

# The application of componentised modelling techniques to catastrophe model generation

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## Abstract.

In this paper we show that integrated environmental modelling (IEM) techniques can be used to generate a catastrophe model for groundwater flooding. Catastrophe models are probabilistic models based upon sets of events representing the hazard and weights their likelihood with the impact of such an event happening which is then used to estimate future financial losses. These probabilistic loss estimates often underpin re-insurance transactions. Modelled loss estimates can vary significantly, because of the assumptions used within the models. A rudimentary insurance-style catastrophe model for groundwater flooding has been created by linking seven individual components together. Each component is linked to the next using an open modelling framework (i.e. an implementation of OpenMI). Finally, we discuss how a flexible model integration methodology, such as described in this paper, facilitates a better understanding of the assumptions used within the catastrophe model by enabling the interchange of model components created using different, yet appropriate, assumptions.

## i. Introduction

Global economic losses related to natural hazards are large and increasing. Total economic losses reached US\$130 billion in 2010, US\$380 billion 2011 and US\$160 billion in 2012 (Munich Re 2011, 2012). Insurance is a method of managing these financial risks, the objective of purchasing insurance is to avoid a loss large enough to cause failure by spreading the cost. However, natural hazards or ‘perils’, can affect many insured properties across a wide area (e.g. 100s of km across) in a limited time window (e.g. <72 hours). For

34 example, Hurricane Andrew in 1992 caused an estimated \$26.5bn in losses to property,  
35 leading to the failure of 13 insurance companies (AIR 2002; Cummins 2007). To protect  
36 against this, insurers buy reinsurance. The reinsurers have to cost this insurance by  
37 estimating the insured losses caused by extreme events, such as hurricanes and  
38 earthquakes and then predicting the probable likelihood of such an event occurring. The  
39 difficulty is that insurers previous claim experience is often of little use when trying to  
40 predict insured losses. This is because extreme events are rarely directly comparable, and  
41 insured property 'exposure' changes rapidly. For example inflation, real growth in property  
42 values, varied insurance penetration, and changes in properties' locations within a portfolio  
43 must be accounted for to create a figure for likely insured losses (Tower Perrin, 2005; Swiss  
44 Re 2007). Catastrophe models, developed over the last ~25 years (Grossi et al., 2005), are  
45 one solution to this problem.

46

47 The aim of this paper is to demonstrate a proof-of-concept by showing how Integrated  
48 Environmental Modelling (IEM) methods and techniques can be used to construct a  
49 catastrophe model using the example of groundwater flooding risk of the Marlborough and  
50 Berkshire Downs in the UK. Although there is extra effort required to make models linkable  
51 once a linked modular catastrophe model has been constructed, several advantages can be  
52 gained, for example an increased flexibility by allowing for the interchange of compatible  
53 components. Linked modelling can facilitate both an improved understanding of and better  
54 insight into the interactions between model components, in part because of the need to  
55 fully document and define the models and datasets being exchanged between components.

56

57 This paper will firstly look at flooding in the UK and UK insurance policy; we will then discuss  
58 how the insurance industry use catastrophe models to improve loss calculations and how  
59 IEM modelling methods and techniques could be adopted to generate catastrophe models.  
60 The second part of the paper will work through a case study example of groundwater  
61 flooding in the Marlborough and Berkshire downs.

## 62 **ii. Flooding and the UK Insurance industry**

63 Unlike many other countries, in the UK, the majority of domestic and business flood damage  
64 losses are covered by the insurance market rather than government funds. Under the

65 'Statement of Principles', an agreement setup in 2000 between the British Government and  
66 the Association of British Insurers (ABI), insurers committed to providing cover for almost all  
67 properties, other than where the risk is deemed significant and no plans are in place to  
68 manage the risk within a 5 year time period (DEFRA 2011). In the last 10 years in the UK,  
69 there have been several major flood events. The biggest and most catastrophic were the  
70 2007 floods which consisted of a mixture of surface and groundwater flooding events which  
71 affected large areas of Yorkshire, the Midlands and the West of England. This demonstrated  
72 without doubt that flooding in the UK can be devastating, from social impacts such as loss of  
73 life, dislocation of thousands of people and major economic impacts which cost insurers  
74 over £3 billion (Pitt 2008). Two years later, the 2009 floods affecting a smaller area of  
75 Cumbria, West Wales, Dumfries and Galloway, still cost insurers over £1.5m (Munich RE,  
76 2010). The Association of British Insurers has put the average cost of flood damage (all  
77 types) in the UK to homes affected at between £20,000 and £40,000 each (Dailey et al.  
78 2009).

79

80 In this paper we concentrate on groundwater flooding, because it is both poorly understood  
81 (e.g. Finch et al. 2004; Hughes et al. 2011), and often confused by non-specialists with  
82 surface water flooding. Groundwater flooding presents a substantial problem, but is not  
83 widely recognised either in the UK or internationally (Kreibich and Thielen 2008). Hughes et  
84 al. (2011) suggest four types of groundwater flooding based on their origin:

- 85 a) A high water table in regional aquifers
- 86 b) Short-circuiting of flood defences
- 87 c) A rise of the water table due to cessation of mine dewatering
- 88 d) Barriers to subsurface flow caused by underground structures

89 In the example used in this case study; the risk is primarily of Type 1 resulting from  
90 extremely high intensity and/or long duration rainfall.

91

92 The costs and impacts of just groundwater flooding events in the UK are significant and  
93 almost certainly underestimated (Green et al., 2006, Royse 2011) because unlike surface  
94 water flooding, groundwater floods tend to be longer-lasting, typically remaining for the  
95 order of weeks or months. Groundwater flooding can be defined as flooding caused by the  
96 emergence of water originating from subsurface permeable strata (Cobby et al. 2009). The

97 latest estimates suggest 1.6 million properties may be at risk in the UK (Jacobs, 2004), the  
98 most vulnerable being those located on the exposed Chalk aquifers of southern England e.g.  
99 south Oxford in 1997 (Macdonald et al. 2007, 2008), but events also occur elsewhere, such  
100 as in Pilmuir in Scotland (Macdonald et al. 2008; MacDonald et al., 2008). Typically,  
101 groundwater flooding occurs during winters where recharge is high during the early part of  
102 the recharge season and stays above average. The case study that has been used is in the  
103 Pang and Lambourn catchments within the Berkshire and Marlborough downs (Fig 3A). The  
104 catchments experienced severe flooding during the winter of 2000/1 following unusual  
105 meteorological events in the previous 18 months (Adams et al. 2008), and again in the  
106 winter of 2002/3 (Hughes et al. 2011).

107

108 The actual cost of groundwater flood events, while less nationally than fluvial or marine  
109 flooding, can be significant e.g. the estimated cost of a relatively localised groundwater  
110 flooding event in 2000 in Brighton was £800,000, excluding the cost of the railway closure  
111 (Binnie et al. 2001). Furthermore, groundwater flooding in Hambledon in 2000/01 was  
112 estimated by the local council to have resulted in financial losses of some £1.1 million  
113 (Green et al., 2006).

114

115 After the 2007 flood events in the UK, a review was carried out looking at how the events  
116 were managed and what lessons could be learnt (Pitt, 2008). The review was extremely far-  
117 reaching, covering building regulations, emergency response, prediction and modelling. A  
118 key recommendation was the need to develop a whole system approach to understanding  
119 flood risk in the UK. This required that groundwater flood risk should be included within any  
120 flood risk management system.

121

122 Groundwater flood events often take decision-makers by surprise, as they are not included  
123 in conventional flood risk mapping. In recognition of this problem, the EU's Floods Directive  
124 (2007/60/EC) dictates that groundwater flood risk now has to be taken into account in any  
125 flood risk study. Damage to properties caused by rising groundwater levels is a worldwide  
126 issue (Hagerty and Lippert 1982; Hamdan and Mukhopadhyay 1991). Kreibich and Thielen  
127 (2008) have noted that loss assessment studies have in general neglected damage caused by  
128 groundwater. In order to evaluate the cost effectiveness of, for example, groundwater

129 drawdown measures, the construction of rain surface and floodwater collection networks,  
130 there is a growing need to generate reliable loss assessments (Al-Sefy and Sen 2006).

