

# Submarine Platform Development by Erosion of a Surtseyan Cone at Capelinhos, Faial Island, Azores

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## **Abstract**

Erosion of volcanic islands ultimately creates shallow banks and guyots, but the ways erosion proceeds to create them over time and how coastline retreat rate relates to wave conditions, rock mass strength and other factors are unclear. The Capelinhos volcano was formed in 1957/58 during a Surtseyan and partly effusive eruption that added a  $\sim 2.5 \text{ km}^2$  tephra and lava promontory to the western end of Faial Island (Azores, central North Atlantic). Subsequent coastal and submarine erosion has reduced the subaerial area of the promontory and created a submarine platform. This study uses historical information, photos and marine geophysical data collected around the promontory to characterize how the submarine platform developed following the eruption. Historical coastline positions are supplemented with coastlines interpreted from 2004 and 2014 Google Earth images in order to work out the progression of coastline retreat rate and retreat distance for lava- and tephra-dominated cliffs. Data from swath mapping sonars are used to characterise the submarine geometry of the resulting platform (position of the platform edge, gradient and morphology of the platform surface). Photographs collected during SCUBA and ROV dives on the submarine platform reveal a rugged surface now covered with boulders. The results show that coastal retreat rates decreased rapidly with time after the eruption and approximately follow an inverse power law relationship with coastal retreat distance. We develop a finite-difference model for wave attenuation over dipping surfaces to predict how increasing wave attenuation contributed to this trend. The model is verified by reproducing the wave height variation over dipping rock platforms in the UK (platform gradient  $1.2^\circ$  to  $1.8^\circ$ ) and

Ireland (1.8°). Applying the model to the dipping platform around Capelinhos, using a diversity of cliffs resistance predicted from known lithologies, we are able to predict erosion rate trends for some sectors of the edifice. We also explore wider implications of these results, such as how erosion creates shallow banks and guyots in reef-less mid-oceanic archipelagos like the Azores.

## **1. Introduction**

Submerged banks are common in volcanic archipelagos like the Azores. During periods of their evolution when they were islands or shallow banks they affected wave propagation (Arthur, 1951; Ponce de León and Guedes Soares, 2005), and were therefore important for inferring how wave conditions varied amongst the islands. At human time scales, quantifying such coastal erosion is necessary for planning purposes as waterfront properties and other infrastructures are commonly valuable assets of steep volcanic islands. Finally, from a biological perspective, understanding how long isolated islands survived before becoming submarine banks is also important, as coasts and shallow bottoms constitute critical stepping stones permitting long-distance species colonisation to occur by shorter stages (Whittaker, 1998).

Extensive field experiments and numerical modelling have explored and advanced our knowledge on how width, gradient and roughness of near-shore rock platforms affect wave dissipation and transformation (Trenhaile, 2000; Madin et al., 2006; Farrell et al., 2009; Sunamura et al., 2014; Poate et al., 2016; McCall et al., 2017; Poate et al., 2017). Although the factors affecting erosion are weakly constrained, modelling efforts have successfully reproduced the geometries of resulting rock platforms (e.g., Trenhaile, 2000). However, observations of coastal

retreat history in areas with varied lithology and wave conditions are rare, but are needed in order to refine coastline change models. Improving our understanding of the roles of wave exposure, resistance to erosion, seaward transport of eroded material and other factors could help us to improve predictions of retreat rates of rocky coasts more widely.

Coasts formed by historical volcanic activity provide an opportunity to observe the geomorphological effects of erosion at timescales ranging from the months following the end of eruption to periods reaching several decades. Surtseyan cones in exposed oceanic settings constitute exceptional fast-evolving case studies of coastal development (Quartau, 2010; Ramalho et al., 2013; Quartau et al., 2014; Romagnoli and Jakobsson, 2015).

In Surtseyan eruptions, explosive interactions of lava with water create friable volcanoclastic material (Moore, 1985; Kokelaar, 1983). In the case of Surtsey Island, the eruption produced a subaerial cone of such material that eventually isolated the vent from seawater, allowing lava to start extruding non-explosively (Thorarinsson, 1967; Thorarinsson, 1968). In Surtsey and other similar cones, the earlier friable material was easily eroded by surf, whereas later erupted lavas and palagonitized tephra were more resistant to erosion (Kokelaar and Durant, 1983; White, 1996; Cole et al., 2001; Murtagh and White, 2013; Romagnoli and Jakobsson, 2015; Ma et al., 2018). The poorly-consolidated materials making up Surtseyan cones can be efficiently mobilised by wave erosion and give rise to shallow marine platforms on timescales that are rapid compared with other environments (Romagnoli and Jakobsson, 2015), hence making studies possible, as here, using historical data.

The Capelinhos cone was emplaced as a typical Surtseyan cone (Cole et al., 1996; Cole et al., 2001) on the western-most end of Faial Island (Figure 1a) by an

eruption extending over 13 months (September 1957 - November 1958) (Machado et al., 1962; Cole et al., 1996; Cole et al., 2001). Borges (2004) quantified the Capelinhos rate of shoreline retreat until the year 1981 by assessing post-eruptive coastal development (Machado and Freire, 1985). His rates were averaged over the whole promontory, whereas in practice the lithology of Capelinhos coast varies along the coast. Although he provided no detailed explanation, he highlighted how the high retreat rates that immediately followed the eruption subsequently declined.

In this study, we have quantified coastal retreat rates for the Capelinhos promontory (from August 1958 to November 2014) based on historic coastline positions extracted from topographic maps and aerial images. The rates were quantified in a series of sectors with different lithology and orientation (hence wave exposure). Submarine geophysical data including multibeam and other sonar bathymetry and Chirp shallow seismic profiles provide information on the morphology and nature of the submarine feature carved by erosion. We describe the resulting submarine feature as a “platform” - a term, more typically used to describe the result of coastal erosion of more rigid rocky material over longer periods. We further compared the coastline retreat rates with the history of wave conditions. We have developed a finite difference model to predict how wave erosive force in front of the cliff varies with platform width, platform gradient, cliff resisting force and deep-water wave heights using wave attenuation models and have verified it using wave data. The combined approach has allowed us to investigate how and why the shoreline retreat rate changed with time after the eruption and how it affected the subaerial and submarine morphology of the promontory. We further discuss implications of the results to how some shallow banks are created by coastal erosion.

## 2. Regional Setting

### 2.1 Geological setting

The Azores archipelago comprises nine volcanic islands generally lying along a WNW-ESE trend in the centre of the North Atlantic Ocean. Faial Island lies in the central group of the islands, 130 km to the east of the Mid Atlantic Ridge (Figure 1b). It is 21 km long (WNW-ESE) and 14 km wide. Its highest peak reaches 1043 m above sea level (Madeira et al., 2015).

The Capelinhos volcano, in the western-most promontory of Faial, was formed within the Capelo rift zone that prolongs Faial to the WNW (Romer et al., 2018). According to the seabed contour map of Machado et al. (1959), which is based on a British Admiralty sounding chart, there was a submarine platform at Capelinhos before the eruption. That platform likely resulted from erosion of the earlier Costado da Nau cone, whose remnants are still visible in cliffs east of Capelinhos. Two small islets also existed prior to the Capelinhos eruption and were buried by it (these are presently being unearthed again by erosion). The depth and extent of this earlier platform unfortunately cannot be reliably reconstructed.

The eruption started underwater on 27<sup>th</sup> September 1957 and comprised three major phases of Surtseyan activity (Cole et al., 1996, 2001). Phase I lasted one month (September to October of 1957) and comprised hydromagmatic activity (Figure 2.a-b). Phase II, extending two months from November to December of 1957, included hydromagmatic activity and two days of discharge of lava flows (Figure 2.c-d). Phase III started in January 1958 with hydromagmatic activity and lasted four months (Figure 2.e-h). These phases were followed by additional lava discharges from late April 1958 until the end of the eruption in November 1958 (Figure 2.i-l), with flows covering some sectors of the tephra deposited by earlier

phases (Machado et al., 1962; Waters and Fisher, 1971; Cole et al., 1996; Cole et al., 2001). The physiographic and lithological evolution of Capelinhos during the eruption was well characterised by Machado et al. (1959) (Figure 2). They described how the eruption started underwater (Figure 3a) and was followed by an early phase of violent submarine explosions of gas, steam and black tephra ash (Figure 3b) that eventually gave rise to an emerged cinder ring (Figure 3c). The activity subsequently transitioned from Surtseyan to Strombolian as the cinder ring worked as a barrier isolating the vent from seawater (Figure 3d). The final shape of the Surtseyan cone was settled at the end of the eruption (Figure 3e) and has since been modified by wave erosion (Figure 3f, Machado et al., 1962; Cole et al., 1996; Cole et al., 2001).

The first (westernmost) tephra cone was dismantled by seaward collapses over 8 days in late October 1957. Frequent landslides and a partial collapse destroyed the remaining tephra cones (Cole et al., 1996; Cole et al., 2001) until lava flows emplaced in 1958 on the eastern side of Capelinhos fortified the third and last spatter cone.

By the end of the eruption, a total  $\sim 2.5 \text{ km}^2$  land area had been produced and the edifice reached  $\sim 160 \text{ m}$  above sea level (Machado et al., 1962). Based on topographic maps, Machado et al. (1959) estimated the volume of erupted tephra and lava reached  $\sim 0.15 \text{ km}^3$ , of which 56% was lava and 44% tephra. The tephra was mainly deposited from ash fallout and pyroclastic surges produced by subaerial and submarine explosions (Cole et al., 2001). Waters and Fisher (1971) characterised the continuously-bedded tephra layers, which vary significantly in clast size from finely-sorted and densely-graded impalpable dust to poorly-sorted, unconsolidated and coarse layers containing fragments exceeding  $\sim 50 \text{ cm}$  in size. Abundant lava chips and blocks also occur. Olivine basalt lavas with varied viscosity

flowed over the west and north flanks of the cone, with a larger volume to the northwest. A broad subaerial platform was then built along the seaward rim of the Capelinhos volcano, with most lava flows penetrating the sea (Machado et al., 1962). However, a lava flow emplaced on 23<sup>rd</sup> August 1958 fed by a feeder dyke immediately below the Capelinhos lighthouse (Figure 2k) failed to enter the sea (Cole et al., 2001).

From the coastline evolution of Machado et al. (1959), significant erosion of the seaward lava platform occurred and new beaches of volcanic ashes formed in June 1959 in the northeast and south. During the visits of Cole et al. (1996) in 1994 and 1995, the lava flow emplaced below the lighthouse (Figures 2k-2l) had become exposed to sea erosion. Large angular lava boulders resulting from the dismantling of the lava flow were found on the underlying southern beach. By 2007, the area of Capelinhos had been reduced to  $\sim 0.565 \text{ km}^2$  as a consequence of wave erosion, landslides, wind, precipitation and actions of visitors to the site (Forjaz, 2007; Forjaz et al., 2010).

## 2.2 Oceanographic setting

Faial Island is exposed to high-energy swells generated by distant storms in the Atlantic and to waves created by local winds. Their propagation through the islands has been modelled by Rusu and Soares (2012). The nearest windward lands to Faial are Flores and Corvo (Figure 1b) which lie  $\sim 234 \text{ km}$  to the WNW and represent only a minor interference to the prevailing swells hitting Faial from the west or northwest. The deep water surrounding the Azores islands and their narrow shelves imply that waves experience little attenuation before reaching the coasts when compared with continental shelf environments (Rusu and Soares, 2012).



Wave hindcast data presented in Carvalho (2003) for the period 1989-2002 suggest that the prevailing swells impinge Faial from the northwest (29%) and west (24%), with monthly-averaged offshore wave heights ranging between 1 and 4 m (with stronger wave conditions in winter than in summer). Violent storms associated with extratropical storms or hurricanes affect the Azores every 7 years on average (Andrade et al., 2008), a frequency mainly dominated by the North Atlantic Oscillation and partially affected by Eastern Atlantic atmospheric circulation. They bring extreme waves to Faial with heights exceeding 16 m and peak periods exceeding 18s (Quartau, 2007). “Christina” (also called storm “Hercules”) was the latest extreme cyclone to approach the Azores archipelago (5-7 January, 2014). The waves generated reached 9-11 m (Melo et al., 2018) and significantly damaged coastal structures (Santos et al., 2014). Faial’s mean annual tidal range is only ~0.9 m (Quartau et al., 2012), which corresponds to a microtidal regime (Short, 1996).

### **3. Materials and methods**

#### **3.1 Coastal change**

We digitised the shoreline positions of November 1958, May 1959, July 1964, September 1975 and March 1981 from the maps of Machado and Freire (1985). The coastlines of November 2004 and October 2014 were interpreted and digitised from Google Earth images ([google.com/earth](http://google.com/earth)). The coastlines are shown in Figures 4 and 5 georeferenced using a Universal Transverse Mercator projection (UTM, zone 26N). The Root Mean Square Errors (RMSEs) of georeferencing and digitizing were estimated using the georeferencing tool in ArcGIS to be 11–41 m (Table A1). In the following, we refer to elapsed time from the first map of the sequence following the eruption (November 1958).

Machado et al. (1959) classified the coasts as lava- and tephra-dominated. We have slightly extended their classification, using lava, tephra and mixed lava and tephra ("lava+tephra") classes. They were further divided them by location (north or south) resulting in a total of six sectors (Figure 5).

Areal changes were derived from the plan-view polygons lying between historical coastline positions, and laterally delimited by the sector boundaries (key in Figure 5). In each polygon, the lengths of coastline at dates  $T_a$  and  $T_b$  were measured as  $L_a$  and  $L_b$  (Table A2). The average coastline length  $L'$  for this time interval ( $\Delta T = T_b - T_a$ ) was then derived from  $L' = 0.5 * (L_a + L_b)$ . The areal change produced by erosion  $\Delta A$  in time interval  $\Delta T$  was measured using ArcGIS. From these values, the average incremental costal retreat rate of each sector  $\Delta D = \Delta A / L'$  and its average retreat rate  $R_r = \Delta D / \Delta T$  were determined. The total coastal retreat distance  $D = \sum \Delta D$  was also determined. The above calculations were conducted separately in the different sectors (Table 1). By repeating the measurements and calculations, the following uncertainties were estimated:  $L$ , ~5%;  $\Delta A$ , ~3%;  $\Delta D$ , ~8% and  $R_r$ , ~10% (including date uncertainty).

As the early coastline evolution was poorly characterised in both Capelinhos and Surtsey, we have studied this stage by resorting to a series of remote-sensing images (Appendix 4) of the Sholan Island (Red Sea), which erupted from 18 December 2011 (Xu et al., 2015). Although wave conditions are different in the Red Sea, and therefore rates will be different, those data suggest a different form of early coastal retreat distance with time and  $R_r$  with  $D$ .

### 3.2 Submarine geomorphology

Data from two bathymetric surveys were used to characterise the submarine

245 platform created by wave erosion. Deeper sections (depths 19 m to 216 m) were  
 246 surveyed in 2003 (Mitchell et al., 2008) using a Reson 8160 multi-beam sonar. The  
 247 near-shore area (depths 2 m to 77 m) was mapped with a Submetrix interferometric  
 248 swath sonar in 2004 (Tempera, 2008) (Figures 1a and 6a). Both datasets were  
 249 processed with tidal and attitude corrections and combined into a 5 m resolution grid  
 250 (Tempera, 2008) in UTM coordinates (zone 26N). Six bathymetric cross-sections  
 251 were selected to characterise the morphology of the submarine platform as shown in  
 252 Figure 6b. Some geometrical characteristics of these profiles are summarized in  
 253 Table 2. From these profiles, the positions of the platform edge were interpreted from  
 254 where seabed gradient changed prominently. They are marked by the orange circles  
 255 on the bathymetric profiles and vertical dashed orange lines in Figure 6b. Platform  
 256 width  $W$  was measured as the horizontal distance between the platform edge and  
 257 the present coastline. As the repose angle of loose volcanic talus is  $\sim 30^\circ$  (Mitchell et  
 258 al., 2000; Mitchell et al., 2012a), a possible geometry of the initial shallow submarine  
 259 slope can be represented by a surface running from the earliest post-eruption  
 260 coastline position at a  $30^\circ$  dip, as shown by the dipping dashed lines in Figure 6b.  
 261 Uncertainty in this early slope surface arises because the coastline position  
 262 immediately at the end of the eruption may not have been recorded exactly by the  
 263 maps of Machado and Freire (1985) and wave agitation may have caused the  
 264 volcanic material to deposit at a gradient smaller than the angle of repose.  
 265 Nevertheless, comparing this surface with the platform edge in the geophysical data  
 266 give us a possible measure of how much the platform edge has prograded by  
 267 material re-deposition. For comparison with the subaerial eroded volume, the  
 268 approximate volume of sediment deposited at and below the platform edge was  
 269 estimated by measuring and averaging the area of sediment deposition in each

sector and then multiplying by the November 1958 coastline length.

The three high-resolution seismic profiles shown in Figure 6c were collected in 2001 with a 1.5–10 kHz Chirp source across the submarine platform (Quartau, 2007) and illustrate its surficial morphology. Interpretation of the data followed the method of Quartau (2007) but was simplified to separate the rugged and smooth morphologies.

The seabed images shown in Figure 7 were acquired in 2004/2005 using Remotely Operated Vehicle (ROV) and SCUBA divers at locations S1 and S2 marked in Figure 6a. As no underwater acoustic positioning system was available, the photographs were located using GPS recordings of the research vessel position (Tempera, 2008). Photograph depths were not recorded, but were estimated from the bathymetric map to be ~38 m (ROV) and ~10 m (SCUBA dives).

### 3.3 Wave conditions

Using the hindcast data of Carvalho (2003), a rose diagram for offshore wave heights and their associated percentages and originating directions was produced (Figure 8a). We further characterised the wave properties during times when significant wave heights exceeded 5 m (Figure 8b), as 5 m is the minimum wave height for broken wave to exceed the threshold of erosion of less resistant cliff material (tephra) to initiate coastal erosion (Sunamura, 1992). (This 5 m value is further justified in Appendix 6.)

The European Centre for Medium range Weather Forecasts (ECMWF) 40-yr Re-Analysis (ERA-40) (Uppala et al., 2005) and ECMWF interim Re-Analysis (ERA-Interim) (Dee et al., 2011) are reconstructions of sea surface and meteorological conditions from a numerical model using meteorological observations as inputs.

