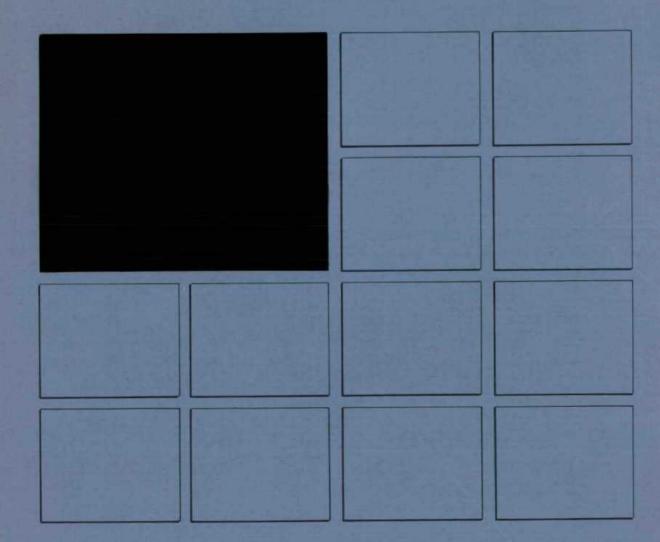


INSTITUTE of HYDROLOGY



MOGADISHU WATER SUPPLY

EXPANSION

STAGE I

This report is prepared for

Sir Alexander Gibb and Partners (Africa)

Nairobi

Kenya

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Wallingford

Oxon

UK

INTRODUCTION

The area inland of Muqdisho bounded by the Balcad and Afgooye roads and the Shabeelle River formed the area examined in the water resources study 1. The report recommended that a wellfield should be constructed close to the observation well MGQ2P on the Afgooye road.

Stage I consists of the construction of the first part of the wellfield with associated civil and electrical works. This report presents the results of the borehole construction and testing as given in Contract 1^2 .

The wellfield is situated 17.5 km from Muqdisho on the Afgooye road and is eight production wells at 300 m intervals along a bearing of 055° from MGQ2P. In addition three observation wells were also drilled in the general area to determine lithology and water quality for both Stage I and the wellfield expansion of Stage II A.

The construction phase started in June 1981 and lasted for a year. However one production well, PW4B, has not been completed at the time of reporting and results will be issued as a separate appendix. The production wells have been given the reference numbers PW1 to PW8, with PW1 being nearest to the Afgooye road. The observation wells numbers are OW1 to OW3. In the event of a borehole being abandoned the rig was moved about 20 m and the hole redrilled with the reference having the suffix A then B.

The form of this report is such that the data collected during the contract period are presented as an appendix of computer listings at the rear of the report.

In order not to interrupt the text the figures referred to in Section 2 have been inserted between Section 6 and the Data Appendix.

Muqdisho Water Supply Expansion: Groundwater Exploration and Modelling Studies, Institute of Hydrology, March 1980.

Muqdisho Water Supply Expansion: Stage 1 Works - Contract No 1 Drilling of Production Wells, Sir Alexander Gibb & Partners (Africa), October 1980.

LITHOLOGY

The lithological logs were prepared from the inspection of samples taken every three metres from the drilling returns. Electric logs were also run for single point resistance (SPR) and self potential (SP) at each site. Because of problems with the logger it was not always possible to run a log in each hole, however logs were run at every site. At sites PWlB and PW2 gamma and casing collar location (CCL) logs were also run.

Figures 2.1A to 2.10B show the logs at each site drilled. The figure numbers suffixed A show the rate of penetration log, screen setting with rest water level and the main lithological divisions with descriptions; scales showing depth below ground level and elevation relative to sea level are included also. The rate of penetration shows the time taken to drill one metre, the wear on the drill bit is not taken into account. For example the decrease in drilling rate between 170 and 195 m in PW6A is due to bit wear not to change in formation. The figures suffixed B show the electric logs with rest water level marked for reference. The casing collar log on PW1B and PW2 gives a mark at each joint of casing, the quiet section at the bottom of the log represents the screen.

The electric logs of single point resistance and self potential exhibited no unusual characteristics. The general form of the logs is similar to those run in the same lithological sequence during the feasibility study. The gamma logs on PW1B and PW2 showed that there was natural activity with some peaks. These peaks tend to be characteristic of clay horizons although there was no evidence to support this from the drilling returns. As these are the only gamma logs for the area that we have seen it is not possible to determine how characteristic they are.

The aquifer comprises of buff coloured fine grained quartz sands which contain some medium sand. The subangular to rounded quartz grains are mostly set in a carbonate matrix which forms poorly to moderately developed cementing. These buff sands were shown in our previous work to pass laterally into marine limestones nearer to the coast indicating a marine origin.

The wellfield area is blanketed by red aeolian sands which have a thickness of 40 to 65 m. These sands lie well above the watertable and are generally uncemented although there was some cementing found at PW4, PW8 and to the south west at OW3A.

About 6 km to the northwest of the wellfield lies the flood plain of the Shabeelle. Observation well OW2 was drilled to a depth of 100 m in that area and proved 35 m of alluvial silts before passing into sands. The red sands were struck at 55 m below ground level, forming in that area the aquifer, and contained carbonate cementing. The silt and sandy silts above the red sands contained gypsum in the form of crystals and also some rounded fragments of carbonate material.

WELL DESIGN AND DEVELOPMENT

All the boreholes were drilled using direct circulation rotary methods. Initially a pilot hole was drilled and from the lithological and geophysical logs the position of the screen was determined. For the observation wells no reaming was carried out.

The pilot hole for the production wells was reamed out to accept the 254 mm (10 inch) internal diameter steel casing and 30 m of 203 mm (8 inch) wire wound stainless steel screen, which had a slot size of 0.38 mm (0.015 inch). A galvanised steel pipe 32 mm in diameter was secured to the outside of the casing with an elbow welded onto the casing just above the adaptor. This 32 mm pipe provides an external dipping facility. Figure 3.1 shows the dimensions of a typical production well.

Once the screen and casing had been placed correctly the annulus was filled with a filter pack to a level of 10 m above the top of the screen. The filter pack is a rounded quartz material graded from 0.3 mm to 2.0 mm (0.012 to 0.08 inch). This grading was derived from the grading of the uncemented aquifer material as shown in Figure 3.2. There are several methods of determing the filter pack grading and the curve we have chosen falls within the envelope of the other methods. A slightly coarser filter pack, which still fell within the limits, was used for wells PW3A, 4B, 7 and 8.

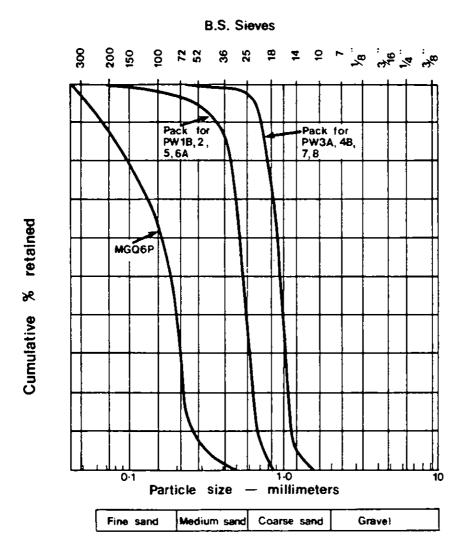
The observation wells were also constructed using steel casing and screen both of 102 mm (4 inch) diameter. However observation well OW2 was constructed using 102 mm plastic casing and slotted screen, the slot size being 0.4 mm.

Typical production well construction 444mm reamed hole 254mm LD. steel casing fitted with sprung barrel centralizer every 18 m | [3 lengths] Sand backfill 32mm steel pipe as dipping facility Crushed coral backfill 254/203 mm adaptor-381mm 30mx 203mm Johnson wire wound screen reamed hole Graded siliceous with 0.38mm slot size sand filter 3m×203mm plain steel sediment sump with blanked base Sand backfill

Figure 3-1

-244mm pilot hole

Filter pack grading curves



The drilling fluid used was Revert made by Johnson Well Screens Ltd. This fluid is an organic polymer which breaks down, looses it's viscosity, under bacteorological action or by using a suitable chemical. Because of the high ambient temperature the fluid would have broken down too quickly so that a temperature stabiliser also had to be used to maintain the drilling properties.

Following the construction of the wells, the wells have to be cleaned and developed so that the full potential can be realised. The development removes the effects of drilling by breaking down the drilling fluid coating the borehole walls and invading the aquifer and then removing the fines from the aquifer and filter.

The manufacturers of the drilling fluid specified a chemical breaker which causes the fluid to loose its cohesive properties. However because of the fine grained nature of both the aquifer and filter pack there was difficulty in getting the breaker into contact with the fluid. Initially a variety of standard methods were used but in later wells a combination of introducing the breaker with the filter pack and then jetting in additional breaker was more successful.

With organic polymers such as Revert some of the breakdown is caused by micro-organisms and the use of stabilisers in effect disinfects the drilling fluid. This then creates additional breaking problems as under normal circumstances the fluid would break down without any additional breaker needed, hence making it easier to remove invading fluid from the aquifer.

For the removal of the fines the best method adopted was that using the test pump and surging the well. It was not possible to develop the wells to the recommended one and a half times the production yield because of pump capacity limitations, however development up to $80 \, \mathrm{m}^3 / \mathrm{hr}$ took place until there was no further significant improvement in the drawdown characteristics, when the well was then tested.

The observation wells were firstly broken by the addition of breaker with the filter pack. Further breaker was then added to the well which was then airlifted. Airlifting continued until the sand content was at a minimum.

As the aquifer material is very fine grained the problem of sand entering the pumped well is a recurrent one in the area. However with the pack grading and screen slot size that we selected this problem appears to have been overcome. Because of the aquifer grading there is little chance of developing a natural pack around the screen. This means that unless there is a complete filter pack surrounding the screen then the well will always be producing some sand and indeed this is possibly the reason that wells PW3 and PW4 have had to be redrilled.

PUMP TESTING

After there appeared to be no more significant improvement with development the production wells were test pumped. The testing consisted of step drawdown tests of either 4 or 5 stages each of two hours duration, these tests provide information on yield drawdown characteristics, borehole efficiency and also give an estimate of transmissivity.

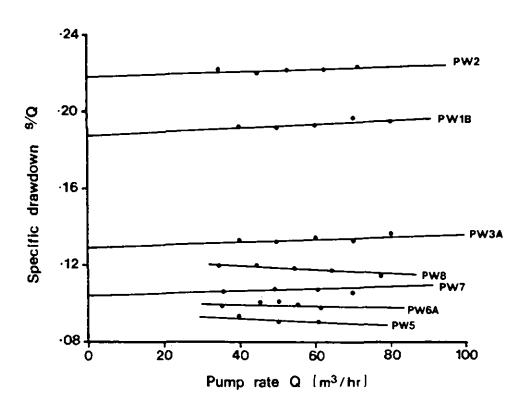
It is possible to separate the total drawdown into aquifer loss which is caused by the resistance of the aquifer to flow, and the well loss which is caused by turbulent flow within and around the well. The well efficiency is defined as the aquifer loss expressed as a percentage of the total drawdown.

The results of the seven steptests are shown as specific drawdown and yield drawdown curves in Figure 4.1, the data and time drawdown plots for the tests are presented in the Appendix. Of these tests three, PW5, 6A and 8, could not be interpreted as they display a decrease in specific drawdown with an increase in discharge. This is an indication of incomplete development despite the extensive airlifting and pump development programme carried out.

