



**British
Geological Survey**

NATURAL ENVIRONMENT RESEARCH COUNCIL

Effects of a conductive rail on parallel apparent resistivity measurements

Physical Hazards Programme

Internal Report IR/06/096



BRITISH GEOLOGICAL SURVEY

PHYSICAL HAZARDS PROGRAMME

INTERNAL REPORT IR/06/096

Effects of a conductive rail on parallel apparent resistivity measurements

P B Wilkinson

The National Grid and other Ordnance Survey data are used with the permission of the Controller of Her Majesty's Stationery Office. Ordnance Survey licence number Licence No: 100017897/2006.

Keywords

Electrical Resistivity
Tomography, Apparent
Resistivity, Railway.

Front cover

Apparent resistivity data being collected at the GCR test site.
Photo credit: Dr. J.E. Chambers.

Bibliographical reference

P B WILKINSON. 2006. Effects of a conductive rail on parallel apparent resistivity measurements. *British Geological Survey Internal Report*, IR/06/096. 14pp.

Copyright in materials derived from the British Geological Survey's work is owned by the Natural Environment Research Council (NERC) and/or the authority that commissioned the work. You may not copy or adapt this publication without first obtaining permission. Contact the BGS Intellectual Property Rights Section, British Geological Survey, Keyworth, e-mail ipr@bgs.ac.uk You may quote extracts of a reasonable length without prior permission, provided a full acknowledgement is given of the source of the extract.

© NERC 2006. All rights reserved

Keyworth, Nottingham British Geological Survey 2005

BRITISH GEOLOGICAL SURVEY

The full range of Survey publications is available from the BGS Sales Desks at Nottingham, Edinburgh and London; see contact details below or shop online at www.geologyshop.com

The London Information Office also maintains a reference collection of BGS publications including maps for consultation.

The Survey publishes an annual catalogue of its maps and other publications; this catalogue is available from any of the BGS Sales Desks.

The British Geological Survey carries out the geological survey of Great Britain and Northern Ireland (the latter as an agency service for the government of Northern Ireland), and of the surrounding continental shelf, as well as its basic research projects. It also undertakes programmes of British technical aid in geology in developing countries as arranged by the Department for International Development and other agencies.

The British Geological Survey is a component body of the Natural Environment Research Council.

British Geological Survey offices

Keyworth, Nottingham NG12 5GG

☎ 0115-936 3241 Fax 0115-936 3488
e-mail: sales@bgs.ac.uk
www.bgs.ac.uk
Shop online at: www.geologyshop.com

Murchison House, West Mains Road, Edinburgh EH9 3LA

☎ 0131-667 1000 Fax 0131-668 2683
e-mail: scotsales@bgs.ac.uk

London Information Office at the Natural History Museum (Earth Galleries), Exhibition Road, South Kensington, London SW7 2DE

☎ 020-7589 4090 Fax 020-7584 8270
☎ 020-7942 5344/45 email: bgs london@bgs.ac.uk

Forde House, Park Five Business Centre, Harrier Way, Sowton, Exeter, Devon EX2 7HU

☎ 01392-445271 Fax 01392-445371

Geological Survey of Northern Ireland, Colby House, Stranmillis Court, Belfast, BT9 5BF

☎ 028-9038 8462 Fax 028-9038 8461

Maclean Building, Crowmarsh Gifford, Wallingford, Oxfordshire OX10 8BB

☎ 01491-838800 Fax 01491-692345

Sophia House, 28 Cathedral Road, Cardiff, CF11 9LJ

☎ 029-2066 0147 Fax 029-2066 0159

Parent Body

Natural Environment Research Council, Polaris House, North Star Avenue, Swindon, Wiltshire SN2 1EU

☎ 01793-411500 Fax 01793-411501
www.nerc.ac.uk

Foreword

This report examines the effects of a conductive metal rail on apparent resistivity measurements made along a line running parallel to it.

Acknowledgements

This work was undertaken as part of the Railway Geotechnics project, funded by the NERC (BGS) Science Budget.