These ERA model outputs have been shown to be reliable when compared against local wave buoy data collected in deep-water and for some coastal settings where waves are not shadowed by adjacent coasts (Caires and Sterl, 2003; Sterl and Caires, 2005; Mitchell et al., 2012b) as is the case of the fully-exposed shore of Capelinhos for waves not propagating from the east. ERA outputs of wave properties were extracted for a sea position adjacent to Capelinhos (38.625°N, 28.875°W) for the period 1957 to 2016 (60 years). In order to represent the properties of the most extreme waves, wave heights observed during each year were sorted and only the upper 5 percentile was retained. The mean and range of those heights are shown in Figure 9, and compared with historical coastal retreat rates. Appendix 7 shows the corresponding periods of these waves along with an analysis of extreme waves based on extreme value theory.

### 3.4 Coastal lithological observation

Capelinhos was visited on 5<sup>th</sup> and 6<sup>th</sup> July 2017 to make detailed observations from shore (Figures 10a, 10b, 10d and 10f), and combined with earlier observations by author F.T. in January 2011 from offshore (Figure 10c) and on land (Figure 10e). The rock mass strength of lava boulders protecting coastal cliffs in the south was assessed during the 2017 visit using a HT-225B concrete rebound test Schmidt hammer. The equipment was tested prior to fieldwork on a large steel object, returning a rebound value of 78, which is within the range of values ( $80 \pm 2$ ) that the manufacturer suggests should be obtained on steel anvils. In total, 30 measurements were taken using the Schmidt hammer along the south Capelinhos lava cliffs (located in Figures 10b and 10g). A further test after the fieldwork on the same large steel object produced again a value of 78. Schmidt hammer rebound

values ( $R$ ) were converted to rock comprehensive strengths ( $S_c$ ) using the equation of Kahraman (2001) as suggested in Sunamura et al. (2014):

$$S_c = 6.97e^{0.014\rho R} \quad (1)$$

where  $\rho$  is the rock density of cliff material in g/cm<sup>3</sup>.

Machado et al. (1962) estimated the density of lava and tephra from Capelinhos eruption as 2.6 g/cm<sup>3</sup> and 1.1 g/cm<sup>3</sup> respectfully. We then averaged these rock densities to derive a density for lava+tephra sector cliffs (1.85 g/cm<sup>3</sup>). No Schmidt hammer tests were possible on the tephra coast, so the average Schmidt hammer rebound value of 35 for tephra from Kahraman (2001) was used. The value of 45 for lava+tephra sectors was then derived from the average of the above values for lava and tephra materials. The calculated compressive strength  $S_c$  of lava, tephra and lava+tephra (appendix 6) was then used in the following numerical modelling section.

### 3.5 Wave height attenuation

A finite difference model was developed to predict how wave height is reduced by attenuation when crossing the dipping platforms. Within the model, we idealise a dipping platform with a series of very small horizontal steps (Figure 11) and apply attenuation rates from equations of Sunamura et al. (2014) to work out the small reduction in wave height across each step. Integrating the effect of those rates with varying water depth yields wave height at the coastline. This is a simpler approach than that used by McCall et al. (2017), which considered effects of finer-

scale bed topography, as our data are insufficient to constrain roughness in earlier stages of the platform development. Although the equations of Sunamura et al. (2014) were derived from wave attenuation measurements across nearly flat platforms, we assume here that they will faithfully represent the attenuation in small steps where the variation in depth is very small across each step. The tests of the model employ the wave data of McCall et al. (2017), which apply only to shallow dipping platforms ( $1.2^\circ$  to  $1.8^\circ$ ), so the model has not yet been tested with wave data on more steeply dipping platforms. Nevertheless, wave attenuation will be much smaller over the more steeply dipping platforms (e.g.,  $30^\circ$ ) where the water depth is larger, so we suggest the model should still capture the contrasting effects of steep and shallow platforms.

Using field measurements of wave height across a horizontal reef surface (Madin et al., 2006), Sunamura et al. (2014) proposed the following equations to represent wave attenuation over a horizontal platform:

$$\frac{H}{H_e} = \alpha(e^{-\beta X} - 1) + 1, \quad (2)$$

$$\alpha = \exp\left[-0.016\left(\frac{h}{H_e}\right)^4\right], \quad (3)$$

$$\beta = 0.030 \exp\left[-0.70\left(\frac{h}{H_e}\right)\right], \quad (4)$$

where  $H$  is the attenuated wave height at a distance  $X$  from the platform edge,  $H_e$  is the wave height at the platform edge,  $\alpha$  is a dimensionless coefficient and  $\beta$  is a decay coefficient (Sunamura et al., 2014). Values for  $\alpha$  and  $\beta$  were determined from data of Ogawa et al. (2012).

These Sunamura et al. (2014) equations were derived from wave data on sub-horizontal shore platforms (gradient  $<1^\circ$ ). Each cell has width  $d$  in  $X$  and the number of cells  $n$  is related to the platform width  $W$ ,  $n = \frac{W}{d}$ . The attenuated wave

height at the landward end of each cell (e.g.  $H_j$  in Figure 11) was used as the input value for the seaward end of the next cell (e.g.  $H_{i+1}$  in Figure 11). The calculation was repeated for each model cell until reaching the coast.

In one form of the model, we varied the gradient of platform from  $\theta_a$  to  $\theta_b$  while varying the platform width from  $w_a$  to  $w_b$ . The platform width at intermediate stages  $w_k$  ( $w_a \leq w_k \leq w_b$ ) is then linearly related to the gradient of platform:  $\theta_k = \theta_a - \left(\frac{w_k - w_a}{w_b - w_a}\right) (\theta_a - \theta_b)$ .

The equations of Sunamura et al. (2014) were adapted as follows for cell  $i$  ( $0 \leq i \leq n-1$ ), which has its seaward edge at  $X_i$  m from the dipping platform edge:

$$\frac{H_j}{H_i} = \alpha_i (e^{-\beta_i d} - 1) + 1, \quad (5)$$

when  $\frac{h_i}{H_i} < 1$ :

$$\alpha_i = 1, \quad (6)$$

when  $\frac{h_i}{H_i} \geq 1$ :

$$\alpha_i = \exp \left[ -0.016 \left( \frac{h_i}{H_i} \right)^4 \right], \quad (7)$$

$$\beta_i = 0.030 \exp \left[ -0.70 \left( \frac{h_i}{H_i} \right) \right], \quad (8)$$

$$h_i = (w_k - X_i) \tan \theta_k, \quad (9)$$

$$X_i = (i - 1)d. \quad (10)$$

where  $\alpha_i$  is a dimensionless coefficient and  $\beta_i$  is a decay coefficient,  $H_j$  is the attenuated wave height at the landward edge of cell  $i$ ,  $H_i$  is the wave height at the seaward edge of cell  $i$ . When  $i = 0$ ,  $H_i = H_e$  which is the initial wave height at the dipping platform edge.  $H_j$  equals to the attenuated wave height at the coastline when  $i = n-1$  ( $H_j = H_n$ ).  $h_i$  is the water depth of the seaward edge of the cell and, as the cell is horizontal, it is also the depth for the cell.



For verification purposes, the model was run using the platform seaward edge wave heights and platform dips derived from the data of Poate et al. (2017) and McCall et al. (2017) for some topographically rough dipping platforms in shallower water. Running the model with the wave heights shown along the left of each panel in Figure 12, using the platform dips shown, resulted in the model outputs (cell size: 0.5 m). The model fits the training observations with average RMS misfits (wave height minus model predicted height) of only 6 cm. Note that there were no free parameters set during this procedure.

The geometrical conditions more appropriate for Capelinhos were chosen based on the platform geometry in Figures 6b and 6c (600 m width, 3° dip for fixed gradient platform and 30° varied to 3° dip for varied gradient platform). Extreme wave heights of 8 m were used as explained in section 3.3 (other wave heights of 6, 10 and 12 m were also used to simulate attenuated wave heights across a dipping platform with the varied wave heights at the platform edge in Figure 13c). Attenuated wave height at different distances from the coast was simulated for uniformly dipping platforms with different total width, dip and initial wave height, producing the results shown in Figure 13.

Sunamura (1977) suggested that the cliff erosion rate  $dD/dt$  should be proportional to the wave erosive force  $F$ :

$$\frac{dD}{dt} = CF \quad (11)$$

where  $D$  is the eroded distance,  $t$  is the elapsed time of erosion and  $C$  is the constant of proportionality. Dimensionless parameter  $F$  (unit less) was defined by Sunamura et al. (2014) as:

$$F = \frac{F_W}{F_R} - 1 \quad \text{for } F_W > F_R \quad (12)$$

$$F = 0 \quad \text{for } F_W \leq F_R \quad (13)$$

where  $F_W$  is the wave assailing force (N/m<sup>2</sup> or Pa) and  $F_R$  is the cliff resisting force given by:

$$F_W = A\rho gH_f \quad (14)$$

$$F_R = BS_c \quad (15)$$

$H_f$  (m) is the wave height in front of the cliff,  $S_c$  is the compressive strength of the cliff materials (MPa),  $\rho$  is the density of sea water (1025 kg/m<sup>3</sup>),  $g$  is the gravitational acceleration (9.8 m/s<sup>2</sup>), and  $A$  and  $B$  are dimensionless coefficients that are related:

$$k = \frac{A}{B} \quad (16)$$

where  $k$  is a coefficient equal to 667 for breaking waves and 250 for broken waves. Sunamura et al. (2014) combined equations (12) to (16) to produce:

$$F = k \left( \frac{\rho g H_f}{S_c} \right) - 1 \quad \text{for } F_W > F_R \quad (17)$$

Both breaking and broken waves can attack the shore and determining which are the more important is difficult. We therefore used both equations (13) and (17) to calculate the erosive force for both breaking and broken waves (using different  $k$  values in equation (16)) in Figures 13e and 13h from the attenuated wave heights in front of the cliff shown (at 0 m distance) in Figures 13d and 13g. The results are shown in Figures 13f and 13i with logarithmic axes to expose whether they suggest power-law trends comparable with the coastline retreat rates described later. Wave height (Appendix 8) and erosive force (Appendix 8 and Figure 14) for six different coastal sectors were also simulated using similar method as for Figure 13.

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## 4. Results

### 4.1 Field observations of the modern coastlines

Owing to the rapid on-going wave erosion, the lithology of exposed cliffs, their joint intensity and consequently their rock strength (i.e., cliff resisting force  $F_R$ ) have changed both spatially and temporally (Cole et al., 2001).

In the tephra south sector, the presently exposed southwest cliff comprised bedded submarine pyroclasts (ashes) (Figure 10a) at the time of our visit with a narrow and low gradient sandy beach in front of the cliff base. These submarine pyroclasts were friable and too weak to conduct Schmidt hammer measurements. The pre-eruption lava sea stacks presently exposed in the southwest edge of Capelinhos are marked in Figure 10a. Their base contains submarine pyroclasts according to Forjaz (2007). During our visit, they appeared to contain few fractures, helping to explain their persistence.

The basaltic lava flow emplaced on 23<sup>rd</sup> August 1958 below the Capelinhos lighthouse is presently exposed in south Capelinhos and possibly originally fed by the dyke marked in Figure 10b. Large lava boulders (mean diameter >1.5 m) lie at the cliff base and appear to temporarily armour it in a way similar to rock armour in coastal engineering. These were likely formed by undermining of the lava flow by wave erosion and collapses of the overlying material. The Schmidt hammer measurements conducted on these basalt blocks produced a mean rebound value of 55. Using equation (1), their comprehensive strength is 51.6 MPa.

The presently exposed cliff of lava south and lava+tephra south sectors were observed from land and offshore (Figures 10c and 10d). They comprise basaltic lava flows that have low joint density in their lower section, while their top section comprises reddish (iron rich) subaerial pyroclasts (scorias and ashes). A narrow

beach (Figure 10d) was found in the lava+tephra coast with pebble-sized clasts of the cliff materials. Unfortunately, the presently exposed lava and lava+tephra north cliffs are inaccessible from land and we have very limited offshore observations of them (Figures 10e and 10f).

The presently exposed cliff of the tephra north sector (Figures 10e and 10f) is similar to the southwest Capelinhos cliffs and comprises submarine pyroclasts (ashes). A low gradient sandy beach was found in the base of the cliff. Its northwest edge was topped by pyroclasts blocks caused by recent collapse (the scar of the collapse is indicated in Figure 10f). In 2011, these collapsed materials were observed forming a talus deposit at the cliff base (Figure 10e).

#### 4.2 Historical variation of coastal position

Marine erosion has reduced the area of the Capelinhos promontory from ~2.5 km<sup>2</sup> in 1958 to ~0.42 km<sup>2</sup> in 2014. As shown in Figure 9, all coastlines retreated rapidly in the first year following the eruption and progressively less rapidly since then, though with notable variations between sectors and lithologies (Table 1), some of which we highlight below. The coastal retreat rates plotted logarithmically against coastal retreat distance in Figure 15b reveal that the data form almost inverse power law relationships. Deviations from those power laws reveal anomalies relative to the overall erosional trends, e.g., intervals of unusually fast erosion. The power law gradients also vary between sectors (Figure 15c), implying varied decelerations of retreat rates.

The highest retreat rate ~326 m/yr occurred in the lava+tephra north sector (in Figure 9) 08/1958 to 05/1959 (month/year), when the rates for other sectors were only ~17% (tephra north) to 61% (lava south) of that highest value. In three cases,

short-lived increases of retreat rates were found, violating the general decreasing trends. Two of them occurred in the interval 03/1981-11/2004, which followed the interval 09/1975-03/1981 when no coastal retreat had occurred (lava north and lava south sectors). The third occurred in the tephra north sector during 09/1975-03/1981. Retreat rates for the different sectors all eventually decreased to ~1-3 m/yr by 10/2014, while some of them decreased to and maintained ~2 m/yr (lava+tephra south sector since 1975 and tephra south sector since 1981).

In all sectors, the retreat rates decreased rapidly with time after the eruption, tending towards a more constant and slower rate after a few decades (Figure 9). This is consistent with the suggestion of Trenhaile (2000) that rock platforms formed by wave erosion tend towards a state of equilibrium because of increasing wave attenuation. The retreat rates derived from coastline retreat distances were ~46% faster on the northern coast than on the southern coast between 1958 and 2014.

#### 4.3 Submarine morphology of the platform

The geophysical data reveal the morphology of the gently seaward-dipping submarine platform potentially resulting from wave erosion.

##### 4.3.1 Platform geometry

The profiles selected to represent sectors with different lithologies reveal varied platform geometrical features (Table 2). In Figure 6b, the interpreted platform edge in all profiles lies seaward of the earliest (1958) shoreline position recorded, though by distances varying from 100 to 300 m. The platform is widest in the lava+tephra north sector (profile B3), where it is 832 m wide. In the lava north (profile B2) and tephra north (profile B1) sectors, the platform is narrower, 703 m and 533 m,

respectively. In the southerly sectors, the platform is narrower than in the north with same lithologies. The platform in the lava+tephra south sector (profile B5) is the narrowest at 383 m. The platform lava south (profile, B4) and tephra south (profile B6) sectors are intermediate in width, at 541 m and 475 m, respectively.

The platform dips are generally  $3^{\circ}$  (Table 2), though vary from  $2^{\circ}$  for the lava+tephra north platform to  $5^{\circ}$  for the lava+tephra south platform. The depth of the platform edge is between 14 and 59 m (Table 2). The average depth (33 m) is comparable with the 45 m depth of Surtla, a cinder edifice also produced by Surtseyan activity and eroded by waves over a period of 18 years (Kokelaar and Durant, 1983).

#### 4.3.2 Seabed morphology in Chirp data

The submarine platform is rugged in the Chirp profiles (“rugged” in Figure 6c), corresponding to a surface of angular boulder to pebble-sized clasts visible in the photos (Figure 7). Metre-sized lava boulders have probably moved off the paleo-coastline by rolling or sliding. Below the platform edge, the seabed is smoother, which we interpret as caused by finer sediment deposits (“smooth” in Figure 6c). The surface rugosity (Figures 1 and 6a) is different between the northern part of the platform adjacent to the tephra and the southern part adjacent to the tephra (it is smoother in the north than in the south).

A ridge marked in Figure 1a crossing the platform WNW to ESE is interpreted as a volcanic dyke remnant (ridge left after erosion). It is aligned with the Capelinhos vents and most of the scoria cones of west Faial Island, which also lie WNW-ESE (Cole et al., 2001). A low relief escarpment, ~300 m from the southwest

coast in Figure 1a, runs NW-SE and very close to the 1958 coastline of Figure 4. We suggest the top of this escarpment is the platform edge corresponding to the 1958 eruption, while the platform seaward of it is a pre-existing platform as marked in Figure 1a.

#### 4.4 Interpretation

##### 4.4.1 Subaerial

From the observations of Machado et al. (1959), the lava sectors were initially developed by lava emplaced over the tephra, so their bases are likely tephra-dominated. Undermining by removing their tephra bases explains their rapid cliff retreat. However, large angular lava boulders deposited at the base of the cliffs by collapse of the overlying lava (Cole et al., 1996; Figure 10b) temporarily armoured and likely slowed wave erosion of the cliffs. This armouring might also explain the lack of retreat in the lava coastal sectors from 09/1975 to 03/1981 (Figure 9).

The lava+tephra north-western sector of the headland is fully exposed to prevailing swells (Figure 8). These areas also sheltered the southern and eastern sectors from the westerly and north-westerly swells. The greater exposure of northern and western coasts resulted in their larger coastal retreat distances (Figure 9).

Slow retreat of the tephra north sector (Figure 9) in the earlier stages resulted from coasts being sheltered from swells coming from the west and northwest by the north-western part of the promontory. However, when the westernmost coasts were reduced by marine erosion, these tephra coasts became more exposed and cliffs retreated more rapidly (Figure 9). In addition, waves propagating from the west may

have transported sediments to the eastern edge of the promontory by long-shore drift. They then protected the cliff from coastal erosion, slowing cliff retreat by ~77%. However, as these eroded materials have smaller resisting force, they were quickly removed by waves and the cliff retreat rate increased again (Figure 9). During the visit to Capelinhos in 2017, a large landslide scar was observed in the north tephra cliffs (Figure 10f). Slumping is probably the main mechanism of coastal retreat in Capelinhos (Machado et al., 1962), whereby waves gradually remove materials from the cliff base, leading to undermining and abrupt failure. Failure and swell action then transport the fallen materials onto the foreshore.

