring
549 between 31 January and 3 February.

550 4.2.5. Ripple observations and dynamics

551 The presence of ripples on the Perranporth lower shoreface seabed from the 18 January to 3 February 2017
552 was the most common situation, occurring ~64% of the time (Fig. 4 f, g). Ripple crestlines were aligned
553 in a north-south direction, nearly parallel to the coastline (which is ~11° to North). Most ripple crestlines
554 were oriented almost perpendicular to the wave direction approach (west-east) and parallel to the dominant

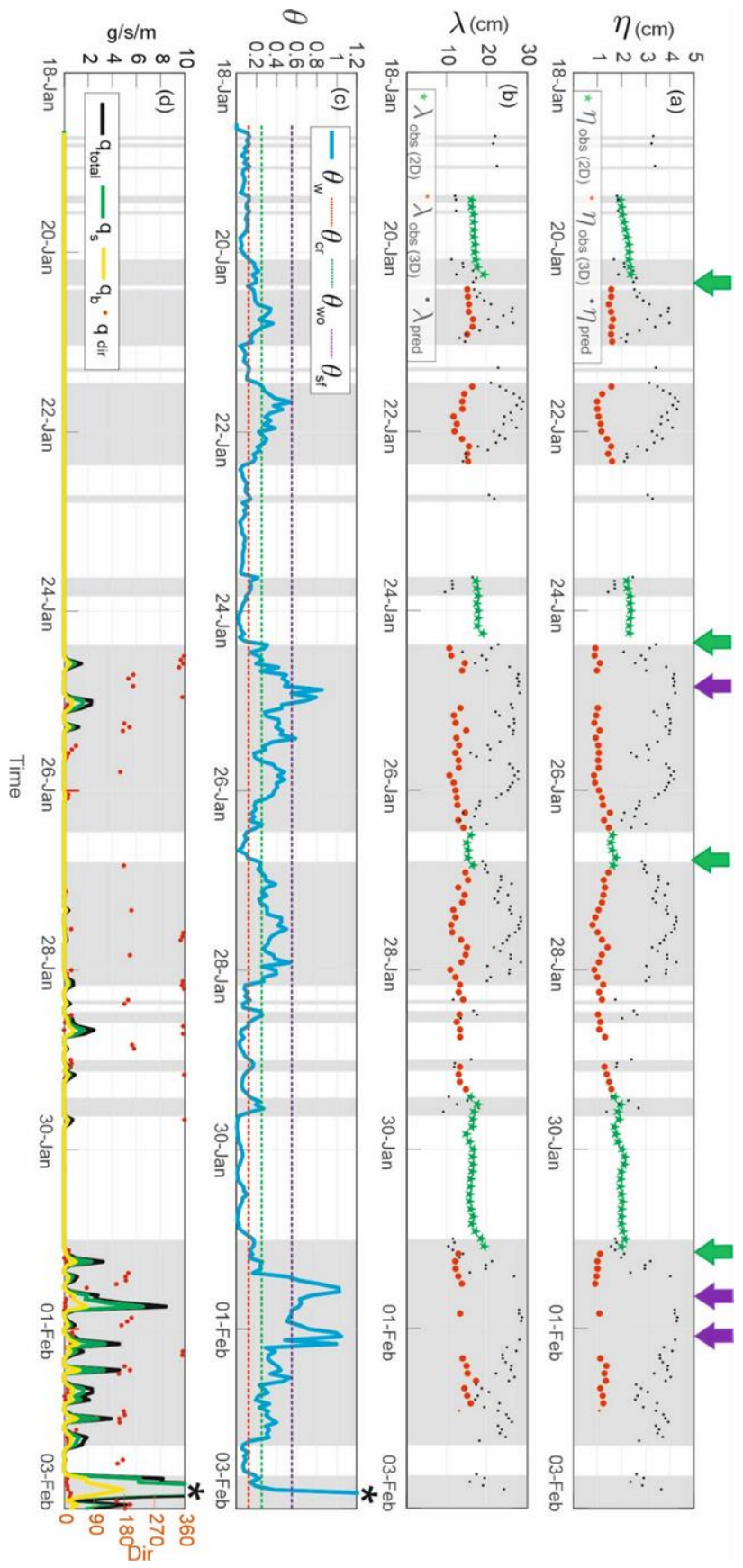
555 current direction (north-south). Thus, ripple occurrence was mainly related to wave action. The orientation
 556 of the ripples also has important implications for the bed roughness that is effectively felt by the flow: in
 557 particular, the ripple-induced roughness (eq. 4) associated with the 2D wave ripples observed here is
 558 unlikely to affect the roughness felt by tidal currents, which primarily flows along ripple crests. Ripple
 559 morphology ranged from 2D to 3D, smaller ripples with sinusoidal or curved crests (Fig. 5 a and b,
 560 respectively). During periods when ripples were not observed (gaps in the data in Figure 4 f, g), the scans
 561 displayed a flat bed and on occasions seabed morphologies with a zig-zag pattern. These patterns, show
 562 complex seabed morphologies and ripple coalescence (Rousseaux 2006). Because of their uncertain
 563 interpretation, they were discarded from the present analysis. The development of 2D and 3D ripples
 564 occurred during ~19% and ~45% of the time studied, respectively (Fig. 6 a, b). In general, 2D ripples
 565 displayed heights up to 2 cm and wavelengths ~15-20 cm, while 3D ripples displayed slightly lower heights
 566 ~1-1.5 cm and wavelengths ~10-15 cm (Fig. 6 a, b).



567
 568 Figure 5.- Examples of 3D-ARP images for using cmocean colormaps (Thyng et al., 2016): (a) 2D ripple
 569 morphologies with bigger dimensions and rectilinear crests (31/01/2017 0h) and (b) 3D ripple
 570 morphologies with smaller dimensions and sinusoidal or curvilinear crests (31/01/2017 8h).

571
 572 In general, 2D ripples occurred under low-energy wave conditions ($H_{rms} < 1$ m and $T_z < 8$ s) (orbital
 573 velocities < 0.2 m/s) and tidal currents lower than 0.2 m/s. Under increasingly energetic conditions, 2D
 574 ripples slightly increased their dimensions until a maximum size (~2.4 cm height and ~19.5 cm wavelength,

575 see for example around 20 January). Beyond these conditions, ripple size dropped significantly
576 corresponding with a transition from 2D to 3D ripple, which is interpreted as ripple degradation when
577 ripple wash-out conditions were reached (Fig. 6, 20 - 21 January, 24 January). Observations also showed
578 gradation from 2D to 3D ripples to flat bottom with increasing bottom shear stress (Fig. 6, 24-25 January,
579 31 January).



