Libyan Arab Republic

Kufra and Sarir Authority

Jalu - Tazerbo Project: Phase 2

APPENDIX 4

T(Q1-65)

SITE REPORT

Hydrogeological Department
Institute of Geological Sciences
Exhibition Road, London SW7 2DE
1974

The Institute of Geological Sciences was formed by the incorporation of the Geological Survey of Great Britain and the Museum of Practical Geology with Overseas Geological Surveys and is a constituent body of the Natural Environment Research Council.

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Jalu-Tazerbo Project: Phase 2

Appendix 4: T(Q1-65) Site Report

- 1. Location: 27 54' 39" North, 21 00' 21" East
- 2. Ground elevation: 532 feet above mean sea level at oil exploration well site, Q1-65
- 3. Site plan and elevations: Figure 1 and Table 1

Ground and casing top elevations (in feet above mean sea level) at T (Q1-65)

Location	Ground Elevation	$\frac{ ext{Casing}}{ ext{Top}}$
Q1-65 WW North WW South T(Q1-65)A	532 535. 1 534. 4 534. 1	536. 9 536. 4 536. 5

4. Existing Water Wells: BP Exploration Co.

(Libya) Ltd water well records show three water wells to have been drilled on this site (Table II).

TABLE II
BP Exploration Co. (Libya) Ltd water well
records

1	2	3
243	576	528-576
244	596	542-596
245	586	538-586

Columns:

- 1. Well number
- 2. Total depth in feet on completion
- 3. Perforated interval in feet bgl
 - NB Only two wells could be found at the site and were designated North and South (Table III)

		TA	BLE	Π			
Static	water	level	data	in	water	wells	a.t
Q1-65	in Jur	ie 197	3				

WW South	258.2	278, 2
WW North	258.8	278.1
T(Q1-65)A	257.8	278.7

Columns:

- 1, Well location
- 2. SWL in feet below casing top
- 3. SWL in feet amsl
- 5. Geophysical logs: The following logs are available on file but not enclosed with this report
 - (a) Schlumberger logs of Q1-65:
 - 1. Final lithological log from 200 to 10, 848' below rotary table (brt)
 - 2. IES from 150 to 2730 feet below rotary table
 - 3. Sonic log from 150 to 2730 feet below rotary table
 - (b) BP Co. mud log from surface to 4000 feet
 - (c) IGS gamma-ray log from surface to 978 feet bgl

6. Drilling and completion:

(a) T(Q1-65) was drilled by rotary rig using Quiktrol mud to a depth of 1250 feet bgl and was finally abandoned at this depth leaving the bit, five drill collars and a considerable length of drill pipe in the hole. Abandonment was a consequence of hole collapse following upon loss of circulation.

- (b) T(Q1-65)A was drilled using Quiktrol mud to 2365 feet bgl and was completed with a combination string of slotted and blank 6 3/8 inch casing. The slotted sections numbering seven in all, were wrapped with wire mesh to prevent sand entrance. The hole was lithologically sampled from 280 feet to total depth.
- 7. <u>Lithology and stratigraphy:</u> A summary of stratigraphic data is shown in Table IV, and a graphical log in Figure 2.

TABLE IV Stratigraphic data at T(Q1-65)

Ground	elevat	tion at Q1-65	1	2 532
Static v	vater l	evel	257	275
Base of	Calan	scio Formation	201	331
11 11	LMM	(Zone a)	386	146
11 11	It	(Zone b)	465	67
†I I1	If	(Zone c)	656	124
f1 f1	t I	(Zone d)	870	462
11 11	11	(Zone e)	1264	732
Base of	Oligo	cene (Zone a)	1770	1238
13 11	11	(Zone b)	2266	1754

Columns:

- 1. Depths in feet below general ground level
- Elevation in feet above or below mean sea level

The base of the Oligocene which overlies the Upper Eocene is picked out on the BP Final lithological log but no other sub-divisions are shown. These latter are mainly defined in relation to boundaries more apparent elsewhere in the Phase 2 Area but significant changes do occur also at this particular site which serve to differentiate them. The top of the Oligocene is based on a sonic change which has been traced over a large part of the Phase 2 Area and may indicate increased compaction in the Oligocene as compared with the Lower and Middle Miocene Formations above.

