1 #Running header: 'Cardiff Urban Geo-Observatory'

3	Case study: Establishing an urban geo-observatory to support sustainable development of
4	shallow subsurface heat recovery and storage
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19	Abstract
20	Low-enthalpy ground source heating and cooling is recognised as one strategy that can contribute
21	towards reducing reliance on traditional, increasingly insecure, CO2-intense thermal power
22	generation, as well as helping to address fuel poverty. Development of this technology is applicable in
23	urban areas where high housing density often coincides with the presence of shallow aquifers. In
24	urban areas groundwater temperatures can be elevated due to the subsurface Urban Heat Island effect.
25	Uptake and development of this technology is often limited by initial investment costs, however,
26	baseline temperature monitoring and characterisation of urban aquifers, conducted in partnership with
27	local authorities, can provide a greater degree of certainty around resource and sustainability that can
28	facilitate better planning, regulation and management of subsurface heat. We present a novel high-

density, city-scale groundwater temperature observatory and introduce a 3D geological model aimed
at addressing the needs of developers, planners, regulators and policy makers. The Cardiff GeoObservatory measures temperature in a Quaternary aged sand and gravel aquifer in 61 boreholes and
at a pilot shallow open-loop ground source heating system. We show that repurposing existing
infrastructure can provide a cost effective method of developing monitoring networks, and make
recommendations on establishing similar geo-observatories.

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Anthropogenic factors, including land cover, heat loss from buildings, basements and subsurface
infrastructure, can result in the warming of shallow groundwater in urban areas, known as the
subsurface Urban Heat Island effect (sUHI) (Allen *et al.* 2003; Ferguson & Woodbury 2007; Hayashi *et al.* 2009; Taylor & Stephan 2009; Zhu *et al.* 2010; Menberg *et al.* 2013a; Epting & Huggenberger
2013; Benz *et al.* 2016 & Farr *et al.* 2017; Bidarmaghz *et al.* 2019). Both open and closed loop ground
source heat pumps can utilise the shallow urban subsurface which can also be used to provide space
heating and cooling for buildings and for thermal storage.

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44 Currently, domestic and industrial heating make up nearly 50 % of all energy consumption across the 45 EU (Sanner et al. 2011). In the UK 32 % of energy is used for space heating, which can be broken 46 down into; industrial (19%) and domestic (13%) heating (BEIS 2017). In The UK 80% of space heating is derived from the burning of fossil fuels (DECC 2013), a large contributor to anthropogenic 47 greenhouse gas emissions. The UK Government has committed to the Climate Change Act, 2008, 48 pledging to reduce CO<sub>2</sub> emissions by at least 80 % by 2050 compared to 1990 levels (BEIS 2017). In 49 50 the UK 83 % of the population (Office for National Statistics 2018) live in urban areas, however development of ground source heat recovery and storage has been on a case-by-case basis with little 51 strategic subsurface planning or policy, and significant challenges, including the regulation and 52 ownership of heat, still need to be fully addressed (Sanner et al. 2011; Abesser et al. 2018). To reduce 53 our dependency on fossil fuels for domestic space heating, increase long-term energy security and 54 55 help alleviate fuel poverty there is a need to de-risk the development of a mix of renewable, 56 sustainable, low-carbon technologies so they can be integrated into district heating networks.

Commonly documented risks of shallow geothermal energy systems include thermal interference 58 between unregulated closed-loop systems and the competitive use of subsurface opportunities (e.g. 59 Fry 2009; Herbert et al. 2013). Evidence of subsidence associated with open loop ground source 60 61 heating schemes has been documented in Germany (Fleuchaus & Blum 2017). Conflict may occur 62 between other users of the urban subsurface, e.g. buried services, water abstraction, and sewerage. A 63 paucity of baseline temperature data from shallow urban aquifers could also result in poor system 64 design and performance, which could undermine investor and public confidence. It is already well 65 recognised that subsurface conditions are not considered adequately during the planning stage of heat 66 recovery and storage and that regulation and licencing could benefit from an evidence-base on which 67 decisions can be made (Blum et al. 2011; Vienken, et al. 2015; Stephenson et al. 2019). We propose 68 that a strong evidence-base is one of the key attributes that can help to 'de-risk' shallow urban heat 69 recovery and storage. Such an evidence base could allow policy makers, regulators, investors and 70 developers to implement sustainable projects.

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72 In the UK a lack of information on shallow urban groundwater temperatures has, in addition to high 73 drilling costs and low gas prices, limited the sustainable development of ground source heat recovery 74 and storage systems. Greater understanding of urban groundwater systems will provide the evidence-75 base needed to de-risk future development (e.g. Blum et al. 2011; Vienken et al. 2015). Among the 76 pressing challenges to the uptake of the sustainable use of urban aquifers for heat recovery is the over-77 regulation of open-loop heat recovery operations, which can be a barrier to development, deterring 78 investors (e.g. Bonsor et al. 2017; Herbert et al. 2013). Under-regulation of closed-loop heat recovery 79 and storage can also have potentially negative consequences as systems can be installed anywhere, which may result in negative feedback between systems and loss of performance (Fry 2009 & Herbert 80 et al. 2013). Regulatory challenges are compounded by a lack of consensus on ownership of heat in 81 the subsurface (Abesser et al. 2018). Subsurface thermal management policies are therefore required 82 to regulate heat in urban areas (e.g. García-Gil et al. 2015a; Epting et al. 2018) and these are best 83 84 addressed before large-scale deployment of ground source heat recovery and storage systems.

Globally, many cities have started to address the challenges of sustainably recovering and storing heat
in shallow urban aquifers (Table 1). The sUHI has been characterised in many cities, with elevated
groundwater temperatures being recognised as a potential source for low enthalpy heat recovery using
heat pump technology (Allen *et al.* 2003; Arola & Korkka-Niemi 2014; Benz *et al.* 2016; Casasso *et al.* 2017; Farr *et al.* 2017; Ferguson *et al.* 2007; Janža *et al.* 2017; Taniguchi *et al.* 2007). 3D heat
flow and groundwater models (García-Gil *et al.* 2015a; Mueller *et al.* 2018) have been used in Basel
and Zaragoza to sustainably manage subsurface heat resources.

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94 In Berlin, Germany, the Senate Department for Urban Development and Housing integrates ground 95 source heat into their planning regime, and this is complemented by groundwater temperature 96 monitoring programs (e.g. Benz et al. 2016). Urban groundwater monitoring networks are required to 97 increase confidence for investors whilst supporting evidence-based regulatory targets (Epting et al, 98 2018). The Common Vision for the Renewable Heating and Cooling sector in Europe lists a need for 99 an observatory to provide better quality data related to renewable heating and cooling as one of its 100 priorities (Sanner et al. 2011). However urban areas can be highly geologically variable and it is 101 acknowledged that there is no single design of city-scale monitoring or modelling of groundwater and 102 heat resources appropriate for all cities (Bonsor et al. 2017).

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104 To address these challenges the British Geological Survey and City of Cardiff Council have worked in partnership to deliver a high-density, city-scale, urban geo-observatory. The 'Cardiff Urban Geo-105 106 Observatory' comprises four years of baseline temperature data, an operational shallow open-loop ground source heat pump, and a 3D geological model of the superficial geology focused on the target 107 unconsolidated sand and gravel aquifer. The observatory is the largest of its kind in the UK, providing 108 open access data though a bespoke web-portal (www.ukgeos.ac.uk/observatories/cardiff). Lessons 109 learned from this approach could be used to benefit the development of other urban geo-observatories, 110 111 underpinning evidence-based environmental regulation and supporting sustainable development. 112 Groundwater levels and temperatures obtained from the monitoring sites can be used to develop

groundwater and heat flow models to support regulation of heat and water recovery. In this paper we present a case study from Cardiff describing a method for establishing a geo-observatory comprising a network of groundwater temperature sensors, 3D geological model, and an introduction to the shallow open loop groundwater heat pump research site. The Cardiff urban geo-observatory is thought to be the UK's first city-wide groundwater temperature network and illustrates the advantages of repurposing existing infrastructure and working in partnership with local authorities to deliver data to underpin low-carbon energy technologies.