Contents

Foreword.....	4
Acknowledgements.....	4
Contents.....	5
Summary.....	7
1 Introduction & Method	8
2 Results	9
3 Conclusion.....	13
4 References	14

FIGURES

- Figure 1 Schematic diagram indicating the hemi-cylinder used to simulate the rail and the locations of the electrodes.
- Figure 2 Simulated ERT measurement configurations showing current (blue) and potential (red) electrodes.
- Figure 3 Dependence of apparent resistivity on depth-of-investigation for Pole-Pole arrays.
- Figure 4 Dependence of apparent resistivity on depth-of-investigation for Pole-Dipole arrays.
- Figure 5 Dependence of apparent resistivity on depth-of-investigation for Dipole-Dipole arrays.
- Figure 6 Dependence of apparent resistivity on depth-of-investigation for Wenner-Schlumberger arrays.
- Figure 7 Dependence of apparent resistivity on depth-of-investigation for Gradient arrays.
- Figure 8 Dependence of apparent resistivity on depth-of-investigation for Pole-Pole (red), Pole-Dipole (green) and Dipole-Dipole (blue) arrays.
- Figure 9 Dependence of apparent resistivity on depth-of-investigation for Pole-Pole (red), Pole-Dipole (green) and Dipole-Dipole (blue) arrays, and $c = 0$ to $c = 100$. Note that the vertical scale of each graph is different.

Summary

Apparent resistivity measurements made in proximity to a rail track are likely to be affected by preferential current channelling through the conductive rails. This report quantifies these effects using a simplified semi-analytic model to represent the rail. The results show that the commonly used measurement configurations are all affected in a similar manner, with greater distortion of the data at larger depths of investigation. The degree of distortion also depends on the contact resistance between the rail and the ground. The effect is least, however, for the Dipole-Dipole configuration, which is therefore recommended for resistivity surveys undertaken parallel to conductive rails. It is also recommended that the rail-ground contact resistance be measured during repeat resistivity surveys to allow the effects of the rail to be evaluated.

1 Introduction & Method

A conductive metal rail will affect apparent resistivity measurements made on the ground surface adjacent to it. Intuitively, one would expect the apparent resistivity to be reduced, since some current will be preferentially channelled through the rail. The purpose of this report is to quantify these effects on measurements made along a line running parallel to the rail. The examples shown relate specifically to electrical resistivity tomography (ERT) surveys to be undertaken at the Great Central Railway (GCR) test site as part of the Railway Geotechnics project (E2117S83).

The effect of the rail line is modelled using an infinitely long hemi-cylinder of radius $r_c = 0.05$ m embedded in an otherwise homogeneous half-space of resistivity $\rho = 1000 \Omega\text{m}$. The cylinder is assumed to be a perfect conductor. However, it has a finite interface conductance per unit area of $g \text{ Sm}^{-2}$ to account for the effect of contact resistance between the rail and the ground. The ERT electrodes are placed at spacings of 2 m along a line parallel to the rail and 2.6 m away from it (Figure 1).

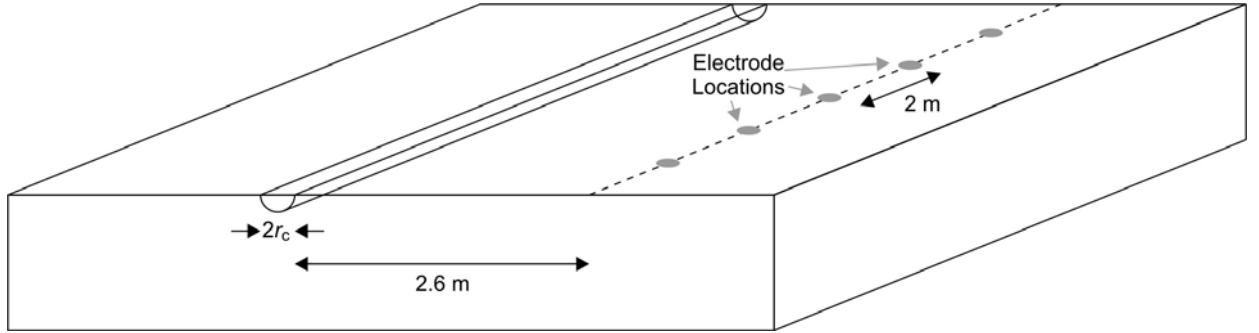


Figure 1: Schematic diagram indicating the hemi-cylinder used to simulate the rail and the locations of the electrodes.