#### 4.4.2 Submarine

We have hypothesized that particles deposited at the shoreline may have initially built a submarine slope (dashed brown line in profile B1 of Figure 6b) at the angle of repose of 30° (Mitchell et al., 2000; Mitchell et al., 2012a). The inferred platform edge in Figure 6b is everywhere seaward and shallower than this surface. We estimate  $\sim 7 \times 10^6$  m<sup>3</sup> of sediments have been deposited in the uppermost slope to prograde the platform edge based on the cross-sectional area between the 30° surface (dashed brown line in Figure 6b) and modern slope, delimited by the inferred platform edge and 1958 coastline.

We postulate the varied depth of the platform edge reflects cliff resisting force (deeper edge where materials are less cohesive) and wave properties (deeper edge exposed to taller and longer period waves, which affect the bed to greater depths). For example, the lava south platform edge lies at only 30 m depth, which is shallower than the tephra south platform edge at 50 m. However, the tephra north



platform edge at 40 m is shallower than the lava north platform edge at 45 m. On average, the three northern platform edges at 50 m are slightly deeper than the southern platform edges at 40 m.

The boulders imaged in Figure 7a immediately below the platform edge presumably represent pyroclasts sourced from the eroding volcano flanks that spent little time being rolled over the platform. Finer components were possibly transported by storm-generated down-welling balance currents (Meireles et al., 2013), contributing to the smooth seabed morphology below the platform edge. Large rounded boulders in SCUBA dive images in Figure 7b and 7c at shallower location S1 suggested they had been abraded in the surf zone for a while, although their ages and lithologies are unclear. The clasts photographed during the nearshore SCUBA dive at S2 (Figure 7d-7j) are more angular, implying a lack of abrasion and a short transport distance from the nearby lava cliffs (Figure 10b).

#### 4.5 Modelling of wave height attenuation

Figure 13a shows that increasing the width of a uniformly dipping platform of  $3^\circ$  has little effect on wave heights arriving at the coastline. Similarly, varying the deep-water wave height has little effect (Figure 13c). However, waves reaching the coastlines vary greatly with platform dip (Figure 13b), as shallower dips imply a greater distance travelled over shallower water and hence will be more attenuated.

In Figures 13d and 13g, we show how the attenuated wave height at the cliff base declines rapidly with increasing platform width (to 100 m for uniform dip and 20 m for varying dip). Changes become more gradual when widths are  $> 100$  m for uniform dip and  $> 20$  m for varying dip and the conditions assumed. The cliff-incident

608 wave erosive  $F$  in Figures 13e and 13h was computed as described in section 3.5  
 609 using equation (12) and comprehensive strengths for lava cliffs of 51.6 MPa (section  
 610 4.1.2) and for tephra of 12 MPa (appendix 6). The different forms of the graphs in  
 611 Figures 13e and 13h from that in Figures 13d and 13g reveal the effect of the  
 612 threshold ( $F_R$ ).

613 The model outputs for a platform with fixed dip are plotted logarithmically in  
 614 Figure 13f, so that we can see if wave erosive force follows an inverse power-law  
 615 similar to the coastline retreat rates in Figure 15. Although the independent variables  
 616 are different (platform width in Figure 13f and coastal retreat distance in Figure 15),  
 617 we might nevertheless expect to see similar patterns emerge if erosion rates are  
 618 proportional to erosive force (Sunamura et al., 2014). Differences between the two  
 619 curves in Figure 13f are due to the different coefficient  $k$  for breaking and broken  
 620 waves. The decline of  $\log_{10}F$  with  $\log_{10}W$  over the interval  $\log_{10}W$  0.8 to 1.4 (6 to 25  
 621 m) for breaking waves and  $\log_{10}W$  0.8 to 1.1 (6 to 13 m) for broken waves roughly  
 622 follows the trends in Figure 15b. However, this range of  $\log_{10}W$  only corresponds to  
 623 platforms up to 25 m wide, not the major range of the data.

624 In Figure 13i for variably dipping platforms, the model for breaking waves  
 625 predicts  $\log_{10}F$  declining from  $\log_{10}W$  0.8 to 2.5 ( $W = 6$  to 316 m) somewhat like the  
 626 data in Figure 15b (comparing with those trends in aggregate, rather than individual  
 627 coastal sectors). The model for broken waves predicts  $\log_{10}F$  declining from  $\log_{10}W$   
 628 0.8 to 2.0 ( $W = 6$  to 100 m) also somewhat like the data in Figure 15b. The model  
 629 gradients differ from the data trends for  $\log_{10}W \geq 2.5$  ( $W \geq 316$  m) for breaking  
 630 waves and for  $\log_{10}W \geq 2.0$  ( $W \geq 100$  m) for broken waves, but these parts of the  
 631 graphs are sensitive to cliff resistance, which is uncertain.

## 5. Discussion

Our results show that over the past six decades erosion has rapidly reduced the area of the Capelinhos cone to 17% of its original size but at rates that have dramatically decreased as the submarine platform left by erosion has widened. The geomorphology of the different sectors of the promontory varies, reflecting different post-eruptive development. Below, we discuss possible explanations for the varied coastline retreat rates between different lithologies and coastal orientations, as well as interpret the rapid decline in retreat rate with time. Finally, wider implications are considered for how rapidly Surtseyan cones and some analogous structures are eroded to form shallow banks.

### 5.1 Varied coastal erosion rates

Different cliff retreat rates and their changes over time may reflect varying intensity of wave effects (Trenhaile, 1987). The average of the Capelinhos coastal retreat rates briefly peaked at 164 m/yr (Table 1) for all sectors in the first half year of the post-eruptive development, but then rapidly decreased to 3%-17% of the peak value in the following decade, gradually slowing to 1-2 m/yr towards the time of our analysis. It is unclear exactly when erosion rates peaked, as that information would have required a more frequent monitoring in the earlier phase. The collapses of the early edifice reported by Machado et al. (1962) suggest erosion was concurrent with the eruption during which unmeasured amounts of material were being added as well as evacuating on to the island slope. Similar post-eruption changes were found in Surtsey (Romagnoli and Jakobsson, 2015), which may be explained by the following factors:

a) *Rock resistance*. In general, we expect loose tephra and thin and fractured

lava to be easily eroded, whereas well-bedded tephra layers containing lava chips and weakly jointed basaltic lava flows to have higher cliff resisting force. Similar varied resistance has been suggested previously for Surtsey (Jakobsson et al., 2000; Jakobsson et al., 2009; Romagnoli and Jakobsson, 2015). Lava cliffs with tephra bases were eroded rapidly, so the friability of the tephra clearly dominates the resistance of the entire cliff. On the whole, erosion occurs rapidly on cliffs formed with loose materials or with their base formed of them and gradually slows as more resistant material is exposed as found in the tephra south sector.

The Schmidt-hammer mean rebound value for the basalt blocks of 55 is typical of “strong rocks” according to the classification of Goudie (2006). For comparison, Schmidt hammer tests conducted on basalts from the Bodrum Peninsula (Turkey) produced rebound values of 35 to 55 (Dinçer et al., 2004) and tests on basalt cliffs on Lord Howe Island (SE Australia) yielded rebound values of 30 to 65, with the highest values associated with low joint density (Dickson et al., 2004).

In our study, we found some evidence for lower retreat rate for lava cliffs. For example, the north lava+tephra sector retreated more rapidly than the north lava sector in Figure 9. However, the tephra coast retreated more slowly. Nevertheless, we interpret these discrepancies as due to sediment dynamic effects as outlined earlier in section 4.4.1. Even if complicated by them, we anticipate some effect of cliff resistance to be present as in other sections.

b) *Local wave conditions.* Masselink et al. (2016) suggested the rate of morphologic evolution of coastlines is proportional to the frequency and height of extreme waves. The ERA models suggest upper 5-percentile wave heights of 4-12 m

(Figure 9) and periods of 11-16s in this site (Appendix 7b). However, the means of these wave heights have increased by 3% and their associated period has increased by 6% over the last six decades (Appendix 7), so it is unlikely the coastal retreat rates have slowed because of declining wave impacts over time. Although there are individual occurrences of rapid erosion coinciding with short-lived greater wave heights in Figure 9 (e.g., tephra north from 17 to 22 years), there is no general correlation between retreat rate and extreme wave height.

c) *Coastal orientation*. Coasts facing the strongest waves would be expected to erode faster. This can explain the faster coastal retreat rates in the north and west sectors (coastal sectors facing north and west in Figure 9). Refraction of shoaling waves may also leave more obliquely oriented coasts affected by waves, leading to their rapid erosion. Erosion has gradually modified coastal configuration through time and left small headlands. Refraction of northwesterly swells may explain why the southern Capelinhos coast (tephra and facing southwest) eroded nearly as rapidly as the south lava coastline, which is more exposed to strong waves from northwest (Figure 9). It was also affected by less frequent large swells from the SW.

d) *Changing wave exposure*. The northern tephra coast of Capelinhos was initially sheltered from westerly waves (Figure 21), perhaps explaining why it was the slowest retreating coast in the first 20 years in Figure 9. The bay might also represent a cul-de-sac for evacuating material. The tephra north sector subsequently eroded more rapidly (Figure 9). Similarly, the lack of coastline retreat observed in the northeast sandy beach of Surtsey from 1967-2007 (Romagnoli and Jakobsson, 2015) may be interpreted as the south part of the island protecting the northeast sandy beach from exposure to west-southwest originating waves, which occurred

52% of the time. Other possible explanations include the leeward side of the island accumulating sediments quarried and moved by longshore drift from the exposed side.

e) *Protection by eroded materials.* Our recent observations helped to verify the role of protection by eroded materials. In three locations, eroded materials deposited at the cliff base were found protecting the cliff from wave erosion. First, large angular lava boulders in southern Capelinhos (Figure 10b) were found armouring the cliff base. Second, protective talus formed by the failure of undermined high cliff was found in north Capelinhos (Figure 10e). The talus of hard blocks shields the friable pyroclasts as suggested elsewhere (Emery and Kuhn, 1982; Dickson, 2004). The amount of talus material that needs to be removed by waves after cliff collapses and before undermining resumes increases considerably as the cliff being dismantled grows taller around a conical edifice. This might also be a major factor slowing down the rate of coastal retreat. Third, a sandy beach (Figure 10f) emplaced by longshore sediment drift originating from the west protected the north Capelinhos tephra coast. The longshore shift itself disaggregated the loose materials, while the sandy beach forces waves to break and absorbs wave energy. Similarly, a palagonitized tephra cliff on Surtsey was found protected by lava boulder platforms/beaches built up by swash (Romagnoli and Jakobsson, 2015).

f) *Tectonic movement:* Romagnoli and Jakobsson (2015) suggested that tectonic subsidence of 1 m until 1991 caused by compaction of Surtsey affected the island's coastal retreat rates. Stephenson et al. (2017) suggested that a tectonic uplift of 1.01 m associated with the Kaikoura earthquake increased wave attenuation over a shore platform, consequently reducing coastal erosion rates there. At longer

time scales it has been shown that subsidence increases coastal retreat rates (Quartau et al., 2018). Catalão et al. (2006) suggest that the Fajã sector of Faial Island subsided by up to 1.5 m between 1937 and 1997 in relation to the Capelinhos eruption, while the Capelinhos area itself is placed between the isoclines representing 0 to 0.5 m subsidence. Although there are no vertical displacement data for the Capelinhos promontory itself, metre-scale subsidence is possible for reasons similar to Surtsey. We suggest that these reduced wave attenuation by only a minor amount as the platform is much deeper than 1 m.

## 5.2 How the submarine platform evolved by wave erosion

We suggest that submarine platform developed in five phases (Figure 16). Phase I: Capelinhos was shaped as a cone/promontory by a Surtseyan eruption with its seaward flanks exposed to waves. Phase II: the post-eruptive wave erosion of the coast created a submarine platform. Phase III: wave erosion progressively widened and lowered the platform. Phase IV: a rugged surface covered with eroded boulders was left by erosion. The eroded boulders on the platform surface were moved there by the offshore sediment transport in response to storms (Scott et al., 2016; Burvingt et al., 2017), perhaps moving to greater depths below the platform edge during more violent storms (Rebelo et al., 2018). The platform edge may either represent the edge of the original cone (Figure 16d), or it was extended by the deposition of eroded materials (Figure 16e) as suggested by our analysis of the cross-sections in Figure 6b. Phase V: in absence of further volcanism and mass wasting events, continued wave erosion will eventually turn the promontory into a submerged bank (Figure 16f).

### 5.3 The inverse power law relationship between coastal erosion rate and retreat distance

The apparently simple inverse power-law relationship between rate of coastal retreat  $R_r$  and retreat distance  $D$  (Figure 15b) stems partly from the increasing attenuation of waves crossing the resulting submarine platform. The data for the Surtsey coasts in Figure 15c (summarized in Table A3) suggest similar behaviours for the lava, but not for tephra coasts. Deviations of retreat rate from the inverse power law relationship can be caused by abrupt cliff collapses arising from undercutting of cliffs by marine erosion.

Figure 15d shows that the square root of Sholan Island's area (approximately coastal retreat distance) decreased nearly linearly with time after the end of its eruption, implying a constant retreat rate in contrast to the later Capelinhos evolution. The 15 m/yr average coastline retreat rate of Sholan Island (2012- 2017) was much smaller than the earliest retreat rates of Capelinhos (56-326 m/yr) and Surtsey (90-107.5 m/yr), reflecting the more moderate wave climate of the Red Sea. The evolution of Sholan Island has been barely studied, so the lithology of the island is poorly known. According to Xu et al. (2015) and Jónsson and Xu (2015), the eruption failed to become effusive, so the edifice is probably mainly formed of hydromagmatic/tephra deposits. The nearby islands of Rugged (located 1 km to the south) and Haycock (3 km to the northeast) (Xu et al., 2015) may also partly shelter Sholan Island from waves from northeast and south, while Capelinhos and Surtsey are fully exposed. Moreover, the seasonal reversal of prevailing wave directions in Red Sea allows Sholan Island to redeposit the loose materials eroded during winter/spring in the north and in the south in summer (Xu et al., 2015). The linear variation in Figure 15d suggests that wave attenuation was not significant during



these early stages of Sholan Island, as attenuation would be expected to reduce erosion rate increasingly with time and make the graph non-linear.

Figure 14 shows predicted cliff-incident wave erosive force declining with increasing platform width. As mentioned earlier, deposition at the platform edge may have widened the platforms. However, extending the deeper part of the platform has little effect on net attenuation (because it is deep) so we can still roughly compare these model trends with platform width  $W$  with the erosion rates plotted against coastline retreat distance  $D$ . In doing so, we acknowledge there is large uncertainty in the resistance to erosion of the cliff materials, so the declines in  $F$  at large  $W$  are not resolved realistically and differences between materials may not be so significant.

The model predictions with varied platform dip in Figure 14 (lines C and D) have somewhat similar gradients to the power-law trends in Figure 15b, but the graphs for constant gradient platforms (lines A and B) mostly do not. Only lines A and B in Figures 14a1 and 14a2 have acceptable graph gradients, but then only for small  $W$ . Along the Tephra and Lava+Tephra coasts, it seems more likely that the platform gradient varied. In other words, the platform was narrow initially, leading to little wave attenuation and hence rapid erosion, but then deepened as it widened. Wave attenuation was only important then in shallow water, hence leading to the moderate decline in erosion rates. This is less clear for the lava cliffs as the predicted erosive forces in both models are too low for erosion to occur.

Nevertheless, these inferences are speculative. We acknowledge that discrepancies between the model predictions and the power law trends are partly caused by the limitation of the numerical modelling that separately simulated erosive force attacking cliff for breaking and broken waves, while types of waves attacking

cliffs (standing, breaking and broken) vary temporally depending on the cliff root water level (Sunamura, 1992) . More importantly, the discrepancies could imply that other factors are also important, in particular, the variation of cliff lithology, its joint intensity (Kennedy, 2010) and consequently its cliff resisting force, along with the temporary protection conferred by shelf deposits of eroded material (Figure 10b).

#### 5.4 Development of shallow banks

The rapid decline found in Capelinhos may not be extended to all Surtseyan cones if erosion rate depends so strongly on lithology, which is likely to vary. However, the range of rates may be useful for suggesting the range of cone longevity that may be possible. For example, the Costado da Nau (Figure 17a) is the remnant of a previous Surtseyan eruption at Capelinhos (Waters and Fisher, 1971; Camus et al., 1981), which occurred between 500 and 800 A.D. according to paleo-magnetic data (Di Chiara et al., 2014). Waves removed most of the promontory before the 1957/58 eruption when the Capelinhos cone was emplaced in front of the Costado da Nau cliff, protecting it from further wave erosion. Monte da Guia located in the SE of Faial Island (Figure 17a) is also a Surtseyan cone that has persisted for longer (Madeira and Brum da Silveira, 2003) possibly partly because of wave sheltering by the island and partly greater cliff resisting force (palagonitized tephra).

We can use our results to estimate how long it will take wave erosion to remove the present Capelinhos promontory. In order to do this, we assume that wave conditions will remain constant and that relative sea level will not change over the next 100 yr significantly compared with the metre or so of vertical cliff interval impacted by waves. Using the average power law relationship from Figure 15b and

solving for the edifice half-width by integration, the Capelinhos promontory will become a submerged bank by 2118 A.D. This is later than the few decades suggested by Cole et al. (2011).

Rapid wave erosion has turned some other Surtseyan cones in the Azores into submerged banks more quickly than this. The features mentioned below are located in Figure 17a. Sabrina Island reached a height of 90 m after its emplacement in 1811 A.D. offshore NW São Miguel. The island stood above sea level for 4 months (June to October, 1811) and is currently reduced to a bank lying 40 m below sea level (Moore and Fairbridge, 1997; Madeira and Brum da Silveira, 2003; Ramalho et al., 2013). NW of São Miguel, within the Terceira Rift, a larger feature, the Dom João de Castro Seamount, erupted in 1720 A.D. forming a subaerial cone that peaked at a maximum height of 250 m and disappeared after a few months. Its top now lies at depths of 13 to 50 m (Santos et al., 2010). Many other Surtseyan cones exist in the Azores but remain undated. One cone on Princess Alice Bank now lies at 55 m depth (Figure 17b) and a littoral cone to the SE of Pico now lies at 10-40 m depth (Mitchell et al., 2018). Several submerged banks of wave erosion origin were also found on the shallow portions of Serreta Ridge and SE of Angra do Heroísmo, lying between 30 and 180 m depth (Quartau et al., 2014). A submerged bank lying at 80 m depth NW of Terceira Island originated from wave erosion of two adjacent cones shown on Figure 17c.