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### 121 Study area

Cardiff, covers an area of 140 km<sup>2</sup> and has a population of 346 000 (Office for National Statistics 122 123 2012). The Port of Cardiff once exported one third of the World's coal (Brabham 2009), however 124 following the decline of the coal industry, the area fell into disrepair. In the mid-1980s, as part of the city's redevelopment, the Cardiff Bay Development Corporation (CBDC) was formed to oversee the 125 construction of a tidal barrage across the mouths of the River Taff and Ely. The barrage closed its 126 locks for the first time on the 4<sup>th</sup> November 1999, creating a 2 km<sup>2</sup> fresh water lake (Hunter & Gander 127 128 2002). Due to the possibility of rising groundwater levels impacting underground structures such as 129 basements, the 'Cardiff Bay Barrage Act, 1993' required groundwater monitoring to be undertaken 130 for a period of 20 years following the closure of the barrage. In response, 236 monitoring boreholes, many of which can be seen in Figure 1, and six dewatering schemes were installed to monitor and 131 manage groundwater levels (Edwards 1997; Heathcote et al. 1997; 2003; Sutton et al. 2004 & 132 Williams 2008). The majority of the boreholes monitor groundwater in the glaciofluvial sand and 133 gravel aquifer. 134

135

Cardiff is underlain by bedrock deposits comprising folded Silurian, Devonian and Carboniferous
strata and unconformably overlying Triassic rocks, including the Mercia Mudstone Group and its
basal Marginal Facies. These are overlain by Devensian glacial deposits and Holocene alluvial and
coastal deposits (Waters & Lawrence 1987; Kendall 2015). The target aquifer for this study is the
Quaternary aged glaciofluvial sand and gravel that underlies the river valley systems that transect the

141 city and principally comprises dense, poorly sorted sandy gravel with cobbles (Heathcote et al. 2003). Edwards (1997) defined the Tidal Flat Deposits to be of low to intermediate permeability overlying 142 the sand and gravel aquifer, generally confining the sand and gravel aquifer in the south of the city 143 centre. However in some localised areas the Tidal Flat Deposits are absent resulting in 144 145 hydrogeological connections between the sand and gravel and the made ground aquifers (Williams 2008). Groundwater in the sand and gravel aquifer generally flows towards the rivers and the coast 146 147 (Edwards 1997). Red mudstones of the Triassic aged Mercia Mudstone Group bedrock form a low 148 permeability base to the aquifer (Edwards 1997; Heathcote et al. 2003). Post impoundment of the 149 barrage, changes in groundwater levels between 2.5 - 3.5 m were measured in the sand and gravel 150 aquifer but were limited to the fringes of Cardiff Bay (Williams 2008). Pumping tests show that the 151 hydraulic conductivity of the sand and gravel aquifer is relatively consistent, with average values of 50 m/d (Heathcote et al. 2003) with groundwater levels 3-4 m below the surface. 152

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In partnership with Cardiff Harbour Authority (a department of Cardiff City Council), who maintain the groundwater level monitoring network, temperature profiles at 168 boreholes were undertaken to characterise aquifer temperatures and the sUHI. The study revealed groundwater temperatures exceeded those forecast by the predicted geothermal gradient by up to 4 °C in over 90 % of the boreholes, with the excess heat attributed to the sUHI (Farr *et al.* 2017)

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#### 160 Methodology

Data from the geo-observatory is intended to be used to address some of the key questions relating to the sustainable development of heat recovery and storage in shallow urban aquifers. For the purposes of this study, the extent of the groundwater temperature monitoring area is defined by the +10 m AOD (above ordnance datum) contour line as this was the extent of the original groundwater level monitoring and covers the majority of the city of Cardiff. The step-by-step process for creating and maintaining the 'Cardiff Urban Geo-Observatory' is described.

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#### 168 *Geological data acquisition and storage*

169 The first step towards developing the geo-observatory was to collate existing sources of geological data. The British Geological Survey acts as custodian for borehole records, enabling data sharing that 170 can further understanding of the subsurface. Borehole data was submitted by developers or 171 172 accessioned from site investigation reports held in the public records at the local authority. Ground 173 investigation data can be abundant in urban areas, however these data are often not centrally held and 174 are often distributed between local authorities, consultancies and their clients. The BGS's National 175 Geoscience Data Centre (NGDC) allows for these data to be brought into one central repository. The 176 data were used to underpin the development of a 3D geological model (Kendall et al. 2018) and to 177 create a database of information on the geotechnical and hydrogeological properties of the main 178 geological units.

179

In addition to the data already held in the NGDC, ground investigation data held in Cardiff City
Council's planning applications public record were identified and captured. In total, over 1000
borehole logs were acquired and interpreted, including all of the borehole logs for Cardiff Harbour
Authority's groundwater monitoring boreholes. These borehole logs are stored in the British
Geological Survey's Single Onshore Borehole Index (SOBI) which be viewed online using the BGS
'Onshore GeoIndex'. Boreholes included in this study are identifiable by their co-ordinates in Table 2.

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### 187 Geotechnical data

188 Geotechnical data were collated from sites investigation reports stored on the NGDC. These data are intended to help reduce the risk of unforeseen ground conditions for future developments, as well as 189 190 provide insight into aquifer properties, and are held in the BGS' National Geotechnical Properties Database available from BGS. Material properties can be used to calculate the thermal conductivity of 191 the geological units, and thus could better inform how heat is transported and stored within the 192 193 subsurface, supporting future thermal management models. In addition, four boreholes drilled specifically for this project (Abstraction, Recharge, OBS1 and OBS2, see Table 2) with full core 194 recovery have been tested for a range of physical properties including bulk density, natural moisture 195 196 content, thermal conductivity, thermal diffusivity and resistivity. Data stored within the Geotechnical

197 Properties Database has been summarised and the Glaciofluvial Sand and Gravels were found to be 'cleaner' in the south of the city with an average of 6 % fines (silt and clay) and a higher permeability 198 than that of the city centre where fines averaged 18 %. This may be related to the confinement of 199 these areas, with the former thought to be confined while the latter is considered generally 200 201 unconfined. The depth of weathering in the Mercia Mudstone Group varies considerably; typically the top 10-15 m are found to be weathered material but this may reach depths of up to 47 m. Standard 202 203 penetration test (SPT) N values were found to be higher in the unconfined areas of the aquifer but 204 were generally varied, ranging from 1-150. The data shows the heterogeneity of soils across the city, 205 highlighting the importance of site-specific data. Other data recorded in the database but not 206 specifically interrogated at the time of writing include 9576 SPTs, 1538 water strikes, 1213 207 contaminant and chemical tests, 1099 point load tests, 842 consolidation tests, 593 particle size 208 distributions, 461 fracture spacing data, 312 triaxial tests, 73 in situ vane tests, 50 weathering grades, 209 2 shrinkage tests, 23 compaction tests, 14 shear box tests, and 6 in situ density tests.

210

## 211 Developing a 3D geological model

To support the use of ground source heat recovery within Cardiff City Council's regeneration plans a city-scale 3D geological model has been produced (Kendall *et al.* 2018). The geological model extends beyond the main urban city centre to encompass some of the surrounding suburbs and the three main rivers. This model describes the vertical and lateral extent of the superficial geology from surface to the underlying geological rockhead (Fig. 2). The following illustrates the main steps used to create the model.

218

# 219 3D geological modelling software

Geological modelling software 'GSI3D<sup>TM</sup>' (Geological Surveying and Investigation in 3 Dimensions)
was used to develop a city-scale model to better understand the extent of the target sand and gravel
aquifer and its relationship to the adjacent units. GSI3D<sup>TM</sup> allows the geologist to create an 'explicit'
model by developing cross sections constrained by the surface intercept (geological map) and
subsurface constraint from interpreting and correlation of borehole information (Kessler *et al.* 2009).

The 3D geological model illustrates the relationship between superficial deposits comprising
Alluvium, Tidal Flat Deposits, Glaciofluvial Sheet Deposits and Till and their contact with the
underlying bedrock.