In general, multi-electrode ERT array configurations can be constructed from sums of basic two-electrode (“pole-pole”) configurations. The effects of the hemi-cylindrical rail on these pole-pole configurations are calculated using the expressions derived in Wait (1983), in particular the approximation given by his Eq. 16. The results are given in terms of ρ_a/ρ , where ρ_a is the apparent resistivity measured by the configuration in the presence of the rail and ρ is the resistivity of the half-space. The resistivity ratio is plotted as a function of the median depth-of-investigation for each array configuration (Edwards, 1977). The median depth-of-investigation $\tilde{z}$ depends on the array type and increases with the overall length of the configuration. For this study, the maximum configuration length was chosen to be 80 m.

If the rail were not present then ρ_a/ρ would be unity, but for a conductive rail in electrical contact with the ground then it should be expected that $\rho_a/\rho < 1$. The quality of the contact is controlled by the interface conductance. It may be possible, using Eq. 10 of Wait (1983) and the general expression for contact resistance $R = V / \int_S \mathbf{J} \cdot d\mathbf{S}$, to calculate a realistic value for g from a contact resistance measurement made between the rail and a point on the ground. However, this calculation will be quite involved numerically and the details have not yet been worked out. It is easy though to simulate the worst-case scenario of zero contact resistance ($g = \infty$), in which the effect of the rail will be greatest. It will be shown that the general conclusions of this study are not changed by the choice of g .

The types of configurations under consideration are shown in Fig. 2. Apart from the basic pole-pole configurations, they were chosen from the many possible arrangements on the recommendations presented in Dahlin & Zhou (2004). For configurations with remote electrodes, these were placed 1000 m from the rail in the direction perpendicular to its axis.

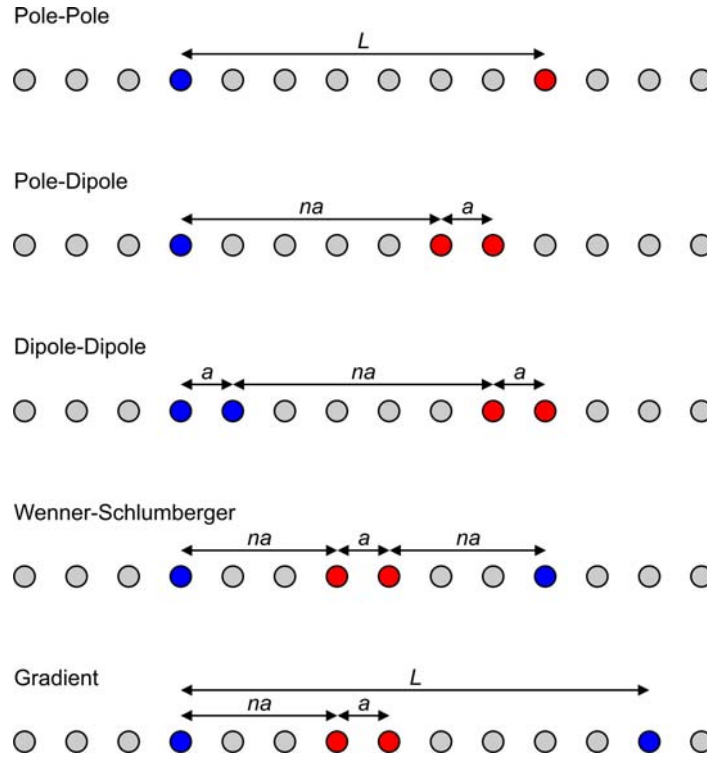


Figure 2 Simulated ERT measurement configurations showing current (blue) and potential (red) electrodes.