131

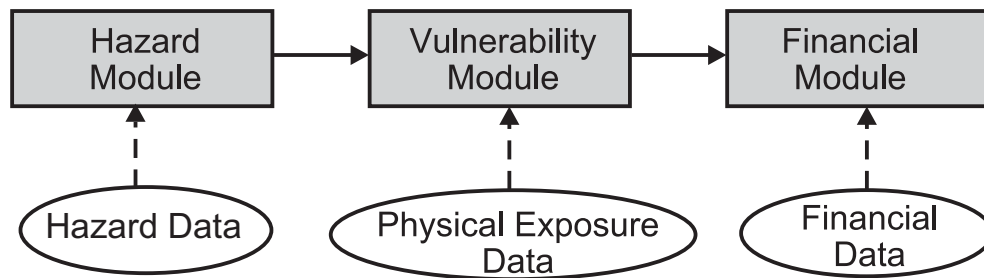
### 132 **iii. Catastrophe Models**

133 Catastrophe models have been used for the last 25 years by the insurance industry to assess  
134 risk by estimating likely losses from extreme events, whether natural or man-made.  
135 Catastrophe models are stochastic, event-set based computer models, which allow the  
136 potential for large losses from an insurer's current exposure (usually property assets) to be  
137 tested by subjecting them to many (e.g. 10,000) events representing scenarios for a hazard  
138 within a peril-region (e.g. 'UK flood') and are used to estimate the location, impact and  
139 frequency of possible future natural disasters (Grossi and Kunreuther, 2005). The purpose  
140 of a catastrophe model is to provide insurers with a better understanding of their liability to  
141 events in the year ahead. The models are then used: to "price" catastrophic risk; to control  
142 an insurer's risk accumulation; to diversify their risk; to estimate the insurer's reserves in  
143 case of loss; to minimise the amount of capital required to cover risks in the insurer's  
144 portfolio and finally to estimate the correct price to reinsure or transfer their risk (Chavez-  
145 Lopez and Zolfaghari 2010). Most catastrophe models are based on an arrival process and  
146 provide tradeoffs between economic losses i.e. an evaluation of the severity and the  
147 probability that a certain level of loss will be exceeded on an annual basis (Haimes 2004,  
148 Grossi and Kunreyther 2005 and Banks 2006).

149

150 Figure 1 provides an illustration of a typical framework for a catastrophe model. The  
151 contents, definitions, and names of each of the modules are not standardised and therefore  
152 do vary (e.g. Grossi 2005; Qu 2010). However, the broad work-flow as illustrated remains  
153 similar. Figure 1 identifies three major 'modules', where processing occurs, and three  
154 inputs. In this paper we will only be considering damage to property exposure. However,  
155 catastrophe models can look at a variety of exposures, such as: loss of life, business  
156 interruption, clean up costs, infrastructure losses etc.

157



158

159 **Figure 1:** One possible proposed conceptual framework of a traditional component based  
 160 catastrophe model. Rectangles are modules, ovals are inputs and arrows indicate the flow  
 161 of information.

162

163 The 'Hazard' module provides the frequency, intensity and areal extent of events, usually as  
 164 spatial intensity maps (i.e. contoured footprints of severity), each associated with a  
 165 probability of occurrence within the next year. For model users (e.g. insurers, brokers), this  
 166 exists as a static database supplied in whichever product they are using. For model  
 167 developers, calculations to generate the event set may also be included. The 'Vulnerability'  
 168 module converts hazard into physical impact, typically via vulnerability (a.k.a. fragility)  
 169 curves linking hazard intensity (e.g. flood depth) to loss as a percentage of the total insured  
 170 value of a property. To achieve this, exposure information is input and losses for every  
 171 property evaluated for every event; therefore, the locations of exposure are critical in  
 172 calculating loss. Modifiers are used to improve the accuracy of the impact assessment by  
 173 indicating which variants on the main vulnerability curves could be used for each exposure.  
 174 Modifiers may include: building construction (e.g. stone, reinforced concrete), number of  
 175 stories, style of occupancy (e.g. residential, commercial), and year built. Lastly, the  
 176 'Financial' module calculates losses by using policy information, primarily the sum the  
 177 property is insured for. This also uses other information such as limits, deductibles, or  
 178 treaties that determine who to assign these losses to: financial perspectives e.g. 'ground  
 179 up', 'net loss pre-cat' (Grossi et al. 2005).

180

181 Like other numerical models, catastrophe models are developed based on certain  
 182 assumptions or simplifications, thus leading to errors (e.g. Grossi 2005) and uncertainties in  
 183 the loss estimates. Therefore catastrophe models need to be used with due caution (e.g. GC  
 184 2011; ABI 2011). To most users, however, catastrophe models are 'black boxes' owned and

185 developed by one of the major catastrophe modelling companies. This suggests that  
186 catastrophe models may not always be used to the insurers' best advantage when  
187 supporting their decision-making processes. After Hurricane Katrina in 2005, it was  
188 recognised that considerable progress had been made in modelling natural catastrophes;  
189 however there were significant limitations in the existing models at that time in predicting  
190 losses for both personal and commercial risks which caused modellers to launch new efforts  
191 to revise their databases and predictive techniques (Cummins, 2007). Catastrophe models  
192 produce two main outputs: the Annual Average Losses (AAL), i.e. the insurer's time-  
193 averaged costs in payouts, and the Occurrence Exceedance Probability (OEP) curve. OEP is  
194 the probability that losses due to any single event will exceed an amount, e.g. an insurer's  
195 financial reserves. So, losses due to a low probability high return period event, perhaps the  
196 250 yr OEP loss, are of great interest, as these tail-end events may bankrupt the company.

197

198 Even when only the losses resulting from damage to property are considered, models'  
199 results differ and are known to be imperfect. First-order sources of error (Grossi 2005)  
200 include:

201 a) Hazard estimates: event sets may be imperfect, for example the 2011 Mw 9.0  
202 Tohoku earthquake was larger than those included in catastrophe models (Avouac  
203 2011; Lay and Kanamori 2011; Ozawa 2011; AIR 2012).

204 b) Vulnerability curves: these estimated relationships may be incorrect, out of date or  
205 may not be applicable to the geographic area under analysis.

206 c) Exposure data: in the insurance industry, this term is used to describe the physical  
207 contact between assets, usually houses (damage), and a peril (hazard). Incomplete or  
208 incorrect details about assets on insurers' books such as errors in localisation and  
209 identification will lead to erroneous estimates.

210

211 The difference that errors including those above can make to estimates of losses can be  
212 demonstrated by the initial estimates of losses caused by the European windstorm 'Kyrill' in  
213 2007. The 5 main models variously reported losses as, \$3-5bn [RMS], \$3.6-8.8bn [AIR], \$2.5-  
214 5bn [EQECAT], \$4-7bn [Hanover Re], \$5-7bn [Munich Re], and \$3.5bn [Swiss Re] (Willis Re,  
215 2007) whereas the actual property losses were estimated to be at around \$5.8bn (Muich Re  
216 2011b). Where catastrophe models exist for perils (and it should be noted that large gaps

217 in the geographic coverage of catastrophe models still remain), there are a number of other  
218 issues known to affect the accuracy of loss estimates because they are either imperfectly or  
219 incompletely included within current catastrophe modelling methodology. Some of the  
220 more notable issues are listed below:

221

222 a) Multi-peril correlation (e.g. Woo, 1999): For instance, tsunami and fire  
223 following earthquake may be included only crudely, e.g. footprints of a few  
224 selected tsunami scenarios, or not at all.

225 b) Hazard clustering in time (e.g. Lennartz et al. 2008; Rybski et al. 2008; Vitolo  
226 et al. 2010): where events do not occur independently of each other;  
227 typically, events are assumed to be independent, although clusters in  
228 European windstorms has now been included,

229 c) Unmodelled exposures: physical (e.g. cars or oil rigs) or conceptual. Business  
230 interruption is normally included for the firm directly insured, but wider  
231 economic losses such as knock-on impact, commercial liability,  
232 compensation, and life insurance are generally not considered. For example,  
233 \$40bn of losses for the recent flooding in Thailand, \$10bn of which were  
234 insured, were mainly due to supply-chain disruption which graphically  
235 illustrates the potential impact of these effects (Munich Re 2012; Willis  
236 2012).

237 d) Demand Surge: an increased cost of repairs due to scarcity and the  
238 consequent cost of construction material and labour going up in the largest  
239 events.