Two wells were retested during the pumping programme. Initially PW2 had a yield of just over $10m^3/hr$ but after a long programme involving additional breaking as well as airlifting the yield was improved. The initial test is shown as a broken line. PW5 was also retested and although it showed an improvement it was still not fully developed.

Table 4.1 gives the well efficiencies for the four tests solved. These are all over 95% at the highest rate of pumping tested. This means that over 95% of the drawdown observed in the well is caused by the aquifer showing that the well design is correct.

Yield - Specific drawdown curves



Yield- Depression curves

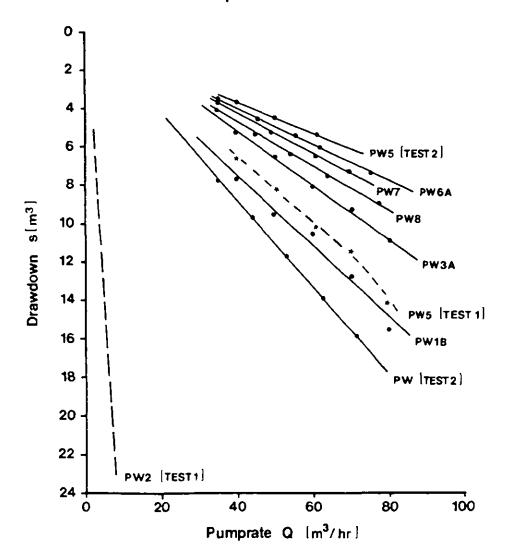


Figure 4.1

Well Efficiency and Transmissivity - Stage I Wells

	Discharge m ³ /d	Efficiency %	Transmissivity m ² /d
PW1B	960 ·	98	2520
	1200	97	
	1440	96	
	1680	96	
	1920	95	
PW2	833	99	1510
	1058	99	
	1270	99	
	1498	98	
	1704	98	
PW3A	960	98	1960
	1200	97	
	1440	96	
	1680	96	
	1920	95	
PW7	847	98	1560
	1178	97	
	1452	96	
	1668	96	

The reason for the difficulty in fully developing the wells probably lies with the very fine nature of the aquifer. As the filter pack is related to grain size of the aquifer it follows that a combination of thick pack with its fine grain sizes also prevents ready access to the drilling fluid coating the borehole walls. By introducing breaker with the filter pack some of this problem was overcome but not entirely and it then becomes a balance between achieving the best development within the most optimum time. As the drilling fluid will degrade with time there should be an improvement in the underdeveloped wells as time passes.

An estimate of the aquifer transmissivity is possible using Jacob's approximation for the first stage data. For the four tests which offered solutions the transmissivities fell within the range 1510 to $2520m^2/d$ which compares favourably with the regional value of $1960m^2/d$ assumed for the 1980 model studies.

WATER QUALITY

In the course of the construction water samples were taken from all three observation wells just before the airlift was completed. Pumped samples were also taken at the end of the steptests on production wells PW2, PW5, PW6A and PW8. These samples were subsequently analysed at IH for the major ions and electric conductivity. The pH values given were those recorded in the field at the time of sampling. There was a delay between sampling and analysis which may have had some effect on the calcium and bicarbonate values. The results, table 5.1, include a value for total dissolved solids (TDS) which is a computed value from the ion determinations instead of a direct measurement.

When compared with the chemistry of MGQ2P, also included in the table, taken in 1978, there is a significant increase in the concentrations of most ions particularly magnesium and sulphate. We have also compared the results with those from the coastal observation wells (MGQ1CP - 3CP). It seems almost certain that the mineralisation is not caused by saline intrusion as the sodium and chloride levels in the new results are relatively low.

In terms of potability the analysis are classed according to the WHO standards as given in Appendix C of our 1980 Report. In all cases the sulphate concentration and most of the total dissolved solids are higher

Water Quality - Stage I Wells
(Ionic concentrations in milliequivalents per litre)

	OW1B	OWS	OW3A	PW2	PW5	PW6A	PW8
Date	15.12.81.	11.11.81.	11.12.81.	26.2.82.	26.10.81.	4.12.81.	21.12.81.
TDS mg/l	2803**	1312*	1866**	1540*	2169**	2689**	2208**
E.C. μs	3350	1500	2450	2000	2850	2800	2650
рH	8.0	8.2	7.9	7.7	7.8	7.8	
Ca	11.1**	4.4*	10.8**	10.5**	9.2*	11.6**	11.8**
Mg	13.5**	5.8*	11.5*	8.9*	11.5*	19.3**	22.2**
Na	15.7	8.7	5.7	3.5	12.6	9.6	4.8
K	0.3	0.1	0.3	0.3	0.2	0.2	0.4
нсоз	5.3	3.5	7.1	6.2	7.3	7.1	6.7
SO ₄	30.2**	11.5**	13.5**	12.5**	18.7**	26.0**	16.7**
Cl	7.3*	4.5	8.2*	3.9	5.4	8.7*	10.2*
NO ₃	0.3	0.4	<0.1	0.2	0.2	<0.1	0.1

^{*} indicates a concentration which exceeds WHO highest desirable level

^{**} indicates a concentration which exceeds WHO highest permissible level

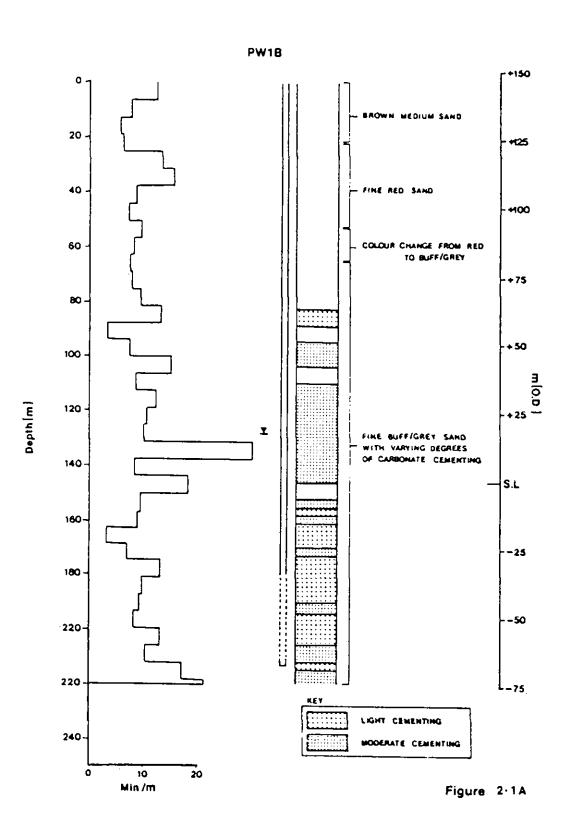
than the maximum permissible level with calcium, magnesium and chloride mostly greater than the highest desirable level. Generally the concentrations recorded suggest that the palatability of the groundwater may be impaired but should not necessarily be harmful.

WELLFIELD OPERATION

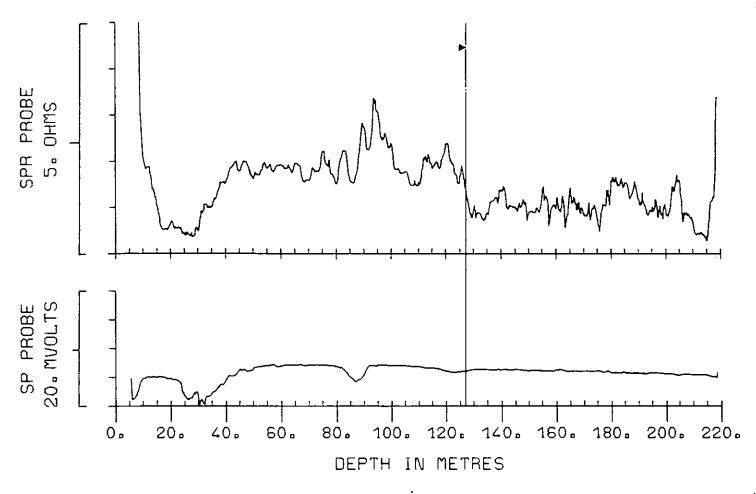
In view of the importance of a potable water supply additional monitoring should be undertaken to ensure that the response of the aquifer is as was predicated and that any deterioration in quality is detected at the earliest possible time.

For monitoring purposes the three observation wells drilled should be maintained and the water levels measured. Additional routine water level measurements should be taken at MGQ1P, 2P, 4P and 10P and at each production well. To compliment these data the volume of water abstracted from each well should also be recorded. The water levels should be measured monthly within the wellfield and every two months elsewhere, with the abstraction rates recorded weekly. These data will enable a check to be made on the behaviour of the wellfield against predictions. It is important to note that our models were based on an annual abstraction of 4.2 million m³/year (60m³/hr per well) for the Stage I wellfield.

Quality monitoring should be carried out on a routine basis of monthly electrical conductivity measurements of each well. At half yearly intervals water samples for major ion analysis should be taken from each well or if a rapid increase in conductivity is found. Annual conductivity profiles should be determined in all the observation wells where water levels are recorded. This should then give an indication if water of a different quality is being drawn into the wellfield area.



PRODUCTION PW1A



PRODUCTION WELL PW1B

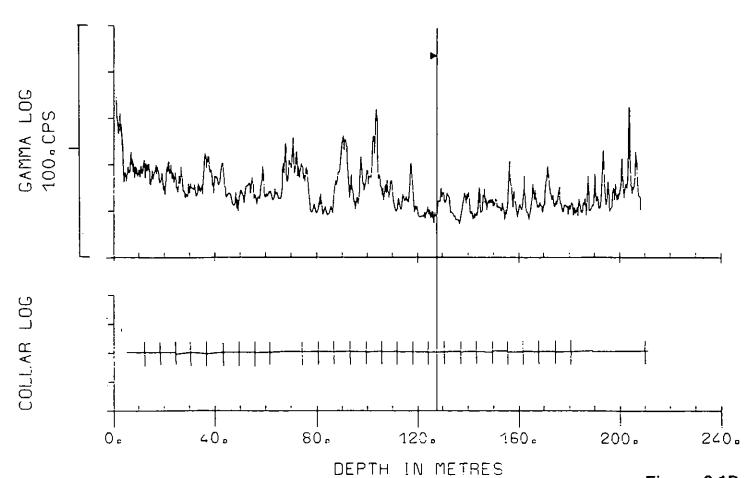
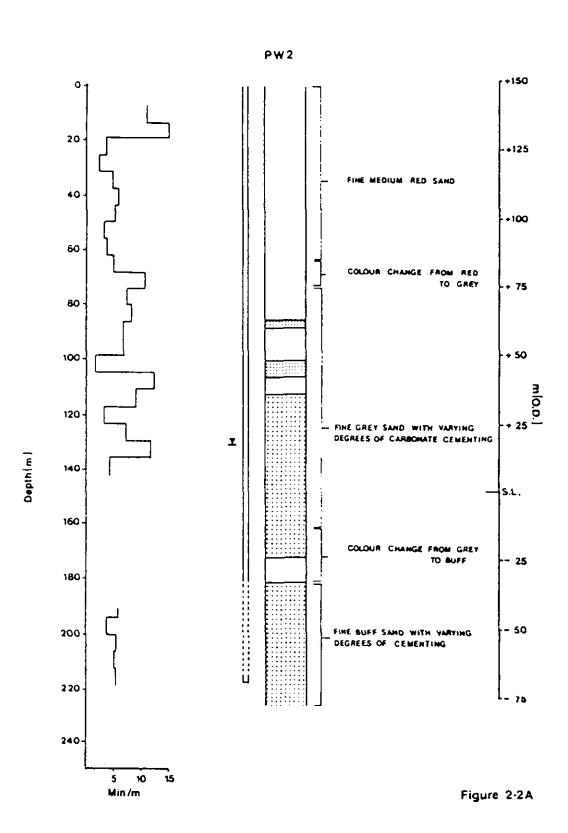
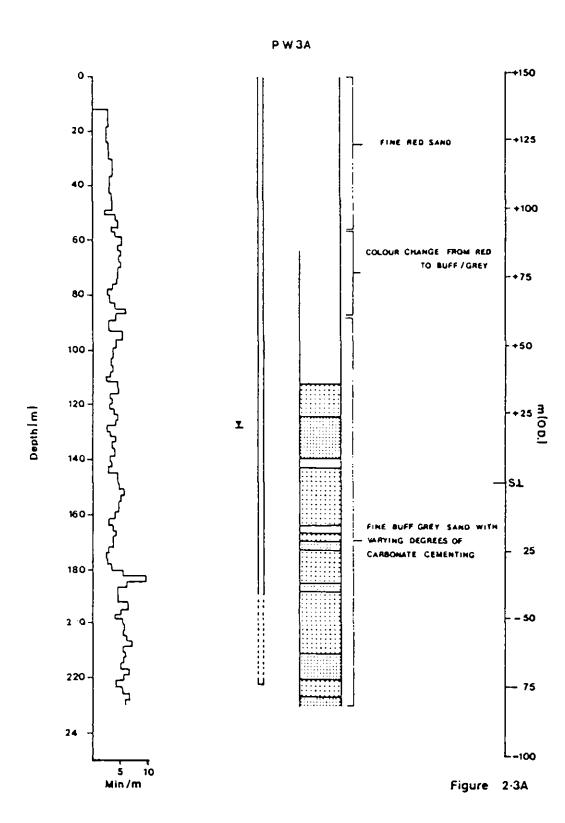