2 Results

The effects of increasing $\tilde{z}$ on the simulated apparent resistivity data are shown in Figs. 3-7 for Pole-Pole, Pole-Dipole, Dipole-Dipole, Wenner-Schlumberger and Gradient configurations respectively. The effect of increasing depth-of-investigation on the measured apparent resistivity is remarkably similar for all the arrays that were tested. In every case, the greater the depth-of-investigation, the greater the reduction in the measured apparent resistivity caused by the conductive rail. This seems intuitively reasonable since greater depths are probed by longer configurations, which one would expect to be influenced more strongly by the rail. For shorter configurations, however, some array types are affected more than others, although not to a great degree. This is illustrated by Fig. 8, which shows the Pole-Pole, Pole-Dipole and Dipole-Dipole results on the same graph and in more detail. Note that Wenner-Schlumberger and Gradient arrays are not shown in Fig. 8. This is because the effect of the rail on these configurations is very similar to that on the Pole-Dipole array (the reason for this can be appreciated on a qualitative level; the Wenner-Schlumberger and Gradient arrays are essentially Pole-Dipole arrays with the distance to the “remote” electrode reduced).

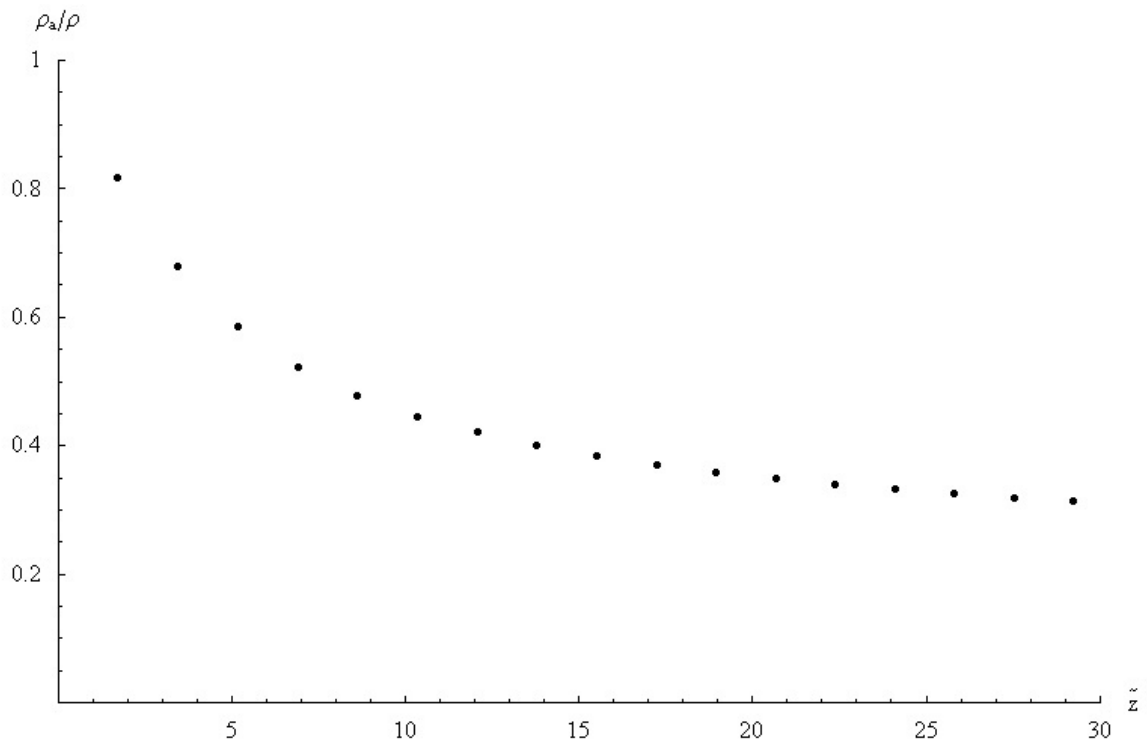


Figure 3: Dependence of apparent resistivity on depth-of-investigation for Pole-Pole arrays.