240

## 241 **1. Solvency II**

242 New regulations (Solvency II) (e.g. Eling et al. 2007; EU 2009; ABI 2011) require insurance  
243 firms to better understand the assumptions underpinning their solvency calculations. The  
244 directive applies to all insurance and reinsurance firms which have gross incomes exceeding  
245 5 million Euros. The directive's main aim is to specify the European Union's requirements on  
246 the capital adequacy and risk management of insurers to make certain that they can survive  
247 difficult periods. This should protect policyholders and also the stability of the financial



248 system in Europe (Eling et al. 2007). The Solvency II directive went live on the 1<sup>st</sup> January  
249 2014 (EU 2009). The directive specifies the minimum amount of financial resources that  
250 insurers and reinsurers must have in order to cover the risks that they are exposed to, in  
251 other words the companies' solvency capital requirements (SCR). Each insurer determines  
252 their SCR by using an internal model that has been accepted by the regulator. One  
253 component of this model is the catastrophe model. This has very significant implications,  
254 because Solvency II makes the insurer responsible for all parts of their internal model (ABI  
255 2011). Therefore, even if they rely, as many do, on a vendor for their catastrophe modelling,  
256 the insurer cannot outsource its 'understanding' of or 'responsibility' for any part of the  
257 catastrophe modelling process (ABI 2011).

258 Therefore, in practice, insurers wanting to implement Solvency II have to  
259 demonstrate a high level of data quality and management, disclosure and transparency as  
260 well as more frequent reporting (ABI 2011). In terms of catastrophe modelling, these new  
261 regulations require the insurer's senior management team to understand the strengths and  
262 weaknesses of the catastrophe models the company are using, to be aware of potential  
263 gaps and quality differences in the company's catastrophic risk modelling landscape, to  
264 actively seek the levels of information and detail they need to feel comfortable with taking  
265 decisions and finally to ensure that the proper policies and procedures for doing so are in  
266 place (ABI 2011). The onus is therefore on the insurance company to understand the  
267 limitations of the catastrophe models that it uses, the differences between model outputs  
268 and actual loss experience and how the results of their modelling impact the company's  
269 internal model for SCR calculation (ABI 2011).

#### 270 **iv. Integrated Environmental Modelling (IEM)**

271 Due to the modular paradigm typically used in catastrophe models as discussed above it is  
272 relatively simple to see how an IEM approach could be successfully adopted. For example,  
273 each module can be thought of as an individual or group of models that are performing  
274 calculations and exchanging data with each other (Zolfaghari 2009). This affords the user  
275 and developer greater flexibility in being able to update and change component parts of the  
276 model framework as and when new data, models or scientific understanding becomes  
277 available.

278

279 IEM methods and techniques have been driven by the need of today's policymakers to  
280 understand complex environmental problems (Beck 2009). To answer these questions an  
281 ever-increasing appreciation of the earth processes and how they interact together is  
282 required (Beck 2009). IEM is about linking computer models together that simulate different  
283 processes to allow scientists to predict how processes interact in particular situations  
284 (Moore and Hughes 2010). The technique is predominantly used in impact analysis,  
285 especially when looking at the wider consequences of events and policies, optimising  
286 resources or what the resultant societal impact will be of new policies to manage the  
287 natural world. IEM focuses on linking models, databases and institutional structures to  
288 support decision making. It is not about the individual models themselves (Laniak et al.  
289 2013). However, integrated modelling is concerned with the design and operation of  
290 integrated analytical frameworks, accessibility of models, repeatability of results and audit  
291 trails, uncertainty passing through the model chain and decision support interfaces (Moore  
292 and Hughes 2010).

293

294 There is an increasing recognition that it is not practical to construct one large monolithic  
295 model which can capture all of the earth-system processes needed for decision making  
296 (Argent 2006). Large models are not only wasteful of resources, rarely reusable and difficult  
297 to understand but they fail to make use of existing process models (Moore and Hughes  
298 2010). IEM methods can be used to make existing numerical models into components or  
299 'building blocks' that can be assembled or linked together to make more complex models  
300 (Warner et al. 2008; Barthel et al. 2008). Using this approach, models become substitutable  
301 and the linking mechanism can be more transparent and better documented (Knapen et al.  
302 2013).

303

304 A model framework can be used to link models together. Several frameworks are currently  
305 available, for example FRAMES (Babendreier and Castleton 2005), CSDMS (Overeem et al.  
306 2013), OMS (David et al. 2002) and OpenMI (Moore and Tindall, 2005). Where these  
307 frameworks are based on open standards such as the case with OpenMI, the framework can  
308 be made widely assessable to a large user community (Knapen et al. 2013). The choice  
309 between modelling frameworks is largely dependent on the project being undertaken and  
310 the researchers involved (Knapen et al 2013). Linking models to enable individual models to

311 conduct a simulation collectively is challenging (Bulatewicz et al. 2010). These difficulties can  
312 be due to a variety of reasons; for example, it could be how the models have been designed,  
313 the programming language or the spatial and temporal discretisation used. A further issue  
314 is that of using components based on a consistent set of assumptions, although this is a  
315 challenge, whether one uses a monolithic or componentized approach, in the latter case this  
316 issue must be addressed if components are going to be interchanged. In situations where  
317 there is a need to link models together, it is advantageous to use a standard protocol, as it  
318 promotes collaboration and reuse of the individual model components (Knapen et al. 2013).

319

320 In this paper we have developed a linked groundwater catastrophe model. However, linking  
321 hydrological models to economic models has been done previously in various ways over a  
322 long time period (Burt 1964; Brouwer and Hofkes 2008; Koundouri 2004; Harou et al. 2009).  
323 Where a modular approach has been taken, the transfer of data has been achieved in  
324 several ways with varying levels of automation (Draper et al. 2003; Volk et al. 2008; Ahrends  
325 et al. 2008; Jackman and Letcher 2003; Cuddy et al. 2005). For example, Jonkman et al.  
326 (2008) developed a surface-water hydrodynamic economic model for the Netherlands to  
327 estimate flood damage due to low probability high impact events. Their approach integrated  
328 different types of data within a geographical information system (GIS). Bulatewicz et al.  
329 (2010) used a more automated approach using an open Framework e.g. OpenMI to  
330 integrate agriculture, groundwater and economic models to evaluate the impacts of water-  
331 use policies to reduce irrigated water use in semi arid grasslands in America. Bulatewicz et  
332 al. (2010) found that the flexible design of the OpenMI framework assisted with the modular  
333 approach that was taken and worked well with models from other domains other than  
334 hydrology, for which OpenMI was originally designed.

335

336 This paper focuses on the use of the OpenMI model framework because it uses an open  
337 framework based on well-defined standards. OpenMI was developed because there was a  
338 need to answer integrated hydrological catchment questions within the EU 5<sup>th</sup> Framework  
339 programme (Gijsbers et al. 2002) OpenMI was developed by a consortium of European  
340 companies, research organisations and universities co-funded by the European Commission  
341 as a standard for model linkage in the water domain that would allow models to exchange  
342 data at run time (Moore et al. 2005) and was initially developed to facilitate an integrated

343 approach to environmental management as specified in the Water Framework Directive  
344 (OpenMI 2009).

345

346 OpenMI works by defining what an individual model must be able to do in order for it to  
347 become OpenMI compliant. Once model entities are made OpenMI compliant, they  
348 effectively turned into objects, or 'components'; multiple components form an OpenMI  
349 composition. To achieve OpenMI compliance, the model component must implement a set  
350 of OpenMI interfaces. This exposes inputs, outputs and run-time operations of the model to  
351 any OpenMI compliant environment and enables its coupling with any other OpenMI-  
352 compliant components without source code changes. Once a model element meets these  
353 requirements, it is then a linkable component and the model has become OpenMI  
354 compliant (OATC 2009).

355

356 Once compliance is achieved it allows the model to exchange data by linking the exposed  
357 variables. One of the features of OpenMI is that a component's owner selects which of the  
358 model variables are accessible by other model components. The owner can also choose the  
359 number of variables that the users can manipulate. This feature could help in addressing  
360 security issues within catastrophe models for the insurance industry, as it could be used to  
361 restrict access to variables within any OpenMI compliant component. Although this appears  
362 at odds with the premise of increased transparency we have to acknowledge that, in some  
363 cases, security issues outweigh the need for greater openness. Using a model standard such  
364 as OpenMI can help ensure that more of the model components remain open to  
365 interrogation than might otherwise have been the case.