581 Figure 6.- Time series of (a) ripple height and (b) ripple wavelength showing observed 3D (red dots) and
582 2D (green stars) ripples and predictions (black dots) from Soulsby et al (2012), eq. (19 and 18); (c) Shield
583 parameter due to waves (θ_w , eq (10)) (Shield caused by currents is very low and is not represented), and
584 threshold of motion (θ_{cr} , eq (12)), wash-out (θ_{wo} , eq (13)), and sheet flow (θ_{sf} , eq (14)); and (d) total
585 sediment transport (eq. (23)), suspended load sediment transport (eq. (27)), bed load sediment transport
586 (eq. (24)) and resultant sediment transport direction with respect to north where 0 and 360 degrees are
587 northward direction (red dots and right vertical axis). (* data out of range). Shaded areas indicate periods
588 when Shields parameter exceeded the threshold of sediment motion. Ripple observations in unshaded areas
589 can correspond to relict ripples whereas plane bed in shaded areas is interpreted as sheet flow conditions.
590 Arrows on top of the figure highlights transitions between 2D and 3D ripples (green) and between 3D
591 ripples and plane bed (sheet flow conditions) (purple).

592
593 The outcome from the migration analysis was somewhat inconclusive. In addition, no ripple migration was
594 visually observed from the scans. No measurable ripple migration was detected during the study period.
595 Based on observations of the seabed morphology, scans from the 3D-ARP indicated the 2D ripples were
596 stationary while 3D ripples sometimes exhibited some dynamism by changing the crests curvature between
597 two successive scans which indicated readjustment of these bedforms rather than migration in a specific
598 direction.

599 4.2.6 Observations and estimated Shields parameters thresholds

600 In order to estimate thresholds of initiation of sediment motion, the Shields parameter due to waves and
601 currents was calculated using the methodology previously described (Fig. 6 c). As expected, the time
602 evolution of the wave Shields parameter is similar to that of the wave shear stress and the orbital velocities
603 and values reach in excess of 0.8. The Shields parameter for current only conditions was almost negligible
604 remaining below the sediment motion threshold during the whole period and is therefore not plotted.

605 In addition, thresholds for the wave Shields parameters were established based on the concurrent
606 observations of ripple development, degradation and disappearance from the time series of the 3D-ARP

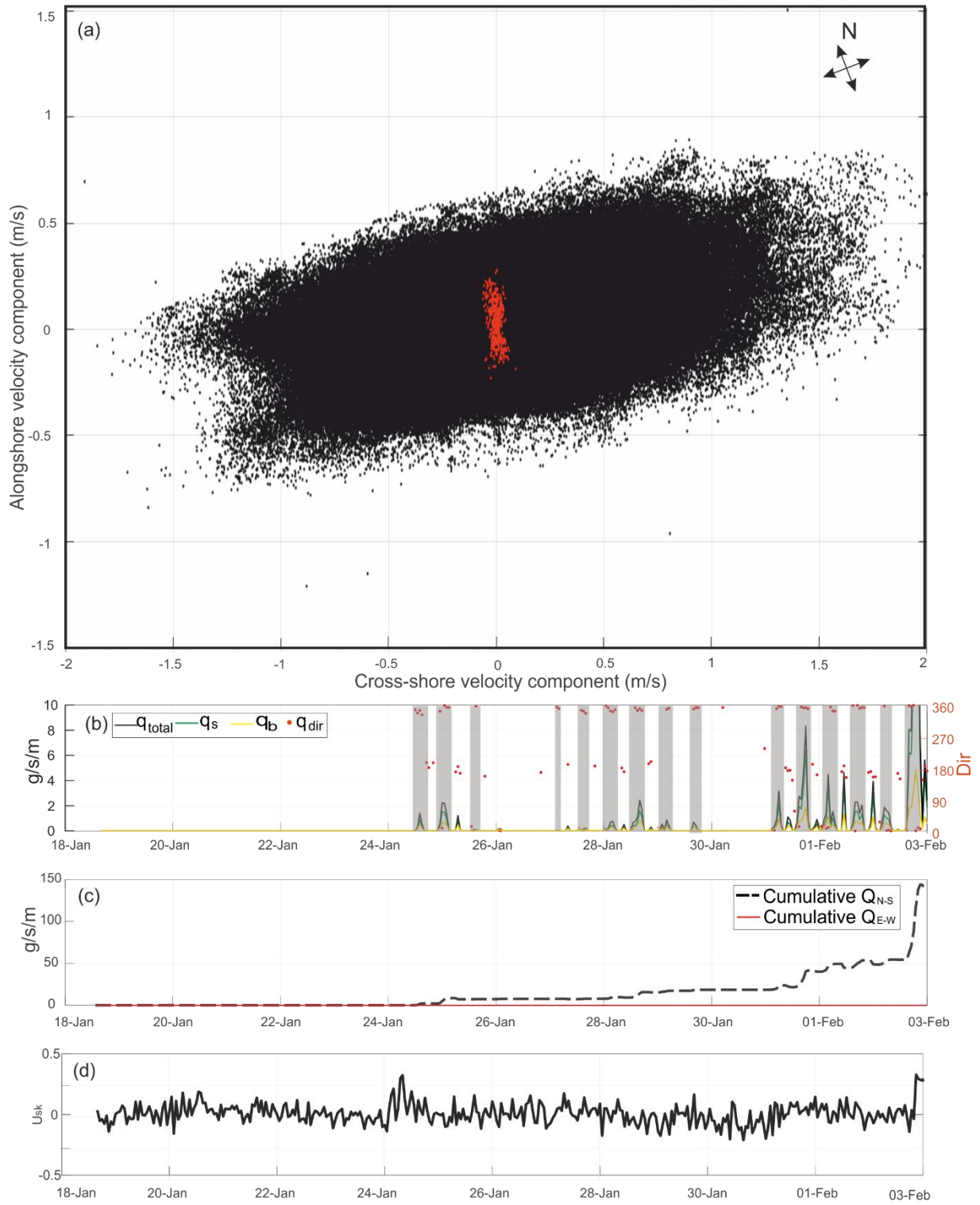
607 data. These values were taken as the threshold values for starting ripple formation ($\theta_{cr} = 0.12$) (vortex
608 ripple), ripple wash-out ($\theta_{wo} = 0.25$) (transition from 2D to 3D ripples) and sheet flow ($\theta_{sf} = 0.55$)
609 regimes based on our time series observations (see Fig. 6). These values roughly correspond with peak
610 values suggested by Thorne et al. (2009) for bedform characteristics under different boundary layer flow
611 conditions (< 0.2 , $0.2-0.7$ and >0.7 for 2D ripples, transition ripples and dynamically plane bed
612 respectively). They are also larger than the values obtained using equations 15-17. Such discrepancies
613 between Shields thresholds and observations of ripple development and disappearance have also been
614 previously reported (e.g. Bagnold, 1946; Hanes et al., 2001; Camenen, 2009). These differences can be a
615 consequence of the strong simplifications involved in calculations (e.g. d_{50} as the representative sediment
616 size, the lack of a uniform sediment grain size, and the complexities of bottom boundary layer dynamics,
617 etc.) (Traykovski et al., 1999). This also impacts the prediction of ripple dimensions since predictors (e.g.
618 equations 18 to 22 here) rely on these threshold values. We therefore used our empirical thresholds instead
619 of the values from equations 15-17 in the predictions of ripple dimensions (black points in Fig. 6 a and b).