These Azores submerged banks mainly lie between 10 and 55 m depth, with one extreme at 180 m. The variation of their depths might be due to varying local wave conditions and different ages, and hence different contemporary sea level, though varied materials and hence resistance to erosion may also have played a

857 role. Modelling of changing wave propagation and its effect on cone erosion,  
858 coupled with dating of samples, may help to resolve this issue.

859         Once submerged by erosion, the resulting shallow banks slow down waves in  
860 comparison with adjacent deeper waters, leading to wave refraction and local wave  
861 convergence over the banks. Hence, while the initial emergence of Surtseyan cones  
862 above sea level inhibits the wave energy reaching the adjacent coasts, the  
863 subsequently formed shallow bank may focus wave energy on the adjacent coastline  
864 (the concave shape of the Costado da Nau coast previous to Capelinhos may have  
865 been formed by this effect from the adjunct shallow platform around the two islets).  
866 Consequently, dating shallow remnants of Surtseyan cones could turn out to be  
867 useful for assessing how wave erosion has varied around adjacent coasts over time.

868

## 869         **6. Conclusions**

870         This study has characterised how rapidly the morphology of the coast and  
871 near shore platforms have changed after the Surtseyan eruption of Capelinhos. The  
872 average coastal retreat rate peaked at 164 m/yr in the first year after the eruption  
873 and since then has quickly declined to 2 m/yr in the last decade. Coasts composed  
874 of mixed lava and tephra and located in the northwest eroded most rapidly, explained  
875 by the combined influences of weak rock, strong waves and orientation towards the  
876 prevailing swells. Marine geophysical data revealed the rugged surface of the  
877 submarine platform left behind by erosion. Seabed photos of the platform have  
878 revealed large, angular and some rounded boulders on its surface. Marine erosion  
879 has evidently lowered the platform as well as widened it.

The rate of coastal erosion varied as an inverse power law with retreat distance, representing a rapid decline in erosion with time. Wave attenuation contributed to this relationship. We find that the decline in wave erosive force predicted using a simple finite difference model most closely (though still only partially) reproduces the trend of the inverse power law if the platform started with a 30° gradient and gradually declined towards the present 3° gradient, rather than maintaining a constant gradient. However, other factors are also important, in particular, the varied cliff lithology and joint intensity, and consequently the cliff resisting force. Protection provided by eroded materials also complicates the interpretation.

Based on the observed inverse power law trend of erosion rates, we estimate that the promontory will eventually be submerged by 2118 A.D. Some other Surtseyan cones have eroded away more quickly than this, while the Monte da Guia has lasted much longer, so persistence in time varies strongly.

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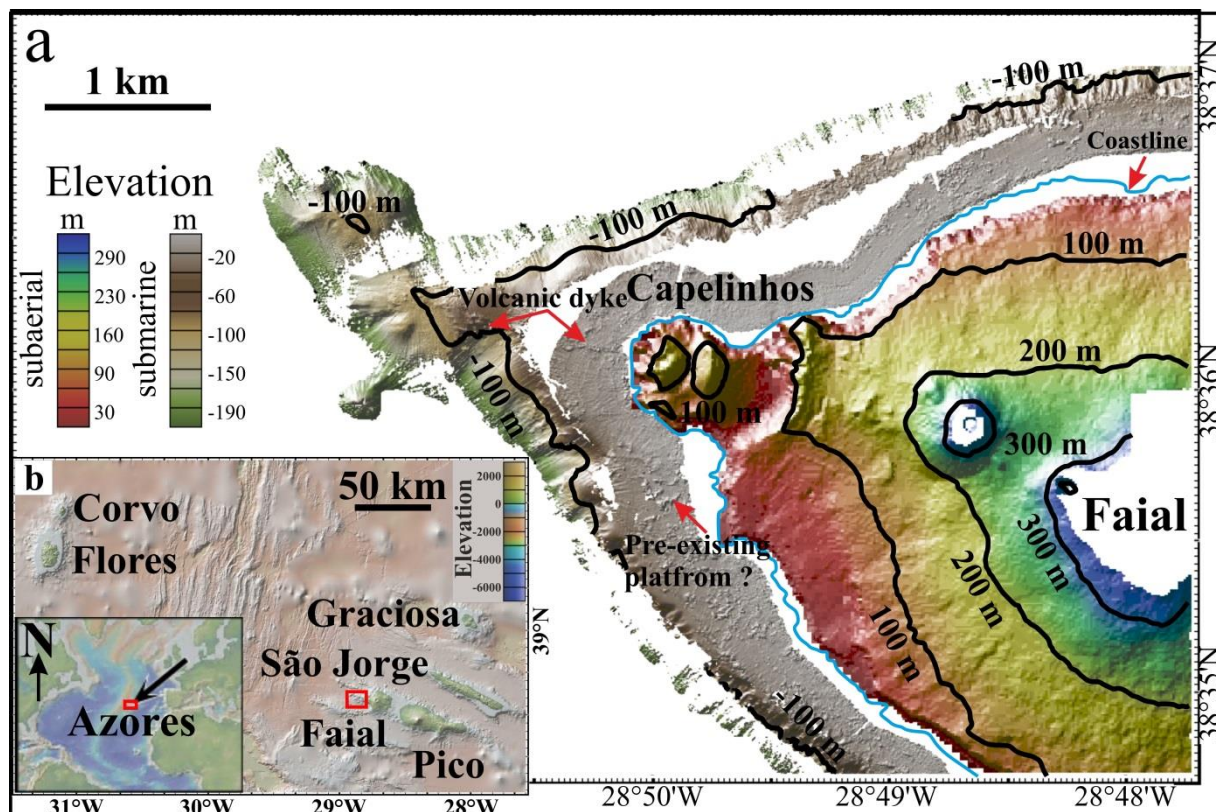
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1171 **Figures:**



1172  
 1173 Figure 1. (a) Morphology of the Capelinhos promontory. Onshore topography  
 1174 and multibeam bathymetry are shown illuminated from the north. Topography  
 1175 is from Instituto Geográfico do Exército (2001). Bathymetry is from Mitchell et  
 1176 al. (2008) and Tempera (2008). (b) Location of panel (a) (red box) overlain on  
 1177 a map produced using GeoMapApp (Ryan et al., 2009).

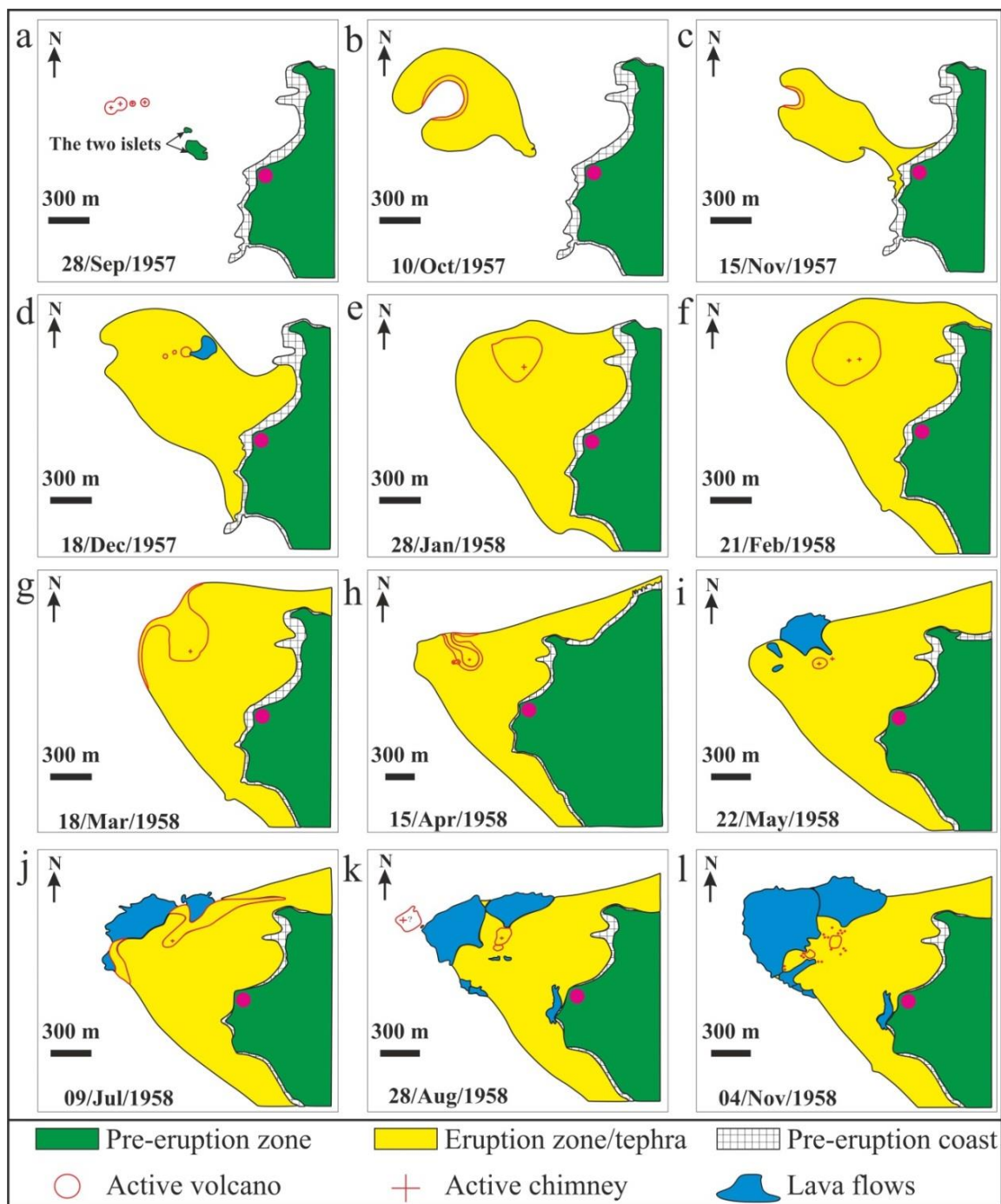
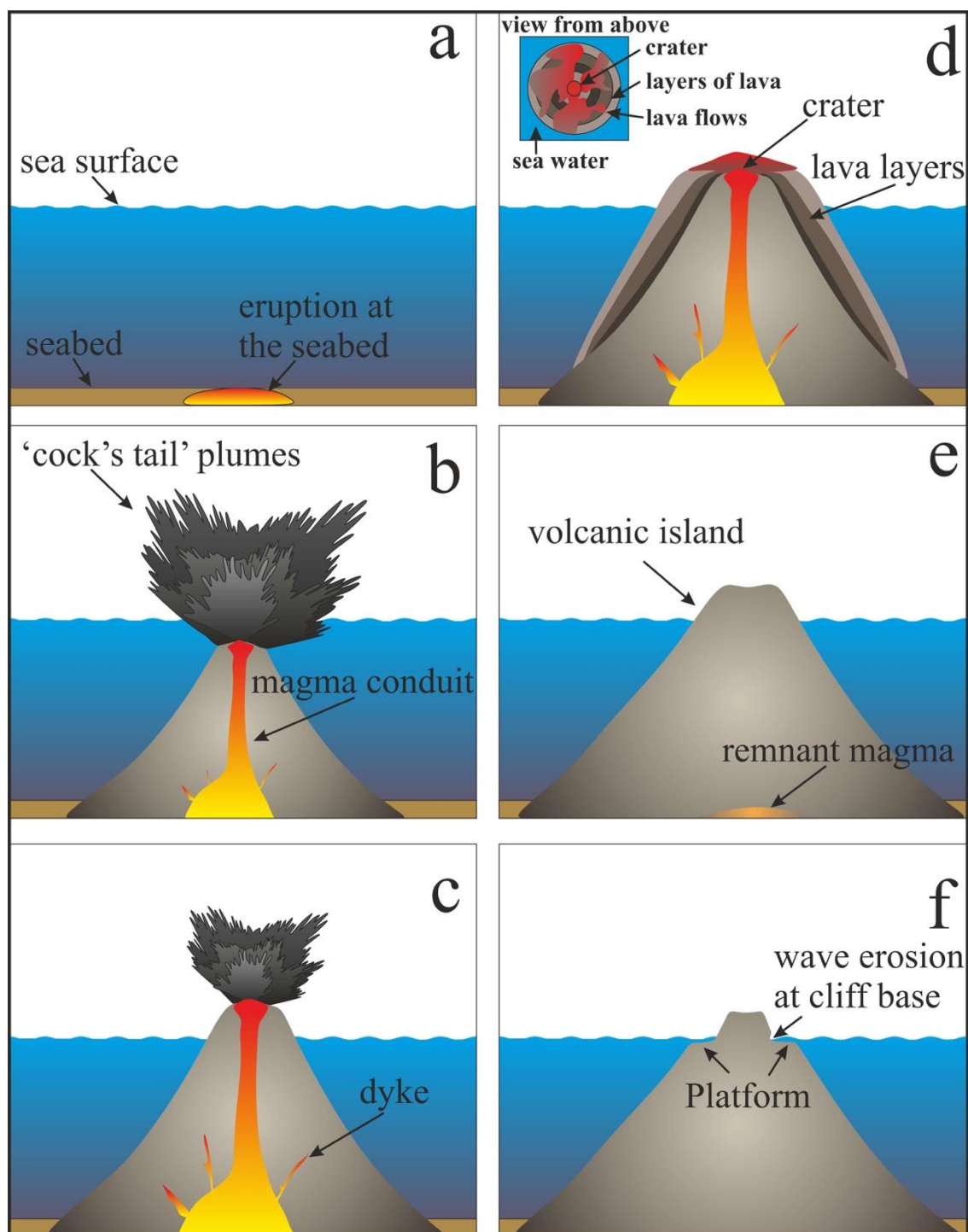


Figure 2. Physiographic and lithologic evolution of Capelinhos promontory from the initial eruption (September 1957) to the end of the eruption (November 1958) adapted from Machado et al. (1959). Pink circle locates the Capelinhos lighthouse.



1183 Figure 3. Stages by which Surtseyan eruptions form volcanic islands, based  
 1184 on work of Moore (1985). (a) Initial eruption of magma at the seafloor. (b)  
 1185 Violent submarine eruption project characteristic "cock's tail" plumes of gas,  
 1186 steam and black tephra subaerially. (c) A cinder ring forms above sea level



from volcanic ashes and other tephra. (d) Cinder ring prevents seawater from entering the vent. Consequently, lava extrudes less violently, eventually with flows topping previous tephra layers. (e) Volcanic activity gradually ceases and magma conduit cools down. (f) Volcanic activity stops, leaving the edifice to evolve purely from erosion and sediment transport. Submarine platform develops on the flanks under the effect of wave erosion.

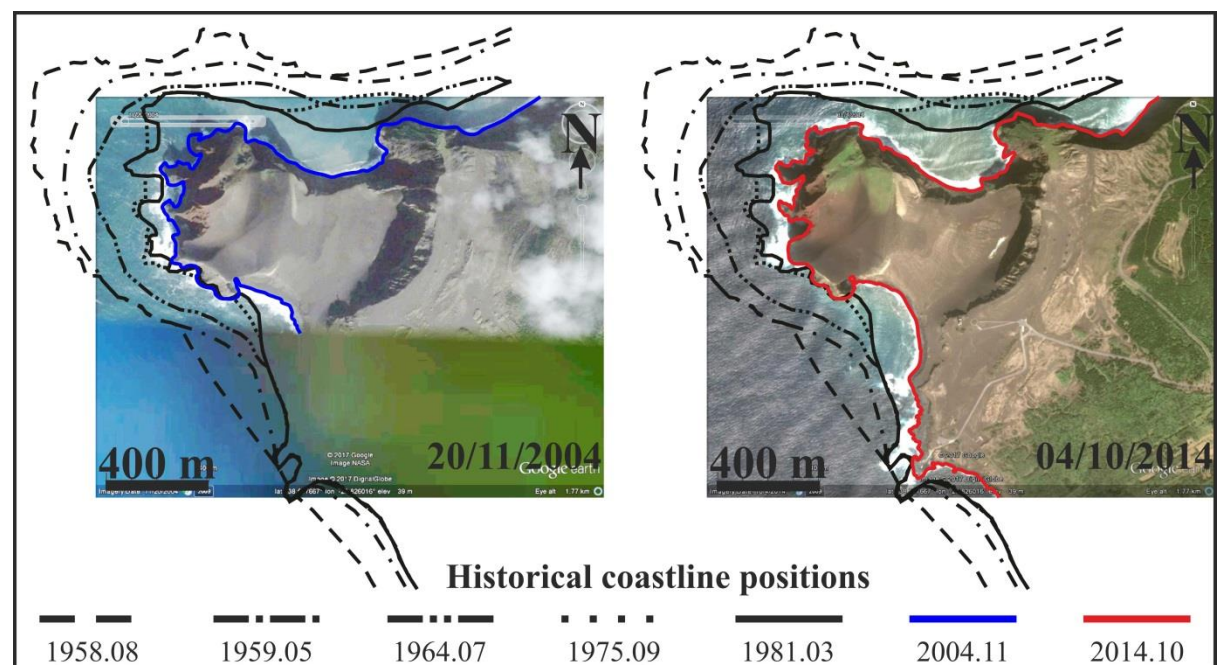


Figure 4. Coastline positions in 2004 and 2014 from Google Earth images (google.com) and previously reported historical positions from Machado and Freire (1985). The length of marked coastline in 2014 was 5079 m (marked in red). The coastline of 2004 (marked in blue) is incomplete due to lack of Google Earth images in the south.