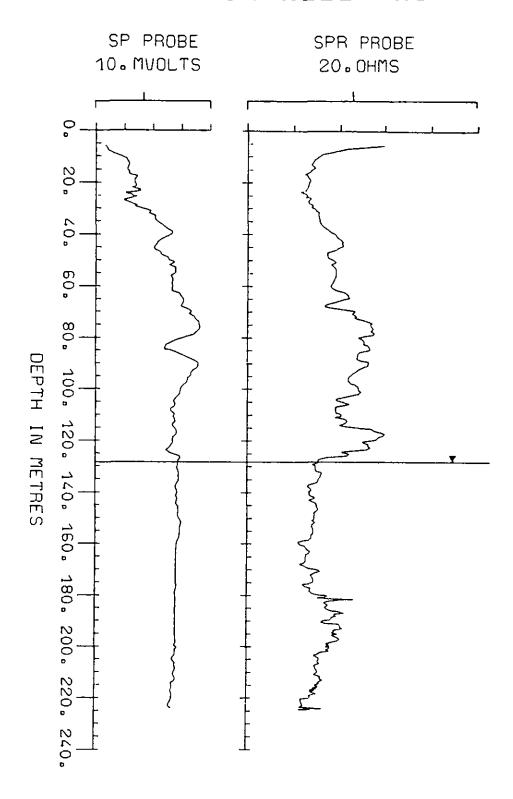
Figure 2.1B

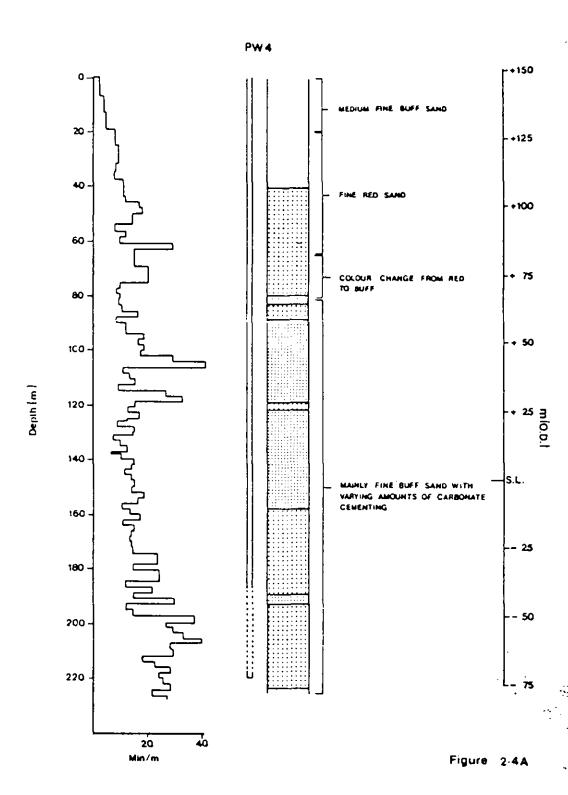


PRODUCTION WELL PW2 SPR PROBE 5. OHMS SP PROBE 20. MVOLTS 180. 200. 220. 240. 40. 160. 120. 140. 0. 20. 60. 80. 100. DEPTH IN METRES GAMMA LOG 100,CPS COLLAR LOG 0. 40. 80. 120. 160. 200. 240. DEPTH IN METRES