228

### 229 Instrumentation

Baseline groundwater temperatures were measured using a variety of sensors installed in the preexisting borehole network to characterise the thermal regime beneath the city. These data provide a baseline with which to compare the thermal regime after the installation of heating and storage systems and to assess any long-term impacts of their use on the surrounding aquifer. The following subsections describe the various sensors, their locations, and installation depths.

235

## 236 In-situ temperature sensors

237 In-situ sensors were installed in 61 monitoring boreholes across a range of depths (Table 2 and Fig. 1; 238 2). The boreholes selected for instrumentation were spatially distributed across the city representing 239 the main geological units and a range of land uses and land cover. In most boreholes one temperature 240 sensor was installed, however in some boreholes multiple sensors were installed both above and 241 below the boundary of the Zone of Seasonal Fluctuation - the depth to which seasonal oscillations in 242 air temperature affect groundwater temperatures - previously characterised at an average depth of 9.5 mbgl (Farr et al. 2017). The Zone of Seasonal Fluctuation was delineated to provide information on 243 the most suitable depth of groundwater pumps for open loop systems. Pumps installed and 244 intercepting groundwater derived from greater than 9.5mbgl should encounter more stable 245 groundwater temperatures, whilst abstractions from aquifers less than 9.5mbgl are more likely to 246 experience seasonal temperature variations that could result in a loss of performance. In boreholes 247 where just one sensor has been installed, depths were chosen to include groundwater both within, and 248 those below the base of the Zone of Seasonal Fluctuation. However, the majority of sensors were 249 installed below the base of the Zone of Seasonal Fluctuation as this is where groundwater heat pumps 250 251 would be sited and thus monitoring of these temperatures is critical to establish baseline temperatures 252 and potential changes which may occur after the development of ground source heating. It is

important to monitor groundwater temperatures to establish a baseline and then to be able to quantify
and attribute changes from this baseline, both seasonally and over a period of years. This baseline data
will allow assessment of any impact of future developments at a local and city-scale.

256

A network of boreholes were instrumented with Hobo® Temp Pro V2 sensors with a resolution of 257  $0.02^{\circ}$ C and an accuracy of  $\pm 0.21^{\circ}$ C. Solinst Leveloggers, with a resolution of  $0.003^{\circ}$ C and an 258 accuracy of  $\pm 0.5^{\circ}$ C, and OTT<sup>®</sup> Hydrometry Orpheus Mini loggers with a resolution of  $\pm 0.1^{\circ}$ C and 259 an accuracy of  $\pm 0.5^{\circ}$ C. Both the Solinst<sup>®</sup> and OTT<sup>®</sup> sensors record water pressure and temperature 260 whilst the Hobo<sup>®</sup> is a dedicated temperature sensor. Sensors used were chosen for their affordability 261 and reliability and record temperature at half-hourly intervals to be consistent with the existing 262 groundwater level monitoring in the network. 3.75 million temperature measurements from boreholes 263 264 (Fig 1; Table 2) collected over a period of three years are illustrated in Figure. 3. The data show temperatures to vary considerably across the year within the top 10 mbgl, becoming more seasonally 265 266 stable below this depth which is significant for the proper siting of groundwater pumps so as to avoid 267 inefficiencies caused by temperature instability.

268

The groundwater temperature data have a greater variation within the Zone of Seasonal fluctuation (0-9.5mbgl) and become less variable with depth, especially below the Zone of Seasonal Fluctuation. However, some boreholes, for example 9/OB1L, show a wide fluctuation in temperature data. The cause of this is unknown but could be related to localised anthropogenic heat loss from subsurface infrastructure or even localised hydrogeological pathways that allow cooler recharge to bypass the low permeability alluvium and recharge the sand and gravel aquifer.

275

### 276 Telemetry

277 Telemetry allows for real-time monitoring of groundwater temperatures which is useful for

278 monitoring dynamic boreholes, including those associated with the ground source heat pump. To

support our decision-making, an initial screening exercise of the borehole network showed that many

280 were unsuitable for telemetry due to practical factors including; poor reception, no power supply or

limited security preventing solar panels from being reliably employed. However, telemetry can be useful at ground source heating system sites as it allows automated messages should changes occur that are outside of permitted values. Automated messages make it possible to detect potential issues early on and remedy them promptly to improve the reliability and functionality of the system. Prior characterisation of the aquifer in Cardiff helped in the selection of suitable sites for telemetry where dynamic changes in groundwater temperature may be observed.

287

288 Six boreholes were selected for telemetry comprising three monitoring boreholes within the sand and 289 gravel (4/PB2, 5/PB2 and 2/PB2), one borehole in the Mercia Mudstone Group Marginal Facies (Techniquest), and the abstraction and recharge boreholes at the pilot groundwater source heat pump 290 scheme. Each borehole was installed with a sensor connected to an OTT/ADCON® telemetry unit. 291 Data is sent to a gateway where it is stored in a database and can be visualised for remote monitoring 292 293 of the system and analysed for research and development. Telemetry provides a novel early warning 294 system for the ground source heat pump demonstrator. In the event of a temperature change outside of 295 pre-defined targets, in this case any temperature below 8°C, staff receive e-mail alerts or SMS text 296 messages allowing them to respond by visiting the site, checking for system issues and altering the 297 system controls.

298

### 299 Groundwater Source Heat Pump Demonstrator

300 As proof of concept that a shallow open loop ground source heat pump could be viable in an urban 301 setting, a pilot scheme, funded by InnovateUK, was constructed at 'Grangetown Nursery School'[GR 302 318117, 174486] (Boon et al. 2019) in partnership with Cardiff City Council and WDS Green Energy. 303 The ground source heating scheme comprising two shallow boreholes (18.6 and 22 m deep) was 304 retrofitted to replace an existing gas central heating system (Fig. 4). Operational since November 2015 it supplies 22 kW of peak heating output. Shallow groundwater from the sand and gravel aquifer 305 is abstracted from a 22 m deep borehole with a pump installed at 15 mbgl. Groundwater is passed 306 through a heat exchanger, which transfers around 2 Kelvin of heat to the heat pump brine circuit, 307 308 before being returning to the same sand and gravel aquifer via a recharge borehole (18.6 m deep)

309 located 20 m away from the abstraction borehole. An abstraction licence and registration of an exemption to discharge were obtained from Natural Resources Wales, the environmental regulator 310 before the site could become operational. The system abstracts and returns on average 36 m<sup>3</sup>/day and 311 is limited by a single speed pump operating on-demand rather than continuously. The system is 312 313 instrumented with an early warning telemetry system, and monitoring of the surrounding aquifer is provided by boreholes CS241, CS317L, OBS1 and OBS2 (Table 2). We monitored the groundwater 314 levels, temperatures, abstraction volume, as well as all parts of the heat pump system including heat 315 316 generated and the brine circuit. Changes in groundwater temperatures at the demonstrator site are tracked in reference to baseline temperatures. Observed changes from the baseline are out of scope for 317 this paper but are the subject of Boon et al. 2019, however this pilot scheme proves shallow open loop 318 319 systems in urban areas can be viable.

320

#### 321 Open Access Data Portal

Half-hourly temperature data from 2014 onward are available via the open access portal;

323 <u>www.ukgeos.ac.uk/observatories/cardiff</u> (Fig. 5). The decision to make the data open access was

324 made to increase confidence for developers, whilst allowing local authorities, environmental

325 regulators and policy makers to underpin evidence-based decisions. Each monitoring location, or

326 'node', is attributed with information on the location, depth, sensor ID and measurement properties

327 e.g. temperature or groundwater level. Once downloaded, the data is prepared in .csv format,

328 validated and matched to the individual node.

329

## 330 Groundwater chemistry

Groundwater chemistries, including elevated concentrations of iron and manganese, can result in the fouling of boreholes, groundwater pumps and heat exchangers, leading to the loss of performance of ground source heating schemes. It is not possible to reduce the source of these metals in the sand and gravel aquifer however an understanding of likely concentrations will allow developers to be better prepared to mitigate against possible system damage. To characterise groundwater chemistry, specifically iron and manganese in the target sand and gravel aquifer, data was collated from
operational dewatering schemes operated by Cardiff Harbour Authority (Fig. 1) (Williams 2008).