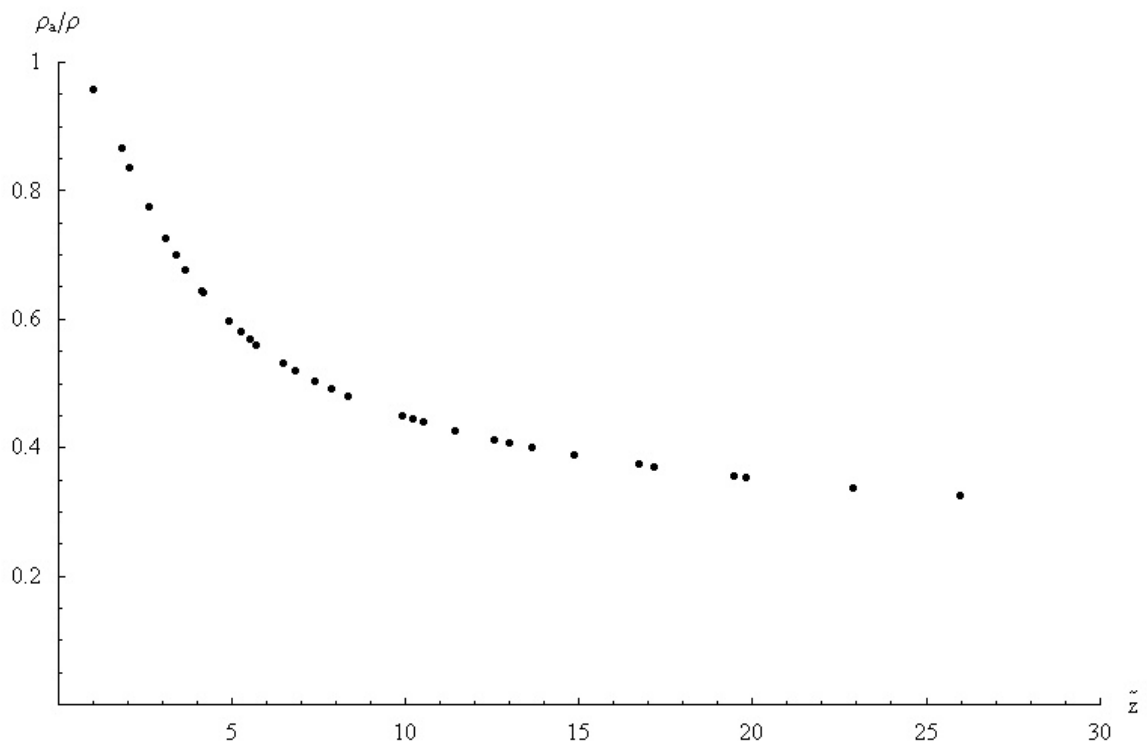


Figure 4: Dependence of apparent resistivity on depth-of-investigation for Pole-Dipole arrays.