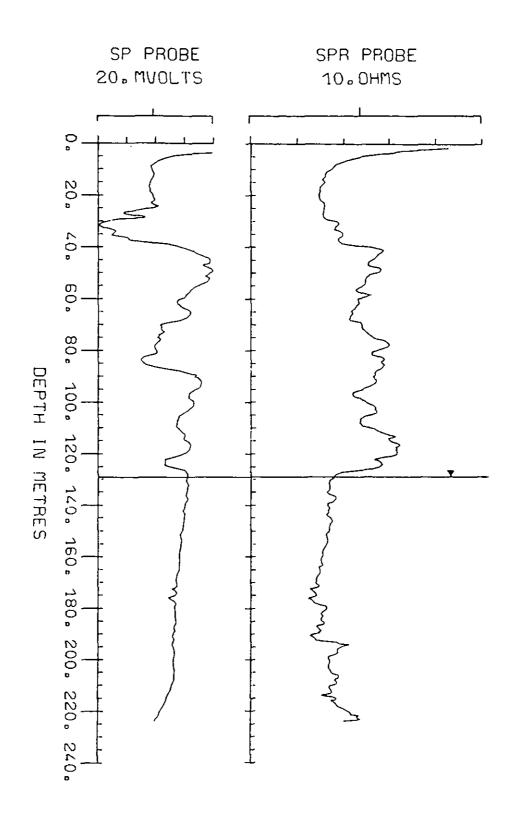
Figure 2.2B

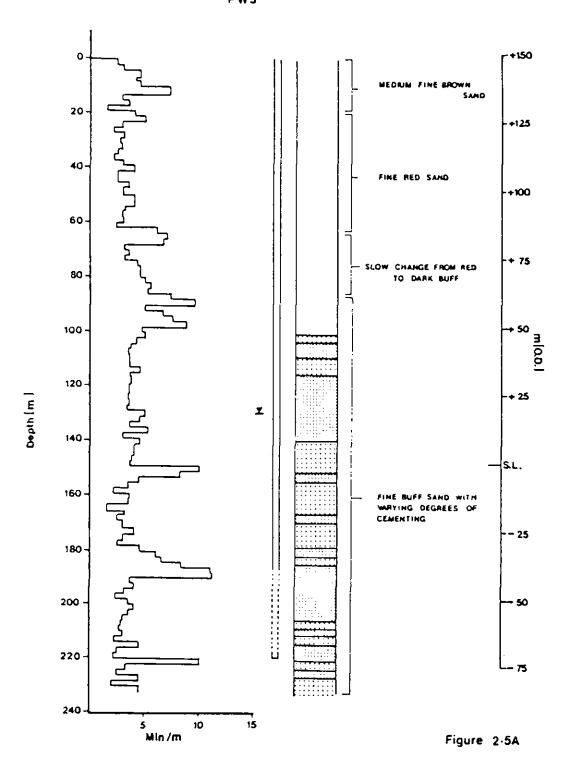


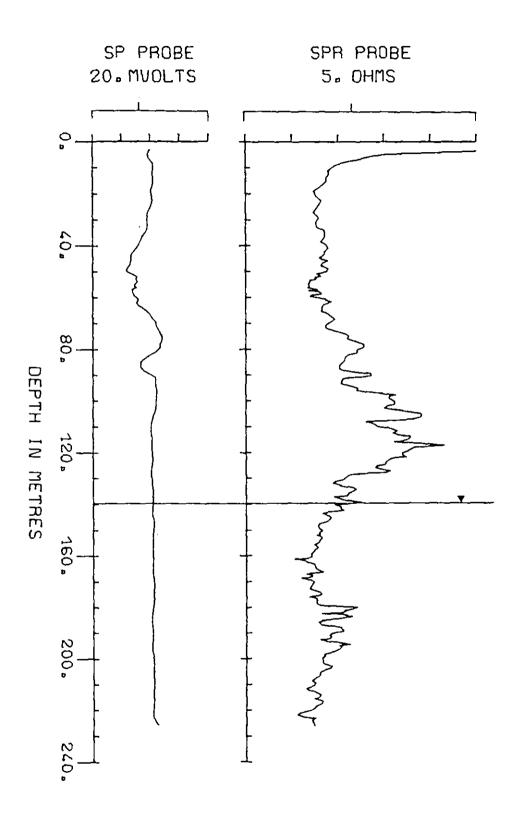


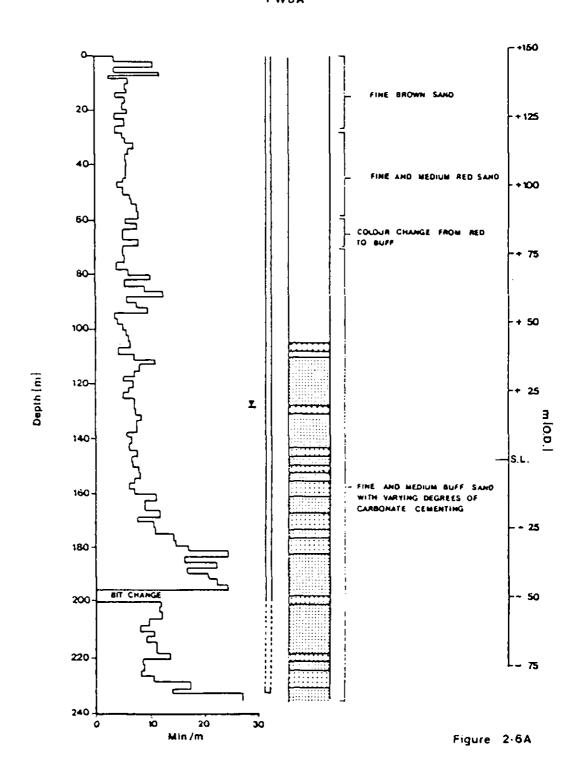


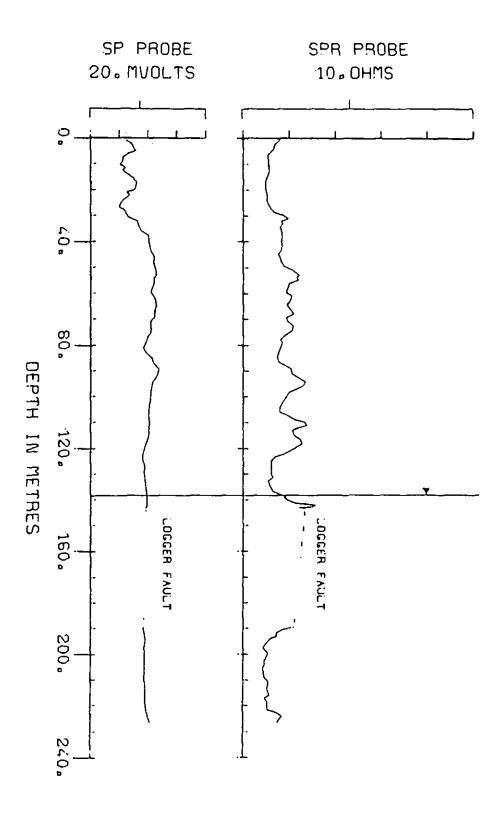
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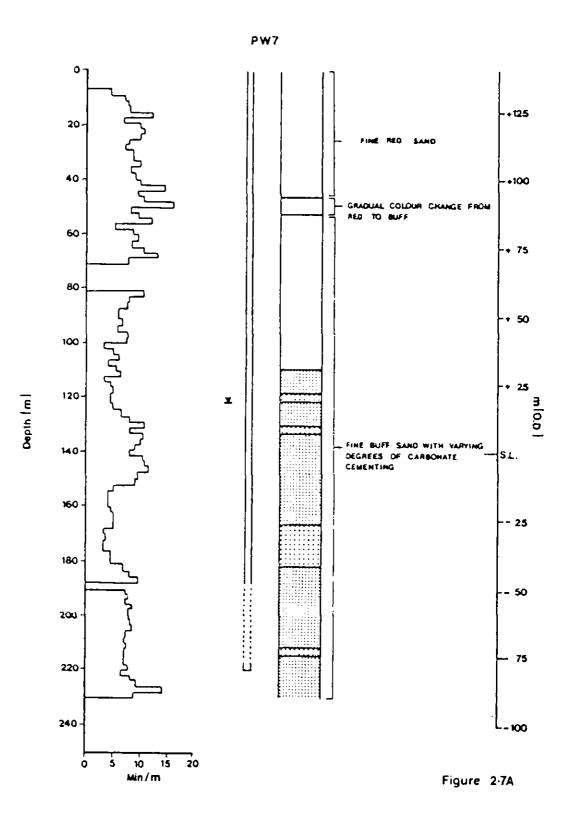