Groundwater chemistry data measured over a period of 12 years are summarised (Fig. 6). The box 339 340 plots show the range of measured values confirming that iron and manganese are both ubiquitous 341 within the target aquifer. De-oxygenated groundwater high in dissolved iron and manganese can, on interaction with oxygen in the atmosphere, result in precipitation of iron and manganese oxides 342 343 creating operational problems such as biofouling in heat exchangers, associated pipework, pumps and 344 boreholes. This information shows the value of baseline water chemistry monitoring data as it highlights a system design constraint to reduce the impact of iron and manganese by sealing the 345 346 systems from the atmosphere where possible. Lessons can be transferred from experience in other aquifers where this is commonly dealt with, e.g. coalfields (Younger 2014; Banks et al. 2017). 347

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#### 349 Discussion

350 Establishment of the Cardiff Urban Geo-Observatory has given rise to a number of discussion points351 which are addressed below.

352

### 353 *Monitoring strategies*

Bonsor et al. (2017) identified it to be best practice to have a clear understanding of the monitoring 354 aims before establishing a geo-observatory. Prior to the commencement of monitoring, it is useful to 355 consider the type of data that will be required, the frequency with which it will be measured, how it 356 will be displayed, what method of analysis will be used and how the data will be stored for future use 357 (Bonsor et al. 2017). Long-term maintenance, staffing costs and funding are also important 358 considerations to ensure the future security of any monitoring network. Monitoring considerations 359 include; vertical and horizontal distribution of monitoring points, geological setting, land use and 360 cover, site security and access, monitoring frequency and duration. Half-hourly monitoring was 361 362 chosen to be constant with other groundwater monitoring networks. New borehole networks can be 363 designed specifically to match the purposes of the geo-observatory, however in Cardiff it has proven

possible to repurpose existing groundwater monitoring infrastructure. Where existing networks can be repurposed a significant cost reduction can be realised. We therefore recommend that where existing infrastructure is suitable for repurposing that it should be used to establish a geo-observatory or supplement new infrastructure. We recommend that where possible city-scale monitoring should be developed in partnership with the local authority as it may complement their renewable energy strategy and raise awareness within the user community.

370

### 371 Monitoring techniques

Low-cost, reliable sensors were chosen to maximise the extent of the monitoring network. The large
memory capacities and battery life of the sensors reduces the number of site visits required for
downloading data. Long periods between downloading data can result in delays in detecting data loss,
however only one sensor has failed during the current study. Downloading sensors requires resources
for staff to visit each site thus large memory capacities reduces the amount of staff resource required
to maintain the geo-observatory, however, manually downloaded sensors do not provide real-time
data.

379

380 Telemetered sensors allow real-time data to be streamed to open access web viewers reducing the need to regularly visit the sites and rapidly highlighting when sensors fail, thus potentially reducing 381 data loss. Telemetry can reduce health and safety concerns where access is difficult or in boreholes 382 where groundwater may be contaminated. Telemetry systems also offer e-mail or SMS alerts of 383 system failures or exceeded pre-defined values which is useful in dynamic situations such as near 384 385 ground source heat recovery operations. However, telemetry can be expensive to install and has ongoing maintenance costs and may not be required where there is less dynamic change in 386 groundwater temperatures. Data hosted or stored by third parties could be potentially at risk in the 387 388 event that the external company cease to provide this service, or in cases of cyber threats, and data 389 should be backed up securely on separate servers.

391 In areas with good access to the boreholes, manually downloaded sensors may prove to be sufficient and financially efficient. In urban areas where security issues may arise, the low cost of these sensors 392 and their lack of external infrastructure needed to support them may make them more suitable. 393 394 However, for remote or dynamic sites where access may be limited or real time data more crucial, 395 telemetry may be preferable. We found that a mixture of both telemetry and manually downloaded 396 sensors provided the best method of data capture and recommend that when establishing a new 397 network consideration is given to the costs and requirements before deciding which method to 398 employ.

399

#### 400 Open access data

To increase the impact of the temperature data, the majority of which has been funded from public resources, it is appropriate for the data to be available via an online, open access data portal. Open access data encourages and enables technical and non-technical stakeholders, including local authorities, planners, developers, policy makers and regulators to better plan and de-risk subsurface development including ground source heat recovery and storage. It is hoped that research and development will also be supported by the open access data.

407

Positive societal and environmental impacts will be realised if low-carbon ground source heat and 408 recovery becomes part of the renewable energy mix, and open access data can raise the profile of this 409 type of work. Open access data allows informed decisions to be taken about the subsurface reducing 410 411 the risks of delays and overspend and increasing investor confidence that systems will be financially 412 viable and technologically reliable. We recommend that particularly where geo-observatories are publically funded data should be made available via open-access portals as this increases the 413 414 likelihood of data being utilised to its full potential and allows for greater collaboration with a host of 415 other interested organisations.

416

417 Integrating evidence into decision making

418 Data from urban geo-observatories could be used to support early-stage integration of low-carbon heat networks into new development areas. Evidence has been shared with partners and stakeholders 419 including the City of Cardiff Council and the National Assembly for Wales in order to support policy 420 planning and decision making that is based on scientific evidence. Positive outcomes of this approach 421 422 have included the addition of shallow geothermal energy into the Heat Network Delivery Unit (HNDU) master plan for Cardiff, and inclusion of the demonstrator ground source heat pump in a 423 424 national briefing paper (National Assembly for Wales 2018). However, challenges such as how to 425 integrate this evidence to support new policy, urban planning and heat regulation decisions remain. 426 Development of geo-observatories in partnership with local authorities can help ensure scientific data 427 is engaged with by planners at an early stage and thus increase the likelihood of sustainable 428 development based on evidence. Similarly, case studies of successful geo-observatories that provide 429 baseline data on which areas such as Cardiff have been able to make strategic decisions can prove 430 useful in illustrating the need for similar investment elsewhere. Baseline data prove resource 431 availability prior to system installation, reducing the risk of unsuitable sites being selected at 432 feasibility stage. Furthermore, these data can be used to characterise change from background 433 conditions thus identifying the long-term effects. Through integration into planning and regulation, 434 this can enable better management of subsurface heat thus making its exploitation a more reliable and 435 sustainable prospect.

436

### 437 Thermal management and ownership of heat

One of the main challenges in the UK is the absence of a regulatory framework that enables 438 management and governance of heat in the subsurface. If not managed properly, issues surrounding 439 ownership of heat resources may lead to conflict between users and interference between systems, 440 reducing the effectiveness of installations and undermining investor and public confidence. 441 Disparities between the regulatory approach applied to closed loop (no regulation) and open-loop 442 systems (abstraction licence and permit to discharge) results in fewer open-loop systems and more, 443 444 unregulated closed-loop systems. The need for better management of subsurface heat in the UK has 445 been highlighted previously (Fry 2009; Herbert et al. 2013; Abesser et al.; 2018) however little has

446 been done at government level to address these concerns. The Common Vision for the Renewable Heating and Cooling sector in Europe recommends that authorisation procedures associated with this 447 type of technology be streamlined, with the cost of permits reduced to encourage uptake, whilst at the 448 same time not compromising the environment (Sanner, et al. 2011). With heat recovery becoming 449 450 ever more topical it is time for policy makers to work closely with scientists and engineers from industry to address these challenges. Whilst they do not address the ownership of heat directly, urban 451 geo-observatories can provide evidence, required to support decision making on the ownership and 452 453 governance of heat in the subsurface. We propose there is an urgent need to update licencing, permitting and policy to reflect the challenges of a low-carbon economy, and that scientists, industry, 454 455 policy makers and regulators need to work together to address this challenge.

456

### 457 Limitations

458 Re-purposing an existing groundwater monitoring network has several logistical and cost advantages however this approach has led to data being limited to the locations of a network not originally 459 460 designed for this purpose. Ideally, boreholes should be drilled where they will be of most use to the 461 purpose of the geo-observatory to yield the best data coverage, however, due to the extensive network 462 in Cardiff the data covers the key lithologies, land use and spatial cover. The total number of sensors was governed by the available funding, however the amount deployed in Cardiff is considered 463 sufficient. We recommend that where possible multiple sensors are installed in boreholes to 464 characterise the depth to the Zone of Seasonal Fluctuation which is variable within urban areas. 465 Finally, it is noted that in order to produce hydrogeological and heat transport models, and enable 466 long-term temperature forecasting, other datasets need to obtained in addition to the groundwater 467 temperature and levels, geotechnical data and the 3D geological model. These data include sewer and 468 water mains, land use and land cover maps, details about recharge potential, and thermal properties 469 470 data.