The LMM which intervenes between the Calanscio Formation of Post-Middle Miocene age and the Oligocene, contains a significant clay percentage although considerably less so than in the central Phase 2 Area. The relations are apparent in the cross-section A-A' in the main Report. The Calanscio Formation consists of sand, sandy limestone and some dolomite, and the base is selected at the top of the first prominent clay horizon. The water table at this

site occurs below the base of the Calanscio Formation.

Samples from 10 feet intervals, except for those with a significant clay or carbonate content, were sieve analysed. A summary of the data is shown in Table V and some average values in Table VI.

The bulk of the Post-Eocene sequence consists of fine to medium uniform sands with clays occurring most significantly in Zones 'b' and 'd' of the LMM and Zone 'b' of the Oligocene. The associated sands in the clayey zones are commonly finer grained than in the other horizons. Sandstones and sandy carbonates are of limited occurrence. The sandstones recorded in Zone 'b' of the Oligocene could well be fine sands as indicated by the sieve analysis data.

The Post-Eocene sequence at Q1-65 is apparently unfossiliferous and the only significant recorded features having some bearing on the depositional environment are the single references to occurrences of lignite and of glauconite, both occurring in Zone 'b' of the Oligocene. The sieve analysis data show distinctive variations between the different zones but with one possible exception, no regular trends occur within the zones. The possible exception is Zone 'c' of the LMM where the D50 sizes show a fairly regular decrease upwards. Cross plots of the standard deviation against skewness and mean size have been produced, samples from each zone being grouped together. The plots for Zone 'e' of the LMM are shown in Figure 3 which also show the boundary lines separating environments according to Moiola and Weiser, 1968. The bulk of the samples fall into the fluviatile field apart from three occurrences within Zones 'd' and 'e' of the LMM for which beach sands are indicated. The feature is consistent with the characteristics of the Lower and Middle Miocene which becomes predominantly marine in the north-central Phase 2 Area. A 3-ft core was obtained from the 10-foot interval between 1100 and 1110 feet below ground level. The core consisted of poorly consolidated, rather clayey yellow brown sand with some streaks of grey clay. Petrographic studies carried out by the Petrological Department of the IGS gave the following information.

"CORE-SAMPLE OF OLIGOCENE SANDSTONE FROM BH T(Q1-65) EB, CENTRAL CYRENAICA, LIBYA. LAT 27 54' 39"N. LONG 21 00' 21"E. Depth between 1100 and 1110 feet below ground level.

Registered number F7791

Introduction

The following report is the result of analysis of the more coherent portion of the sample submitted, taken from the interior of the core in order to avoid contamination.

Grain size analyses, of the sand grade fraction by dry sieving and the silt and clay using the Sartorius sedimentation balance, are by C.W. Wheatley. G.E. Strong determined the statistical parameters from these results.

Petrography

The rock is a very poorly sorted soft silty sand with sand: silt: clay proportions of $60, \frac{4}{4}$: 29, 1: 10. 5 respectively.

In colour the material is dark yellowish orange (Geol. Soc. Am. Color Chart 1972, number 10 YR 6/6) with irregular clay rich bands of moderate reddish brown (1OR 4/6) and moderate greenish yellow (10Y 7/4).

The thin-section, number F7791, shows the rock to be composed of grains of quartz, a little feldspar and chert dispersed in a silty clay, ironstained matrix. Among the clastic grains quartz predominates and is of metamorphic type with abundant inclusions, the feldspar is represented by both microcline and plagioclase in unaltered fragments. Modal analysis of the clastic grains gives the following proportions:

Quartz	94%
Feldspar	3%
Chert	2%
Others (limonite etc)	1%

It is noticeable that the shape of the clasts varies with size. The grains larger than about 0.5mm are well rounded and the smaller are angular to subrounded. Some slight modification of the shapes due to secondary growth on the quartz has occurred.

Matrix and cement

X-ray diffraction examination (Chart DX 1225) of the silt-clay fraction shows this to be composed predominantly of kaolinite and clay mica with approximately 10% quartz and a little feldspar.

Secondary mobilization of quartz has been noted above and some of the same material recorded on the XRD chart probably represents silica cement as well as finely clastic material. Significant amounts of amorphous iron are present.

The cement therefore appears to a mixture of clay, silica and iron hydroxides.

No carbonates are present,

Grain-size distribution

The attached chart shows the size distribution in \emptyset units.