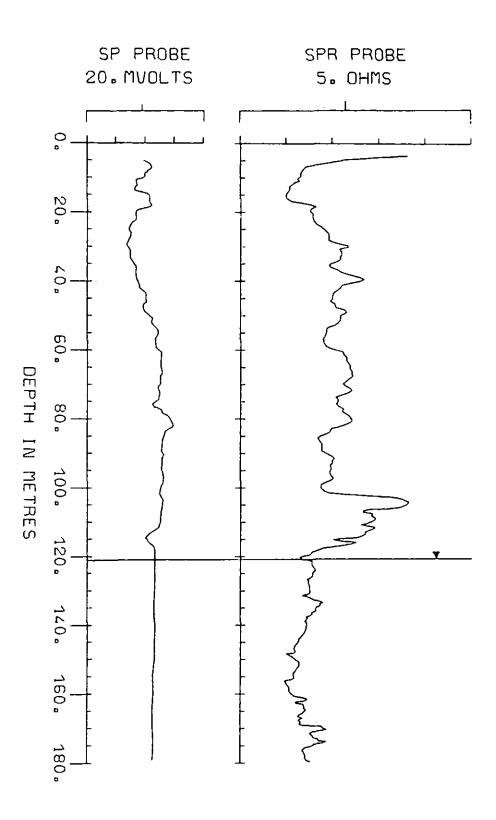


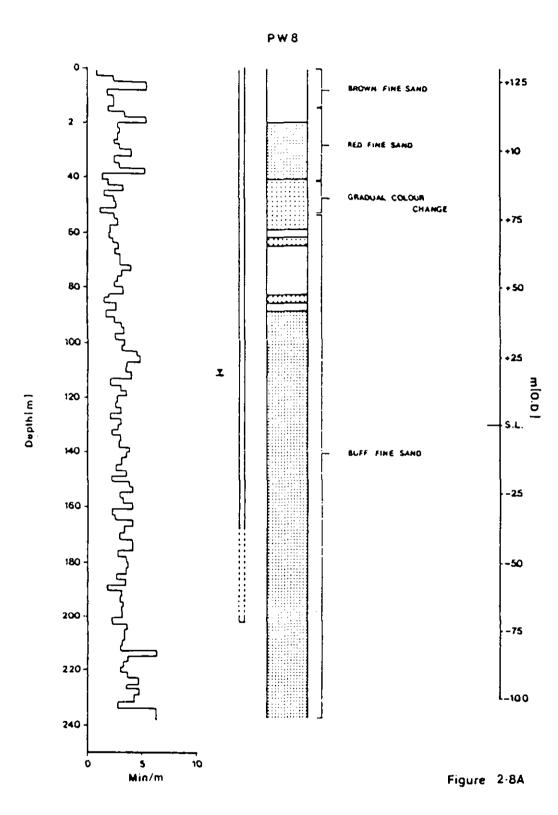


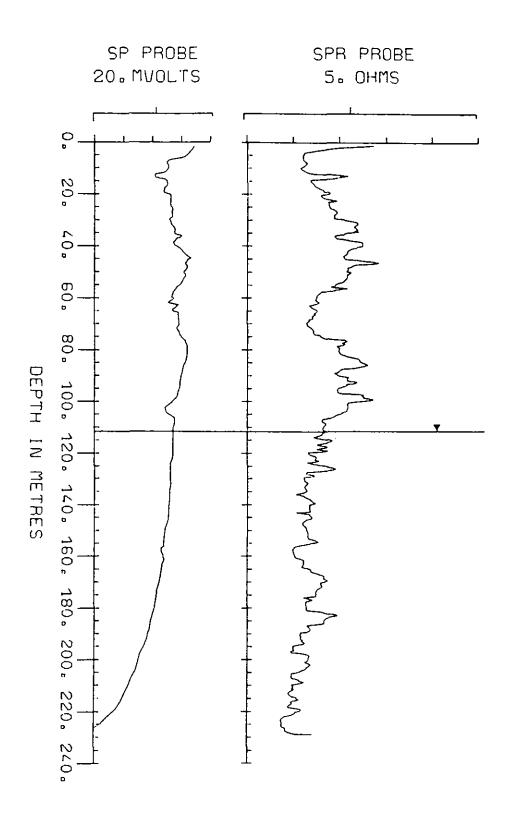


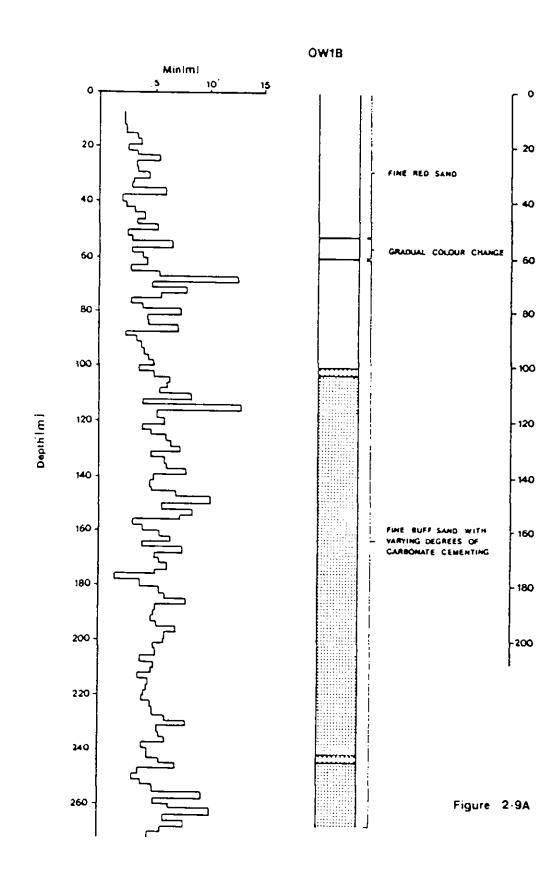




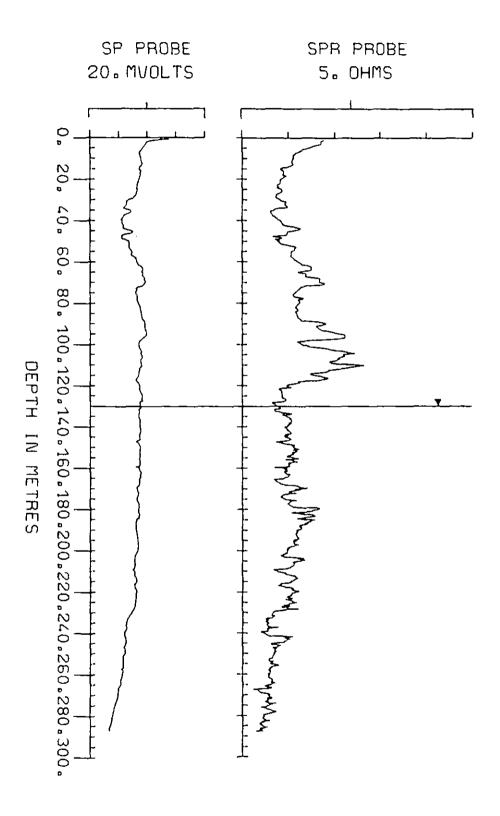








OBSERVATION WELL OW1A



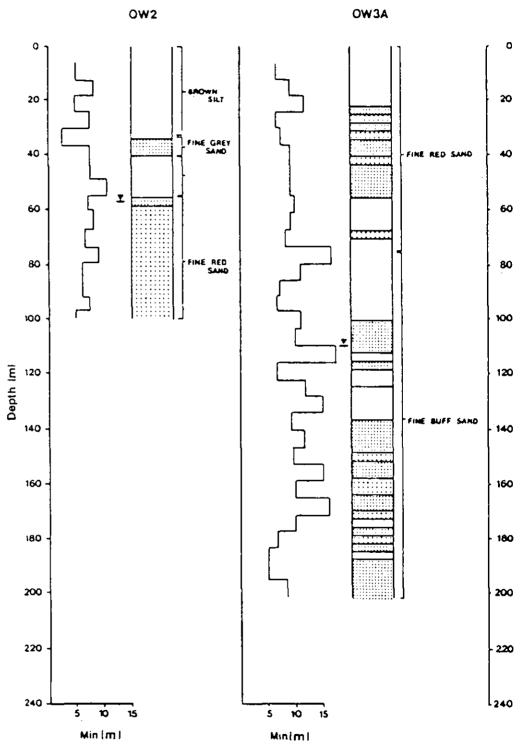
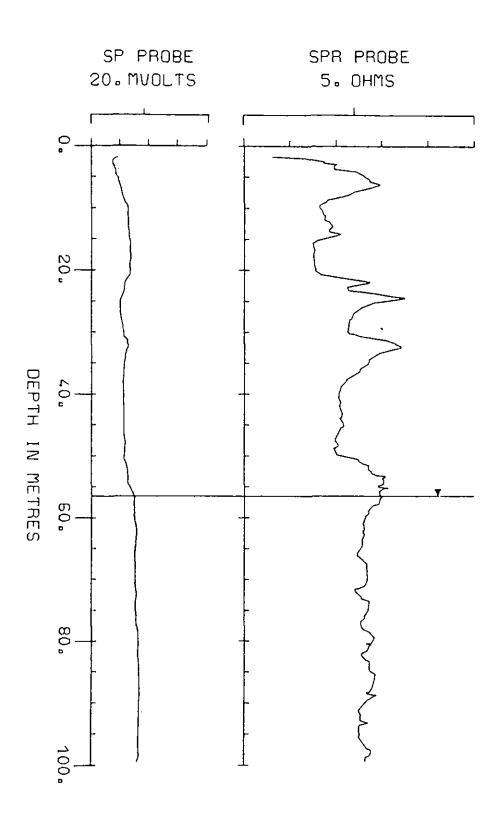
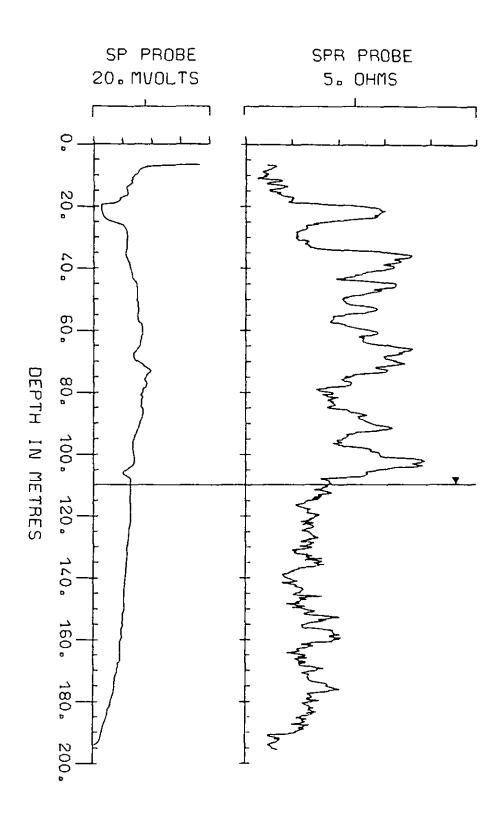


Figure 2:10A

OBSERVATION WELL 0W2



OBSERVATION WELL 0W3



DATA APPENDIX

This appendix presents the data collected during the Stage I construction period. It has been divided into three sections

Well location and construction details

Pump test data

Water levels

The well location list gives details of the grid reference, well number and a brief description of the location. The site summary lists the construction details such as the depth of the screens.

Pump test data present the data in graphical form and as lists of time drawdown numbers, the pump rates are given at the head of each site.

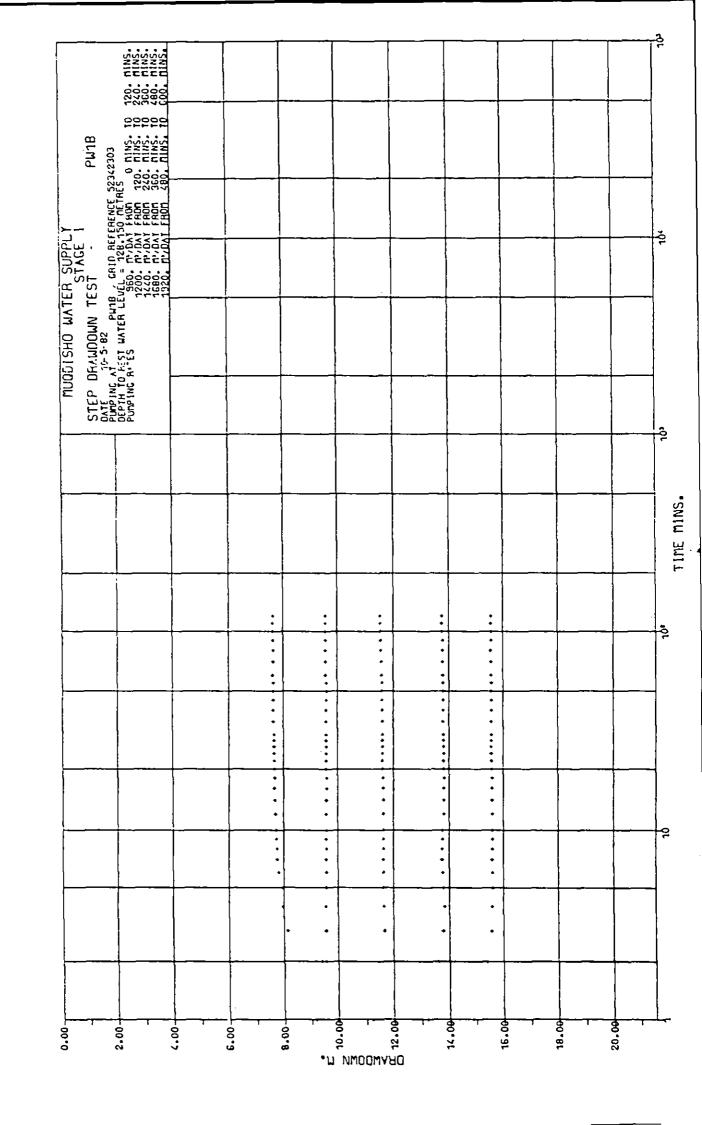
The water level listing presents the depth to water measurements taken at each site between May 1981 and April 1982. The station called 'River' gives the Shabeelle stage levels at the old road bridge Balcad.

All computer lists are given in order of ascending grid reference. Details of the wells shown in the water level list but not in the well location are to be found in Appendix A of our 1980 report. All grid references have been taken off the NA-38 series of maps.

3212 23	WEEL NUMBER	SRID REE
. Will 4.3KM SE OF AFGORYE	S.M.S.	51472334
. WELL 4.5KM WEST OF PW18	2W3-	51 912293
D. WELL 150M NO OF AFGCOYE RO.	PW13	52342383
D. WELL ASOM ME OF AFGOOME RD.	PW?	52352303
D. WELL 750M WE DE AFGORYE RD.	- W34	52402307
. KECL 26M FROM PK5	0w13	52422313
D. WELL 1350M ME OF AFGOOME RO.	PW5	52432311
9. WELL 1530M NE OF AFGOOYE RD.	PWSA	52452313
D. WELL 1980M WE OF AFSORYE RD.	247	52432313
D. WE 2230M NE OF AFGCOYE RD.	5 (a.)	52532317

				MUDDISHD W	ATER SUPPLY
					STAGE I
					ITE SUMMARY
3810 REF	51472334		52342303		52402307
WELL NUMBER	2.42	043A	PW18	₽₩2	2 E W G
SASIN			1	1	1
AQUIFER Source			1 2 3	1 2 3	1 2 3
			_	_	
CONTRACTOR	MOWLEM/WOA	MOWLER/WD#	AGWL SM/WGA	ACWINELWOM	MOWLEM/WOA
CONSTR. DATE	MOV	080 31	7 406 31	28 AUG 81	11 APR 32
DEPTH	130.350	292.300	218.590	221.000	230.500
PUTAC	0.000	128.300	145.800	148.300	145.200
JASING TYPE	PLASTIC	STEEL	STEEL	STEEL	STEEL
DIAMETER	0.132	0.102	0.254	0.254	0.254
SCREEN TYPE	3.43MS_57	MMAIRE	O.4MMWIRE	O.4MMWIRE	O.4MMWIRE
DIAMETER	7,152	0.172	0.203	0.293	0.203
SCREENS					1
DEPTH 1	73 . 000	92.D.	1.1.330	131.000	190.000
LENGTH 1	15.300	2 Miles	30.000	33.000	30.000

				MUQDISHE W	ATER SUPPLY
				S	STAGE I ITE SUMMARY
3910 985			2432313		
Wāli NUMber	D₩14	2.1.3	P W 5 A	PW?	୨୷୧
34SIN 410I5ER			1	1	1
500805			1 2 3	1 2 3	1 2 3
CONTRACTOR	MGWLEM/WD4	WLEM/WDW	MOREEM/WOA	MOWLEM/WOA	ACKYMBINOM
SONSTR. JATE	336	5 E P	TR DCT 81	11 NOV 31	3 DEC 31
DEPTH	305.000	232.300	237.000	197.000	237.000
5 A T U Y	140.500	14 .202	146.900	140.230	130.200
CASING TYPE	STEEL	STEEL	STEEL	STEEL	STEEL
DIAMETER	0.157	. 254	0.254	0.254	9.254
SCREEN TYPE	nawiri	4 MM WIR ±	P. AMMWIRE	0.4MMWIRE	O.4MMWIRE
BIAMETER	0.102	;77	0.203	0.203	0.203
SCREENS					
0:PTS 1	٤٤٥.	7.30	199.000	235.000	169.600
LENGTH 1	1 2.)*	A.300	30.000	30.000	30.000



• - • - • - • - • • • • •

STEP DRAWDOWN TEST - PUMPED WELL

PUMPING AT PW18 GRID REF. 52342303

DATE OF TEST 10 5 82

PUMPING RATES (M*+3/DAY) :

950.0	हर्ञ	0.0	4115	1.3	120.0	MINS
1200.0	EROM	120.0	MINS	70	240.0	MINS
1440.0	#ROM	240.0	MINS	TC	350.0	MINS
1033.0	FROM	360.0	MINS	T 0	435.0	RINS
1920.0	FROM	480.0	MINS	ΤO	a 33.0	MINS

REST WATER LEVEL 128.150 METRES BELOW DATUM

TIME(MINS)	DRAWDOWN(M)	TIME(MINS)	DRAWDOWN (M)
1.0	2.950	125.0	9.560
2.0	9.550	126.0	9.500
3.0	8.123	127.0	9.570
4.0	7.950	128.0	9.570
5.0	7.933	129.0	9.560
٥. ن	7.790	130.0	9.570
7.0	7.750	132.0	9.570
ទ.០	7.750	134.0	9.570
٠.٥	7.720	135.0	9.530
10.0	7.710	138.0	9.580
12.0	7.700	140.0	9.570
14.0	7.530	142.0	9.570
16.0	7.550	144.0	9.570
13.0	7.553	146.0	9.530
20.0	7.550	143.0	9.570
22.0	7.550	150.0	9.560
24.0	7.550	155.0	9.530
2ລ.ປີ	7.350	160.0	9.570
23.0	7.550	155.0	9.580
30.0	7.540	170.0	9.590
35.U	7.530	175.0	9.580
40.9	7.620	180.0	9.570
45.0	7.520	190.0	9.560
50.0	7.520	200.0	9.550
55.0	7.520	210.0	9.560
♦0.5	7.613	220.0	9.560
72.J	7.530	230.0	9.560
30.0	7.130	240.0	9.560
90.0	7.513	241.0	11.230
190.0	7.520	242.0	11.600
110.0	7.513	243.0	11.570
120.0	7.520	244.0	11.550
121.0	≎.170	245.0	11.630
122.0	9.393	245.0	11.540
123.0	9.550	247.0	11.540
120	9.550	248.0	11.540

STEP DRAWDOWN TEST -	- PUMPED WELL
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PUMPING AT PW18 GRID REF. 52342303