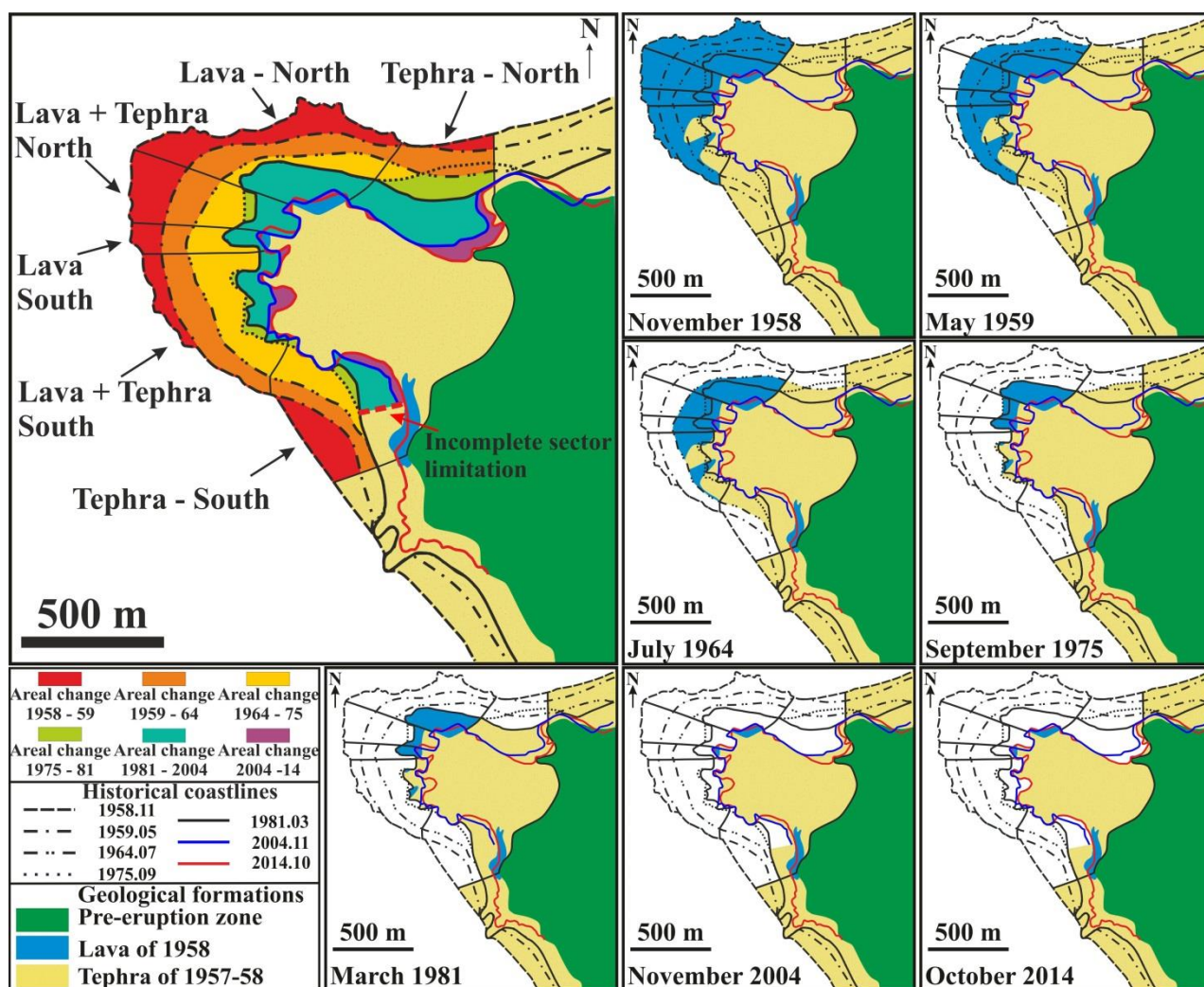
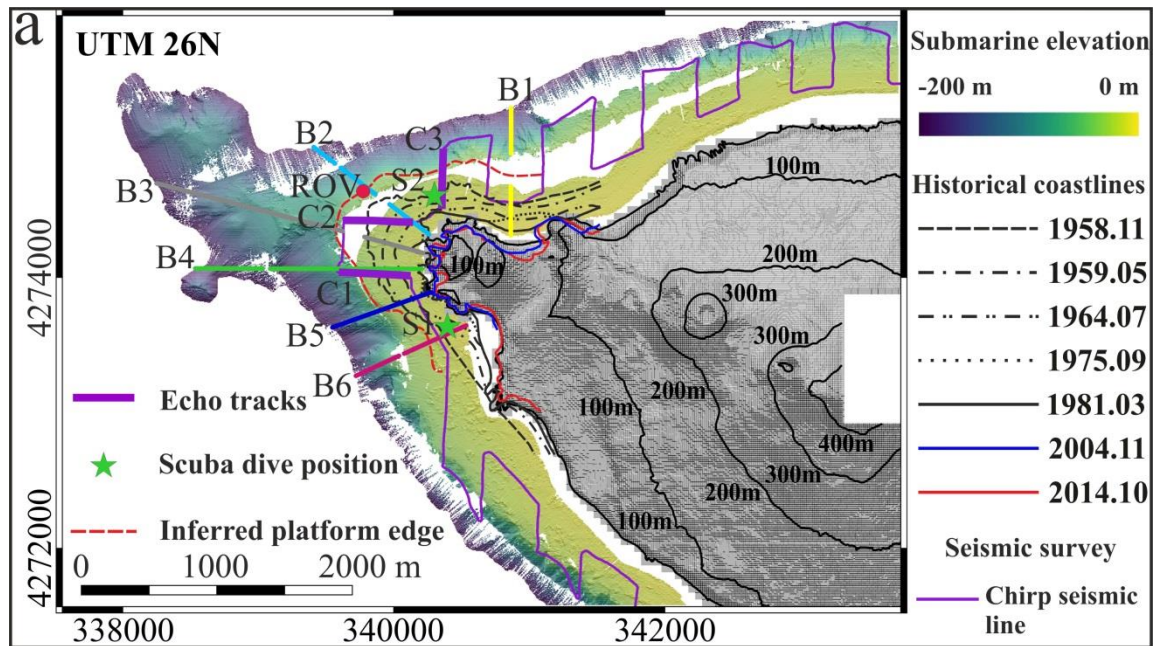


Figure 5. Evolution of Capelinhos based on coastlines of Figure 4. Six sectors were classified based on their different locations (north or south) and lithologies (lava, tephra and mixed lava and tephra). The red dashed line locates the incomplete coastline in the tephra south sector due to lack of data.



1206

1207 Figure 6. Profiles used to analyse the morphology of the platform. (a)

1208 Locations of the six cross-sections in (b) and three Chirp profiles in (c). Red

1209 circle and green stars locate respectively the underwater photographs taken

1210 by ROV and SCUBA divers shown in Figure 7. Submarine bathymetry and

1211 subaerial elevation data are illuminated from the north using GeoMapApp

1212 (Ryan et al., 2009). Elevations are contoured every 100 m. Coordinates are

1213 in Universal Transverse Mercator (UTM) projection metres (zone 26 N).

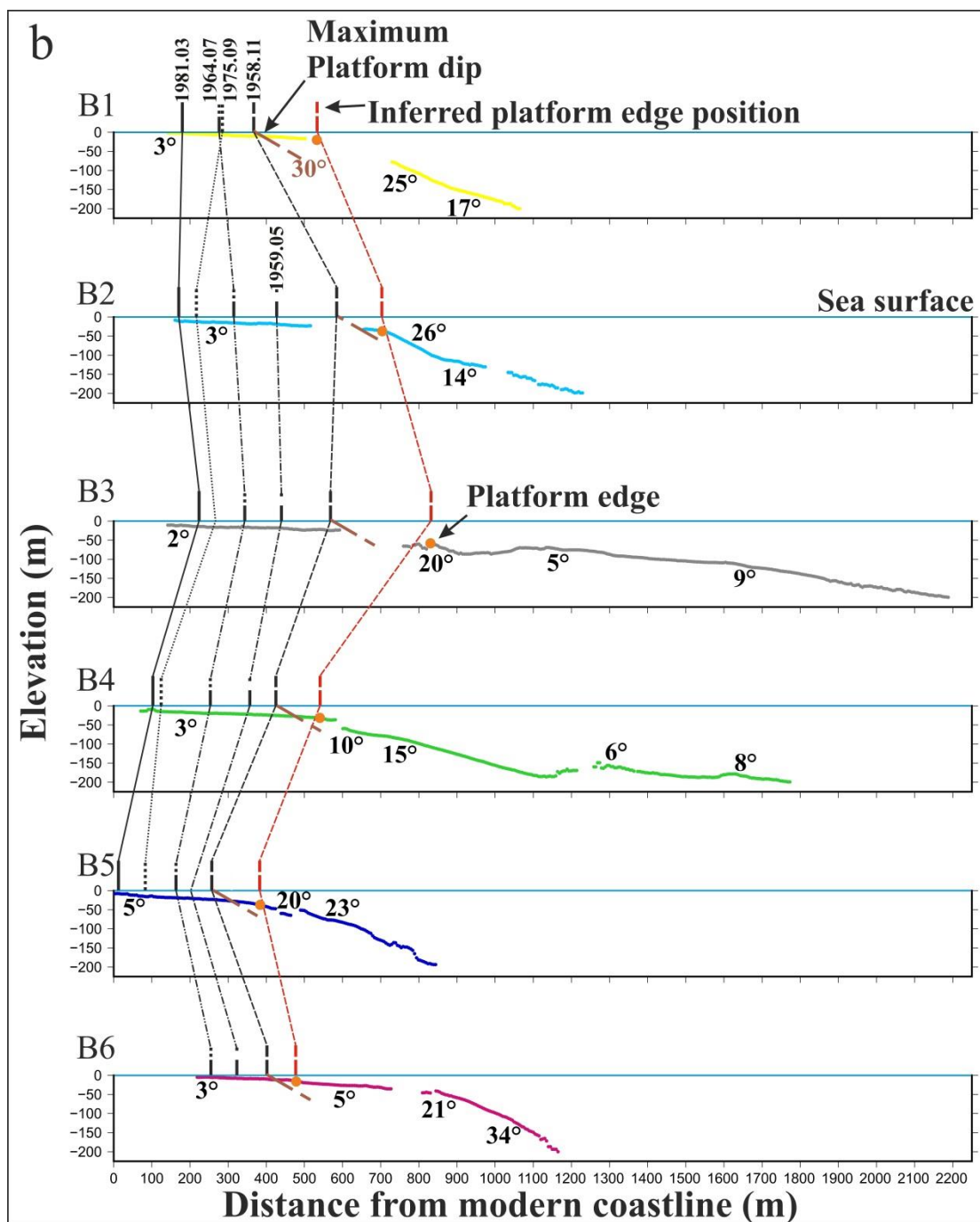


Figure 6(b). Bathymetric cross-sections (data from 2003 and 2004) with historical coastline positions. Orange circles locate the inferred modern platform edge. Numbers are seabed gradients in degrees.



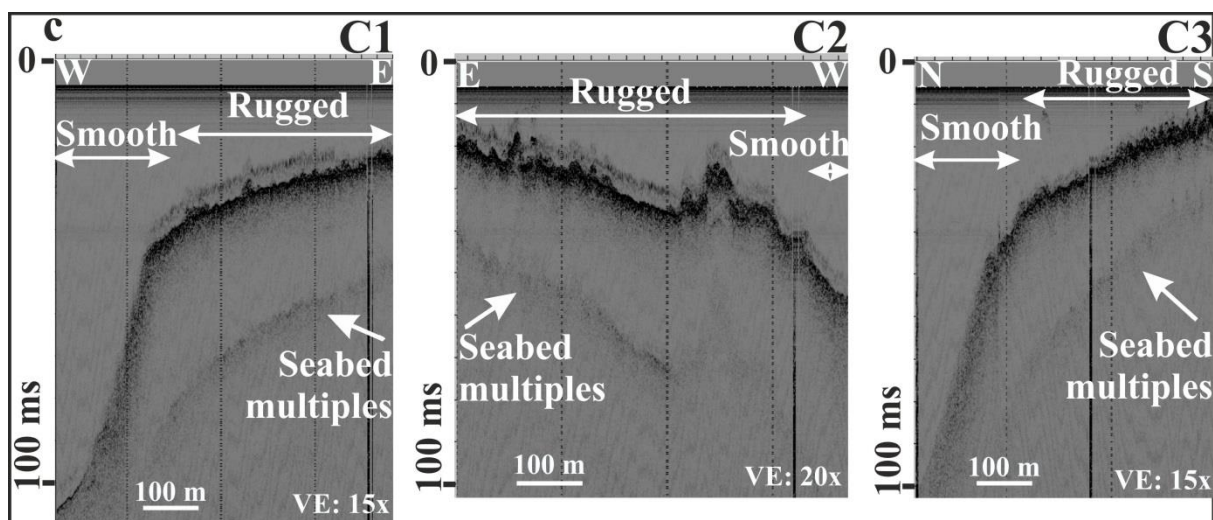


Figure 6(c). Chirp profiles illustrating the rugged morphology left behind after the erosion, and with smooth morphology below the platform. VE: vertical exaggeration.



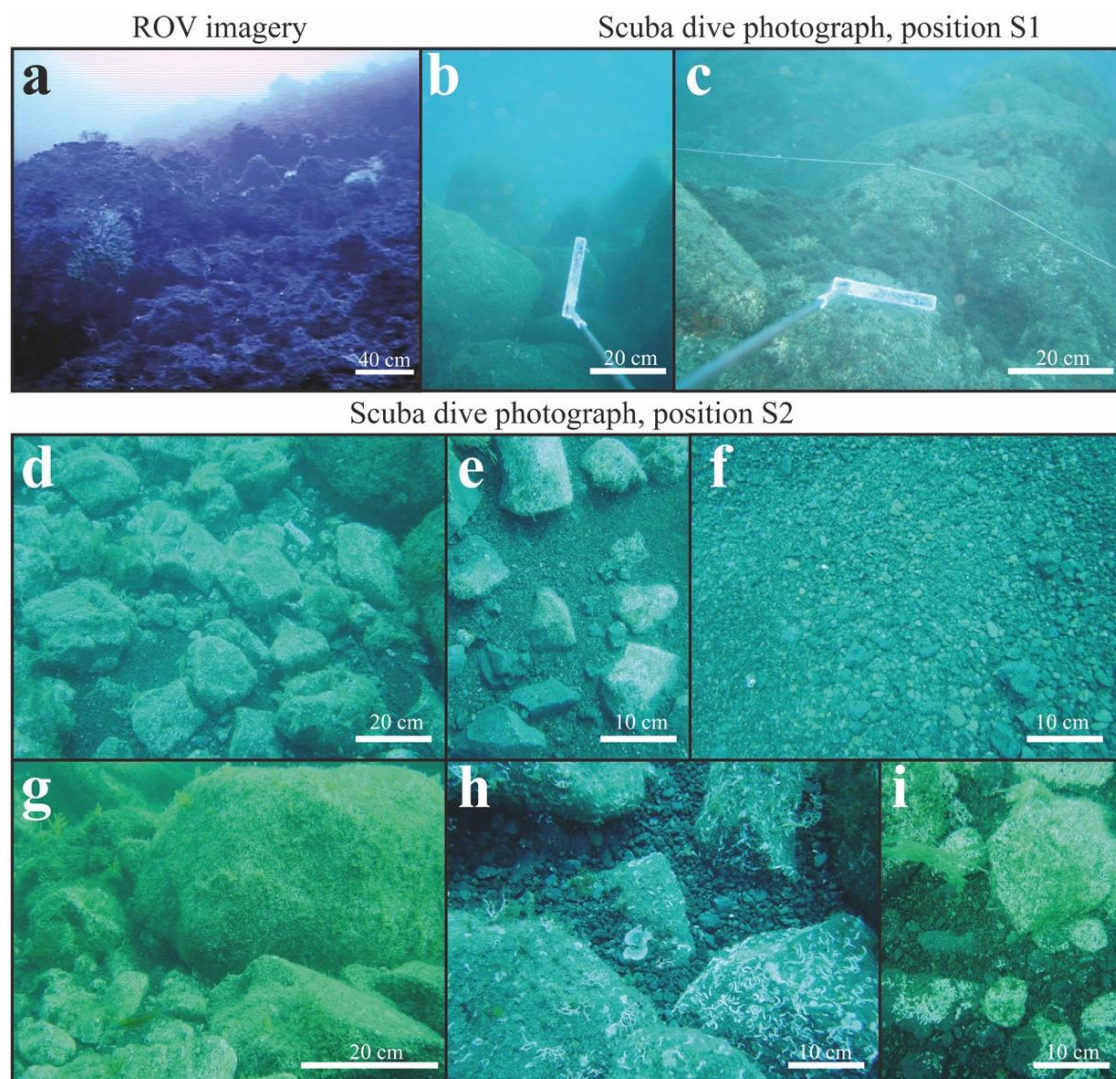


Figure 7. Seabed photographs located in Figure 6a. (a) ROV image showing a boulder field immediately below the platform edge to the northwest of Capelinhos (depth ~38 m). (b)-(c) SCUBA dive images from position S1 (depth~10m) showing rounded boulders on the south platform. (d)- (i) SCUBA dive images from the submarine platform showing angular boulder to pebble-sized clasts (depth ~10 m).

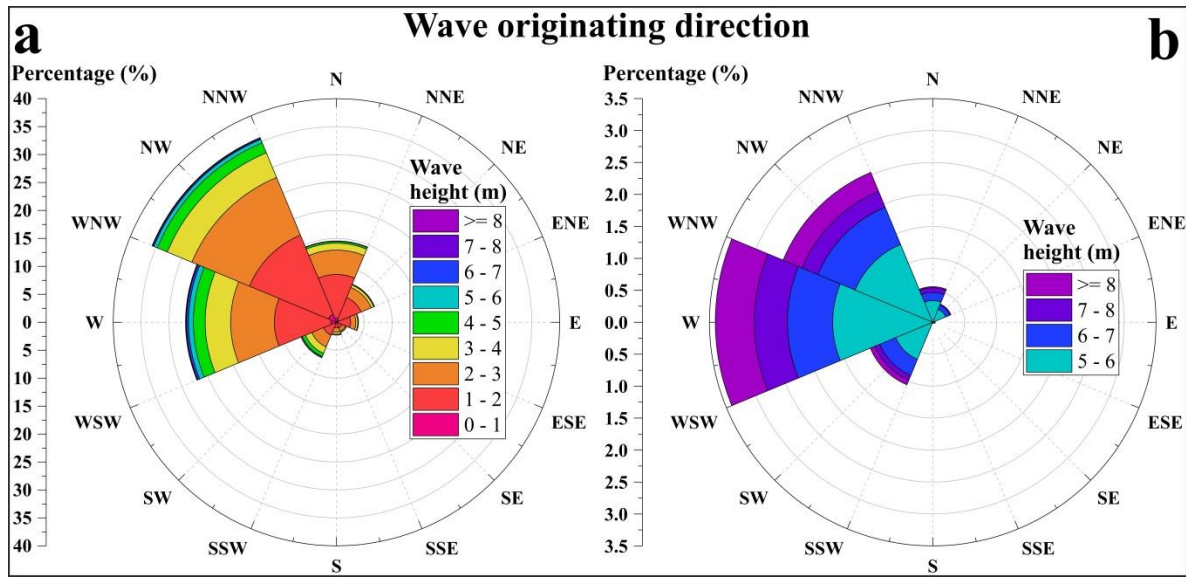


Figure 8. Offshore significant wave heights in the Capelinhos area derived from hindcasts by Carvalho (2003) for (a) all waves and (b) only waves above 5 m height.