G. E. Strong has determined the following statistical parameters following Folk's (1957) usage.

Median	n	3.1 Ø
Graphic mean $^{ m M}_2$	z	4.6 Ø
Inclusive Graphic Standard Deviation	2	3.0 Very poorly sorted
Inclusive Graphic Skewness SK ₁	ē	0.73 Very positive- ly skewed
Inclusive Graphic Kurtosis K _G	=	0, 94 Mesokurtic
(Transformed Kurtosis K	ų:	0,49)

Reference

Folk, R.L., & Ward, W.C. 1957. Brazos River Bar: a study in the significance of grain size parameters. J. Sed. Pet. 27 pp. 3-26"

Aquifer analysis: This is based on sieve and log analysis data combined with the results of testing of the individual screened sections by air lift and casing packers. Since the sands appear to be largely unconsolidated, sieve analysis data may provide a fair indication of the permeability. The correlation between permeability and grain size variations is discussed in detail in the Final Report on the Phase 1 Area (Wright et al, 1974). Permeability appears moderate in zones 'a', 'c', and 'e' of the LMM and zone 'a' of the Oligocene but lower elsewhere. The method of analysis cannot account for the presence of clay and the calculated values tend to be higher than the true values. It is worthwhile noting that zone 'b' of the Oligocene which includes appreciable amounts of fine sand or sandstone in the graphic log also shows fine sand in the sieve analysis. The feature may indicate that the sands are also unconsolidated and that the low porosity relates mainly to fine grain size. It is also significant that no production could be obtained from the screened section within this interval.

Water samples were obtained from each screened section of the hole and chemically analysed. Details of the analyses are included in the Phase 2 Report. An in-casing packer system was used in preference to an in-hole

packer on account of the likelihood of hole collapse in these unconsolidated formations. The packer used was a straddle packer which extended across the screened interval and was set mechanically. Air lifting was carried out with an air line set inside an inner casing. It was assumed that production would be mainly limited to the screened section since demudding and development had mainly been concentrated on these sections. Drawdowns were calculated on the basis of the change in pressure during air lifting.

Details of the testing are shown in Table VII. It is significant to note that no production could be obtained from level 6 which is within the fine sand or sandstone of Zone 'b' of the Oligocene and level 7 which is within sandy carbonates of the Upper Eccene. The testing did incidentically show the efficiency of the packer system across which no significant leakage can have occurred despite a head differential of over 600 feet of water. The result gives increased confidence of the validity of the other data. Static water levels appear to be uniform throughout the Post-Eocene sequence, but possibly a foot higher below interval 3 which between 1680 and 1710 feet bgl. This represents the only information on hydraulic head values in the Oligocene in the Phase 2 Area. Specific electrical conductance values are in the range 2000 - 2700 micromhos at 25° C increasing downwards. The figures can be compared with the shallow company wells set in LMM Zone (a) which produce water of 2500 micromhos/cm. Water appears to be fresh therefore down into the Zone (a) of the Oligocene and confirms the indications of the S.P. electrical log.