366

367 As well as defining, a standard, OpenMI also has a default software implementation which  
368 has been developed by the HarmonIT EU project (

369 <https://sites.google.com/a/openmi.org/home/openmi-around-the-world/development->

370 [tools](https://sites.google.com/a/openmi.org/home/openmi-around-the-world/development-tools) ). The SDK (Software Development Kit) and graphical environment were developed by

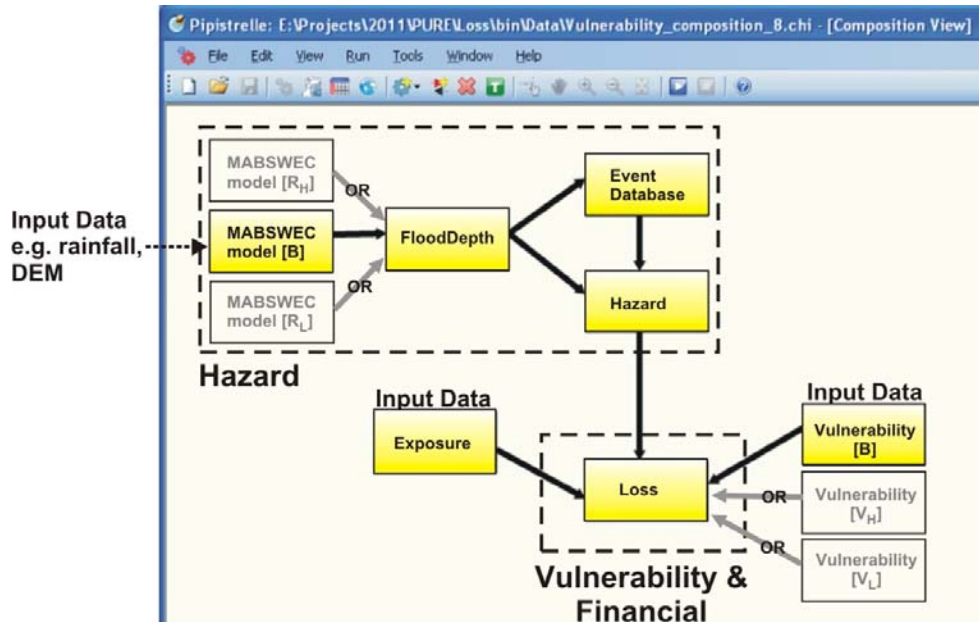
371 the Fluid Earth initiative (2011), and is freely available on SourceForge

372 (<http://sourceforge.net/> ). The implementation has been developed to reduce the amount

373 of work needed to make computational entities OpenMI compliant and to link them

374 together. It includes a software implementation of OpenMI, comprising a SDK and a GUI

375 (Graphical User Interface) called 'Pipistrelle'. The SDK allows models (e.g. groundwater flow  
 376 and climate models) to be adapted into OpenMI compatible 'components' in preparation for  
 377 linking to other models. Fluid Earth's 'Pipistrelle' is a graphical 'point and click' interface  
 378 (Figure 2) that allows users to link components into 'compositions' and run them.  
 379

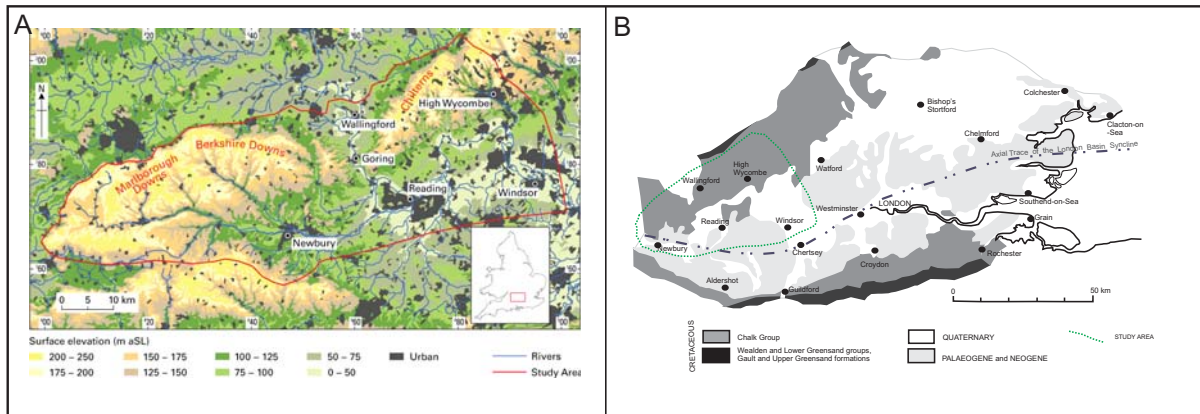


380  
 381  
 382 **Figure 2:** Annotated screen shot of a Pipistrelle composition for the Groundwater Flooding  
 383 Catastrophe. Yellow boxes are the 7 components of the 'baseline' [B] model, comprising  
 384 best-estimates of recharge [R], hydraulic conductivity [K], and vulnerability [V]. Arrows  
 385 indicate data flow detailed in Table 1. Grey text and arrows, added to the screen shot,  
 386 indicate alternative components that could be swapped into the composition by simply  
 387 changing the link (arrow).

388  
 389 **v. Case Study: Development of a Groundwater Flooding**  
 390 **catastrophe model for the Marlborough and Berkshire Downs**

391  
 392 Our case study is located 70 km west of London in the Marlborough and Berkshire  
 393 Downs and South-West Chilterns (MaBSWEc) and covers an area of about 2600 km<sup>2</sup>

394 (see Figure 3A). The elevation of the ground surface ranges from 20 m to the south-east of  
 395 the area to 250 m towards the north-west of the region. The River Thames flows onto the  
 396 area near Wallingford and off the region near Windsor, and its tributaries are the Rivers  
 397 Kennet, Lambourn, Pang, and the Wye (Jackson et al. 2011).  
 398  
 399



400  
 401  
 402 **Figure 3: (A)** Map of the study area, located by red rectangle in the inset. Red outline  
 403 depicts the limits of the Marlborough and Berkshire Downs and South-West Chilterns  
 404 (MaBSWeC) groundwater model used (adapted from Jackson et al. 2011). **(B)** Geological  
 405 sketch map of the London Basin. Based on Figure 1 of Sumbler (1996). Note that  
 406 groundwater flooding is not an issue where clay (Palaeogene) overlies Chalk.

407  
 408 The region lies at the north-western edge of the London Basin which was formed through  
 409 the creation of a synclinal geological structure, principally in the soft white limestone of the  
 410 Cretaceous Chalk (Sumbler 1996; Royse et al. 2012; Figure 3B). The Chalk is the primary  
 411 aquifer in the area and hence the focus for our groundwater model component. This  
 412 primary aquifer is also the main source for drinking water in the region. However, it is also a  
 413 cause of flood events; for example, in early 1994 East Ilsley suffered what were then the  
 414 worst floods to affect the village for 33 years, caused entirely through groundwater flooding  
 415 (Newbury Weekly News, 3 March 1994). Groundwater flooding has a number of different  
 416 manifestations (see Hughes et al., 2010), but in this paper we are only considering the  
 417 situation where the water table rises and reaches the land surface, resulting in surface  
 418 flooding

419                    **a. Constructing a groundwater catastrophe model for the Marlborough and**  
420                    **Berkshire Downs**

421 To create a simple catastrophe model for groundwater flooding in the Marlborough and  
422 Berkshire Downs study area, individual models were linked together using OpenMI. We  
423 will firstly describe how we make the models compliant and then link the following  
424 seven components: *MaBSWeC* model, FloodDepth, EventDatabase, Hazard,  
425 Vulnerability, Exposure and Loss. This process is described in more detail below and the  
426 components are summarized in Table 1 and as illustrated in Figure 2