620 The thresholds extracted from our time series suggest that hydrodynamic forcing remained below the
621 threshold of sediment motion at our study site on the Perranporth lower shoreface during ~38% the study
622 period. The rest of the time (62%) hydrodynamic (wave) forcing was strong enough to exceed the threshold
623 of grain motion. Hydrodynamic conditions were strong enough to be between washout and sheet flow
624 ($\theta_{wo} < \theta_w < \theta_{sf}$) for 30% of the reported time series and exceeded sheet flow threshold for 11% of the
625 reported time series.

626 4.2.7 Near-bottom sediment transport

627 During our study period, near-bed hydrodynamics at our study site on the Perranporth lower shoreface
628 were dominated by waves coming from the west with a mean approach angle of $\sim 280^\circ$ N and north-south
629 currents with slightly rotational component of north-northeast south-southwest corresponding to the flood
630 and ebb tidal flows respectively (Figs. 6 d; 7 a). The sediment transport rates (bedload, suspended load,
631 and total load) estimated from near-bed hydrodynamic observations following equations 23-27 primarily
632 occurred in several peaks typically for relatively energetic conditions during the deployment period (i.e.

633 24, 25, 26, 27, 28, 29 31 January and 1, 2 February) (Fig. 7 b). The estimated suspended load transport
634 widely dominated over the bed load transport (77.2% and 22.8%, respectively). These results are broadly
635 consistent with the lack of observed ripple migration corresponding to small bedload transport since peaks
636 typically coincide with conditions energetic enough to induce ripple washout or sheet flow. The resulting
637 sediment transport component in east-west direction is almost zero (Fig. 7 b) because of the oscillatory
638 velocity component (in black in Fig. 7 a). The peaks of the sediment transport correspond to north-south
639 (360° - 180° , respectively) velocities (Fig. 7 b), with a dominant northern transport (Fig. 7 c).



641 Figure 7.- (a) Dispersion diagram of cross-shore velocity components (x axes) and alongshore
642 velocity component (y axes) considering the east (onshore) and north components positive values.
643 Black dots correspond to intra-burst data and red dots the mean-burst data; (b) total sediment
644 transport (blue line), suspended load sediment transport (green line), bed load sediment transport
645 (yellow line) and resultant sediment transport direction (red dots and right vertical axis). Shaded
646 areas show sediment transport episodes towards the north. The maximum peak on February 3rd (>20
647 g/s/m) is not represented; (c) cumulative sediment transport towards the north-south direction (black
648 line) and towards the east-west direction (red line) considering the north and east directions positive;
649 (d) cross-shore wave velocity skewness.

650

651 **5. Discussion**

652 **5.1. Ripple development, transitions and regimes**

653 In general, the presence of ripples and their morphological changes depend on the flow conditions and the
654 ability of the ripple to adapt to the new hydrodynamic conditions until they reach the equilibrium (Nelson
655 and Voulgaris, 2014). Transitions between 2D, 3D ripples and plane bed conditions in energetically
656 changing conditions as described here for the Perranporth lower shoreface, have also been observed at
657 other sites (Hanes et al., 2001; Nelson and Voulgaris, 2014). But, with energetically variable flow
658 conditions, ripple equilibrium is unlikely to be reached and active changes in ripple height, wavelength,
659 and orientation can be expected. In fact, ripples in flow conditions close to the inception of motion, should
660 be only stable in conditions close to or below the critical value, in this case maintaining relict bedforms
661 (Bagnold, 1946; Camenen, 2009).

662 Because of the orientation of the ripple crestline with respect to wave propagation and tidal current
663 directions, the ripples we observed on the Perranporth lower shoreface were clearly wave ripples. The
664 absence of current-dominated ripples in our observations is the consequence of the relative low-intensity
665 of the recorded tidal currents during the study period. Two ripple categories were recognized as vortex
666 ripples: 2D ripples with rectilinear crestlines, height, $\eta > 2$ cm and length, $\lambda = 15-20$ cm, and 3D ripples with

667 more sinusoidal crestlines, $\eta=1-1.5$ cm and $\lambda=10-15$ cm. Indeed, the displayed crestline morphology, the
668 steepness value (> 0.1), and the d_0/d_{50} relation (< 5000) are characteristic of vortex ripples (Clifton and
669 Dingler, 1984). Even though the 3D ripples have lower steepness and higher d_0/d_{50} ratio than the 2D ripples,
670 their characteristics still correspond to that of vortex ripples (Clifton and Dingler, 1984).