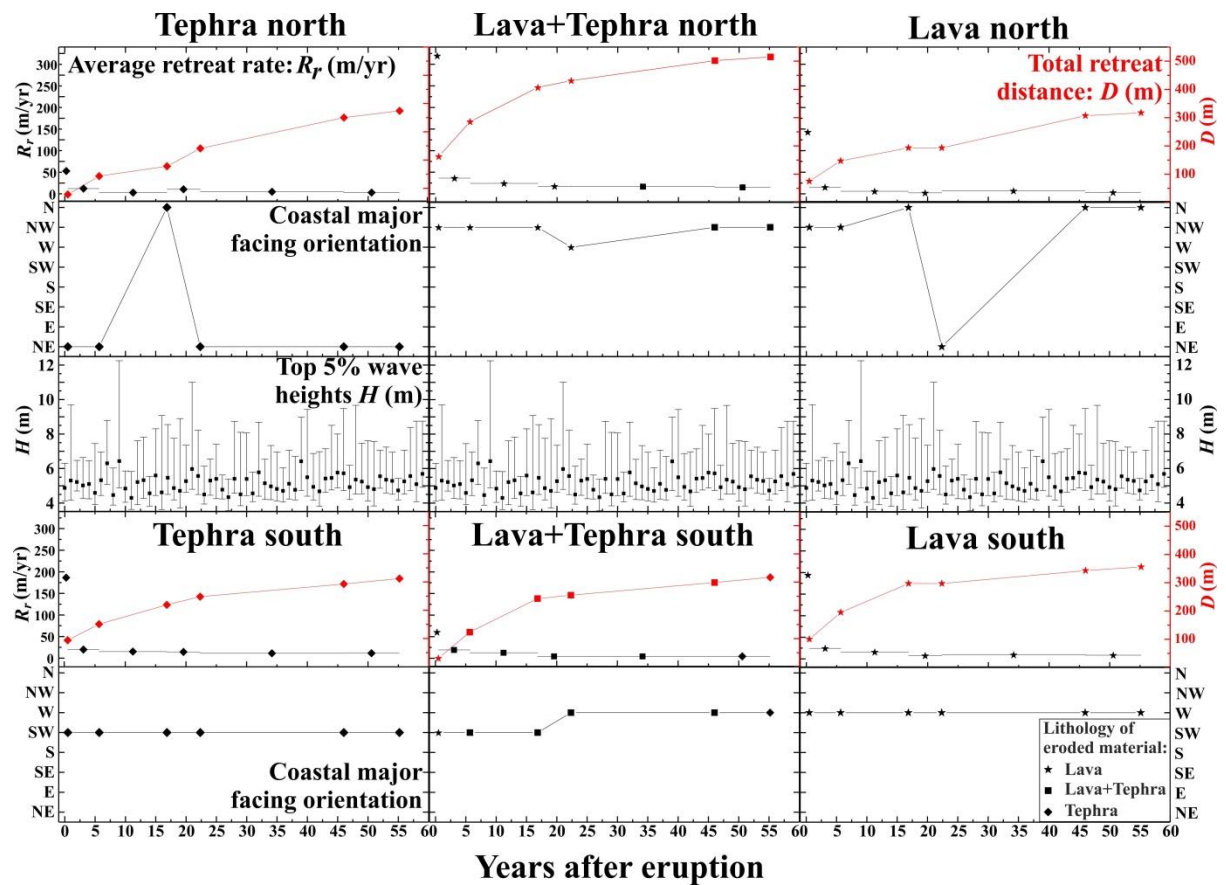


Figure 9. Comparison of retreat rates and distances with varying coastline orientations and extreme major wave heights. In the upper graphs, black data represent the average retreat rate in different periods and red data represent the cumulative retreat distance. Coastal major facing orientation was worked out using the history of coastline change.



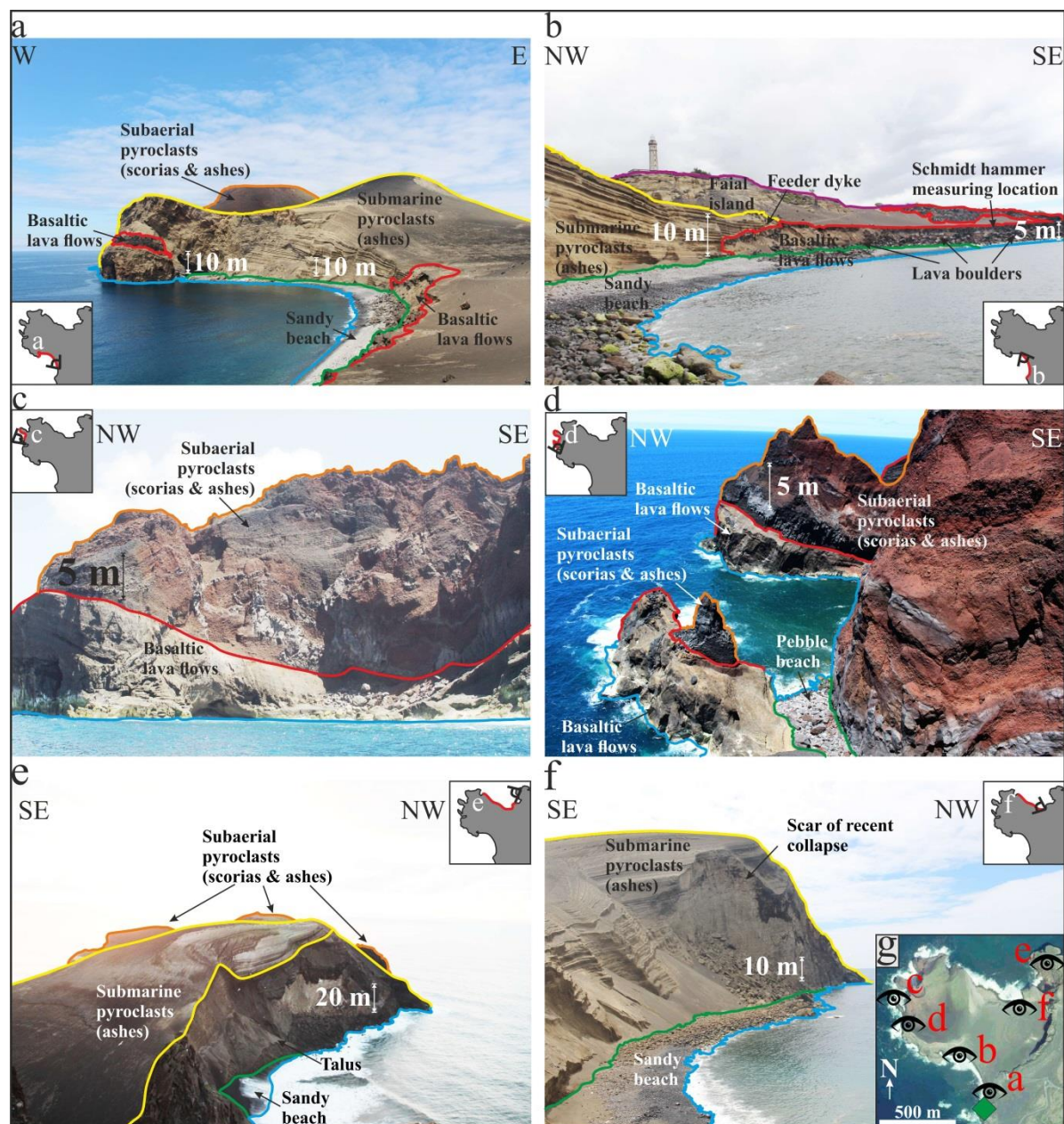
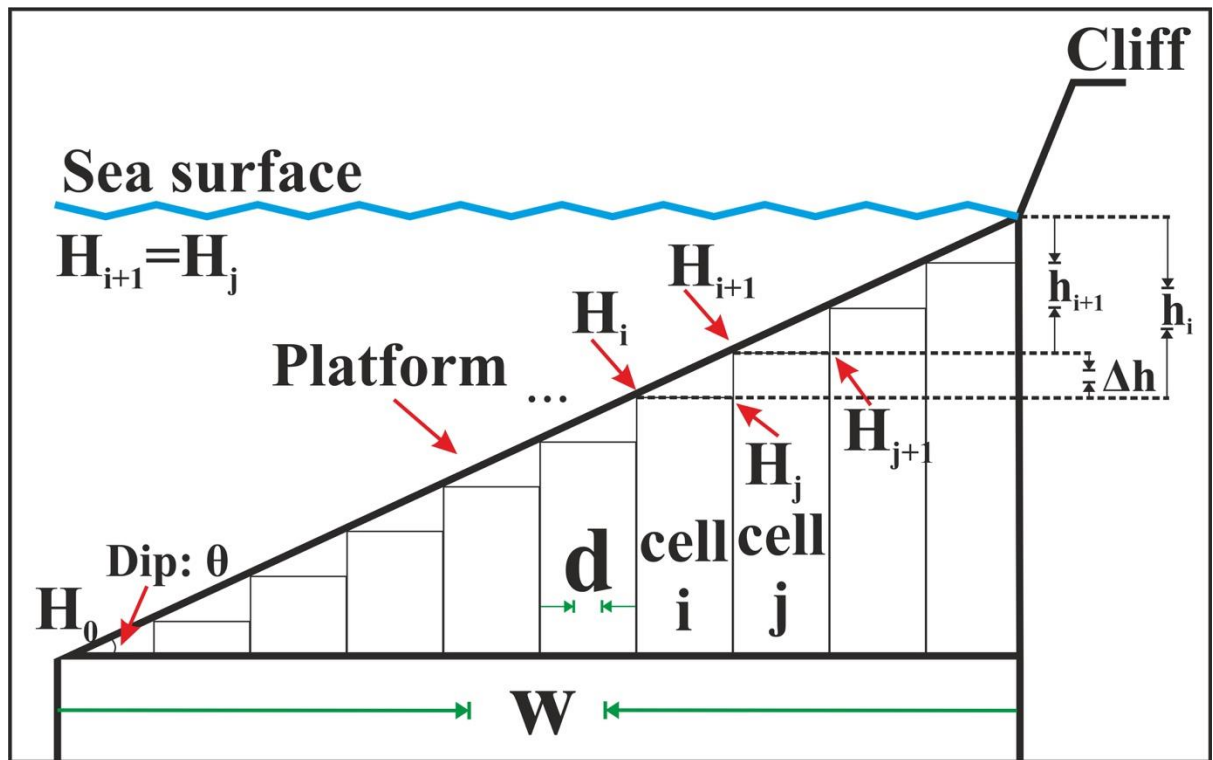


Figure 10. Photographs of Capelinhos coastal cliffs (in insets, red lines locate the exposed cliffs and black angles indicate the camera orientations). Blue lines mark the water lines, green lines mark the upper boundaries of sandy beaches, red lines delimit the basaltic lava flows, orange lines show the upper boundaries of the subaerial pyroclasts and yellow lines show the upper boundaries of the submarine pyroclasts. (a) Southwest coast of Capelinhos.

1247 Note the strata of submarine pyroclasts dipping landward with a steep  
1248 gradient (up to 30°) becoming nearly horizontal towards the easterly edge of  
1249 the photo. The marked basaltic lava flows in the far left is part of two sea  
1250 stacks that existed before the Capelinhos 1957/8 eruption. They are currently  
1251 being re-exposed by marine erosion (Forjaz, 2007). (b) Outcrop on the south  
1252 coast of Capelinhos with the paleo-cliff of Costado da Nau in the background  
1253 below the lighthouse. NW cliff in the image contains horizontally bedded  
1254 pyroclastic strata formed from hydromagmatic eruptions. SE cliff contains a  
1255 basaltic lava flow (distinguished from the overlying feeder dyke). Note in far  
1256 right large angular lava boulders at the base of the cliff caused by collapse of  
1257 the overlying lava flow. (c) Offshore view (taken in 2011) of the westernmost  
1258 cliff facing west showing a lower basaltic lava flow apparently lacking joints or  
1259 faults and topped by red iron-rich subaerial pyroclasts. (d) Westernmost cliff  
1260 of (c) in 2017. (e) Pyroclastic cliffs on the north coast (taken in 2011). Note in  
1261 bottom-centre the talus in the cliff base formed by cliff collapse. (f) Cliff  
1262 northeast of (e) in 2017. Note in far-centre the scar of a recent cliff collapse.  
1263 (g) Locations where photos (a) – (f) were taken (background from  
1264 google.com). Green diamond locates site of Schmidt hammer measurements.



1265

1266 Figure 11. Geometry used in finite-difference wave attenuation model in which

1267 the platform is approximated by a series of horizontal cells.

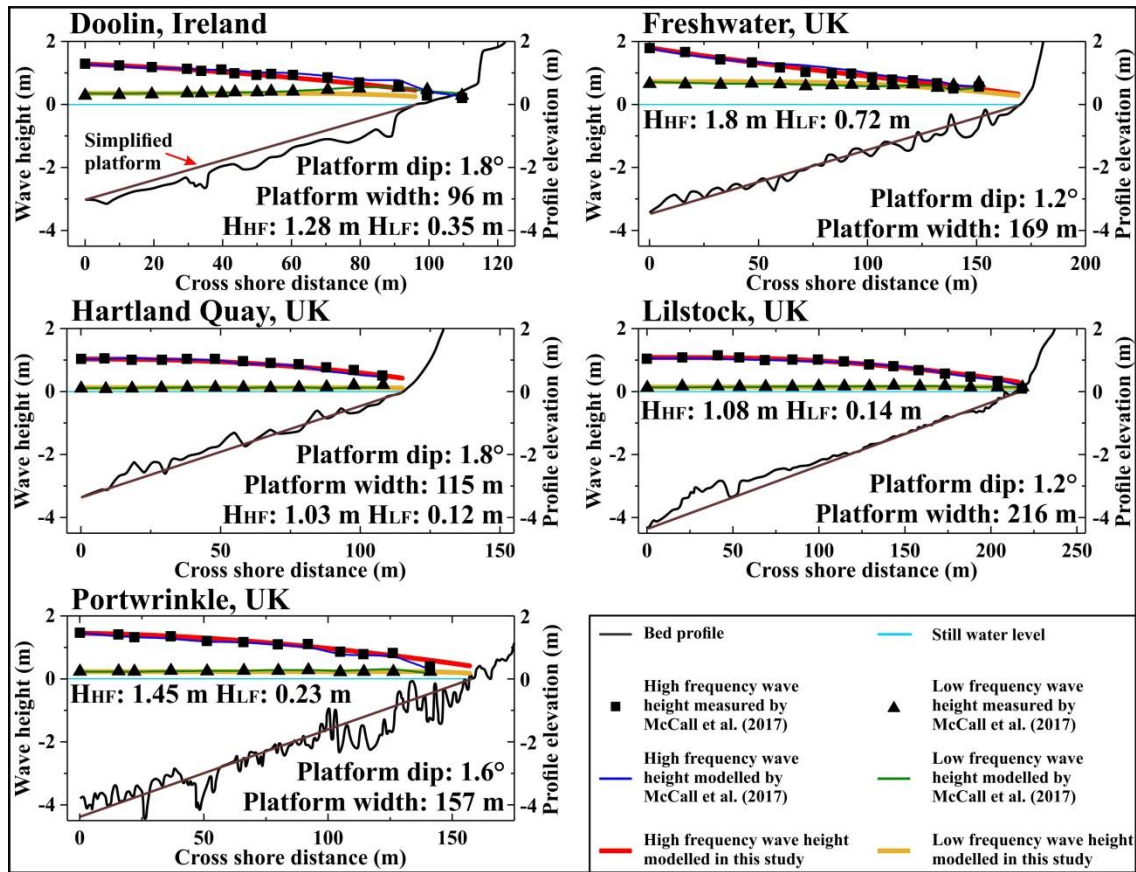


Figure 12. Comparison of observed wave height transformations over dipping platforms from McCall et al. (2017) with our finite-difference model predictions for high frequency (incident-band) and low frequency (infragravity). Split frequencies of 0.033 Hz (for Doolin, Freshwater, Hartland Quay and Portwrinkle) and 0.055 Hz (for Lilstock) were used to separate low frequency and high frequency motions. The model predictions of McCall et al. (2017) are also shown.