427 To make our models OpenMI compliant the models have to comply with three  
428 requirements: the component must implement the  
429 *OpenMI.Standard2.IBaseLinkableComponent*  
430 (<http://sourceforge.net/p/openmi/code/HEAD/tree/trunk/src/csharp/OpenMI.Standard2/>)  
431 interface, it must handle specified state-transitions and invocation of certain methods  
432 in each state/phase, and finally it must have an associated XML file containing information  
433 on each of components, capabilities and availability (OATC 2010). Each component/model  
434 (OATC 2010) must be structured so that: its initialization is separated from its computation,  
435 it can receive run time controls from an external entity, and it can provide values of the  
436 modelled quantities and specify the point or extent in time that the values belong to (these  
437 values should be in the public domain). The first stage is to make the model engine linkable  
438 and this is done by compiling the engine core of the model into a dynamic link library (OATC  
439 2010). The model engine can, when running in an OpenMI environment, perform as  
440 separate operations: initialisation (I), run (R) single time steps/simulations and finalize (F)  
441 (i.e. IRF) interface. This can require the engine core to be rearranged in some cases however  
442 this was not the case in the components used here. The next step was to use the  
443 *MyEngineWrapper* (<http://www.openmi-life.org/>) to implement the  
444 *ITimeSpaceLinkableEngine*  
445 (<http://sourceforge.net/p/openmi/code/HEAD/tree/trunk/src/csharp/OpenMI.Standard2/TimeSpace/ITimeSpaceComponent.cs>)  
446 interface this allows the component model to  
447 run in an OpenMI environment and the *ITimeComponent* interface can then be run. In order  
448 for such a model to link to other models and exchange data we have to define and add the  
449 input and output items (OATC 2010). For example the groundwater model (*MaBSWeC*

450 model) generates groundwater level data which are inputted automatically into the Flood  
451 depth model (FloodDepth). Any data which are exchanged between component models at  
452 run-time must be explicitly defined see Table 1; note that the linking process creates the  
453 appropriate cross-reference table negating the need to synchronize terminology. Once this  
454 is completed we then tested each component to check that it worked correctly, this was  
455 done using the NUnit test tool (<http://www.NUnit.org>). In this example where we are re-  
456 using a pre-existing groundwater model, the preparation of the OpenMI composition took  
457 around 100 hours. This includes coding the 6 additional components, making all of them  
458 OpenMI compliant, and linking the models and other components together (see figure 2).

459

460 A basic workflow used for catastrophe modelling is as presented in Figure 1, but there are  
461 some differences from what may be considered standard (Grossi 2005). It should be noted  
462 however that the contents, definitions, and names of each of the components within a  
463 catastrophe workflow are not standardised and therefore do vary (Grossi 2005; Qu 2010).  
464 The modifications that have been made in this case are that the event set generation is  
465 included in the hazard module (Qu 2010) and that the financial 'loss' module includes  
466 computational elements often split between the vulnerability and financial modules. This is  
467 primarily because the available non-proprietary (Penning-Rowsell et al. 2010) vulnerability  
468 curves are given in the form 'pounds per house', implicitly combining vulnerability and loss.  
469 This highlights the versatility of OpenMI compositions, allowing the user to respond to the  
470 available data to implement compositions.

471

472 The goal of the hazard module is to produce hazard maps of maximum flood depths. In  
473 order to produce these maps the following components need to be tied together: the  
474 *MaBSWeC* groundwater model (generates a model of the groundwater system and  
475 therefore the groundwater levels at any point in time), FloodDepth (creates maps of  
476 flooding and depth), EventDatabase (identifies flood events) and hazard (generates the  
477 hazard maps). So in detail the hazard module is constructed based upon a pre-existing  
478 groundwater model '*MaBSWeC Model*' which is based on two models: a recharge models  
479 built using ZOODRM (Mansour and Hughes 2004) and a groundwater flow model ZOOMQ3D  
480 (Jackson and Spink 2004). ZOODRM and ZOOMQ3D were used to build the recharge and  
481 groundwater flow models that were combined into the '*MaBSWeC Model*' for the study



482 area. Recharge is water entering the groundwater system; it descends through the soil, then  
483 through the underlying unsaturated zone, until it arrives at the top of the saturated zone,  
484 the 'water table'. Groundwater flow is water flowing in the saturated zone, from areas of  
485 high hydraulic head to low ones. Where it meets the land surface, it discharges. In the UK  
486 the significant discharges are rivers, springs and points at which water is abstracted for  
487 domestic and industrial supply purposes. The models and the data used to drive them are  
488 described in more detail below.

489

490 The groundwater recharge model used is ZOODRM, driven by 33 years of daily distributed  
491 rainfall (1971-2003) from Centre for Ecology & Hydrology (CEH) and potential  
492 evapotranspiration datasets provided by Met Office. ZOODRM calculates surface runoff,  
493 routing water based on a 50 m resolution Digital Elevation Model (DEM; Morris and Flavin  
494 1990), and applies the soil moisture deficit (SMD) method (Penman 1948; Grindley 1967) to  
495 calculate the actual evaporation, changes in soil moisture and groundwater recharge. A daily  
496 time step is used to produce the lowest practical error in the soil moisture balance  
497 calculation (see Howard and Lloyd, 1979). The balance between daily rainfall,  
498 evapotranspiration, surface runoff and potential recharge across the area are simulated,  
499 using information on the spatial variation in the DEM and of land use, geology, rainfall and  
500 potential evapotranspiration.

501

502 The regional groundwater flow model used in this study was developed using ZOOMQ3D, a  
503 quasi-3D finite-difference groundwater flow model. It simulates transient fluctuations in  
504 groundwater head, river baseflow, and spring discharge along a chalk scarp slope. The rivers  
505 are simulated using an interconnected river network that exchanges water with the  
506 underlying aquifer according to a Darcian type flux equation. Details are given in previous  
507 applications of ZOOMQ3D (Hughes et al. 2008; Campbell et al. 2010; Guardiola-Albert and  
508 Jackson 2011, Mansour et al. 2011). The model contains three laterally extensive layers to  
509 represent the vertical variations in the hydraulic properties of the chalk and river valley  
510 gravels based on geological models of the lithostratigraphy within the wider London Basin.  
511 The groundwater model was calibrated by comparing the modelled results with  
512 groundwater heads at 207 observation boreholes and river baseflow at 20 gauging stations  
513 (Jackson et al. 2011).

514

515 Groundwater heads across the area are computed at daily intervals in the 'MaBSWeC  
516 model' component (Fig. 2). The 'FloodDepth' component (Fig. 2) compares these to the  
517 DEM used consistently in all models (e.g. CEH-DTM; Morris and Flavin, 1990), creating daily  
518 maps of flooding and its depth whenever water height breaches the land surface. This  
519 assumes that the surface water system is static and does not flow down topographic  
520 gradient. Depths are set to zero where surficial clay deposits (Figure 4) are known to act as  
521 barriers which rule out groundwater flood events in those areas.

522

523 Next, the 'EventDatabase' component identifies flood events, assigning them a number and  
524 probability 1/33 (once in 33 years). Groundwater flooding events are defined when the  
525 groundwater level produced by the model was within 0.1 m of the ground surface for at  
526 least one month. Given the differences in resolution of the groundwater model and the  
527 DEM then the groundwater level was averaged for a groundwater model grid node (2 km by  
528 2 km) and to allow for the variation of ground surface then a tolerance of 0.1 m was used.  
529 The start and end period of the event was identified from the flood maps produced by the  
530 'FloodDepth' component. In all 33 events were identified, coincidentally the same as the  
531 year of the run. As all occurred in 33 years, and were given equal likelihood specifically a 1 in  
532 33 event probability. The final component of the hazard module is 'Hazard', which creates  
533 hazard maps of the maximum flood depths attained during each event. This intensity  
534 measure drives flood losses (e.g. Penning-RowSELL et al. 2010).

535

536 The 'Loss' component combines exposure and vulnerability information with hazard maps  
537 to estimate losses for each event in the database. Exposure has been simplified by  
538 assuming that urban areas (Figure 3) have constant housing density (100 houses per km<sup>2</sup>),  
539 with no exposure outside. Vulnerability uses a residential average for all exposure. Losses  
540 for all properties affected by each event are firstly summed to get an 'event loss table' of  
541 losses per event, and then OEP curves (e.g. Grossi 2005) are generated. Secondary  
542 uncertainty, the uncertainty in losses given that an event has occurred, is not considered.  
543 Table 1 details the components and data exchanged between them.

544

545 **Table 1:** Datasets exchanged by the OpenMI compatible components in the catastrophe  
 546 model composition. See Gregerson et al., (2005) and Moore and Tindall (2005) for more  
 547 information on how OpenMI exchanges data.