471

472 Conclusion

Establis	shment of a geo-observatory can provide evidence of subsurface conditions required by policy
makers	, regulators, planners and developers to implement ground source heat recovery and storage
scheme	es. We conclude that;
•	A city-wide monitoring approach is favoured to be applicable across an aquifer to allow for
	the characterisation of the available resource and the long-term implications of its use. The
	accompaniment of 3D geological models provides a conceptual framework for planning and
	development of subsurface heat recovery and storage schemes.
•	Re-purposing existing groundwater monitoring boreholes is a cost effective way to establish a
	geo-observatory.
•	Partnership with local authorities can highlight the potential of ground source heating in urban
	areas and increases the likelihood that data will be used to make strategic decisions.
•	Temperature sensors should be placed across a range of depth, land use and land cover to
	characterise temperatures throughout target aquifer. Low-cost, reliable sensors allow more
	boreholes to be instrumented, however consideration should be given to required resources.
	Telemetry is not essential for all monitoring points and can be concentrated in boreholes
	where dynamic or rapid changes may occur, for example at active ground source heat pumps.
	Manual sensors are a cost effective alternative to telemetry in accessible sites or where
	security may be an issue.
•	Open access portals allow planners, developers, researchers and heat pump installers to better
	design shallow heat recovery and storage systems, increasing investor confidence. Baseline
	data could benefit regulators and policy makers, allowing evidence-based decisions ensuring
	Establis makers scheme • •

499	sustainable use of subsurface resources. Data is needed for long-term temperature forecasting
500	and can form a basis for hydrogeological and heat transport models.
501	
502	• Thermal management and ownership of heat in the subsurface are still key challenges that
503	need to be addressed in the UK if sustainable subsurface heat recovery and storage is to be
504	achieved. Scientists, policy makers and regulators need to work in partnership to develop a
505	fit-for-purpose regulatory approach to subsurface heat.
506	
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- 735
- 736 Figures
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Fig. 1. Quaternary geological map of the Cardiff Urban Geo-Observatory showing monitoring
boreholes, demonstrator ground source heat pump site and dewatering operations in the target sand
and gravel aquifer. Contains 1:50,000 BGS DiGMap and OS data © Crown Copyright and database
rights 2019.





**Fig. 2.** Above: Initial image from the developing 3D geological model of Cardiff (Kendall et al. 2018)

- 747 with monitoring borehole locations shows as pink dots, 5 x vertical exaggeration. **Below:** an exploded
- version of the same model but without the borehole locations ©British Geological Survey





Fig. 3. Groundwater temperatures, comprising of 3.75 million measurements between 2014 and 2017.
Box Plots show 25<sup>th</sup> and 75<sup>th</sup> percentile, and within the box the black line is the median and the red

- <sup>754</sup> line is the mean. The stalks represent the 5<sup>th</sup> and 95<sup>th</sup> percentile, outliers are not shown in this dataset.
- 755 Location of temperature sensors (Table. 2).

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**Fig. 4**. Schematic diagram of the demonstrator open loop ground source heat system at Grangetown

- , 0,

	Borehole Name	Purpose	Total depth (metres)
	1/OB1	Groundwater Temperature	14
	2/PB1	Groundwater Temperature	6
	3/OB1	Groundwater Temperature	18
	4/PB1	Groundwater Temperature	7
Name: 7/081	4/PB1	Groundwater Temperature	11
Depth: 5m	4/PB2	Groundwater Temperature	8
	4/PB2	Groundwater Temperature	12
	5/PB1	Groundwater Temperature	7
	5/PB1	Groundwater Temperature	10.5
	6/PB1	Groundwater Temperature	6.7
	6/PB2	Groundwater Temperature	10
	6/PB4	Groundwater Temperature	6.3
	7/OB1	Groundwater Temperature	5
	8/OB1	Groundwater Temperature	7
	9/OB1	Groundwater Temperature	6.2

- Fig. 5. The Cardiff Urban Geo-Observatory open-access data portal where groundwater temperature
- data from the manually downloaded and telemetered sensors is archived
- 774 (www.ukgeos.ac.uk/observatories/cardiff). Contains NERC materials ©NERC 2019.





Fig. 6. Box plots showing the range of Fe and Mn (ug/l) in groundwater samples collected between
2000 – 2012 from the 'groundwater control zones' which are dewatering operations in the sand and
gravel aquifer. The box part of the Box Plots show 25<sup>th</sup> and 75<sup>th</sup> percentile, the line through the middle
is the mean and stalks show the 5<sup>th</sup> and 95<sup>th</sup> percentile with the black dots marking the extent of the
outliers. Data reproduced with kind permission of Cardiff Harbour Authority.

# 791 Tables

Country	City / Region	Description	Reference
UK	Cardiff	Mapping groundwater temperatures in a glaciofluvial sand & gravel aquifer. Depth 0-30 m.	Farr <i>et al</i> . 2017
	London	Interaction of open loop ground source heat pumps, thermal modelling of multiple open loop schemes.	Fry, 2009; Headon <i>et al.</i> 2009; Herbert <i>et al.</i> 2013
Republic of Ireland	Cork	Characterising groundwater temperatures in a sand & gravel aquifer. 0-50 m depth.	Allen et al. 2003
Germany	Berlin Munich Cologne Karlsruhe Hamburg	Groundwater temperature monitoring networks in sand and gravel aquifers, heat potential, groundwater modelling, evolution of temperatures and anthropogenic heat fluxes	Benz <i>et al.</i> 2016; Zhu <i>et al.</i> 2010; 2015; Menberg <i>et al.</i> 2013a; b
	Ludwigsburg	Modelling of geothermal potential	Schiel et al. 2016
Netherlands	Amsterdam, The Hague and	Web based viewer for groundwater temperatures	Bonsor et al. 2017
	Herleen		
Finland	Turku, Lohja & Lahti	Characterising geothermal potential i glacial sand and gravel aquifers. Depth 0-60m. Country wide geothermal potential mapping	Arola & Korkka-Niemi 2014; Arola <i>et al.</i> 2014
Spain	Barcelona & Zaragoza	Characterising, monitoring & modelling of quaternary aquifer impacted by ground source heat pumps, management of thermal resources.	García-Gill <i>et al.</i> 2014; 2015a; 2015b; Epting <i>et al.</i> 2017
Slovenia	Ljubljana	Thermal conductivity & groundwater temperature monitoring	
			Janža <i>et al.</i> 2017
Italy	Cuneo province	Assessment and mapping of groundwater temperature	Casasso <i>et al.</i> 2017
Austria	Vienna	Trends in groundwater temperature	Benz et al. 2018a
a : 1 1	Leibnitz	Modelling of fulvioglacial aquifer	Händel <i>et al.</i> 2013
Switzerland	Zurich & Basel	Characterising, monitoring and modelling of urban aquifers. Sustainable management of thermal resources.	Benz <i>et al.</i> 2016; Epting <i>et al.</i> 2013; Epting & Huggenberger 2013; Epting, 2017; Mueller <i>et al.</i> 2018; Epting 2017; Epting <i>et al.</i> 2018
Japan	Tokyo & Osaka	Groundwater temperature monitoring network, with repeat temperature profiling of boreholes and assessment of urban heat island	Taniguchi <i>et al.</i> 2007; Hayashi <i>et al.</i> 2009; Arimoto <i>et al.</i> 2015; Benz <i>et al.</i> 2018b.
Korea	Seoul	National groundwater temperature monitoring network	Lee 2006; Taniguchi et al. 2007
Canada	Winnipeg	Groundwater temperature measurements in 40 wells	Ferguson et al. 2007; Zhu et al. 2010

793 Table 1. Global examples groundwater characterisation, monitoring and modelling of shallow groundwater aquifers and the subsurface Urban Heat Island