DATE OF TEST 10 5 82

		54:1 5 1131	10 7 62
TIME (MINS)	DRAWDOWN(M)	TIME (MINS)	DRAWDOWN (M)
249.3	41.543	303.0	13.800
250.0	11.543	კიე.ე	13.300
252.0	11.542	395.0	13.790
254.0	11.550	400.0	13.790
255.3	11.640	425.0	13.790
253.0	11.520	410.0	13.790
200.0	11.520	415.0	13.790
262.0	11.410	420.0	13.790
264.3	11.512	430.0	13.750
266.0	11.610	440.0	13.780
263.0	11.610	450.0	13.780
270.0	11.510	- £3.0	13.760
275.0	11.520	479.0	13.760
280.3	11.510	480.0	13.700
285.0	11.500	481.0	14.350
290.0	11.570	482.0	15.400
295.0	11.539	433.0	15.580
		434.0	15.600
300.3	11.503	485.0	15.620
310.0	11.590	480.0	15.510
320.0	11.570	437.0	15.520
330.0	11.550	497.0 498.0	15.520
340.0	11.560		15.620
350.0	11.550	439.0	15.610
360.0	11.550	490.0	
301.0	13.220	492.0	15.620
362.0	13.513	494.0	15.610
303.0	13.720	496.0	15.610
354.0	13.545	498.0	15.510
355.j	13.780	500.0	15.500
300.0	13.750	502.0	15.600
307.3	13.750	504.0	15.590
308.0	13.750	506.0	15.570
364.0	13.750	503.0	15.580
370.0	13.750	510.0	15.590
372.0	13.820	515.0	15.590
374.Ū	13.810	520.0	15.600
375.0	13.810	525.0	15.590
373.9	13.320	530.0	15.530
530.0	13.829	535.0	15.590
352.0	13.810	540.0	15.590
354.0	13.310	550.0	15.580
33 0. 0	13.800	5 50. 0	15.570

(CONTINUED)

MUGDISHO WATER SUPPLY

STAGE I

STEP DRAWDOWN TEST PUMPED WELL

PUMPING AT PW18 GRID REF. 52342303

DATE OF TEST 10 5 82

TIME(MINS)	DR4WD0WW(M)
570.0	15.530
550.0	15.590
590.0	15.580
500.J	1\$.380

STEP DRAWDOWN TEST - PUMPED WELL

PUMPING AT PW2 GRID REF. 52362305

DATE OF TEST 26 2 82

PUMPING RATES (M++3/DAY) :

332.3	FROM	0.0	2115	TO	120.0	MINS
1053.4	FROM	120.0	MINS	TO	240.0	MIRS
1209.5	FROM	240.0	MINS	TΒ	360.0	MINS
1497.6	FROM	360.0	MINS	Ŧ٦	480.0	MINS
1705-4	EROM	430.0	6.7 M/S	TΩ	233.0	MINS

REST WATER LEVEL 130.575 METRES BELOW DATUM

TIME (MINS)	ORAWOOWN(M)	TIME (MINS)	ORAWDOWN(N)
1.0	9.230	125.0	9.720
2.3	3.220	125.0	9.720
3.0	7.590	127.0	7.740
4.0	7.550	128.0	9.740
5.0	7.570	129.0	9.740
6.0	7.540	130.0	9.740
7.C	7.520	132.0	9.730
ð.U	7.530	134.0	9.730
ម.ប	7.503	136.0	9.730
10.3	7.633	138.0	7.740
12.3	7.610	140.0	9.740
14.0	7.500	142.0	₹.720
15.0	7.623	144.0	9.770
13.0	7. 5t3	146.5	9.780
20.5	7.530	143.0	9.740
22.0	7.570	150.9	9.770
24.0	7.693	155.0	9.720
25.0	7.690	160.0	9.720
22.0	7.050	165.0	9.720
30.0	7.590	170.0	9.720
35.0	7.730	176.9	9.740
40.0	7.710	190.0	9.740
45.0	7.700	199.0	9.770
50.0	7.593	200.0	9.760
55.0	7.700	210.0	9.77D
ەن. ق	7.590	220.0	9.770
70.0	7.720	230.0	9.770
30.0	7.720	240.0	9.750
90. 0	7.710	241.0	11.420
100.0	7.712	242.0	11.500
110.0	7.710	243.0	11.690
120.0	7.710	244.0	11.730
121.0	9.470	245.0	11.720
122.0	7.590	246.0	11.719
123.0	4.599 	247.0	11.700
124.0	2.720	248.0	11.730

STEP DRAWDOWN TEST - PUMPED WELL

PUMPING 4T PWR GRID REF. 52362305

DATE OF TEST 26 2 32

		9412 OF 1231	20 2 32
TIME (MINS)	DRAWDOWN (M)	TIME (MINS)	CM) NWOOWARC
249.0	11.732	388.0	13.860
250.0	11.730	390.0	13.860
252.0	11.710	395.0	13.900
254.0	11.739	400.0	13.850
256.0	11.730	405.0	13.360
258.0	11.730	410.0	13.360
260.0	11.790	415.0	13.360
202.3	11.750	420.0	13.360
264.0	11.730	430.0	13.560
265.0	11.723	440.0	13.360
258.0	11.719	450.0	13.350
270.0	11.747	450.0	13.370
275.0	11.732	470.0	13.370
280.0	11.713	430.0	13.910
235.0	11.730	481.0	15.460
290.5	11.592	432.0	15.750
295.0	11.753	430.0	15.310
300.0	11.740	434.0	15.330
310.0	11.7:3	435.0	15.330
320.0	11.750	4% 5. 0	15.330
330.0	11.745	487.0	15.340
340.U	11.7:2	483.0	15.360
350.0	11.750	439.0	15.860
360.0	11.770	490.0	15.860
361.0	13.650	492.0	15.360
352.0	13.820	494.0	15.850
363.0	13.250	495.0	15.350
364.0	13.350	498.0	15.860
365.0	13.879	500.0	15.870
300.0	13.890	502.0	15.860
367.0	13.370	504.0	15.360
308.3	13.250	506.0	15.370
369.0	13.370	503.0	15.860
370.0	13.370	513.0	15.360
372.0	13.360	515.0	15.350
374.0	13.870	523.0	15.370
376.0	13.830	525.0	15.350
373.3	13.550	330.0	15.370
350.0	13.380	535.0	15.330
352.3	13.370	540.0	15.860
384.0	13.050	550.0	
		560.9	15.860 15.880
305.0	13.350	255.3	15.380

(CONTINUED)

MUGDISHO WATER SUPPLY

STAGE I

STEP DRAWDOWN TEST PUMPED WELL

PUMPING AT

PW2 GRID REF. 52352305

DATE OF TEST 26 2 82

TIME(MINS)	DRAWGEWN(M)
570.0	15.670
580.0	15.330
594.3	15.390
500.0	15.390

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STEP DRAWDOWN TEST PUMPED WELL

PUMPING AT PWSA GRID REF. 52402307

DATE OF TEST 29 4 82

PUMPING	RATES	(M**5/)	(Y2)	:
953.0	FROM	0.0	MINS	70
4 3 6 6 7				

, , , ,	7.0	J. U	1.1 7 1.4 2	_	ل⊹متن ∟ ا	T i/ 🤈
1290.9	FROM	120.0	MINS	TD.	240.0	MINS
1440.0	FROM	243.0	MINS	7.0	350.0	MINS
1650.0	FROM	3გე.ე	MINS	70	430.0	RINS
1927.0	FROM	435.0	対す扱く	T 7	<u>ለበግ.በ</u>	MTHS

REST WATER LEVEL 128.380 METRES BELOW DATUM

TIME (MINS)	ORAWBOWK (M)	TIME(MINS)	DRAWDOWN(M)
1.0	5.625	125.0	6.700
2.0	5.450	126.0	5.590
3.0	5.420	127.0	6.700
4.0	5.340	128.0	6.550
5.0	5.273	129.0	5.550
ა. მ	5.270	130.0	6.520
7.0	5.250	132.0	5.530
8.0	5.240	134.0	5.520
ହ.୍ତ	5.240	135.0	6.520
10.0	5.230	135.0	6.530
12.0	.5.230	140.0	5.590
14.0	5.230	142.0	5. 590
16.3	5.220	144.0	6.590
18.J	5.310	146.3	6.530
20.0	5.290	143.0	6.580
22.0	5.320	150.0	5.530
24.0	5.320	155.0	5.570
20.0	5.300	160.0	5.580
28.0	5.300	165.0	5.530
30.0	5.310	170.0	5.570
35.0	5.310	175.0	á.570
40.0	5.250	190.0	6.500
45.0	5.300	193.0	6.570
30 . 0	5.290	200.0	5.570
35.0	5.290	210.0	ó.58D
ამ. ა	5.290	220.0	5.590
70.0	5.300	230.0	6.590
30.0	5.230	240.0	5.580
90.0	5.290	241.0	7.960
100.0	5.320	242.0	7.980
110.0	5.313	243.0	7.940
120.0	5.310	244.0	მ. ესე
121.5	5.570	245.0	3.010
122.0	5.523	345.0	გ.ევე
123.3	⊅. 059	247.0	3.010
124.0	5.673	243.0	3.020

STEP DRAWDOWN TEST PUMPED WELL

PUMPING AT PWSA GRID REF. 52402307

DATE OF TEST 29 4 32

		JA12 5: 1251	27 4 32
TIME (MINS)	DAAWDOWN(M)	TIME (MINS)	DRAWDOWN (M)
249.0	9.010	388.0	9.280
250.0	3.000	390.0	9.290
252.3	7.973	395.0	9.300
254.0	7.950	400.0	9.300
250.0	8.020	405.0	9.300
258.0	5.030	410.0	9.300
260.0	3.050	415.0	9.310
262.3	3.040	420.0	9.310
204.0	2.040	430.0	9.320
266.0	3.050	440.0	9.310
253.0	8.050	450.0	9.320
270.0	3.050	460.0	9.320
275.3	3.050	470.0	9.320
250.Û	8.050	430.0	9.320
285.0	3.030	431.0	10.700
290.0	8.070	432.0	10.210
295.0	8.350	493.0	10.840
300.0	8.050	434.O	10.850
310.0	3.050	485.0	10.850
320.0	8.050	486.0	10.370
330.0	3.070	437.0	10.830
340.0	9.030	483.O	10.880
350.0	3.050	439.0	10.350
360.0	3.070	4°5.0	10.370
361.0	9.270	492.0	10.390
362.0	3.220	494.0	10.390
363.3	<.220	496.0	10.900
304.0	9.190	498.0	10.900
355.0	9.17 <u>0</u>	500.0	10.890
365.0	9.210	502.0	19.379
357.0	9.190	504.0	10.860
305.0	9.180	50 ბ. 0	10.370
364.5	2 . 150	503.0	10.570
370.0	9.270	510.0	10.380
372.C	9.300	515.0	10.380
374.0	9.280	520.0	19.379
370.0	9.270	525.0	10.360
373.0	9.28D	530.0	10.350
350.D	9.290	535.0	10.850
332.0	9.270	540.0	10.560
334.0	>.₹ეე	550.0	10.350
386.0	9.333	560.0	10.860

(CONTINUED)