Component	Input data	Output data	purpose
MaBSWeC model	<ul style="list-style-type: none"> <li>• File containing a recharge scenario: gridded for each daily time step. Derived from rainfall, potential evaporation, land-use, topography data.</li> <li>• Files of boundary conditions: Specifically, locations of rivers and springs, and location and rates of groundwater abstraction.</li> <li>• File of hydraulic parameters (hydraulic conductivity, storage coefficients).</li> </ul>	<ul style="list-style-type: none"> <li>• Grid (i.e. map) of groundwater head at each time step.</li> </ul>	Simulates the groundwater part of the hydrogeological cycle. Generates groundwater level information
FloodDepth	<ul style="list-style-type: none"> <li>• Gridded groundwater heads for each time step.</li> <li>• DEM (Digital Elevation Model) CEH-DTM (Morris and Flavin,1990).</li> </ul>	<ul style="list-style-type: none"> <li>• Distributed depth of groundwater flooding in X, Y, Z format.</li> </ul>	Produces maps of where groundwater breaches the land surface
EventDatabase	<ul style="list-style-type: none"> <li>• Daily distributed flood depth of groundwater flooding in X, Y, Z format.</li> <li>• Lower and upper limits of the range used for calculating the average groundwater flooding depth across the area. Groundwater model calibration is imperfect, so limits are necessary to screen out anomalous values.</li> <li>• Threshold value of average groundwater height exceeded during flooding events.</li> </ul>	<p>For each flood event:</p> <ul style="list-style-type: none"> <li>• Event number</li> <li>• Start time</li> <li>• End time</li> <li>• The distributed depth of groundwater flooding in X, Y, Z format for each day within the event</li> </ul>	Identifies flood events and assigns them a probability
Hazard	<p>For each flood event</p> <ul style="list-style-type: none"> <li>• Event number</li> <li>• Start time</li> </ul>	<p>For each event</p> <ul style="list-style-type: none"> <li>• Event number</li> <li>• Hazard intensity maps</li> </ul>	Creates hazard maps of

	<ul style="list-style-type: none"> <li>• End time</li> <li>• Flood depth maps for each day within the flood in X, Y, Z format.</li> </ul>	of maximum flood depth attained during the event	maximum flood depths for each event
Vulnerability	<ul style="list-style-type: none"> <li>• File of vulnerability curves.</li> </ul>	<ul style="list-style-type: none"> <li>• flood damage costs</li> </ul>	Assesses the vulnerability of the assets exposed and damage costs
Exposure	<ul style="list-style-type: none"> <li>• File containing exposure data.</li> </ul>	<ul style="list-style-type: none"> <li>• Exposure information in X, Y, format</li> </ul>	The distribution of assets
Loss	<ul style="list-style-type: none"> <li>• Hazard intensity maps of maximum groundwater flooding depth for each numbered event</li> <li>• flood damage costs;</li> <li>• Exposure information in X, Y, format</li> </ul>	<ul style="list-style-type: none"> <li>• OEP curves</li> </ul>	Combines the hazard information with the vulnerability and exposure to generate losses per event and OEP curves

548

549

#### **b. Model Evaluation**

550

Catastrophe models are used in decision-making and as such it is essential that we establish our confidence in the output of such models to justify their continuing use while recognising their limitations (Bennett et al 2013). In a linked modelled system the models must be validated not just as single standalone models but also when they are linked together, to check that, when executed as a collective model, the results are still feasible. This is a particular issue when using simulated data from one model as input data into another model within the linked model chain (Bulatewicz et al. 2010), as any errors within the simulated input data may induce smaller or greater errors in the final model results.

558

559

Bennett et al (2013) has suggested a five step evaluation procedure that is beneficial to the modelling process as a whole. This involves assessing the aims, scale and resolution of the model, checking the data to determine that sufficient data is used for calibration and performance, visual analysis of model results, selection of performance criteria and finally refinement of the model (Bennett et al 2013). We have therefore based our evaluation and validation on the steps above assessing each model's performance relative to our

564

565 understanding of the system and available observational data (Bennett et al 2013,  
566 Alexandrov et al 2011 and McIntosh et al 2011). For example, the groundwater model is  
567 calibrated and validated by comparing the modelled surface water component (i.e. fast flow  
568 in the river) with observation data. The pre-existing ZOOM suite of groundwater models  
569 used here has been verified for numerical precision by Jackson and Spink, (2004). Validating  
570 the absolute values of the losses of catastrophe models is notoriously difficult. The main  
571 commercial models are calibrated to past observed losses, i.e. they are evaluated using  
572 claims data held by the insurance industry. In this case, the economic losses generated  
573 within the groundwater flooding catastrophe model, have been qualitatively validated  
574 against known historical events in the region where losses have been recorded, i.e. the  
575 model's performance was compared to available datasets of known financial losses for the  
576 region. This showed that the model accurately predicted where the major flood events had  
577 occurred and provided an equatable estimate of previous financial loss. A final evaluation  
578 of the model's performance can be made by comparing our models results against  
579 alternative publically available models; such models currently do not exist. However, as  
580 computationally this is a simple model we compared computations carried out in Excel to  
581 our model outputs to verify computational accuracy for all components individually  
582 throughout the whole linked model and in all cases, model output results matched  
583 computations done in Excel.

584

### 585 **c. Financial Loss generated from Groundwater Flooding Scenarios**

586 Assumptions used within catastrophe models can make huge differences to the modelled  
587 results (Grossi 2005; AIR 2012; Willis Re 2007). However, it is common for most users not to  
588 understand or know all the assumptions that have been made. To get around this problem  
589 it is considered good practice within the insurance industry to use a variety of models from  
590 several vendors, so that an holistic 'multi-model' view of risk is developed (GC 2011; ABI  
591 2011). In this section, we will look at the impact on model results of changing the scenarios  
592 used within the groundwater flooding catastrophe model presented above. By using an  
593 open framework such as OpenMI to develop the catastrophe model, it would also be  
594 possible for whole modules to be freely exchanged and swapped in and out of the

595 composition. In this example we will focus on changing components: different instances of  
596 the groundwater model and different vulnerability models.

597 The *MaBSWeC* groundwater model component is dependent upon rainfall scenarios to drive  
598 groundwater recharge; the baseline model uses observed rainfall values (Jackson et al.  
599 2011), the alternative models for high [ $R_H$ ] and low [ $R_L$ ] recharge are achieved by scaling  
600 rainfall by  $\pm 20\%$ . Thus, effectively 3 different groundwater scenario models have been  
601 created based upon different climatic assumptions which can be swapped in and out of the  
602 linked groundwater catastrophe model. A range of  $\pm 20\%$  is chosen since this is typical for a  
603 preliminary sensitivity analysis (Sterman 2000) and has been used in assessments of the  
604 hydraulic consequences of climate change (e.g. Gleick 1987). We know that in the UK  
605 between, 1961 to 2006 there has been a percentage increase in rainfall in the winter in  
606 some parts of the SE of up to 20-40% and a corresponding decrease in the summer of  
607 between 10-20% (Maraun et al 2008) therefore a value of  $\pm 20\%$  provides us with a valid  
608 scenario to work from. Hydraulic conductivity [ $K$ ] was also varied by  $\pm 20\%$ , giving scenarios  
609 [ $K_L$ ] and [ $K_H$ ] (Sterman 2000). This value was identified as being reasonable from the initial  
610 calibration of the model (Jackson et al., 2011). The changes in hydraulic conductivity were  
611 implemented by changing  $K$  within the *MaBSWeC* [B] model, demonstrating that it is also  
612 possible to change parameters within model components.

613 Vulnerability models can also be interchanged. Here, alternative datasets are curves of low  
614 [ $V_L$ ] and high [ $V_H$ ] property vulnerability, but each could as easily be different vendor  
615 databases. The curves are selected from the Penning-Rowell et al., (2010) to reflect the  
616 ranges of houses stock found within the study area giving a known average and a worst and  
617 best case scenario. Two types of housing are chosen: Terrace housing and Bungalows.  
618 Again, a different component is developed for each one and swapped into and out of the  
619 composition.