TABLE V
Summary of sieve analysis data

T>		~		1					_
	th Interval bgl)	D50 (microns)	D40/D90	K ¹ (US galls/d/ft ²)	Dept	h Interv	al D50	D40/D90	K ¹
(ree	, ngi/	(microns)		(US galls/d/ft ⁻)	(feet	bgl)	(microns)	D40/ D80	(US galls/d/ft ²
(i)	Calanscio	Formation	ı (Post Mid	ldle Miocene):		Zone l	di inana ese	020 50-	
	0 - 201 fe	et bgl	, 1311342			20116	u , 151VIIVI. 050	- 0/0 lee	r pgr
					66	0 670	295	1.94	310
		No San	nples		67	0 680	245	2,45	200
(::)		.			68		290	2.00	290
(ii)	Zone 'a',	Lower and	Middle Mi	ocene (LMM):	69		260	2,35	215
	201 - 386	ieet bgi			70		Sandy	Clay	
28	0 290	400	0.00		76		167	1.99	145
29		490	2.67	410	77		230	1.69	235
31		Clay		~	78		240	1.82	285
32		235	2.04	245	79		257	1.79	290
33		150 290	2.23	140	80		258	1.90	300
34		370	2.83	235	810		335	2, 3 6	390
350			2.16	340	820		275	2.57	215
360		No Sar			830		185	2.16	165
370		315 390	1.89	290	840		213	1,98	185
380		265	2.23	385	850		260	2.77	205
000	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	203	2.46	195	860	870	290	2.37	250
2	Zone 'b', I	LMM: 386	- 465 feet l	ogl		Zone 'e	, LMM: 870	- 1264 fee	et bgl
390	400	240	2, 14	195	870	088 (905	0.44	
400		Sandy (880		295 303	2.44	250
410	420	195	1,72	192	890		230	2.34	250
420	430	185	1.82	165	900		263	3,12	180
430	440	190	1.78	172	910		280	2.59	205
440	450	190	1.78	182	920		278	2, 51	195
450	460	225	2.00	215	930		255	2,62	220
460	470	215	2.00	185	940		265	2.64	200
				~00	950		285	2, 45	230
Z	one 'c', L	MM: 465 -	656 feet b	ρÌ	960		230	2.46	245
				5 -		980	255	2,60 2,36	160
470	480	240	1.95	238		1000	Sandy (188
480	490	240	2.20	220		1010	245	2.03	940
490	500	260	1.11	245		1020	250	2.03	240
500	510	222	2.06	205		1030	240	1.85	230
510	520	220	2.09	212		1040	355	2.08	250 430
520	530	315	2.03	270		1050	290	1.88	
530	540	330	2.12	180		1060	155	2.71	320 140
540	550	207	2.38	165		1070	285	2.00	280
550	560	270	2,50	235		1080	230	2.04	180
560	570	270	2.07	275		1090	230	2.21	
570	580	270	1.76	295		1100	175	1.81	180
580	590	275	2.67	205	1100		No Sample	1.01	145
590	600	360	1.94	560	1110		270	2.44	228
600	610	390	2.34	345	1120		215	1.81	
610	620	540	2.81	400	1130		295	2.34	190 260
620	630	530	3, 53	285	1140		290	1,67	390
630	640		2.00	340	11 50		450	1.60	
640	650		2.05	370	1160		285	2.03	760 290
650	660		1.73	340	1170		430	1.57	720
									120

¹ K: permeability in US galls/day/ft 2 calculated on a cross plot of standard deviation and D50

1	Denth	Interval	D50		K ¹	Donth	Interval	D50		к1
	(feet b		(microns)	D40/D90	(US galls/d/ft ²)	(feet b	gl)	(microns)	D40/D90 _{(U:}	K S galls/d/ft ²)
	•	.	,		(8 ,,,,	(0-7	(,	- 8/ -/ /
	1180	1190	430	1.61	710	1800	1810	420	2.64	340
	1190	1200	365	1.83	560	1810	1820	275	2.13	200
	1200	1210	210	2.95	165	1820	1830	245	2,24	200
	1210	1220	280	2.52		1830	1840	255	2.24	215
	1220	1230	200	2.68	150	1840	1850	230	2.08	190
	1230	1240	175	3.55	115	1850	1900		ine Sand-Silt	
	1240	1250	No Sample			1900	1910	185	2,18	142
	1250	1260	303	3,82	205	1910	1940		Silt-Clay	
	1260	1270	450	2.25	410	1940	1950	180	2,80	118
ίi	ii) <i>Z</i> .c	nne la!	Oligocene:	1264 - 17	70 feet hal	1950	1960	200	2,65	140
1-	.11/ 22/	J.10 a ,	ongocene.	1201 - 11	TO TOOL DET	1960	1970	285	2,83	203
	1270	1280	540	3,24	305	1970	1980	215	2.77	158
	1280	1290	480	5. 82	155	1980	1990	235	2.39	182
	1290	1300	410	4.95	215	1990	2000	205	2.72	155
	1300	1310	540	2.48	540	2000	2010	150	2,90	1.13
	1310	1320	290			2010	2020	135	2.87	108
	1320	1360		2, 41	225	2020	2030	150	2,50	125
				dy Clay C		2030	2040	160	2,80	125
	1360	1370	378	2.33	350	2040	2050	145	2.92	115
	1370	1380	400	2.42	370	2050	2060	175	2.86	128
	1380	1390	435	2,38	520	2060	2070	220	2.00	185
	1390	1400	415	2, 12	435	2070	2080	200	2.25	162
	1400	1420	Sandy			2080	2090	195	2,20	158
	1420	1430	445	2.02	470	2090	2100	170	2.78	130
	1430	1440	440	2.51	400	2100	2110	175	2.70	128
	1440	1450	220	2.41	170	2110	2120	230	2.75	162
	1450	1460	350	2.50	300	2120	2130	175	2.71	132
	1460	1470	390	2,22	410	2130	2140	175	2.38	138
	1470	1480	290	4.30	185	2140	2150	195	2.68	152
	1480	1490	Silt			2150	2160	190	3.07	145
	1490	1500	420	3,09	335	2160	2170	185	2.87	140
:	1500	1550	Sandy S	Silt		2170	2180	175	2.67	138
	1550	1500	203	2.86	155	2180	2190	185	2.87	140
-	1560	1570	320	3,02	250				3,68	
1	1570	1580	No San	nple		$\frac{2190}{2200}$	2200	185		139
1	1580	1590	544	3,27	390		2210	190	2.99	142
1	1590	1600	360	2.86	240	2210	2220	170	3.14	130
1	1600	1610	313	3.52	230	2220	2230	195	2.20	158
1	1610	1620	340	2.59	270	2230	2240	205	2.55	155
1	1620	1630	223	2.64	175	2240	2250	145	3.24	120
3	1630	1640	258	2,68	185	2250	2260	145	3.21	122
1	l640	1650	182	2.95	132	2260	2270	150	3.60	118
1	1650	1660	190	4.16	122					
	1660	1700	No San							
	700	1710	195	2.79	148					
	710	1720	180	2.68	135					
	720	1730	185	2,55	145					
	730	1740	200	2.35	162					
	740	1750	335	3, 52	232					
	750	1760	370	2.62	325					
	760	1770	330	2.75	275					
_		•	~~~		2.0					
	Zor	ne 'b', C	Oligocene:	1770 - 226	6 feet bgl					
	770	1780	255	2,11	235					
	780	1790	300	1.96	332					
7	700	1000	250	9 99	940					