1/OBI       318511       174275       S&G       1       14.0         2/PB1       318801       174561       S&G       1       6.0         2/PB2       318851       174749       S&G       3       15.0         3/OBI       318857       17478       S&G       1       18.0         4/PB1       317766       174778       S&G       1       17.0 & 11.0         4/PB2       317973       17428       S&G       1       1.1       7.0 & 11.0         5/PB2       317886       175652       S&G       3       10.0       6       6         6/PB1       317733       175652       S&G       1       10.0       6       6         6/PB1       317373       175628       S&G       1       6.3       7.0       8/0B1       316633       17653       S&G       1       6.3         9/OB1L       318181       176098       S&G       1       13.0       CS037C       317624       17358       S&G       1       14.5         CS037C       317641       174789       S&G       1       13.2       CS074AL       315834       174789       S&G       1       13.2       CS163AL	Borehole ID	Easting	Northing	Geology	Sensor Type	Sensor depth mbgl
2/PB1         318809         174561         S&G         1         6.0           2/PB2         318851         174749         S&G         3         15.0           3/OB1         318857         174859         S&G         1         18.0           4/PB1         317766         174778         S&G         1         7.0 & 11.0           4/PB2         317973         174828         S&G         1,1         7.0 & 10.0         8.12.0           5/PB1         317866         175652         S&G         1         10.0         6           6/PB2         317616         176069         S&G         1         10.0         6           6/PB4         317307         176228         S&G         1         6.3         7           9/OB1U         318181         176098         S&G         1         13.0         2           CS002A         317162         175103         S&G         1         13.2         2           CS017A         31872         17469         S&G         1         13.2         2           CS037A         31872         17469         S&G         1         1.5         2           CS167A         318972<	1/OB1	318511	174275	S&G	1	14.0
2/PB2         318851         174749         S&G         3         15.0           3/OB1         318857         174859         S&G         1         18.0           4/PB1         317766         174778         S&G         1         7.0 & 11.0           4/PB2         317973         174828         S&G         1,1,3         8.0,10.0 & 12.0           5/PB1         317866         175652         S&G         3         10.0           6/PB1         317786         175652         S&G         1         10.0           6/PB2         317861         176052         S&G         1         6.3           7/OB1L         317147         176374         S&G         1         6.3           7/OB1L         318181         176098         S&G         1         6.3           9/OB1U         318181         176098         S&G         1         13.0           CS037C         317624         173558         S&G         1         13.2           CS047A         318972         174669         S&G         1         13.2           CS074AL         318581         174738         S&G         1         15.5           CS133CL         <	2/PB1	318809	174561	S&G	1	6.0
3/OB1       318857       174859       S&G       1       18.0         4/PB1       317766       174778       S&G       1       7.0 & 11.0         4/PB2       317973       174828       S&G       1       7.0 & 11.0         5/PB1       317866       175652       S&G       3       10.0         5/PB2       317866       175652       S&G       1       6.7         6/PB1       317737       1747373       S&G       1       6.7         6/PB2       317616       176069       S&G       1       6.7         6/PB4       317377       176228       S&G       1       6.3         7/OB1L       317147       176374       S&G       1       6.3         9/OB1U       318181       176098       S&G       1       13.0         CS002A       317162       175103       S&G       1       13.0         CS007A       318972       174669       S&G       1       13.2         CS074A       318341       175882       S&G       1       13.2         CS133CL       320293       176158       S&G       1       1.5         CS133CL       320293	2/PB2	318851	174749	S&G	3	15.0
4/PB1       317766       174778       S&G       1       7.0 & 11.0         4/PB2       317973       174828       S&G       1,1,3       8.0,10.0 & 12.0         5/PB1       317886       175652       S&G       3       10.0       6         5/PB2       317866       175652       S&G       1       6.7         6/PB2       317616       176069       S&G       1       10.0         6/PB4       317307       176228       S&G       1       6.3         7/OB1L       317147       17674       S&G       1       5.0         8/OB1       316683       176653       S&G       1       6.2         9/OB1U       318181       176098       S&G       1       6.2         9/OB1U       318181       176098       S&G       1       14.5         CS037       31765       174736       S&G       1       15.2         CS038       317655       174736       S&G       1       14.5         CS038       317675       174736       S&G       1       15.2         CS174AL       315834       174789       S&G       1       15.2         CS1304L	3/OB1	318857	174859	S&G	1	18.0
4/PB2       317973       174828       S&G       1,1,3       8.0,10.0 & 12.0         5/PB1       317886       175652       S&G       3       10.0         6/PB1       317783       175973       S&G       1       6.7         6/PB2       317616       176069       S&G       1       10.0         6/PB4       317307       176228       S&G       1       6.3         7/OB1L       317147       176374       S&G       1       6.3         7/OB1L       317147       176374       S&G       1       6.2         9/OB1U       318181       176098       S&G       1       13.0         CS002A       317162       175103       S&G       1       14.5         CS037C       317624       173558       S&G       1       13.2         CS074AL       315834       17582       S&G       1       13.2         CS074AL       315834       17489       S&G       1       10.3         CS116AL       31828       174638       S&G       1       10.3         CS159AL       317873       175526       S&G       1       15.5         CS217       318478	4/PB1	317766	174778	S&G	1	7.0 & 11.0
5/PB1       317886       175652       \$&G       3       10.0         5/PB2       317886       175652       \$&G       3       10.0         6/PB1       317783       175973       \$&G       1       10.0         6/PB2       317616       176069       \$&G       1       10.0         6/PB4       317307       176228       \$&G       1       6.3         7/OB1L       317147       176573       \$&G       1       6.3         9/OB1U       318181       176098       \$&G       1       6.2         9/OB1L       318181       176098       \$&G       1       13.0         CS002A       317162       175103       \$&G       1       14.5         CS037C       317624       173558       \$&G       1       6.0         CS047A       318972       174669       \$&G       1       13.2         CS074AL       315834       174789       \$&G       4       6.5         CS116AL       318258       174638       \$&G       1       10.3         CS178AL       319076       174919       \$&G       1       8.5         CS207AL       316639       1746	4/PB2	317973	174828	S&G	1, 1, 3	8.0, 10.0 & 12.0
5/H82       31/886       175522       S&G       3       10.0         6/PB1       317783       175973       S&G       1       6.7         6/PB2       317616       176069       S&G       1       10.0         6/PB4       317307       176228       S&G       1       6.3         7/OB1L       317147       176374       S&G       4       6.2         9/OB1U       318181       176098       S&G       1       6.2         9/OB1L       318181       176098       S&G       1       13.0         CS002A       317162       17353       S&G       1       14.5         CS038       317685       174736       S&G       1       6.0         CS047A       318972       174669       S&G       1       13.2         CS074A       315834       174789       S&G       4       6.5         CS116AL       318258       174638       S&G       1       10.3         CS178AL       319076       174911       S&G       1       8.8         CS207AL       31639       174699       S&G       1       8.0         CS217       318478       174785 <td>5/PB1</td> <td>317886</td> <td>175652</td> <td>S&amp;G</td> <td>1,1</td> <td>7.0 &amp; 10.5</td>	5/PB1	317886	175652	S&G	1,1	7.0 & 10.5
6/FB1         317/83         1759/3         S&G         1         6.7           6/FB2         317616         176069         S&G         1         10.0           6/FB4         317307         176228         S&G         1         6.3           7/OB1L         317147         176374         S&G         1         5.0           8/OB1         316683         176653         S&G         4         7.0           9/OB1L         318181         176098         S&G         1         13.0           CS002A         317162         175103         S&G         1         14.5           CS037C         317624         173558         S&G         1         14.5           CS038         317685         174736         S&G         1         13.2           CS074AL         315834         17582         S&G         1         6.0           CS074AL         318278         174639         S&G         1         1.5           CS116AL         318278         174639         S&G         1         1.5           CS178AL         319076         174911         S&G         1         8.0           CS217         318478         <	5/PB2	317886	175652	S&G	3	10.0
b7B2       317616       170069       S&G       1       10.0         67B4       317307       176328       S&G       1       6.3         7/OB1L       317147       176374       S&G       1       6.3         8/OB1       316683       17653       S&G       1       6.2         9/OB1U       318181       176098       S&G       1       13.0         CS002A       317162       175103       S&G       1       14.5         CS037C       317624       173558       S&G       1       6.0         CS067A       318972       174669       S&G       1       6.0         CS074AL       315834       17582       S&G       1       6.0         CS074AL       315834       17582       S&G       1       6.0         CS1996       318483       174789       S&G       1       12.5         CS133CL       320293       176158       S&G       1       1.5         CS178AL       319076       174911       S&G       1       8.0         CS211       315617       177038       S&G       1       7.0         CS233       318300       174920	6/PB1	317/83	175973	S&G	1	6.7
6/P34       31730/       176228       \$&G       1       5.3         7/OBIL       317147       176374       \$&G       1       5.0         8/OBI       316683       176653       \$&G       1       6.2         9/OBIU       318181       176098       \$&G       1       13.0         CS002A       317162       175103       \$&G       1       7.9         CS037C       317624       173558       \$&G       1       14.5         CS038       317685       174736       \$&G       1       6.0         CS07AA       318972       174669       \$&G       1       13.2         CS074AL       315834       174789       \$&G       4       6.5         CS16AL       318258       174638       \$&G       1       10.3         CS178AL       319076       174699       \$&G       1       8.0         CS217       318478       174789       \$&G       1       8.0         CS217       318478       174790       \$&G       1       7.0         CS229       317833       175143       \$&G       1       1.5         CS2248       318300       174920	6/PB2	31/010	17(009	S&G	1	10.0