671 Observed trends of small scale seabed morphology can be linked to the strength of wave forcing during
672 the study period. For low energy conditions, typically such that the threshold of motion is not reached, the
673 seabed was stable and static. Ripples, when present, displayed close to constant dimensions, suggesting
674 relict ripples (Fig. 6, e.g. 19, 23 -24, 26, 28, 29 -30 January). Interestingly, while ripple development would
675 be expected about the 51% of the study period when $\theta_{cr} < \theta_w < \theta_{sf}$, ripples were observed during 64%
676 of the study period further supporting the presence of relict ripples for significant periods of time. For
677 increasing wave forcing, stationary vortex ripples were generated with changes in size and dimensionality
678 depending on the wave forcing. The transition from larger 2D vortex ripple to the smaller 3D vortex ripples
679 generally was abrupt (see green arrows in Fig. 6) and interpreted as ripple degradation under increasing
680 energetic conditions (exceedance of wash-out threshold), while the reverse transition (small 3D to large
681 2D) vortex ripples was progressive and typically occurred with decreasing wave energy (Fig. 6, e.g. 25-27
682 January,). For the highest energy conditions, ripples disappeared when the Shields parameter surpass the
683 sheet flow threshold (purple arrows in Fig. 6). Under these intense conditions, scour started to form on the
684 seabed around the legs of the deployed instrument frame, consistent with previous results showing scour
685 increasing with hydrodynamic forcing (Bolaños et al., 2011).

686 **5.2. Comparison with ripple predictor**

687 Since waves largely dominated near-bed hydrodynamics and the current Shields parameter was
688 consistently below the threshold of motion during the study period (Fig. 6 c), we only applied the
689 formulation for wave-generated ripples, using Shields parameter thresholds determined empirically from
690 our time series. The presence of ripples versus flat bed conditions are well reproduced with erroneous
691 predictions of 2D vortex ripples instead of flat bed only occurring twice on the 18 and 22 January (Fig. 6
692 a and b). Such an outcome is likely to be a consequence of using empirically determined thresholds rather

693 than validation of the general predictor and highlights the importance of accurate estimates of these
694 thresholds.

695 Predictions of 2D ripple dimensions are satisfactory under low energy conditions, but ripples dimensions
696 are poorly predicted under several other conditions. Under low energy conditions ($\theta < \theta_{cr}$) a flat bed is
697 predicted from the model, but ripples were observed and interpreted as relict ripples during approximately
698 10% of the time during the reported study period on the Perranporth lower shoreface (Fig. 6, e.g. 24
699 January). From the comparison with the observed ripples, predictions for low energy conditions appear to
700 be particularly challenging because our observations do not consistently report constant ripple dimensions
701 (relict ripples) for each period below the threshold of motion (see unshaded sections in Fig. 6).

702 Predictions of 3D ripple dimensions systematically and significantly overestimate observations. The
703 predictor also results in larger variability in both height and wavelength than the observations, with η
704 between 2 and 4.5 cm and λ between 15 and 30 cm (Fig. 6 a and b). The explanation for these large
705 discrepancies is relatively simple in that the predictor used here (Soulsby et al., 2012) does not account for
706 the reduction of ripple dimensions above the washout threshold for wave-generated ripples. Similar results
707 were obtained in other studies under wash-out conditions (Hanes et al., 2001; Camenen, 2009; Soulsby et
708 al., 2012) and highlight an important deficiency of such a wave ripple predictor.

709 **5.3. Contribution to embayment sediment pathways and budgets**

710 The estimated dominant near-bottom sediment transport direction was close to alongshore and almost
711 parallel to the ripple crestlines, switching between north and south following the ebbs and floods tidal
712 flows (red dots in Figs. 7 a, b) but with a clear net transport northward owing to the flood dominance of
713 the near-bed tidal currents at this location (Fig. 7 c). This pattern is likely the result of sediment
714 resuspension by wave stirring and subsequent transport due to tidal currents, which is characteristic in
715 environments dominated by combined waves and currents (Traykovski et al., 1999; van Rijn, 2007a,
716 2007b). Sediment transport mostly occurring along ripple crestlines also explains the observed changes in
717 the morphology of the 3D ripples (mostly ripple crest realignment) until higher energetic regimes
718 completely washed-out to result in sheet flow conditions. These seabed modifications and ripple dynamics

719 occurred relatively rapidly according to 3D-ARP observations with ripple reorientation between 2
720 consecutive scans two hours apart.

721 An important consequence of the orientation of the coast in this specific location is that the predicted net
722 northward sediment flux results in both longshore and (smaller) offshore components. While this is
723 consistent with measured alongshore and offshore burst averaged currents, further observational evidence
724 of sediment fluxes would be necessary for complete confirmation. The inferred alongshore transport under
725 mild to moderate wave conditions at one location is consistent with sediment fluxes modelled over the
726 entire embayment (Valiente et al., 2020). The dominance of the longshore residual transport over cross-
727 shore transport fluxes also agrees with numerical modelling (Valiente et al., 2020) and sediment budgets
728 (Valiente et al., 2019b) for the Perranporth embayment. Circulation patterns and resulting sediment fluxes
729 are not spatially uniform and vary depending on wave / storm forcing because of the interaction between
730 currents, waves, and bay geomorphology (McCarroll et al., 2018; Valiente et al., 2020). The estimated
731 residual sediment flux appears to intensify towards the end of the study period, which also appears to be
732 consistent with the numerical results of Valiente et al. (2020).

733 In absence of currents crossing the crestlines, wave-dominated ripples would mainly migrate in response
734 to the asymmetry in the near-bed wave orbital velocities that typically occurs in shallow waters
735 (Traykovski et al., 1999; Crawford and Hay, 2001; Soulsby and Whitehouse, 2005; Miles et al., 2014).
736 This wave asymmetry mechanism is not included in the sediment transport equations used here. Instead,
737 we estimated the cross-shore wave velocity skewness based on the velocity measurements in order to assess
738 the importance of this mechanism. Results indicate close to symmetric near-bed wave velocities with
739 values of velocity skewness being generally near zero and always below 0.35), which is consistent with
740 the lack of wave ripple migration observed and suggest that wave-asymmetry-induced cross-shore
741 sediment transport is not important for most of the study period (Fig. 7 d).