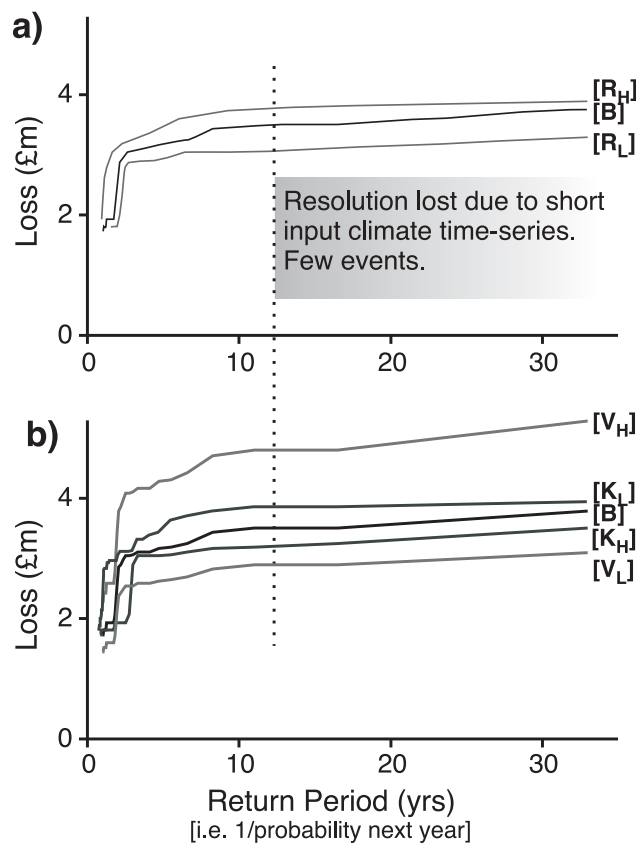
620 By choosing to vary recharge and hydraulic conductivity we can develop five different  
621 instances of the groundwater flow model (*MaBSWeC* model) and these can be combined  
622 with two vulnerability components. This results in seven different components which can  
623 be readily interchanged within the composition. This approach has been used to undertake  
624 a sensitivity analysis which combines parameter uncertainty (recharge derived from rainfall

625 and hydraulic conductivity) combined with type of housing. Whilst it could be argued that  
626 parametric uncertainty can be dealt with in a conventional modelling system, this is a proof  
627 of concept and the different components could easily be groundwater models that exhibit  
628 fundamental differences (i.e. finite difference vs finite element). The important outcome is  
629 that the composition can be re-run to generate the loss information as discussed below.

630

631 The insurance industry standard representations of likely loss information are expressed as  
632 annual average loss (AAL) and occurrence exceedance probability (OEP) curves. Grossi et al.  
633 (2005) details their calculation. Figure 6 presents the baseline [B] OEP curve for  
634 groundwater flooding in the study area. Expected losses are in the order of £3.8 million for  
635 the largest event in the time-series, a roughly 33yr OEP loss. It should be noted, however,  
636 that OEP losses above 10-15 years contain significant uncertainty due to the small number  
637 of events defining the curve above this point. In a more formal study, a longer input time-  
638 series, perhaps created by a climate model, would reduce the epistemic uncertainty here  
639 and allow rarer events to be considered.

640



641

642 **Figure 4:** Occurrence Exceedance Probability (OEP) curves. a) Baseline model [B] is black line,  
643 and dark grey lines are for high [ $R_H$ ] and low [ $R_L$ ] recharge scenarios, with shading  
644 representing a plausible range. b) Baseline as a), dark grey are hydraulic conductivity  
645 scenarios [ $K_L$ ] and [ $K_H$ ], and light grey are vulnerability datasets [ $V_H$ ] and [ $V_L$ ] (Figure 4). Loss  
646 at a probability of 0.05 next year is referred to as 'a 20yr OEP loss'.  
647

648 **Table 2:** Analysis of catastrophe model outputs as assessed by changes within the  
649 composition (Figure 2). Expressed as percentage change from baseline scenario. Scenarios  
650 denoted in text using letter (B, V, R, K) and a subscript where L is Low, H is High, e.g.  $V_L$ . 20  
651 yr OEP values calculated by linear interpolation between data, i.e. as plotted on Figure 4.

Scenarios			Output			% Change		
			Events	20 Year OEP (£m)	AAL (£m)	Event	20 Year OEP	AAL
<b>Baseline (B)</b>	-		33	3.57	2.54	-	-	-
<b>Vulnerability Curves (V)</b>	Terrace (L)	-	33	2.94	2.11	0	-17.50	-16.94
	Bungalow (H)	-	33	4.91	3.42	0	37.65	34.60
<b>Recharge (R)</b>	L	-20%	23	3.16	1.76	-30.30	-11.42	-30.52
	H	+20%	41	3.79	3.58	24.24	6.29	41.18
<b>Hydraulic Conductivity (K)</b>	L	-20%	42	3.81	3.54	27.27	6.77	39.39
	H	+20%	40	3.31	2.66	21.21	-7.22	4.88

652  
653 On average, one event per year and £2.5M of damages are expected, with worst cases being  
654 above £3.6M. Therefore, attritional losses (i.e. losses from high frequency, low severity  
655 events) appear to dominate over discrete, devastating events but this in all likelihood  
656 reflects the limited time-series and spatial region considered. Tail-end (i.e. high impact, low  
657 probability events) groundwater losses will probably be driven by higher return period  
658 rainfall (recharge) scenarios causing correlated flooding at sites separated by length-scales  
659 of up to ~100s of km across the UK; 2000/1 groundwater flooding occurred in Oxford,



660 Berkshire and Brighton (MacDonald et al. 2008). Whilst loss figures from this study are  
661 small, UK-flood is typically an important peril region so will materially affect insurers if they  
662 occur in compound with other flood types as happened in Oxford in 2001 (MacDonald et al.  
663 2007) perhaps increasing 25yr OEP losses by as much as 5%.

664  
665 The results of various scenarios on financial losses derived from the groundwater flooding  
666 catastrophe model are presented in Figure 6 and Table 2. Each scenario represents  
667 variations upon the assumptions incorporated in the model. These scenarios are not  
668 intended to form a comprehensive sensitivity analysis, as here we look at the impact of just  
669 varying one factor at a time (OAT). While the shortcomings of using OAT are known from  
670 the literature ie that of the assumption of model linearity and not accounting for parameter  
671 interactions (Saltelli and Annoni 2010) some preliminary insights can still be gained. For  
672 example, varying the property type within the exposure model from the residential average  
673 within the UK (Figure 4) to bungalows had the biggest effect on 20yr OEP increases losses by  
674 37% up to a maximum of £4.9M. The converse was true when the property type was  
675 changed to terraced houses resulting in a decrease of 17% in 20 year OEP. When the  
676 amount of rainfall was changed this increased/decreased the recharge within the  
677 groundwater aquifer affected the number of events rather than their severity. When  
678 comparing the effects of changing the amounts of recharge on the model results it clearly  
679 impacts AAL more than the 20yr OEP suggesting that differing assumptions made within the  
680 model will impact the model results in dissimilar ways with some scenarios making an  
681 impact only in specific circumstances. Similarly changes in hydraulic conductivity increases  
682 the overall number of events and again effects AAL more than OEP but only when the  
683 hydraulic conductivity is low.

684  
685 The model results are sensitive to simplifications used in each model component.  
686 Furthermore, for more complex models this sensitivity is likely to increase significantly. In  
687 this paper we have used variations in vulnerability, recharge and conductivity to illustrate  
688 how components from different providers could be exchanged in and out of the model  
689 chain. The added flexibility afforded through the use of OpenMI has allowed for a far  
690 greater level of interrogation to be carried out by the user.

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## **vi. Discussion and conclusions**

In this paper we have looked at how IEM modelling methods and technologies can be used to develop catastrophe models for the insurance industry. We have discussed at the beginning of this paper that are several advantages to using IEM methodologies such as increased flexibility due to the ability to interchange components, and increased transparency due to the need to fully document and define models and datasets. In this section we will discuss these in more detail.

We have shown that by using IEM model integration methods to develop a catastrophe model for groundwater flooding, the resulting model chain is repeatable and transparency is increased. This is due to the need, in componentised modelling to provide a detailed explanation of what each component does and what is being exchanged, so that each component can be understood by a community of users, not just the individual modellers involved in the development. With Solvency II regulations being implemented in 2014 there will be a need for insurers to understand and take responsibility for all parts of the catastrophe modelling process. This will mean that they will be required to understand the limitations and assumptions of the models that they use, such as the first-order sources of error (Grossi 2005) discussed in section iii and the fact that there are a number of known elements within catastrophe models that are not perfectly modelled such as multi-peril correlation and hazard clustering, see section iii for further details. This will include models from outside vendors i.e. an increased level of transparency will be required between model developers and their user community. If IEM methods are adopted by the insurance industry this will provide one way of ensuring compliance with solvency II legislation as well as ensuring a better understanding of the use of catastrophe models by insurers.