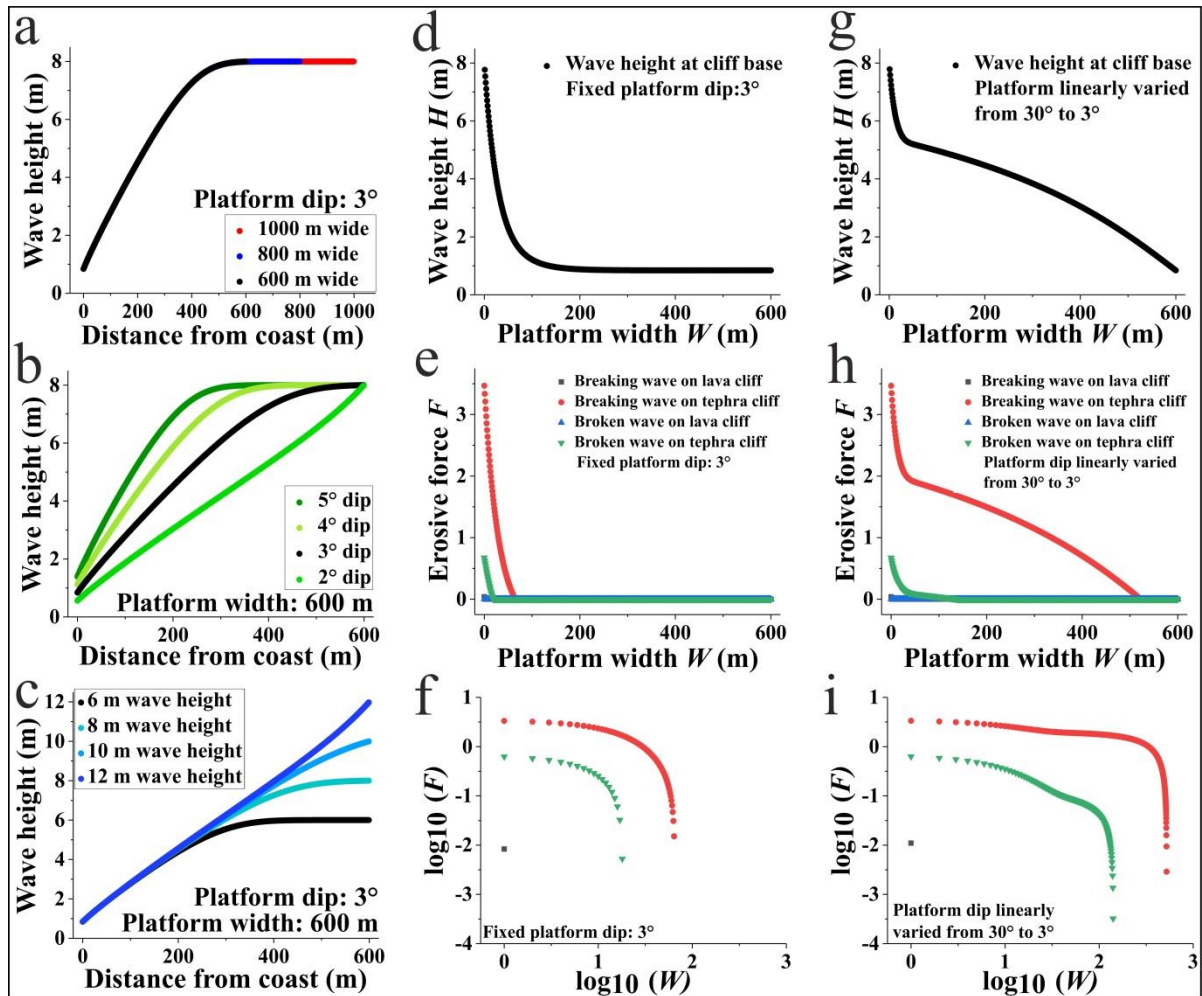
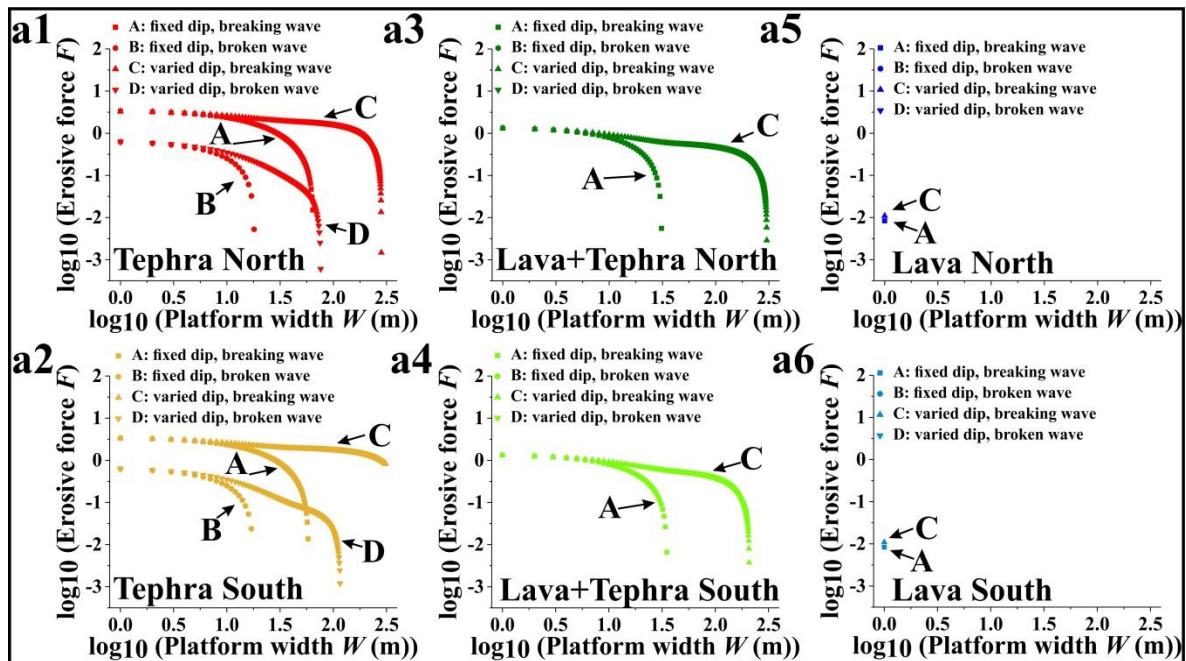


Figure 13. Simulations of effects of wave attenuation over dipping platforms of comparable dimensions to those of Capelinhos, using a cell size of 1 m. (a) Attenuated wave heights across platforms with varied widths marked in key. Wave height at platform edge is 8 m (critical wave height in appendix 6) and platform dips  $3^\circ$  (average dip in Table 2) seawards in direction of incoming waves. (b) Attenuated wave heights across dipping platforms with the varied platform dip angles marked. Wave height at platform edge is 8 m and platform width is 600 m (average platform widening distance in Table 2). (c) Attenuated wave heights across a dipping platform with the varied wave heights at the



1287 platform edge marked. Platform width is 600 m and platform dips 3°. (d) and  
 1288 (g) Variation of platform dip and wave height at the cliff base with platform  
 1289 width up to 600 m. Wave height at platform edge is 8 m. (e) and (h) Graphs  
 1290 of wave erosive force  $F$  for breaking and broken wave on lava and tephra cliff  
 1291 against platform width. (f) and (i) logarithmic graphs of (e) and (h). Note in (e)  
 1292 and (h) curves for broken waves on lava cliffs are obscured because they are  
 1293 overlain by the curves for breaking waves on lava cliffs. In (f) and (i) curves  
 1294 for broken waves on lava cliffs were unplotable to plot due to the logarithmic  
 1295 axis (zero values).



1297 Figure 14. Simulations of erosive force for six different coastal sectors using a  
 1298 cell size of 1 m (corresponding simulations of wave height are shown in  
 1299 Appendix 8). The initial conditions were obtained from the interpreted  
 1300 geometry in Figure 6b (values in Table 2) for different coastal sectors and

extreme wave conditions in Appendix 7a (wave height at platform edge is 8 m which is the average height of top 5 percentile wave conditions). (a1)-(a6) Logarithmic graphs showing how model wave erosive force for breaking and broken waves varies with platform width for six coastal sectors. The following compressive strengths were used: lava cliff 51.6 MPa from this study, tephra cliff 12 MPa and lava+tephra cliff of 22.4 MPa from appendix 6). For the A and B curves, models were run with a constant 3° dip. For C and D, models were run with dip varying from 30° to 3°. Note in a3-a6, curves B and D for broken waves were unplottable due to the logarithmic axis (zero values).

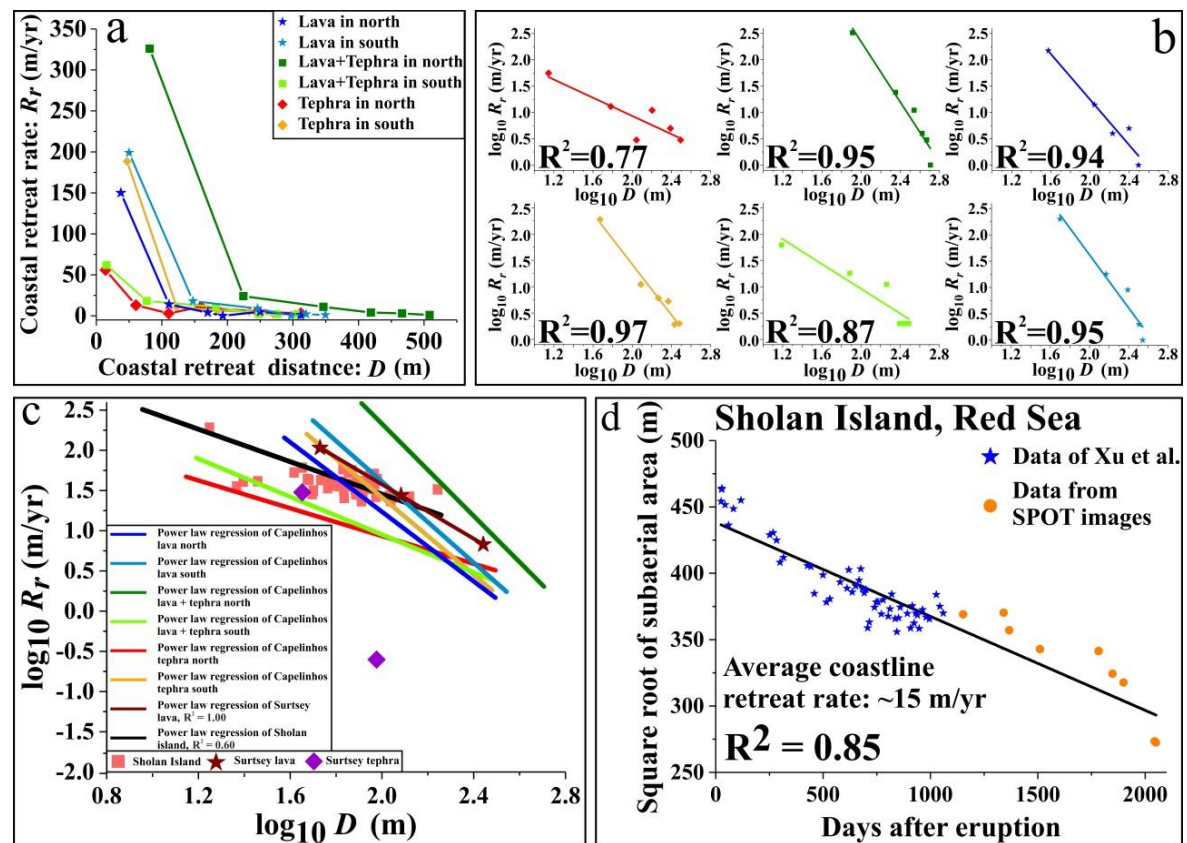


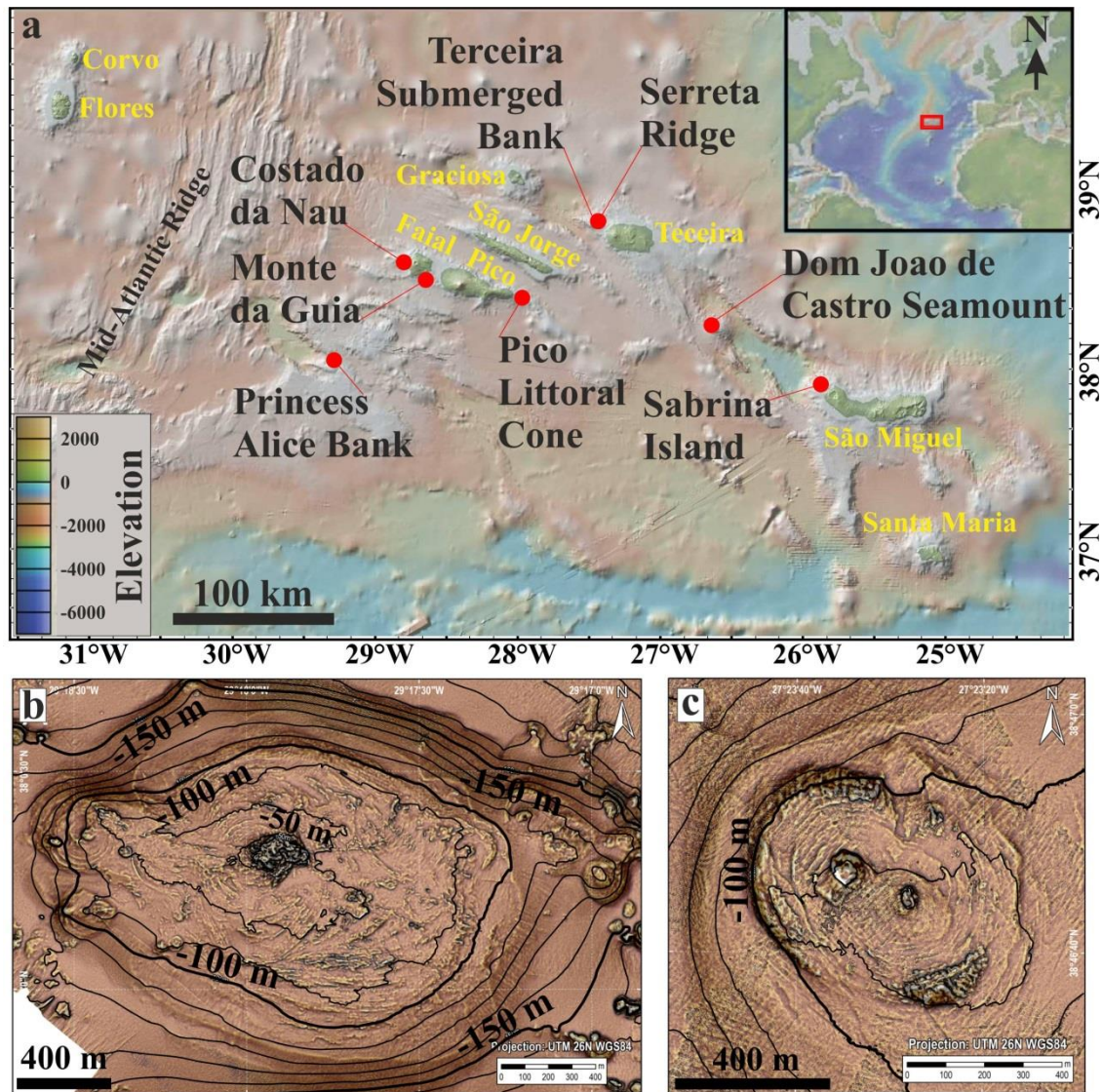
Figure 15. Relationships between coastal retreat rates ( $R_r$ ) and coastal retreat

1312 distance ( $D$ ) derived from the data in Figure 9. (a) Retreat rates versus the  
1313 coastal retreat distance for the six different coastal sectors (data in Table 1).  
1314 (b) The data plotted with two logarithmic axes revealing inverse power law  
1315 relationships for the six different coastal sectors. (c) Relationships of (b)  
1316 combined and compared with those for (brown line) Surtsey Island (for the  
1317 period 1963–2012 from data of Romagnoli and Jakobsson (2015), see Table  
1318 A2 for calculations) and (black line) Sholan Island (for the period 2011-2017,  
1319 data derived from (d)). (d) Post-eruptive areal changes of Sholan Island in the  
1320 Red Sea illustrating the early evolution not recorded at Capelinhos or Surtsey.  
1321 See Appendix 5 and Table A4 for images and interpreted coastlines.





1332  $h_d$ . (f) How the present subaerial part of the Surtseyan cone could eventually  
 1333 be removed by erosion. The horizontal positions of cliff base in stages I-IV are  
 1334 represented as  $w_0$ ,  $w_a$ ,  $w_b$  and  $w_c$ . Symbols  $\theta_0 - \theta_c$  represent the dips of  
 1335 platform in stages I-IV.  $h_a-h_c$  are depths of platform edge in stages I-IV.



1336  
 1337 Figure 17. Azores submerged banks of likely Surtseyan origin in multibeam  
 1338 bathymetry data (contour interval 10 m and highlighted every 50 m). (a)  
 1339 Locations of submerged Surtseyan cones. Submarine bathymetry and

1340 subaerial elevation data are from Global Multi-Resolution Topography Data  
1341 Synthesis (GMRT) of GeoMapApp (Ryan et al., 2009). (b) Top of the Princess  
1342 Alice Bank exhibiting a main Surtseyan cone in the centre and a smaller cone  
1343 to the left. Roughly concentric fine ridges on the bank likely represent different  
1344 stages of pyroclastic deposition throughout the eruption and effects of varied  
1345 resistance to erosion of the strata. (c) Submerged bank to the northwest of  
1346 Terceira Island exhibiting two adjacent extrusion centres and concentric fine  
1347 ridges.

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Table 1. Coastal retreat rates, areal changes and retreat distances for various coastal sectors of Capelinhos for the period 11958.11 – 2014.10. Values for incomplete coast are marked with \*.

Coastal Sector	Date $T$	Time interval $\Delta T$ (yr)	Elapsed time after eruption	Areal change $\Delta A$ (m <sup>2</sup> )	Average coastline length $L'$ (m)	Coastal retreat distance $\Delta D$ (m)	Total Coastal retreat distance $D$ (m)	Average retreat rate: $R_r$ (m/yr)
Tephra north	1958.11-1959.05	0.5	0.5	9538	340	28	28	56
	1959.05-1964.07	5.17	5.67	24179	370	65	93	13
	1964.07-1975.09	11.17	16.84	14358	416	34	128	3
	1975.09-1981.03	5.5	22.34	28396	450	63	191	11
	1981.03-2004.11	23.67	46.01	68130	627	109	300	5
	2004.11-2014.10	9.17	55.18	21120	868	24	324	3
Tephra south	1958.11-1959.05	0.5	0.5	40183	426	94	94	188
	1959.05-1964.07	5.17	5.67	28453	498	57	151	11
	1964.07-1975.09	11.17	16.84	37905	560	68	219	6
	1975.09-1981.03	5.5	22.34	12360	427*	29	248	5
	1981.03-2004.11	23.67	46.01	23602	523*	45	293	2
	2004.11-2014.10	9.17	55.18	11163	609*	18	312	2
Lava + Tephra north	1958.11-1959.05	0.5	0.5	39950	245	163	163	326
	1959.05-1964.07	5.17	5.67	25249	205	123	286	24
	1964.07-1975.09	11.17	16.84	21956	182	121	407	11
	1975.09-1981.03	5.5	22.34	4588	195	24	431	4
	1981.03-2004.11	23.67	46.01	17561	246	71	502	3
	2004.11-2014.10	9.17	55.18	3461	262	13	515	1
Lava + Tephra south	1958.11-1959.05	0.5	0.5	22285	724	31	31	62
	1959.05-1964.07	5.17	5.67	57477	625	92	123	18
	1964.07-1975.09	11.17	16.84	66292	557	119	242	11
	1975.09-1981.03	5.5	22.34	6696	561	12	254	2
	1981.03-2004.11	23.67	46.01	24705	551	45	299	2
	2004.11-2014.10	9.17	55.18	10756	597	18	317	2
Lava north	1958.11-1959.05	0.5	0.5	72788	970	75	75	150
	1959.05-1964.07	5.17	5.67	51365	715	72	147	14
	1964.07-1975.09	11.17	16.84	27092	586	46	193	4
	1975.09-1981.03	5.5	22.34	0	548	0	193	0
	1981.03-2004.11	23.67	46.01	45501	402	113	307	5
	2004.11-2014.10	9.17	55.18	2613	241	11	317	1
Lava south	1958.11-1959.05	0.5	0.5	12196	122	100	100	199
	1959.05-1964.07	5.17	5.67	10220	107	95	195	18
	1964.07-1975.09	11.17	16.84	16211	158	102	297	9
	1975.09-1981.03	5.5	22.34	0	212	0	297	0
	1981.03-2004.11	23.67	46.01	6784	148	46	343	2

	2004.11-2014.10	9.17	55.18	985	79	12	356	1
	1958.11-1959.05	0.5	0.5	196940	2827	82	82	164
	1959.05-1964.07	5.17	5.67	196943	2520	84	166	16
Average of all sectors	1964.07-1975.09	11.17	16.84	183813	2458	82	248	7
	1975.09-1981.03	5.5	22.34	52040	2393	21	269	4
	1981.03-2004.11	23.67	46.01	186283	2497	72	341	3
	2004.11-2014.10	9.17	55.18	50098	2656	16	357	2

Table 2. Geometry of platforms on selected bathymetric cross-sections (Figure6 B1-B6).