742 On the Perranporth upper shoreface, onshore ripple migration was observed because of velocity skewness
743 (> 0.2 m/s) during mild waves with wave orbital velocities around 0.25-0.50 m/s (Miles et al., 2014). Under
744 similar wave orbital velocities, the skewness on the lower shoreface is lower and not large enough to cause

745 similar onshore bedform migration. Normalized velocity skewness values beyond 0.5 were correlated with
746 ripple migration periods under non-rip current conditions at Perranporth shoreface (Thorpe et al., 2014).
747 Even though such onshore bedform migration may be seen as a process helping beach recovery, this would
748 not provide a pathway from the lower shoreface to the beach under mild wave conditions, but only from
749 the upper shoreface to the beach. However, post storm recovery does not only occur during calm to mild
750 wave conditions, high-energy wave events also appear to be essential for beach recovery after storm
751 erosion (Scott et al., 2016). In our observations, a wave skewness around 0.2 m/s was only reached for
752 wave orbital velocities of 0.6 m/s, when ripples were washed-out. The implication is that potential onshore
753 wave-asymmetry-induced transport is unlikely to be related to ripple dynamics and migration, and likely
754 to primarily occur under sheet flow conditions, thus requiring high-energy wave events. There is no
755 evidence of wave-induced offshore sediment transport during our study period, but our deployment did not
756 include extreme wave conditions (maximum wave height (~3 m) was well below the wave height with
757 annual return period (~6 m)). Our observations do suggest a small offshore residual-current-related
758 transport of sediment due to the orientation of tidal currents with respect to the shoreline, which is likely
759 to be affected by wave-current interactions. It is, however, unclear how these separate wave and current
760 contributions to cross-shore sediment transport balance over longer time scales (year to decade). Wave-
761 asymmetry-generated onshore sediment fluxes under sheet flow conditions are not directly observed here
762 and only inferred from near-bed hydrodynamics and the sediment bed state; observational confirmation of
763 this flux would require not only new field deployments but likely new instrumentation and/or analysis
764 techniques to accurately measure near-bed sheet flow sediment flux.

765 In summary, our in situ observations support the following understanding for sediment fluxes over the
766 lower shoreface. Under calm to mild wave conditions, wave-generated onshore flux is negligible, and
767 current supported fluxes result in significant residual alongshore and a small offshore residual. Under high
768 energy event, wave-generated onshore flux may be possible under sheet flow conditions, and current
769 supported fluxes are intensified both alongshore and offshore. As mentioned previously, the alongshore
770 components are consistent with results from numerical modelling (Valiente et al., 2020) and sediment
771 budgets (Valiente et al., 2019b). Our observations do not support the hypothesis that the lower shoreface

772 acts as a source of sediment to the upper shoreface (and the beach) via cross-shore fluxes. Nevertheless,
773 the cross-shore components during high energetic events could contribute to the pathways to the upper
774 shoreface inferred by Valiente et al. (2019b).

775 These results provide clear evidence of small-scale seabed and sediment dynamics on the lower shoreface
776 beyond the depth of closure, which is a typically under-sampled region (Anthony and Aagaard, 2020). For
777 the specific embayment and lower shoreface considered, these observations support the existence of an
778 active zone between the depth of closure and the depth of transport as proposed by Valiente et al (2019a),
779 which would be dominated by sediment resuspended by wave stirring and subsequently transported by
780 tidal currents. Such observations are not unexpected given that similar small-scale seabed and sediment
781 dynamics have also been observed in deeper waters of the Celtic Sea (Thompson et al., 2017; Thompson
782 et al., 2019).

783 **6. Conclusions**

784 Observed ripples on the lower shoreface of Perranporth were divided into 2D ripples (rectilinear crests)
785 and 3D ripples (more sinusoidal or curved crests), and both 2D and 3D ripples can be considered as vortex
786 ripples. The small-scale seabed morphology was linked to changing hydrodynamics during the study
787 period and ripple occurrence and evolution was primarily related to wave action. Under low-energy regime,
788 such that the threshold of motion is not reached, the seabed was static and ripples, when present, were
789 relict ripples. For mid-energy conditions corresponding to shear stresses broadly between threshold of
790 motion and sheet flow limit, stationary ripples were generated. The size of 2D vortex ripples increased
791 with hydrodynamic forcing until a wash-out threshold is reached, at which point ripples abruptly transition
792 to smaller 3D vortex ripples. The reverse transition from 3D ripples to 2D ripples is progressive with
793 decreasing wave forcing. Under high-energy conditions, corresponding to exceedance of the sheet flow
794 limit, ripples disappear, and sediment is inferred to be transported under sheet flow conditions.

795 Wave skewness was close to zero during most of the study period and no ripple migration was observed,
796 suggesting that wave-induced cross-shore sediment transport is negligible except possibly under conditions
797 strong enough to result in sheet flow sediment transport. Instead, sediment transport is dominated by

798 alongshore transport by tidal currents of sediment suspended by waves over vortex ripples. This
799 mechanism results in a northward alongshore sediment flux, as well as a small offshore component. These
800 results do not support the hypothesis of the Perranporth lower shoreface acting as a sediment source to the
801 upper shoreface and beach via cross-shore exchanges, and further emphasises the importance of the
802 embayment circulation, alongshore processes, and headland bypassing (McCarroll et al., 2018; Valiente et
803 al., 2019b; Valiente et al., 2020). However, how potential cross-shore fluxes due to wave asymmetry
804 balance with the small offshore current-induced residual would need further investigation under high-
805 energy conditions (sheet flow sediment transport).

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819 **8. References**

- 820 Allen, J. R. L., 1968. Current ripples: Their relation to patterns of water and sediment motion. Nord
821 Holland, Amsterdam. 433pp
- 822 Anthony, E.J, Aagaard, T., 2020. The lower shoreface: Morphodynamics and sediment connectivity
823 with the upper shoreface and beach, *Earth-Science Reviews*, 210,
824 <https://doi.org/10.1016/j.earscirev.2020.103334>