7/081L $317/14$ $176374$ $8&G$ $1$ $5.0$ $8/0B1$ $316683$ $176653$ $8&G$ $4$ $7.0$ $9/0B1U$ $318181$ $176098$ $8&G$ $1$ $6.2$ $9/0B1L$ $318181$ $176098$ $8&G$ $1$ $13.0$ $CS002A$ $317162$ $175103$ $8&G$ $1$ $14.5$ $CS037C$ $317624$ $173558$ $8&G$ $1$ $14.5$ $CS037C$ $317624$ $173558$ $8&G$ $1$ $16.0$ $CS067A$ $318972$ $17469$ $8&G$ $1$ $13.2$ $CS074AL$ $315834$ $175822$ $8&G$ $1$ $6.0$ $CS096$ $318483$ $174789$ $8&G$ $1$ $6.0$ $CS096$ $318483$ $174789$ $8&G$ $1$ $10.3$ $CS174AL$ $318258$ $174638$ $8&G$ $1$ $10.3$ $CS178AL$ $319076$ $174911$ $8&G$ $1$ $8.8$ $CS207AL$ $316639$ $174699$ $8&G$ $1$ $8.8$ $CS217$ $318478$ $174785$ $8&G$ $1$ $7.0$ $CS213$ $318300$ $174920$ $8&G$ $1$ $7.0$ $CS238A$ $318427$ $17453$ $8&G$ $1$ $11.5$ $CS244B$ $318310$ $175193$ $8&G$ $1$ $11.4$ $CS266$ $316841$ $173938$ $8&G$ $1$ $7.0$ $CS275$ $31877$ $176639$ $8&G$ $1$ $7.0$ $CS278$ $318092$ </td <td>6/PB4</td> <td>31/30/</td> <td>176228</td> <td>S&amp;G</td> <td>1</td> <td>6.3</td>	6/PB4	31/30/	176228	S&G	1	6.3
a) (3) (3) (3) (3) (3) (3) (3) (3) (3) (3	//OBIL 8/OD1	31/14/	176652	S&G	1	5.0
9/OB1L       318181       176098       S&G       1       6.2         9/OB1L       318181       176098       S&G       1       13.0         CS002A       317162       175103       S&G       1       7.9         CS037C       317624       173558       S&G       1       14.5         CS038       317685       174736       S&G       1       6.0         CS074AL       315834       175882       S&G       1       6.0         CS096       318483       174789       S&G       4       6.5         CS116AL       318258       174638       S&G       1       10.3         CS178AL       319076       174911       S&G       1       8.8         CS207AL       316639       174699       S&G       1       8.0         CS211       315617       174699       S&G       1       8.0         CS217       318478       174785       S&G       1       1.5         CS223       318300       174420       S&G       1       1.5         CS244       317980       174455       S&G       1       1.5         CS245       317632       17445	0/OP1U	210105	176008	Sau	4	7.0
57.0512       318161       17050       3&G       1       15.0         CS002A       317162       175103       3&G       1       7.9         CS037C       317624       173558       S&G       1       14.5         CS038       317685       174736       S&G       1       6.0         CS07AL       318972       174669       S&G       1       6.0         CS096       318483       174789       S&G       4       6.5         CS116AL       318258       174638       S&G       1       10.3         CS159AL       317873       175526       S&G       1       10.3         CS178AL       319076       174911       S&G       1       8.0         CS211       315617       177038       S&G       1       8.0         CS217       318478       174785       S&G       1       1.5         CS229       317833       175143       S&G       1       1.5         CS211       315617       177038       S&G       1       1.5         CS2233       318300       17420       S&G       1       1.5         CS244       317980       174445	9/OB10 9/OB11	218181	1760098	S&C	1	0.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$CS002\Delta$	317162	175103	S&G	1	79
CS03C317645174736S&G114.5CS038317685174736S&G16.0CS067A318972174669S&G113.2CS074AL315834175882S&G16.0CS096318483174789S&G46.5CS116AL318258174638S&G110.3CS159AL3120293176158S&G11.5CS178AL319076174911S&G8.8CS207AL316639174699S&G18.0CS211315617177038S&G13.9CS217318478174785S&G11.5CS229317833175143S&G11.5CS241317980174455S&G11.5CS243318300174920S&G7.0 &11.0CS238A318427174553S&G11.5CS241317980174445S&G11.5CS248318510175193S&G17.8CS266316841173938S&G11.4CS272317632174343S&G11.4CS274B319528177162S&G45.0CS27431802173967S&G11.8.9CS276319891174627S&G11.5.5CS304L319822175375S&G11.5.5CS30631934	CS037C	317624	173558	5&G	1	14.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS038	317685	174736	5&G	1	6.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS067A	318972	174669	5&G	1	13.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS074AL	315834	175882	S&G	1	60
CS116AL       318258       174638       S&G       1       12.5         CS116AL       318258       174638       S&G       1       10.3         CS159AL       317873       175526       S&G       1       1.5         CS178AL       319076       174911       S&G       1       8.8         CS207AL       316639       174699       S&G       1       8.0         CS211       315617       177038       S&G       1       3.9         CS217       318478       174785       S&G       1       7.0         CS229       317833       175143       S&G       7.0 &11.0         CS233A       318300       174920       S&G       7.0 &11.0         CS238A       318427       174553       S&G       1       1.5         CS241       317980       174445       S&G       1       1.5         CS248       318510       175193       S&G       1       1.5         CS266       316841       173938       S&G       1       1.4         CS268       317646       175838       S&G       1       1.9         CS275       318177       17639       S&G	CS096	318483	174789	S&G	4	6.5
CS133CL320293176158S&C110.3CS159AL $317873$ 175526S&G11.5CS178AL $319076$ $174911$ S&G18.8CS207AL $316639$ $174699$ S&G18.0CS211 $315617$ $177038$ S&G13.9CS217 $318478$ $174785$ S&G17.0CS233 $318300$ $174920$ S&G7.0 &11.0CS238A $318427$ $174553$ S&G115.5CS241 $317980$ $174445$ S&G111.5CS245B $318368$ $175683$ S&G111.5CS2448 $318510$ $175193$ S&G17.8CS266 $316841$ $173938$ S&G111.4CS268 $317646$ $175838$ S&G17.0CS272 $317632$ $174343$ S&G11.1.0CS274B $319528$ $177162$ S&G44.7CS276 $319891$ $174627$ S&G44.7CS278 $318002$ $173967$ S&G118.9CS283 $318639$ $175375$ S&G11.5.5CS304L $319892$ $175455$ S&G11.0.2CS307L $319251$ $174489$ S&G114.2CS308L $319448$ $174447$ S&G118.1CS313L $317761$ $176618$ S&G43.0CS317L<	CS116AL	318258	174638	S&G	1	12.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS133CL	320293	176158	S&G	1	10.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS159AL	317873	175526	S&G	1	1.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS178AL	319076	174911	S&G	1	8.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS207AL	316639	174699	S&G	1	8.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS211	315617	177038	S&G	1	3.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS217	318478	174785	S&G	1,1	7.5 & 11.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS229	317833	175143	S&G	1	7.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS233	318300	174920	S&G		7.0 &11.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS238A	318427	174553	S&G	1	15.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS241	317980	174445	S&G	1	11.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS245B	318368	175683	S&G	1	8.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS248	318510	175193	S&G	1	7.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS266	316841	173938	S&G	1	11.4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS268	317646	175838	S&G	1	7.0
CS274B $319528$ $177162$ $S\&G$ $1$ $5.2$ CS275 $318177$ $176639$ $S\&G$ $4$ $5.0$ CS276 $319891$ $174627$ $S\&G$ $4$ $4.7$ CS278 $318002$ $173967$ $S\&G$ $1$ $18.9$ CS283 $318639$ $175375$ $S\&G$ $1$ $7.7$ CS285 $314982$ $178077$ $S\&G$ $1$ $3.0$ CS301L $317779$ $172783$ $S\&G$ $1$ $15.5$ CS304L $319892$ $175445$ $S\&G$ $1$ $13.7$ CS306 $319349$ $174529$ $S\&G$ $1$ $10.2$ CS307L $319251$ $174489$ $S\&G$ $1$ $14.2$ CS308L $319448$ $174447$ $S\&G$ $1$ $18.1$ CS317L $318139$ $174388$ $S\&G$ $1$ $12.4$ CS318 $317761$ $176618$ $S\&G$ $4$ $3.0$ CS329 $317408$ $175515$ $S\&G$ $1$ $6.5$	CS272	317632	174343	S&G	1,1	7.0 & 11.0
CS275 $318177$ $176639$ $S\&G$ $4$ $5.0$ CS276 $319891$ $174627$ $S\&G$ $4$ $4.7$ CS278 $318002$ $173967$ $S\&G$ $1$ $18.9$ CS283 $318639$ $175375$ $S\&G$ $1$ $7.7$ CS285 $314982$ $178077$ $S\&G$ $1$ $3.0$ CS301L $317779$ $172783$ $S\&G$ $1$ $15.5$ CS304L $319892$ $175445$ $S\&G$ $1$ $13.7$ CS306 $319349$ $174529$ $S\&G$ $1$ $10.2$ CS307L $319251$ $174489$ $S\&G$ $1$ $14.2$ CS308L $319448$ $174447$ $S\&G$ $1$ $18.1$ CS313L $317526$ $174252$ $S\&G$ $1$ $11.0$ CS317L $318139$ $174388$ $S\&G$ $4$ $3.0$ CS318 $317761$ $176618$ $S\&G$ $4$ $3.0$	CS274B	319528	177162	S&G	1	5.2
CS276       319891       174627       S&G       4       4.7         CS278       318002       173967       S&G       1       18.9         CS283       318639       175375       S&G       1       7.7         CS285       314982       178077       S&G       1       3.0         CS301L       317779       172783       S&G       1       15.5         CS304L       319892       175445       S&G       1       13.7         CS306       319349       174529       S&G       1       10.2         CS307L       319251       174489       S&G       1       14.2         CS308L       319448       174447       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0	CS275	318177	176639	S&G	4	5.0
CS278       318002       173967       S&G       1       18.9         CS283       318639       175375       S&G       1       7.7         CS285       314982       178077       S&G       1       3.0         CS301L       317779       172783       S&G       1       15.5         CS304L       319892       175445       S&G       1       13.7         CS306       319349       174529       S&G       1       10.2         CS307L       319251       174489       S&G       1       14.2         CS308L       319448       174447       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       6.5	CS276	319891	174627	S&G	4	4.7
CS283       318639       175375       S&G       1       7.7         CS285       314982       178077       S&G       1       3.0         CS301L       317779       172783       S&G       1       15.5         CS304L       319892       175445       S&G       1       13.7         CS306       319349       174529       S&G       1       10.2         CS307L       319251       174489       S&G       1       14.2         CS308L       319448       174447       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       6.5	CS278	318002	173967	S&G	1	18.9
CS285       314982       178077       S&G       1       3.0         CS301L       317779       172783       S&G       1       15.5         CS304L       319892       175445       S&G       1       13.7         CS306       319349       174529       S&G       1       10.2         CS307L       319251       174489       S&G       1       14.2         CS308L       319448       174447       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       6.5	CS283	318639	175375	S&G	1	7.7
CS301L       317779       172783       S&G       1       15.5         CS304L       319892       175445       S&G       1       13.7         CS306       319349       174529       S&G       1       10.2         CS307L       319251       174489       S&G       1       14.2         CS308L       319448       174447       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       6.5	CS285	314982	178077	S&G	1	3.0
CS304L       319892       175445       S&G       1       13.7         CS306       319349       174529       S&G       1       10.2         CS307L       319251       174489       S&G       1       14.2         CS308L       319448       174447       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       6.5	CS301L	317779	172783	S&G	l	15.5
CS306       319349       1/4529       S&G       1       10.2         CS307L       319251       174489       S&G       1       14.2         CS308L       319448       174447       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       65	CS304L	319892	175445	S&G	l	13.7
CS30/L       319251       1/4489       S&G       1       14.2         CS308L       319448       174447       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       6.5	CS306	319349	174529	S&G	l	10.2
CS308L       319448       1/444/       S&G       1       18.1         CS313L       317526       174252       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       6.5	CS30/L	519251 210449	1/4489	S&G	1	14.2
CS313L       31/326       1/4232       S&G       1       11.0         CS317L       318139       174388       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       65	CS308L	519448 217526	1/4447/	S&G	1	18.1
CS31/L       518159       1/4588       S&G       1       12.4         CS318       317761       176618       S&G       4       3.0         CS329       317408       175515       S&G       1       6.5	CS313L	51/526 218120	1/4252	S&G	1	11.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	CS31/L CS319	318139 217761	1/4588	S&G	1	12.4
	CS320	317/01	175515	520	4 1	5.0