MUQDISHE WATER SUPPLY

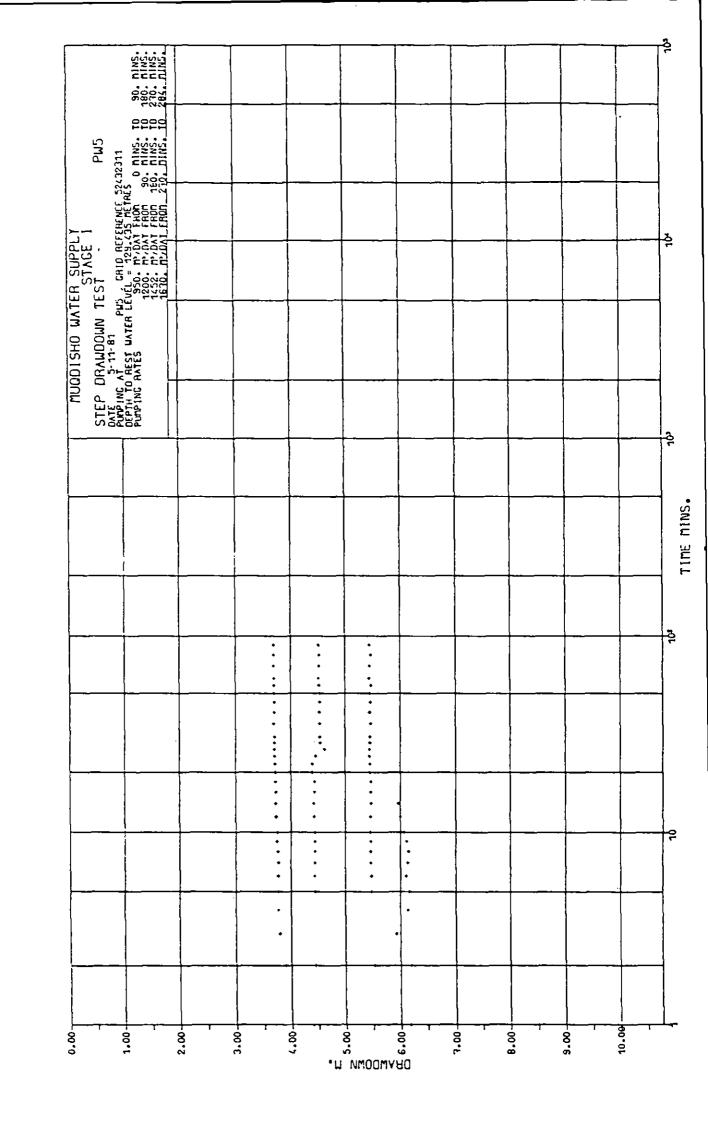
STAGE I

STEP DRAWDOWN TEST PUMPED WELL

PUMPING AT PW3A GRID REF. 52402307

DATE OF TEST 29 4 82

******	0.04.10.01.1.4.4
TIME(MINS)	DKEMBBMV(A)
570 . 0	10.250
530.0	10.883
590.0	10.370
600.0	10.430



STEP DRAWDOWN TEST PUMPED WELL

PUMPING AT

PW5 GRID REF. 52432311

DATE OF TEST 5 11 81

PUMPING RATES (M*+3/04Y) :

950.4 FROM 0.0 MINS TO 90.0 MINS 1200.0 FROM 90.0 MINS TO 130.0 MINS 1452.0 FROM 130.0 MINS TO 270.0 MINS 1670.4 FROM 270.0 MINS TO 234.0 MINS

REST WATER LEVEL 129.435 METRES BELOW DATUM

TIME(MINS)	ORAWOOWA(M)	TIME(MINS)	ORAWDOWN (M)
1.0	4.430	93.0	4.430
2.3	3.390	99.0	4.430
3.0	3.790	190.0	4.430
ن 💂 ن	3.7:0	102.0	4.420
5.0	3.750	104.0	4.410
6.0	3.750	106.0	4.420
7.5	3.770	105.0	4.420
3.0	3.750	110.0	4.390
9.0	3.740	112.0	4.330
10.0	3.747	114.0	4.450
12.0	3.730	115.0	4.520
14.0	3.729	113.0	4.540
15.0	3.720	120.0	4.530
18.9	3.710	125.0	4.530
20.0	3.720	130.0	4.530
22.0	3.710	135.0	4.530
24.0	3.700	140.0	4.530
20.3	3.700	145.0	4.520
28.0	3,700	150.0	4.510
30.3	3.700	150.0	4.520
35.0	3.690	170.0	4.520
40.0	3.700	130.0	4.510
45.0	3.700	181.0	5.510
50.0	5.599	152.0	5.520
55.3	3.500	153.0	5.500
ან.მ	3.730	154.0	5.490
70.5	3.690	185.0	5.470
30.0	3.590	1%6.0	5.470
≎ິ0.0	3.590	137.0	5.450
91.0	4.530	132.0	5.450
92.0	4.439	139.0	5.400
¥3.Ĵ	4.430	198.0	5.450
94.0	4,443	172.0	5.400
95.0	4.433	194.0	5.470
70.J	4.420	195.0	5.450
97.0	4.423	1 ୧୫.୦	5.400

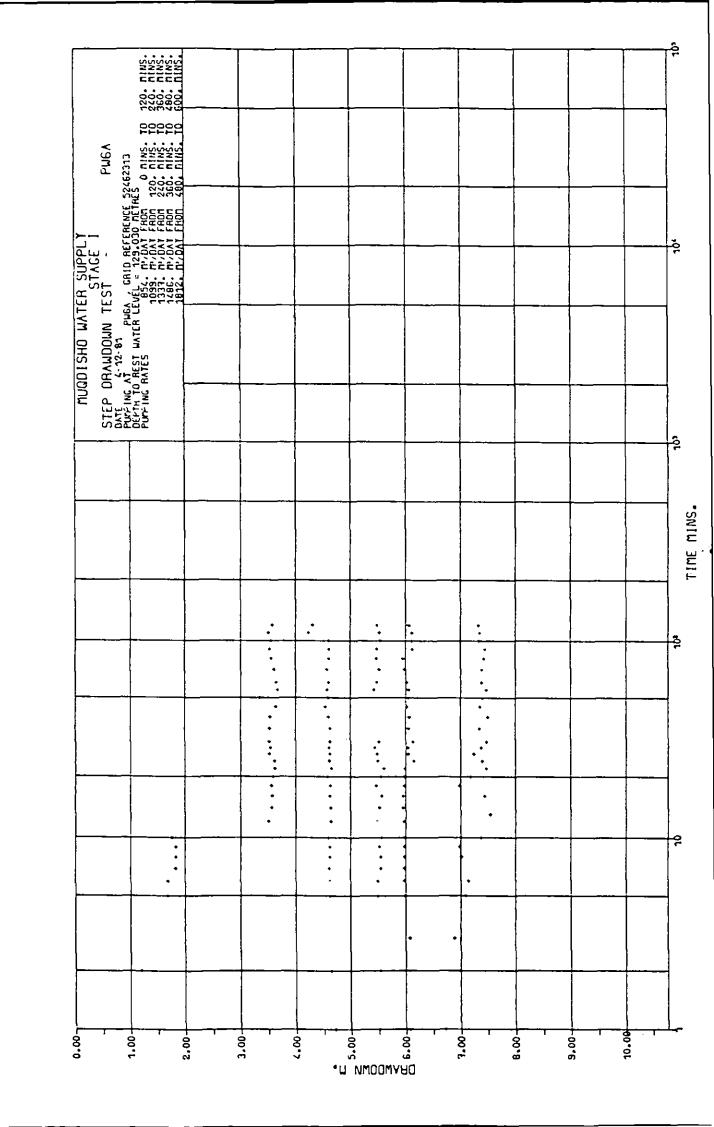
STEP DRAWDOWN TEST PUMPED WELL

2	1 1	١,	5	1	N/G	ДΤ	

PW5 GRID REF. 52432311

DATE OF TEST 5 11 81

TIME (MINS)	DRAWDOWN(M)	TIME(MINS)	ORAWDOWN(M)
200.0	5.450	270.0	5.440
202.0	5.459	271.0	6.170
204.0	5.443	272.0	6.130
206.0	5.440	273.0	5.920
208.0	5.450	274.0	5.130
210.0	5.450	275.0	6.160
215.0	5.470	275.0	6.100
220.0	5.450	277.0	6.130
225.3	5.450	273.0	5.15 0
230.0	5.440	279.0	5.110
235.0	5.470	230.0	5. 960
240.0	5.440	28,2.0	5.000
250.0	5.430	234.0	5.760
250.0	5.470		



STEP GRAWDOWN TEST - PUMPED WELL

PUMPING AT PWSA GRID REF. 52462313

DATE OF TEST 4 12 81

1335.3 FROM 240.0 MINS TO 360.0 MINS 1465.6 FROM 360.0 MINS TO 480.0 MINS 1512.0 FROM 435.0 MINS TO 600.0 MINS

REST WATER LEVEL 129.030 METRES BELOW DATUM

TIME(MINS)	ORAWDOUN(M)	TIME (MINS)	ORAWDOWN(M)
2.0	1.190	127.0	4.500
3.0	1.590	123.0	4.519
5.J	1.579	129.0	4. ó 1 D
6.0	1.533	130.0	4.530
7. ü	1.820	132.0	4.530
3.5	1.620	134.0	4.630
o . c	1.823	136.0	4.510
10.5	1.750	138.0	4.520
12.5	3.500	140.0	4.570
14.0	3.500	142.0	4.540
16.0	3.570	144.0	4.500
18.0	3.550	145.0	4.510
20.0	3.580	149.0	4.590
22.0	3.610	150.0	4.510
24.0	3.510	155.0	4.520
26.0	3.51)	160.0	4.590
23.0	3.530	1:5.0	4.530
30.5	3.510	170.0	4.580
35.0	3.520	175.0	4.560
40.0	3.530	130.0	4.590
45.0	3.630	190.0	4.500
50.0	3.340	200.0	4.500
55.0	3.000	210.0	4.500
٥٠٠٥	3.630	220.0	4.590
70.J	3.600	239.0	4.220
30. 0	3.550	240.0	4.290
90.0	3.520	241.0	5.510
100.0	3.540	242.0	5.530
110.0	3.500	243.0	5.530
120.0	3.573	244.0	5.520
121.0	4.710	245.0	5.480
122.0	4.530	245.0	5.420
123.0	4. 520	247.0	5.540
124.0	4.500	243.0	5.540
125.Ü	4.513	249.0	5.510
125.0	4.513	250.0	5.550

STEP DRAWDOWN TEST PUMPED WELL

2	11	1.1	כ	т	NG	ΔT
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PW6A GRID REF. 52462313

DATE OF TEST 4 12 31

		0415 GE 1531	4 12 31
TIME (MINS)	DRAWDOWN(M)	TIME(MINS)	DRAWDOWN(M)
252.0	5.470	410.0	6.J40
254.0	5.520	415.0	6.050
255.0	5.550	420.0	6.010
253.0	5,450	430.0	5.970
200.0	5.540	440.0	5.950
262.0	5.633	450.0	6.120
264.0	5.480	450.0	5.110
200.3	5.470	470.0	6.110
263.0	5.420	430.0	5.050
270.0	5.500	481.C	6.720
275.3	5.520	482.0	5.970
295.0	5.410	483.0	5.390
300.0	5.450	484.0	ბ. რინ
310.3	5.510	435.0	7.080
320.0	5.450	455.0	7.130
330.0	5.470	497.0	7.530
340.0	5.330	493.O	7.310
35U.J	5.523	439.0	5.980
360.0	5.470	490.0	7.370
361. J	5.070	493.0	7.540
362.0	6. 960	494.C	7.490
3 63.0	5.375	495.0	7.440
365.0	5.970	493.0	6.970
355.0	5.970	500.0	7.170`
357.0	5.270	502.0	7.470
353.0	5.270	504.0	7.390
369.0	5.970	506.0	7,230
37ù.3	5.970	508.0	7.370
372.0	5.950	510.0	7.470
374.0	5.750	515.0	7.340
376.0	5.950	520.0	7.500
378.0	5.970	525.0	7.350
350.0	5,970	530.0	7.400
382.3	5.930	535.0	7.470
354.0	5.14ĵ	540.0	7.380
335.0	5.040	550.0	7.330
338.3 (03.3	0.030 - 130	960.G	7.430
390.3	o.120	570.0	7.450
395.0	6.050	5 ° 0 • 0	7.330 7.350
400.0	5.050 6.030	590.0 .aa.a	
405.5	6.020	500.0	7.320