- 825 Austin, M., Scott, T., Brown, J., Brown, J., MacMahan, J., Masselink, G., Russell, P., 2010. Temporal
826 observations of rip current circulation on a macro-tidal beach. *Cont. Shelf Res.* 30, 1149–1165.
827 doi:10.1016/j.csr.2010.03.005
- 828 Austin, M.J., Scott, T.M., Russell, P.E., Masselink, G., 2013. Rip Current Prediction: Development,
829 Validation, and Evaluation of an Operational Tool. *J. Coast. Res.* 2, 283–300.
830 doi:10.2112/JCOASTRES-D-12-00093.1
- 831 Baas, J.H., Best, J.L., Peakall, J., 2016. Predicting bedforms and primary current stratification in
832 cohesive mixtures of mud and sand. *J. Geol. Soc. London.* 173, 12–45. doi:10.1144/jgs2015-024
- 833 Bagnold, R.A., 1946. Motion of waves in shallow water. Interaction between waves and sand bottoms.
834 *Proc. R. Soc. A Math. Phys. Eng. Sci.* 187, 1–18. doi:10.1098/rspa.1946.0062
- 835 Bell, P.S., Thorne, P.D., 1997a. Measurements of sea bed ripple evolution in an estuarine environment
836 using a high resolution acoustic sand ripple profiling system, in: *Oceans '97. MTS/IEEE*
837 *Conference Proceedings.* pp. 339–343. doi:10.1109/OCEANS.1997.634386
- 838 Bell, P.S., Thorne, P.D., 1997b. Application of a high resolution acoustic scanning system for imaging
839 sea bed microtopography. *Seventh Int. Conf. Electron. Eng. Oceanogr. - Technol. Transf. from*
840 *Res. to Ind.* 128–133. doi:10.1049/cp:19970673
- 841 Bell P. S., Thorne P D., 2007. Field measurements of wave induced sand ripples in three dimensions.
842 Published in the 'Underwater Acoustic Measurements: Technologies and results' conference
843 CDrom, held on Crete 25-29 June at F.O.R.T.H. pp 1045-1052.
- 844 Bolaños, R., Amoudry, L.O., Doyle, K. 2011. Effects of Instrumented Bottom Tripods on Process
845 Measurements, *J. Atmos. Oceanic Tech.*, 28, 827-837.
- 846 Camenen, B., 2009. Estimation of the wave-related ripple characteristics and induced bed shear stress.
847 *Estuar. Coast. Shelf Sci.* 84, 553–564. doi:10.1016/j.ecss.2009.07.022
- 848 Camenen, B., Larson, M., 2006. Phase-lag effects in sheet flow transport. *Coast. Eng.* 53, 531–542.
849 doi:10.1016/j.coastaleng.2005.12.003.
- 850 Channel Coastal Observatory, 2020. Annual Wave Report 2017: Perranporth. Available online at:
851 [https://www.channelcoast.org/reports/index.php?link=&dla=download&id=2601&cat=128/Wave](https://www.channelcoast.org/reports/index.php?link=&dla=download&id=2601&cat=128/WaveReport2017_Prp.pdf)
852 [eReport2017_Prp.pdf](https://www.channelcoast.org/reports/index.php?link=&dla=download&id=2601&cat=128/WaveReport2017_Prp.pdf) [Accessed 18 November 2020].
- 853 Clifton, H.E., Dingler, J.R., 1984. Wave-formed structures and paleoenvironmental reconstruction. *Mar.*
854 *Geol.* 60, 165–198. doi:10.1016/S0070-4571(08)70146-8
- 855 Crawford, A.M., Hay, A.E., 2001. Linear transition ripple migration and wave orbital velocity skewness:
856 Observations. *J. Geophys. Res.* 106, 14113–14128.
- 857 Dalrymple, R.W., Rhodes, R.N., 1995. Estuarine dunes and bars, in: *Geomorphology and*
858 *Sedimentology of Estuaries. Developments in Sedimentology.* pp. 359–422.
- 859 Davidson, M.A., Turner, I.L., Splinter, K.D., Harley, M.D., 2017. Annual prediction of shoreline erosion
860 and subsequent recovery. *Coast. Eng.* 130, 14–25. doi:10.1016/j.coastaleng.2017.09.008
- 861 Davies A.G., Thorne P.D., 2005. Modelling and measurement of sediment transport by waves in the
862 vortex ripple regime. *Journal of Geophysical Research.* Vol 110, C05017,
863 doi:10.29/2004JC002468, 20
- 864 Davies, A. G., Thorne, P. D., 2008 Advances in the study of moving sediments and evolving
865 seabeds, *Surveys in Geophysics*, 29 (1). 1-36.

- 866 Elgar, S., 1987. Relationships involving third movements and bispectra of a harmonic process. *IEEE*
867 *transctins Acoust. speech, signal Process.* ASSP-35. N.
- 868 Fenton, J.D., McKee, W.D., 1990. On calculating the lengths of water waves. *Coast. Eng.* 14, 499–513.
869 doi:10.1016/0378-3839(90)90032-R
- 870 Glenn, S.M., Grant, W.D., 1987. A suspended sediment stratification correction for combined wave and
871 current flows. *J. Geophys. Res.* 92, 8244–8264. doi:10.1029/JC092iC08p08244
- 872 Goring, D.G., Nikora, V.I., 2002. Despiking Acoustic Doppler Velocimeter Data. *J. Hydraul. Eng.* 128,
873 117–126. doi:10.1061/(ASCE)0733-9429(2002)128:1(117)
- 874 Grant, W.D., Madsen, O.S., 1979. Combined Wave and Current Interaction With a Rough Bottom. *J.*
875 *Geophys. Res.* 84, 1797–1808
- 876 Hamon-Kerivel, K., Cooper, A., Jackson, D, Sedrati, M, Guisado Pintado, E., 2020. Shoreface
877 mesoscale morphodynamics: A review. *Earth-Science Reviews*, 209, 103330
- 878 Hanes, D.M., Alymov, V., Chang, Y.S., Jette, C., 2001. Wave-formed sand ripples at Duck, North
879 Carolina. *J. Geophys. Res.* 106, 22575–22592. doi:10.1029/2000JC000337
- 880 Hurther D., Thorne P.D., 2011. Suspension and near-bed load sediment transport processes above a
881 migrating, sand-rippled bed under shoaling waves. *J. Geophys. Res.*, Vol 116, C07001,
882 doi:1029/2010JC006774
- 883 Inch, K., Davidson, M., Masselink, G., Russell, P., 2017. Observations of nearshore infragravity wave
884 dynamics under high energy swell and wind-wave conditions. *Cont. Shelf Res.* 138, 19–31.
885 doi:10.1016/j.csr.2017.02.010
- 886 Kramer, K., Winter, C., 2016. Predicted ripple dimensions in relation to precision of in situ
887 measurements in the southern North Sea. *Ocean Sci.* 12, 1221–1235. [https://doi.org/10.5194/os-](https://doi.org/10.5194/os-12-1221-2016)
888 [12-1221-2016](https://doi.org/10.5194/os-12-1221-2016).
- 889 Li, M.Z., Amos, C.L., 1998. Predicting ripple geometry and bed roughness under combined waves and
890 currents in a continental shelf environment. *Cont. Shelf Res.* 18, 941–970. doi:10.1016/S0278-
891 4343(98)00034-X
- 892 Li, M.Z., Wright, L.D., Amos, C.L., 1996. Predicting ripple roughness and sand resuspension under
893 combined flows in a shoreface environment. *Mar. Geol.* 130, 139–161. doi:10.1016/0025-
894 3227(95)00132-8
- 895 Lichtman, I. D., Baas, J. H., Amoudry, L. O., Thorne, P. D., Malarkey, J., Hope, J. A., Peakall, J.,
896 Paterson, D. M., Bass, S. J., Cooke, R. D. Manning, A. J., Davies, A. G., Parsons, D. R., Ye, L.,
897 2018. Bedform migration in a mixed sand and cohesive clay intertidal environment and
898 implications for bed material transport predictions. *Geomorphology*, 315, pp. 17–32.
899 <https://doi.org/10.1016/j.geomorph.2018.04.016>
- 900 McCarroll, R.J, Masselink, G., Valiente, N.G., Scott, T., King, E.V., Conley, D. 2018. Wave and Tidal
901 Controls on Embayment Circulation and Headland Bypassing for an Exposed, Macrotidal Site.
902 *Journal of Marine Science and Engineering*, *J. Mar. Sci. Eng.*, 6, 94; doi:10.3390/jmse6030094
- 903 Malarkey, J., Davies, A.G., 2012. A simple procedure for calculating the mean and maximum bed stress
904 under wave and current conditions for rough turbulent flow based on Soulsby and Clarke’s (2005)
905 method. *Comput. Geosci.* 43, 101–107. doi:10.1016/j.cageo.2012.02.020
- 906 Marine Electronics Ltd., 2009. User Manual for the 3D Sand Ripple Profiling Logging Sonar
- 907 Masselink, G., Scott, T., Poate, T., Russell, P., Davidson, M., Conley, D., 2016. The extreme 2013/2014