Borehole ID	Easting	Northing	Geology	Sensor Type	Sensor depth mbgl
CS332L	317494	172439	S&G	1	6.0
CS335	317880	176242	S&G	4	4.0
CS337	317372	177025	S&G	4	5.5
MG023	317928	174829	MG	1	1.50
Ground Source Heat Pump Demonstrator Site					
Abstraction	318104	174495	S&G	3	10.0
Recharge	318120	174502	S&G	3	8.0
OBS1	318066	174436	S&G	2	10.0
OBS2	318008	174384	S&G	2	10.0
Techniquest	318987	174408	MM	1,3	10.0, 15.0, 50.0 &120.0

- 797 Mercia Mudstone Group (bedrock)
- 799 Sensor Type:
- $1 = \text{Hobo Temp Pro V2}^{\text{(Bange 0 to + 50 °C, resolution 0.02°C, accuracy } \pm 0.21^{\circ}\text{C})}$
- 2 =Solinst Levellogger<sup>®</sup> (Range 0 to +50 °C, resolution 0.003 °C, accuracy  $\pm 0.05 °C$ )
- $3 = OTT^{\text{®}}$  Hydrometry<sup>®</sup> Orpheus Mini (Range (Range 0-70°C, resolution 0.1°C, accuracy  $\pm 0.5^{\circ}$ C) via
- 804 telemetry
- $4 = OTT^{\text{®}}$  Hydrometry<sup>®</sup> Orpheus Mini (Range (Range 0-70°C, resolution 0.1°C, accuracy ±0.5°C)

- **Table 2.** Locations of groundwater temperature sensors (all borehole logs are open access and can be
- 809 viewed on the British Geological Survey 'Onshore GeoIndex' viewers (<u>www.bgs.ac.uk</u>))

<sup>796</sup> Geology: MG = Made Ground, S&G = Quaternary Glaciofluvial Sand and Gravel, MM = Triassic