Cross section	Coastal sector	Total platform width (m)	Platform edge depth (m)	Dip of platform (°)
B1	Tephra north	533	22	3
B2	Lava north	703	36	3
B3	Lava+Tephra north	832	59	2
B4	Lava south	541	31	3
B5	Lava+Tephra south	383	38	5
B6	Tephra south	475	14	3

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**Appendices:**

Table A1. Root Mean Square Error of georeferencing and digitizing of maps.

Source	Historical shorelines	Resolution (dpi)	Reference scale	Root Mean Square Error (m)
Google Earth images	2004 and 2014	72	1:1,200	10.88
Historical map of Machado and Freire (1985)	1958, 1959, 1964, 1975 and 1981	68	1:1,200	39.44
Figure 5 in this study	1958, 1959, 1964, 1975, 1981, 2004 and 2014	600	1:500	41.01

Table A2. The digitised lengths of coastlines for different coastal sectors of Capelinhos for the period 1958 – 2014. Values for incomplete coast are marked with “\*\*”.

				Digitised coastline length $L$ (m)					
Date $T$				Tephra north	Tephra south	Lava + Tephra north	Lava + Tephra south	Lava north	Lava south
1958.11-	$T_a$	1958.11	$L_a$	336	391	273	757	1134	135
1959.05	$T_b$	1959.05	$L_b$	343	462	216	691	805	110
1959.05-	$T_a$	1959.05	$L_a$	343	462	216	691	805	110
1964.07	$T_b$	1964.07	$L_b$	397	535	194	559	624	104
1964.07-	$T_a$	1964.07	$L_a$	397	535	194	559	624	104
1975.09	$T_b$	1975.09	$L_b$	436	584	169	555	548	212
1975.09-	$T_a$	1975.09	$L_a$	436	384*	169	555	548	212
1981.03	$T_b$	1981.03	$L_b$	465	469*	221	567	548	212
1981.03-	$T_a$	1981.03	$L_a$	465	469*	221	567	548	212
2004.11	$T_b$	2004.11	$L_b$	789	576*	272	535	256	84
2004.11-	$T_a$	2004.11	$L_a$	789	576*	272	535	256	84
2014.10	$T_b$	2014.10	$L_b$	946	641*	251	659	227	75

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Table A3. Coastal retreat rates, areal changes and retreat distances in Surtsey for different cliff rock types in the period 1963 – 2012 calculated from Figure 12 of Romagnoli and Jakobsson (2015).

Cliff rock type	Date	Retreat rate (m/yr)	Areal change (km <sup>2</sup> )	Average retreat rate: $R_r$ (m/yr)	Coastal retreat distance $D$ (m)
Tephra and tuff	1964 - 1967	30	0.48 - 1	30	90
	1967 - 2006	0.2 - 0.3	0.4 - 0.48	0.25	99.75
Lava	1967 - 1968	75 - 140	1.8 - 1.9	107.5	107.5
	1969 - 1970	20 - 35	1.65 - 1.7	27.5	135
	1967 - 2012	1.5 - 12	0.8 - 1.65	6.75	418.5

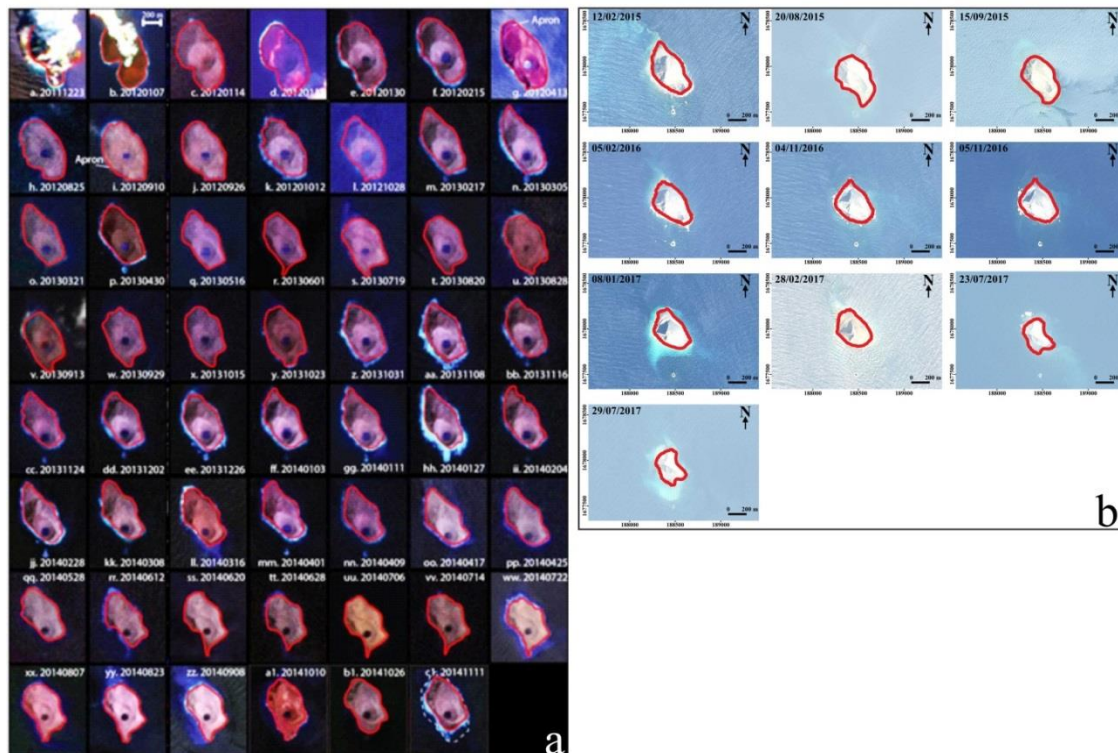
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Table A4. Root Mean Square Error from georeferencing and digitizing of Sholan Island satellite images.

Source	Historical shorelines	Spatial resolution (m)	Resolution in dots per inch	Reference scale	Root Mean Square Error (m)
Images from Xu et al. (2015)	2011.12-2014.11	30	4.23	1:5000	16.77
SPOT	2015.02-2017.07	2.5	101.6	1:10000	1.25

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1367 Appendix 5. Satellite images showing the 2011-2017 subaerial area of Sholan  
 1368 Island following the eruption. Coastline positions interpreted here are  
 1369 highlighted in red. (a) The images from EO-1, ALI, Landsat-7 and Landsat-8,  
 1370 typically with spatial resolutions of 30 m (Xu et al., 2015). (b) The images from  
 1371 SPOT with spatial resolutions of 2.5 m (esa.com).

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1378 Appendix 6.

1379 Sunamura et al. (2014) specified an equation of Kahraman (2001) to  
1380 estimate compressive strength  $S_c$  from cliff rock density and Schmidt hammer  
1381 rebound values:

$$1382 \quad S_c = 6.97e^{0.014\rho R} \quad (1)$$

1383 where  $S_c$  is the compressive strength in MPa,  $R$  is the Schmidt hammer  
1384 rebound value, and  $\rho$  is the rock density of cliff material in g/cm<sup>3</sup>.

1385 Machado et al. (1962) estimated the density of lava and tephra from  
1386 Capelinhos eruption as 2.6 g/cm<sup>3</sup> and 1.1 g/cm<sup>3</sup> respectfully. We averaged  
1387 these rock densities for lava+tephra sector cliffs (1.85 g/cm<sup>3</sup>). The average  
1388 Schmidt hammer rebound value measured from Capelinhos lava cliff is 55.  
1389 We used the average value of 35 for tephra from Kahraman (2001). The value  
1390 of 45 for lava+tephra sectors was obtained by averaging the above values for  
1391 lava and tephra materials.

1392 The compressive strength  $S_c$  of lava, tephra and lava+tephra is then  
1393 calculated as following from equation (1): Lava cliff:  $S_c = 51.6$  MPa; Tephra  
1394 cliff:  $S_c = 12.0$  MPa; Lava+Tephra cliff:  $S_c = 22.4$  MPa.

1395 Using the critical wave height equation of Sunamura (1992) for cliff  
1396 erosion:

$$1397 \quad H_{crit} = \frac{S_c}{\rho g} e^{-\Gamma} \quad (2)$$

1398 where  $S_c$  is the comprehensive strength of cliff material,  $\rho$  is the density of  
1399 seawater (1025 kg/m<sup>3</sup>),  $g$  is the gravity acceleration (9.8 m/s<sup>2</sup>) and  $\Gamma$  is a

1400 constant ( $\Gamma = \ln \frac{A}{B}$ ), A and B are constants and  $B/A = \epsilon = 0.0015$  for breaking  
 1401 waves or 0.0040 for broken waves (Sunamura et al., 2014).

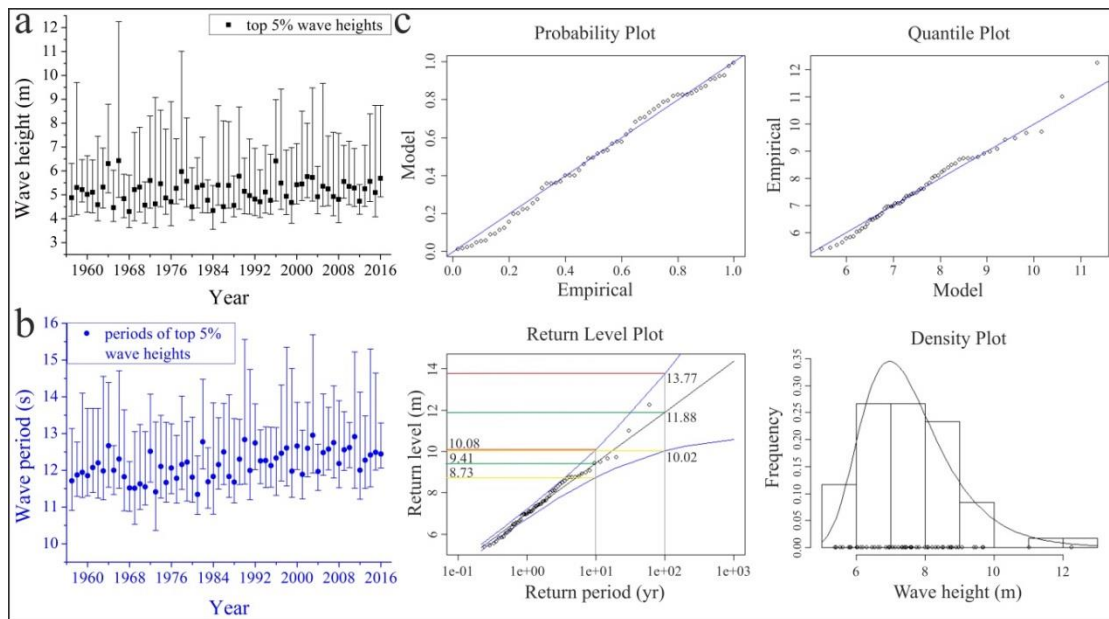
1402 From the comprehensive strength  $S_c$  for cliffs with different lithologies  
 1403 calculated above, we estimated the wave height threshold to initiate the cliff  
 1404 erosion for lava, tephra and lava+tephra cliffs under the attack of breaking  
 1405 and broken waves:

1406 Lava cliff: a) breaking wave:  $H_{crit} = 7.7$  m; b) broken wave:  $H_{crit} = 20.5$   
 1407 m;

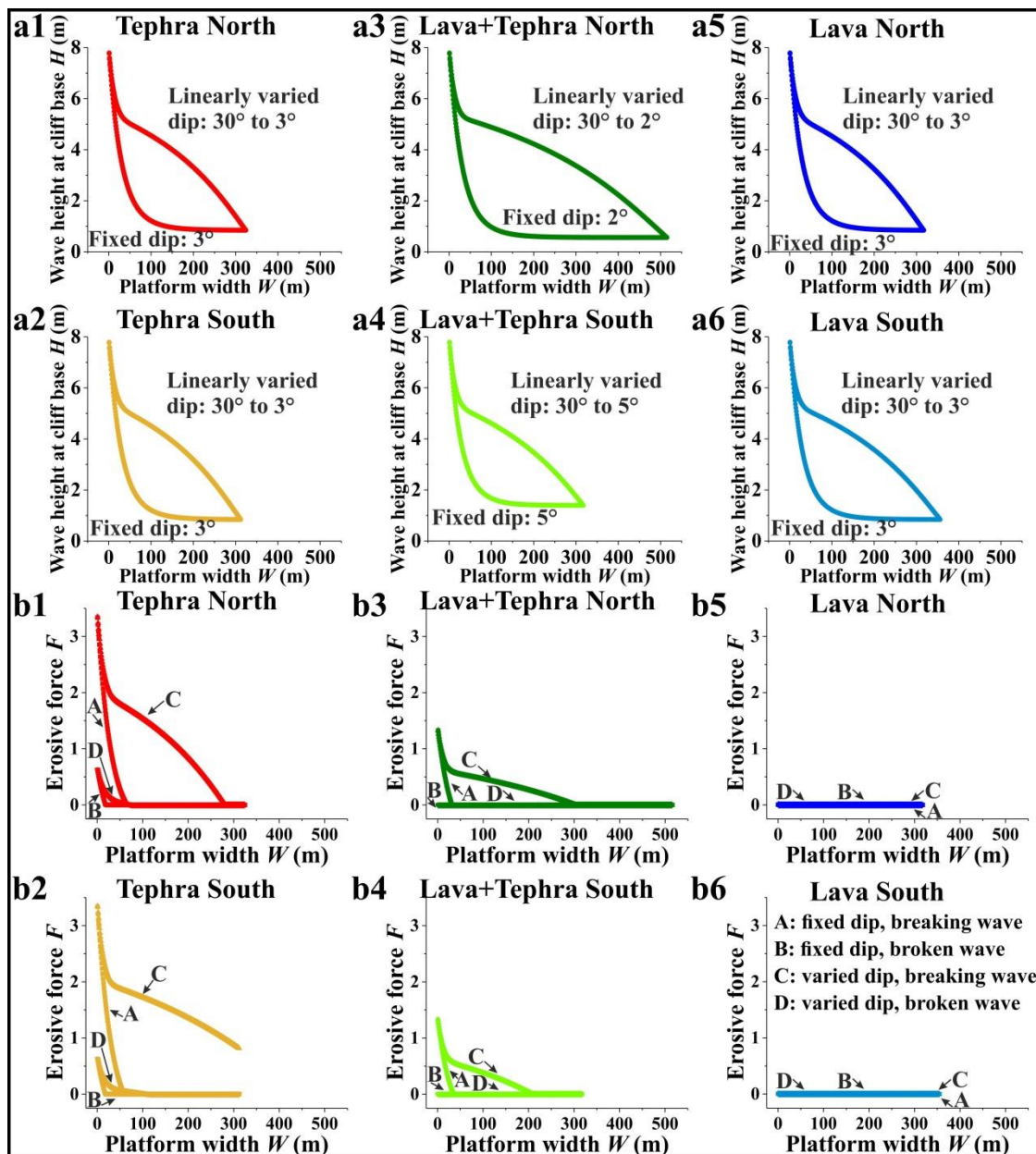
1408 Tephra cliff: a) breaking wave:  $H_{crit} = 1.8$  m; b) broken wave:  $H_{crit} = 4.8$   
 1409 m;

1410 Lava+Tephra cliff: a) breaking wave:  $H_{crit} = 3.3$  m; b) broken wave:  $H_{crit}$   
 1411  $= 8.9$  m.

1412 Hence, wave heights >5 m are likely to exceed the critical wave height  
 1413 allowing even broken waves to erode tephra cliffs. Wave heights >8 m were  
 1414 used in the numerical modelling part (Figures 13 and 14 and appendix 8) as 8  
 1415 m heights yield the critical wave height (breaking wave) of all cliff materials  
 1416 and dominate initiate coastal erosion.



Appendix 7. Extreme wave properties for the period 1957 – 2016 for a sea position adjacent to Capelinhos (38.625°N, 28.875°W) derived from ERA-40 and ERA-Interim outputs (Uppala, 2005; Dee, 2011). (a) For times when significant wave heights were in the top 5 percentile, solid circles represent their average heights and black bars show the range of heights. (b) For the same data durations as in (a), blue-filled circles represent their mean periods and blue bars the range of periods. (c) Diagnostic plots of generalised extreme value fit to extreme wave conditions modelled from the 60 maxima in the 1957 to 2016 extreme wave heights. The probability plot (top left panel) and quantile plot (top right panel) compare the simulated values to the empirical values. A return level plot (bottom left panel) indicates the expected extreme wave heights for different return periods. The density plot (bottom right panel) is the histogram of the extreme quantile against its probability (Tank et al., 2009; Lee, 2014).



Appendix 8. Simulations of wave height and erosive force for six different coastal sectors using a cell size of 1 m. (a1-a6) Variation of wave height at cliff base with respect to platform width for six coastal sectors. (b1-b6) Graphs of wave erosive force for breaking and broken waves on six coastal sectors using attenuated wave heights from a1-a6. The colour scheme follows the one of Figures 14 and 15.