- 908 winter storms: Hydrodynamic forcing and coastal response along the southwest coast of England.
909 Earth Surf. Process. Landforms 41, 378–391. doi:10.1002/esp.3836
- 910 Miles, J., Thorpe, A., 2015. Bedform contributions to cross-shore sediment transport on a dissipative
911 beach. Coast. Eng. 98, 65–77. doi:10.1016/j.coastaleng.2015.01.007
- 912 Miles, J., Thorpe, A., Russell, P., Masselink, G., 2014. Observations of bedforms on a dissipative
913 macrotidal beach. Ocean Dyn. 64, 225–239. doi:10.1007/s10236-013-0677-2
- 914 Moate, B.D., Thorne, P.D., Cooke, R.D., 2016. Field deployment and evaluation of a prototype
915 autonomous two dimensional acoustic backscatter instrument: the Bedform And Suspended
916 sediment Imager (BASSI). Cont. Shelf Res. 112, 78–91.
- 917 Nelson, T.R., Voulgaris, G., 2014. Temporal and spatial evolution of wave-induced ripple geometry:
918 Regular versus irregular ripples. J. Geophys. Res. Ocean. 119, 664–688.
919 doi:10.1002/2013JC009020.Received
- 920 Nelson, T.R., Voulgaris, G., Traykovski, P., 2013. Predicting wave-induced ripple equilibrium
921 geometry. J. Geophys. Res. Ocean. 118, 3202–3220. doi:10.1002/jgrc.20241
- 922 Nielsen, P., 1981. Dynamics and Geometry of Wave-Generated Ripples. J. Geophys. Res. 86, 6467–
923 6472.
- 924 Poate, T., Masselink, G., Russell, P., Austin, M., 2014. Morphodynamic variability of high-energy
925 macrotidal beaches, Cornwall, UK. Mar. Geol. 350, 97–111. doi:10.1016/j.margeo.2014.02.004
- 926 Raudikivi, A. J. (1988). The roughness height under waves. *J. Hydr. Res.*, 26 (5), 569-584
- 927 Rousseaux, G., 2006. Physical distinction between rolling-grain ripples and vortex ripples: An
928 experimental study. Phys. Rev. E - Stat. Nonlinear, Soft Matter Phys. 74, 1–7.
929 doi:10.1103/PhysRevE.74.066305
- 930 Ruessink, B.G., Michallet, H., Abreu, T., Sancho, F., Werf, J.J. Van Der, Silva, P.A., 2011. Observations
931 of velocities, sand concentrations, and fluxes under velocity - asymmetric oscillatory flows. J.
932 Geophys. Resear 116. doi:10.1029/2010JC006443
- 933 Scott, T., Masselink, G., O’Hare, T., Saulter, A., Poate, T., Russell, P., Davidson, M., Conley, D., 2016.
934 The extreme 2013/2014 winter storms: Beach recovery along the southwest coast of England. Mar.
935 Geol. 382, 224–241. doi:10.1016/j.margeo.2016.10.011
- 936 Soulsby, R.L., 1983. The bottom boundary layer of shelf seas. In: Johns, B. (Ed.), Physical
937 Oceanography of Coastal and Shelf Seas. Elsevier, Amsterdam, pp. 189–266.
- 938 Soulsby, R.L., 1997. Dynamics of marine sands. A manual for practical applications. Thomas Telford,
939 London, ISBN 0-7277-2584-X
- 940 Soulsby, R.L., 2006. Simplified calculation of wave orbital velocities, in: Sand Transport in Oscillatory
941 Flow. HR Wallingford, p. 12.
- 942 Soulsby, R.L., Clarke, S., 2005. Bed Shear-stresses Under Combined Waves and Currents on Smooth
943 and Rough Beds, Estuary Processes Research Project (Est Proc)/Defra project FD1905.
- 944 Soulsby, R.L., Whitehouse, R.J.S., 2005. Prediction of Ripple Properties in Shelf Seas - Mark 1
945 Predictor (Report TR 150).
- 946 Soulsby, R.L., Whitehouse, R.J.S., Marten, K.V., 2012. Prediction of time-evolving sand ripples in shelf
947 seas. Cont. Shelf Res. 38, 47–62. doi:10.1016/j.csr.2012.02.016
- 948 Styles, R., Glenn, S.M., 2005. Long-term sediment mobilization at a sandy inner shelf site, LEO-15. J.