A lack of openness within the insurance industry has restricted, to some extent, its ability to make use of existing models or new scientific developments. By utilising open source model frameworks such as OpenMI, it is possible to lower the entry barrier significantly for individuals wanting to be involved in catastrophe model development. There is always a worry when lowering entry barriers that this would be detrimental to the quality of the

723 product being produced or developed, however the advantages of increasing the number of  
724 models and thereby increasing competitiveness within the community, and preventing over-  
725 dependence on a few model vendors are likely to push up the management and quality of  
726 the models being produced in fact this has already been recognised with the insurance  
727 industry backed OASIS loss modelling framework project ([oasislmf.org](http://oasislmf.org)). This gives several  
728 advantages to the insurance industry, for example the ability to attract academic developers  
729 who might be able to supply the industry with specialist modelling components, thereby  
730 providing the catastrophe modelling and insurance community with direct access into the  
731 research community (exploitable research in hazard and vulnerability). It can also provide  
732 access to a ready source of model components (particularly for hazard modules which take  
733 a considerable amount of time to develop) for areas that don't currently have catastrophe  
734 models but may have been an area of active academic research; this could be for a number  
735 of reasons such as a low level of perceived financial risk or that the resulting models are  
736 unaffordable to the user community. IEM could decrease the time that risk managers  
737 currently spend working with catastrophe modelling companies to better understand the  
738 assumptions used in the models, running various scenarios of losses under different model  
739 assumptions and validating the models by generating their own internal models. Access to a  
740 large number of open, well documented modelling components would thereby reduce the  
741 time spent in validating models and understanding assumptions used. Finally within the  
742 industry there are still risk managers who do not use catastrophe models because they are  
743 too expensive so by using an open source modelling framework such as described in this  
744 paper it would be possible to increase the use of catastrophe models in insurance.

745

746 The flexibility of the OpenMI framework makes it a suitable platform to bring together the  
747 various components required (e.g. models, functions and data) to generate such a  
748 catastrophe model. Data has been freely exchanged within the model framework, and  
749 plausible losses have been produced. By utilising an open standard such as OpenMI, all the  
750 components can be reused without the need for additional programming and thus can  
751 contribute to a common repository of model components for use in the wider community.  
752 This could effectively result in lowering the entry barrier to evaluating problems relating to  
753 natural hazards using probabilistic event-set based modelling, opening the door to the  
754 participation of different stakeholders (e.g. local government) and perhaps considering

755 problems other than the purely financial.

756

757 A repository for models would have many benefits, such as enabling users to test model  
758 compositions and demonstrate the effects of model component choice on end results. It  
759 would therefore have the potential to assist insurers to fulfil their obligations under  
760 Solvency II. For example, in most proprietary catastrophe models, it is not currently  
761 possible for users to run different future scenarios of their choice in a realistic manner,  
762 without going back to the proprietary models owners.

763

764 By using OpenMI's SDK and 'Pipistrelle' interface to link components into 'compositions' and  
765 run them the structure of data flows between components is made transparent (for more  
766 information: [fluidearth.net](http://fluidearth.net); Harpham et al. In press). As not only do the components have to  
767 be defined and documented but the datasets that are exchanged between the components  
768 at run-time must also be explicitly defined. By utilising an IEM model structure, it is easy to  
769 make substitutions within the model composition or add components to include models  
770 incorporating future climate-change scenarios, or even add a surface water flooding model.  
771 Modelling companies and insurers work to maintain security of their intellectual property  
772 and data; therefore, using a framework which enables parts of or whole models to remain  
773 restricted (e.g. shields proprietary data), will be something that will be required from an  
774 industry standpoint. It is possible to do this using OpenMI which in the future could be  
775 developed to form the basis of a secure, web-based model framework.

776

777 Another use of the IEM modelling system is in generating catastrophe models for areas  
778 where none exist currently. Flooding in Thailand (August 2012) highlighted the need for  
779 flood risk models for SE Asia. Reasons for not having catastrophe models could be due to a  
780 lack of exposure or hazard data, a perceived low level of financial risk or the catastrophe  
781 model itself could be unaffordable. Catastrophe models are being used to help create risk  
782 transfer mechanisms in the developing world (the Review 2008). Probabilistic catastrophe  
783 models have been used to estimate the benefits of disaster risk reduction measures for  
784 hurricane risk on residential structures on the island St Lucia and earthquake risk on  
785 residential structures in Istanbul, Turkey (Michel-Kerjan et al 2013). The ability of low to  
786 middle income countries to cope with natural disasters and limit their economic exposure is

787 becoming a priority (Cummins and Mahul 2008, Michel-Kerjan et al 2013) as when a natural  
788 hazard hits countries with limited financial resilience often they will seek support from the  
789 international donor community (Cumins and Mahul 2008). Although there is extra effort  
790 required to make models linkable and a requirement, if each component is to be reusable,  
791 to better manage model components, once a linked modular catastrophe model has been  
792 constructed, it is in situations as described above when the increased flexibility of an IEM  
793 modelling system comes into its own by allowing for the interchange components parts of  
794 the model framework as and when new data, models or scientific understanding becomes  
795 available allowing for updates almost instantaneously, if required

796

797 Finally, advances made in the understanding of hazard, vulnerability and exposure will bring  
798 considerable societal as well as economic benefits. This will translate not only in a reduction  
799 in financial losses incurred, but also in lives saved. We will need to develop a better  
800 understanding of where our vulnerabilities lie, so that we can adapt, monitor and mitigate  
801 against major natural hazard events. It is crucial that all relevant information related to the  
802 distribution and severity of natural hazards and a region's vulnerability to particular natural  
803 hazards are presented in an accessible, reliable and understandable form so that those that  
804 need it are able to make use of the information.

805

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812

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## 1093 **Figure Captions**

1094

1095 **Figure 1:** One possible conceptual framework of a traditional component based catastrophe  
1096 model. Rectangles are modules, ovals are inputs and arrows indicate the flow of  
1097 information.

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1099 **Figure 2:** Annotated screen shot of a Pipistrelle composition for the Groundwater Flooding  
1100 Catastrophe. Yellow boxes are the 7 components of the 'baseline' [B] model, comprising  
1101 best-estimates of recharge [R], hydraulic conductivity [K], and vulnerability [V]. Arrows  
1102 indicate data flow detailed in Table 1. Grey text and arrows, added to the screen shot,  
1103 indicate alternative components that could be swapped into the composition by simply  
1104 changing the link (arrow).

1105

1106 **Figure 3: (A)** Map of the study area, located by red rectangle in the inset. Red outline  
1107 depicts the limits of the Marlborough and Berkshire Downs and South-West Chilterns  
1108 (MaBSWeC) groundwater model used (adapted from Jackson et al 2011). **(B)** Geological  
1109 sketch map of the London Basin. Based on Figure 1 of Sumbler (1996). Note that  
1110 groundwater flooding is not an issue where clay overlies Chalk.

1111

1112 **Figure 4:** Occurrence Exceedance Probability (OEP) curves. a) Baseline model [B] is black  
1113 line, and dark grey lines are for high [ $R_H$ ] and low [ $R_L$ ] recharge scenarios b) Baseline as a),  
1114 dark grey are hydraulic conductivity scenarios [ $K_L$ ] and [ $K_H$ ], and light grey are vulnerability  
1115 datasets [ $V_H$ ] and [ $V_L$ ]. Loss at a probability of 0.05 next year is referred to as 'a 20yr OEP  
1116 loss'.

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1119 **Table Captions**

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1121 **Table 2:** Datasets exchanged by the OpenMI compatible components in the catastrophe  
1122 model composition. See Gregerson et al. (2005) and Moore and Tindall (2005) for more  
1123 information on how OpenMI exchanges data.

1124

1125 **Table 2:** Analysis of catastrophe model outputs as assessed by changes within the  
1126 composition (Figure 2). Expressed as percentage change from baseline scenario. Scenarios  
1127 denoted in text using letter (B, V, R, K) and a subscript where L is Low, H is High, e.g.  $V_L$ . 20  
1128 yr OEP values calculated by linear interpolation between data, i.e. as plotted on Figure 6.

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