<sup>1790 1800 350 2.23 348

1</sup> K: permeability in US galls/day/ft² calculated on a cross plot of standard deviation and D50

TABLE VI

Summarised average values of data in Table V Average Average Thickness Interval D50 K US gpd/ft² (feet) (microns) LMM Zone 'a' 185 313 280 Zone 'b' 79 205 187 Zone 'c' 191 329 283 Zone 'd' 214 253 245 Zone 'e' 394 279 274 Oligocene Zone 'a' 506 338 271 Zone 'b' 496 201 163 TABLE VII Test pumping on T(Q1-65)A 1 2 3 5 6 7 8 Remarks 1-7 None 495 38 69 2200 (x = 8)-----2 hour test 252.6 7 947-880-495 18 166 2100 (x = 20)252.39 4 hour test 997 1002 252.40 6 1094-1066-495 35 92 2160 (x = 59)252.33 4 hour test 1124 1196 252.34 5 1312-1257-495 30 148 2200 (x = 45)252,39 4 hour test 1342 1385 252,44 4 1461-1391-495 22 164 2450 (x = 45)252,31 4 hour test 1491 1522252.4 3 1680-1652-495 16 176 2700 (x = 67)251.41 4 hour test 1710 1785 251.42

Columns:

2 2012-

2042

1 2271-

2301

1978-

2109

2236-

2315

- 1. Screen setting interval in feet below ground level
- 2. Packer setting showing straddle limits

865

679

3. Depth of airline setting within inner casing attached to packer

No production

No production

- 4. Yield in US gpm
- 5. Drawdown calculated from airline pressure differentials
- 6. Conductivity of discharge in micromhos/cm at 25°C
- 7. Rest water level inside interior casing at x min after pumping stopped. NB $\,252.4$ correspond to $\,257'$ + in relation to present casing level
- 8. RWL at x + 15 min after pumping stopped

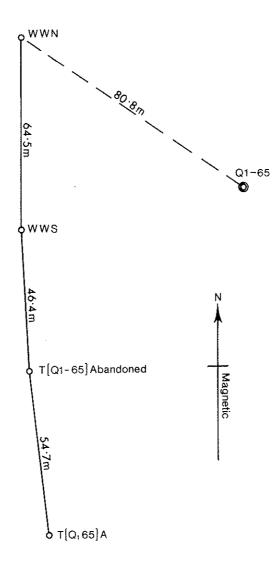


Figure 1. Site plan: T(Q1-65)