		:					10
							200
		•	 :	•	•		
STEP DRAUDOWN TES	PUTPING KATES B4						103
	13. P. DAT FROM 120. DINS. 10 120. P. P. DAT FROM 240. HIRS. 10 560. B. P. DAT FROM 240. HIRS. 10 560. B. P. DAT FROM 360. DIM: 10 400.						\$1

STEP DRAWDOWN TEST PUMPED WELL

PUMPING AT

PW7 GRID REF. 52482315

DATE OF TEST 14 12 31

PUMPING	RATES	(M++3/2AY)	:
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347.2 FROM	0.0	11. N.S	ΤO	120.0	MING
1179.4 FROM	120.0		-	240.0	
1452.0 FROM	240.0			360.0	-
1003.0 FROM	360.G		-	483.0	

REST WATER LEVEL 122.400 METRES BELOW DATUM

TIME(MINS)	DRAWDOWN(M)	TIME(MINS)	DRAWDOWN (M)
1.0	4.650	125.0	5.230
2.0	3.98D	126.0	5.270
3.0	3.770	127.0	5.270
4.0	3.750	128.0	5.270
5.Û	3.750	129.0	5.260
ວ.ບິ	3.720	130.0	5.250
7.5	3.740	132.0	5.270
გ. ე	3.750	134.0	5.240
9.O	3.770	135.0	5.250
10.0	3.750	132.0	5.230
12.0	3.750	140.0	5.250
14.0	3.759	142.0	5.240
15.5	3.750	144.0	5.240
15.0	3.740	145.0	5.300
20.5	3.770	148.0	5.290
23.5	5,740	150.0	5.290
24.0	3.750	155.0	5,230
26.3	3.740	160.0	5.290
28.0	3.750	165.0	5.270
30 . Ú	3.750	170.0	5.270
35.0	3.730	175.0	5.280
-0.0	3.750	130.0	5.270
45.0	3.790	190.0	5.230
50 . 0	3.750	200.0	5.250
55.0	3.730	210.5	5.290
აე.ე	3.750	220.5	5.230
70.0	3.770	230.0	5.270
ن.0•	3.750	240.0	5.240
90.3	3.753	241.0	6.470
100.0	3 .7 50	242.0	5.470
110.0	3.770	243.0	5.450
120.0	3.790	245.0	6.490
121.0	5.240	245.0	5.520
122.0	5.300	246.0	5.480
123.6	5.290	247.0	ó.5a0
124.0	5.250	248.0	5.570

STEP BRANDOWN TEST - PUMPED WELL

PUMPING 4T PW7 GRID REF. 52482315

DATE OF TEST 14 12 31

TIME(MINS)	DRAWDOWN(M)	TIME (MINS)	DRAWDOWN(M)
249.)	5.550	365.0	7.360
250.0	5.550	366.0	7.340
252.3	5.453	36 7. 0	7.350
254.3	6.433	368.0	7.340
250.0	5.540	369.0	7.320
25ä.J	5.550	370.0	7.330
260.0	5. 553	372.0	7.350
202.0	5.550	374.0	7.320
264.3	5.530	370.0	7.450
255.3	€.540	378.0	7.440
268.0	6.550	320.0	7.450
270.0	o.730	392.0	7.300
275.0	5.480	334.0	7.320
230.0	5. 520	385.0	7.310
235.0	6.570	333.0	7.370
290.0	5.530	390.0	7.320
245.0	5.520	395.0	7.320
300.0	5. 50€	400.0	7.310
310.0	6.490	405.0	7.290
320.0	0.500	410.0	7.410
330.0	6.473	415.0	7.440
340.0	5.475	420.0	7.350
350.0	6.490	430.0	7.360
350 . 0	ઝ•ૂક∘ો	449.0	7.300
361.0	7.320	450.0	7.493
362.0	7.355	4 5 0.0	7.380
363.0	7.320	470.0	7.320
364.0	7. ₹50	430.0	7.330

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STEP DRAMDOWN TEST - PUB STEP DRAMDOWN TEST - PUB DATE PUMPING AT PURPING SATES WATER LEVEL = 112.580 RETHES DEPTH TO REST WATER LEVEL = 112.580 RETHES 1070 RY, FROM 120. MINS. TO 1521 RY, DAY FROM 220. MINS. TO									
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STEP DRAWDOWN TEST PUMPED WELL

PUMPING AT

PW3 GRID REF. 52502317

DATE OF TEST 20 12 81

DMIAMCS	RATES	(H**3/34Y)	:		
332.3	FROM	O.C MINE	S TO	120.0	MINS
1073.4	FROM	120.0 MIN:	S TO	240.0	MINS
1300.3	FRUM	240.0 MIN:	S TO	360.0	MINS
1543.2	FROM	360.0 MIN:	5 7 2	430.0	MINS
1357.6	FROM	480.0 MIN:	S TS	33.3	MINS

REST WATER LEVEL 112.360 METRES SELOW DATUM

TIME (MINS)	DRAWDOWN(M)	TIME (MINS)	ORAWDOWN(M)
4.0	3.730	128.0	5.320
5.0	4.150	129.0	5.310
6.J	4.150	130.0	5.300
7.0	4.170	132.0	5.320
3.0	4.150	134.0	5.380
∨.ე	4.130	136.0	5.330
10.5	4.130	133.0	5.380
12.0	4.120	149.0	5.360
14.0	4.059	142.0	5.370
15.J	4.142	144.0	5.360
18.0	4.050	147.0	5.370
20.0	3.770	145.0	5.350
22.0	3.740	150.0	5.360
24.0	4.120	155.0	5.350
26.Û	4.150	160.0	5.350
23.0	4.150	165.0	5.350
30.0	4.153	170.9	5.300
35.3	4.170	175.0	5.330
40.0	4.180	190.0	5.340
45.0	4.130	190.0	5.350
50.0	4.575	200.0	5.350
55.0	4.150	210.0	5.350
იმ.მ	4.140	220.0	5.350
70.0	4.177	230.0	5.340
30.0	4.150	240.0	5.310
90.0	4.133	241.9	5.360
100.5	4.1:0	242.0	6.400
115.3	4.150	243.0	510
120.0	4.133	244.0	5.400
121.0	4.820	245.û	5.420
122.0	5.180	246.0	6.420
123.0	5.340	247.0	5.420
124.0	5.347	248.0	5.430
125.5	5.320	249.0	6.430
120.5	5.330	250.0	0.430
127.0	5.270	252.0	5.430

STEP DRAWDOWN TEST - PUMPED WELL

PUMPING 4T PW8 GRID REF. 52502317

DATE OF TEST 20 12 81

		DATE OF TEST	20 12 81
TIME(MINS)	DRAWDOWN(M)	(ZWIM)EMIT	DRAWDOWN(M)
254.0	6.420	400.0	7.540
256.0	5.430	495.0	7.540
253.0	5.430	410.0	7.550
200.J	0.430	415.0	7.530
262.0	6.420	420.0	7.550
254.0	6.430	450.0	7.530
265.0	6.430	440.0	7.540
268.5	5.410	450.0	7.540
270.0	5.440	450.0	7.540
275.0	5. 430	470.0	7.530
230.0	6.420	430.0	7.550
235.0	5.420	491.0	3.300
298.0	5. 423	452.0	9.940
2∀5.0	5.420	483.0	3.750
300.0	6.430	434.D	8,930
310.0	5.420	485.0	3.960
320.0	5. 425	435.0	3.930
330.0	5.420	487.0	3.910
340.0	5.430	488.0	3.920
350.0	5.430	439.0	8.920
300.0	0.430	490.0	8.910
351.0	7.490	492.0	3.970
352.0	7.530	404 ° Q	3.960
363.0	7.520	495.0	8.960
354.1	7.520	493.0	3.960
365.0	7.530	500.0	8.970
365.0	7.520	502.0	8.980
307.5	7.520	504.0	3.960
358.0	7.525	505.0	3.960
300.0	7.520	503.0	8.950
370.0	7.513	510.0	3.950
372.0	7.530	515.0	8.950
374.0	7.520	520.0	3.960
375.ŭ	7.520	525.0	5.950
375.0	7.570	530.0	3.970
350.0	7.550	535.0	3.350
382.0	7.550	540.0	2.960
334.0	7.550	550.0	3.970
355.0	7.530	560.0	9.950
338.3	7,540	570.0	8.950
390.0 705.0	7.540 2.500	530.0 500.0	3.940 8.940
395.0	7.500	590.0	5.740

MUGDISHO WATER SUPPLY BATER LISTING ATAC S861/1861

GRID REF	SITE #	DATE	DEPTH TO WATER (METRES)
51472334	CW2	13 NOV 31	55.7
51912295	2W34	13 050 81	113.3
52092355	43042	27 403 31	53.5
52122392	MGQ39	29 403 81	57.0
52322332	42052 3	24 MAY 31 7 AUG 81 12 AUG 31 1 DOT 31 19 JAK 32 13 APR 82	123.7 125.716 128.733 123.751 123.741 123.734
52422311	2 # 1 3	16 DEC 81	130.2
52512470	MGQ132	AUG 31	52.3
52762333	ଜନପୁ 1 ଶିଳ୍ୟ	29 AUG 81 13 APR 32	101.4 101.377
3389 2 418	7052	11 MAY 31 7 SEP 31 15 APR 82	105.3 105.372 105.369
53022529	MGQ12P	30 MAY 31 7 SEP 31 6 MAR 92 27 MAR 82 17 APR 82	55.4 56.406 53.233 53.941 52.939
54152322	30302	25 MAY 31 12 SEP 31 15 APR 32	62.0 62.061 62.157
54252350	11 =	7 APR 52	02.3
54302359	1 7 :	3 APR 83	71.5

MUDDISHO WATER SUPPLY DEPTH TO WATER LISTING 1481/1982 DATA

GRID REF	\$ 5 T E	011E	DEPTH TO WATER (METRES)
543423:0	145°	25 MAY 31 12 SEP 31 15 APR 32	69.3 69.346 69.295
543525yi	3 E V E 3	2 MAY 81 13 MAY 81 5 MAR 82 27 MAR 82 17 APP 82	5.3 5.340 4.000 3.260 4.500
54442389	15สรมสิง	25 MAY 31 12 SEP 31 15 APR 32	52.9 62.757 63.013
54442455	MSQ72	13 MAY 31	107.5
54552327	#0220P	25 MAY 31 12 SEP 81 15 APR 52	32.9 32.378 32.785
54712315	M391€?	25 MAY 81 12 SEP 81 15 APR 82	13.3 13.369 13.788
55322437		13 MAY 81 12 SEP 31	63.3 63.359



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