- 950 Thompson, C.E.L., Silburn, B., Williams, M.E., Hull, T., Sivyer, D., Amoudry, L.O., Widdicombe, S.,
951 Ingels, J., Carnovale, G., McNeill, C.L., Hale, R., Laguionie Marchais, C., Hicks, N., Smith,
952 H.E.K., Klar, J.K., Hiddink, J.G., Kowalik, J., Kitidis, V., Reynolds, S., Woodward, E.M.S., Tait,
953 K., Homoky, W., Kröger, S., Bolam, S., Godbold, J.A., Aldridge, J., Mayor, D.J., Benoist, N.M.A.,
954 Bett, B.J., Morris, K.J., Parker E.R., Ruhl, H.A., Statham, P.J., Solan, M., 2017. An approach for
955 the identification of exemplar sites for scaling up targeted field observations of benthic
956 biogeochemistry in heterogeneous environments. *Biogeochemistry*, 135 (1-2), 1-34. doi:
957 10.1007/s10533-017-0366-1
- 958 Thompson, C.E.L., Williams, M.E., Amoudry, L., Hull, T., Reynolds, S., Panton, A., Fones, G.R., 2019.
959 Benthic controls of resuspension in UK shelf seas: Implications for resuspension frequency.
960 *Continental Shelf Research*, 185, 3-15.
- 961 Thorne, P.D., Hanes, D.M., 2002. A review of acoustic measurement of small-scale sediment processes.
962 *Cont. Shelf Res.* 22, 603–632. doi:10.1016/S0278-4343(01)00101-7.
- 963 Thorne P.D., Davies A.G., Williams J.J., 2003. Measurements of near-bed intra-wave sediment
964 entrainment above vortex ripples. *Geophysical Research Letter*. Vol 30, No 20, 2028. 2.1-2.4
- 965 Thorne, P.D., Davies, A.G., Bell, P.S., 2009. Observations and analysis of sediment diffusivity profiles
966 over sandy rippled beds under waves. *J. Geophys. Res.* 144
- 967 Thorne P.D. Hurther D., Cooke R.D., Barraud P.A., Barnoud J.M., Caceres I., Sanches Arcilla A., 2013.
968 On the study of boundary layer transport processes using new developmental acoustic techniques.
969 In: *Proceeding of Coastal Dynamics 2013*, held in Arachon, France, 24-28 June. pp. 1667–1676.
- 970 Thorne P.D., Hurther D., Cooke R.D., Caceres I., Barraud P.A., Sánchez-Arcilla A., 2018. Developments
971 in acoustics for studying wave-driven boundary layer flow and sediment dynamics over rippled
972 sand-beds. *Continental Shelf Research*, 166, 119-137. <https://doi.org/10.1016/j.csr.2018.07.008>.
- 973 Thorpe, A., Miles, J., Masselink, G., Russell, P., 2014. Bedform Dynamics in a Rip Current, *Proceedings*
974 *13th International Coastal Symposium (Durban, South Africa)*, *Journal of Coastal Research*,
975 *Special Issue No. 70*, pp. 700-705, ISSN 0749-0208. Thyng, K.M., C.A. Greene, R.D. Hetland,
976 H.M. Zimmerle, and S.F. DiMarco. 2016. True colors of oceanography: Guidelines for effective
977 and accurate colormap selection. *Oceanography* 29(3):9–13.
978 <http://dx.doi.org/10.5670/oceanog.2016.66>
- 979 Traykovski, P., Hay, A.E., Irish, J.D., Lynch, J.F., 1999. Geometry, migration, and evolution of wave
980 orbital ripples at LEO-15. *J. Geophys. Res.* 104, 1505–1524. doi:10.1029/1998JC900026
- 981 Valiente, N.G., Masselink, G., Scott, T., Conley, D., McCarroll, R.J., 2019a. Role of waves and tides on
982 depth of closure and potential for headland bypassing, *Marine Geology*, 407, 60-75.
- 983 Valiente, N.G., McCarroll, R.J., Masselink, G., Scott, T., Wiggins, M., 2019b Multi-annual embayment
984 sediment dynamics involving headland bypassing and sediment exchange across the depth of
985 closure, *Geomorphology*, 343, 48-64.
- 986 Valiente, N., Masselink, G., McCarroll, R.J., Scott, T., Conley, D., King, E., 2020 Nearshore sediment
987 pathways and potential sediment budgets in embayed settings over a multi-annual timescale.
988 *Marine Geology*, 427, 106270.
- 989 van Rijn, L.C., 2007a. Unified View of Sediment Transport by Currents and Waves. I: Initiation of
990 Motion, Bed Roughness, and Bed-Load Transport. *J. Hydraul. Eng.* 133, 649–667.
991 doi:10.1061/(ASCE)0733-9429(2007)133:7(776)
- 992 van Rijn, L.C., 2007b. Unified View of Sediment Transport by Currents and Waves. II: Suspended

- 993 Tranport. J. Hydraul. Eng. 133, 668–689. doi:10.1061/(ASCE)0733-9429(2007)133:7(776)
- 994 Wiberg, P.L., Nelson, J.M., 1992. Unidirectional flow over asymmetric and symmetric ripples. J.
995 Geophys. Res. 97, 12745–12761. doi:10.1029/92JC01228
- 996 Wiberg, P.L., Sherwood, C.R., 2008. Calculating wave-generated bottom orbital velocities from
997 surface-wave parameters. Computers and Geosciences, 34, 1243-1262
- 998 Wright, L.D., Short, A.D. 1984. Morphodynamic variability of surf zones and beaches: A synthesis,
999 Marine Geology, 56, 1–4, 93-118, [https://doi.org/10.1016/0025-3227\(84\)90008-2](https://doi.org/10.1016/0025-3227(84)90008-2).
- 1000
- 1001 Wright, L.D., Boon, J.D., List, J.H., 1991. Models of cross-shore sediment transport on the shoreface of
1002 the Middle Atlantic Bight. Mar. Geol. 96, 19–51. doi:10.1016/0025-3227(91)90200-N
- 1003 Xiong, J., Wang, Y.P., Gao, S., Du, J., Yang, Y., Tang, J., Gao, J. 2018. On estimation of coastal wave
1004 parameters and wave-induced shear stresses. Limnol Oceanogr. Methods, 16 (9), 594-606
- 1005
- 1006