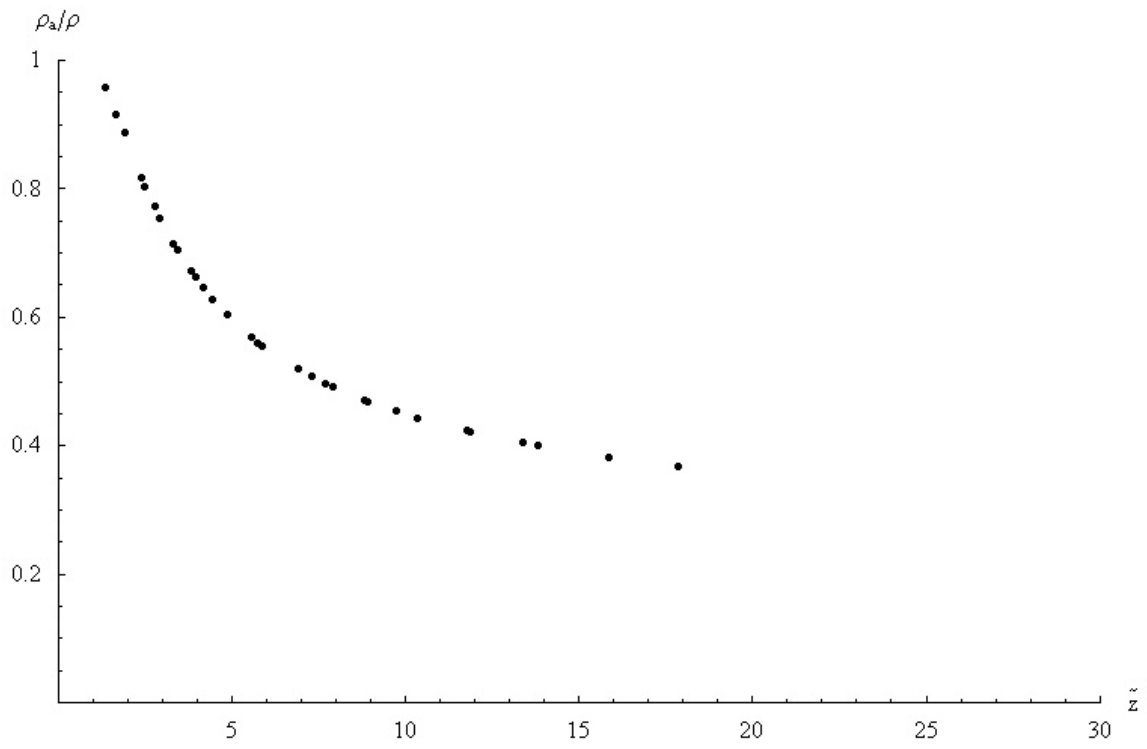


Figure 5: Dependence of apparent resistivity on depth-of-investigation for Dipole-Dipole arrays.

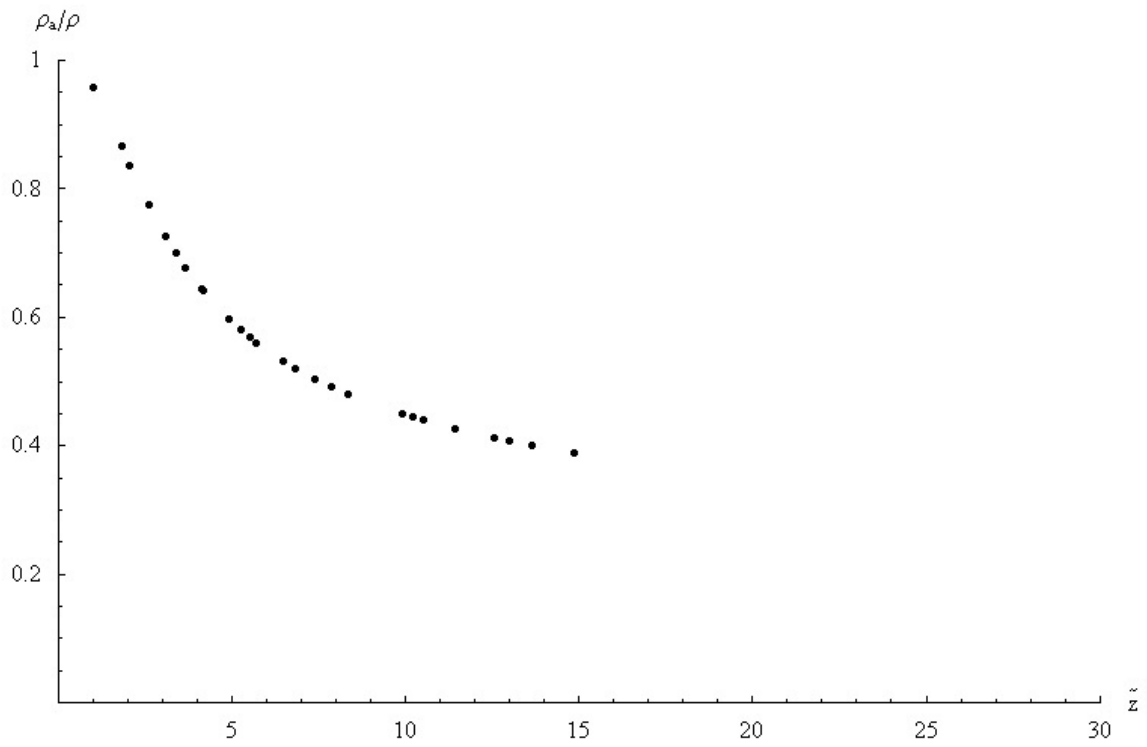


Figure 6: Dependence of apparent resistivity on depth-of-investigation for Wenner-Schlumberger arrays.

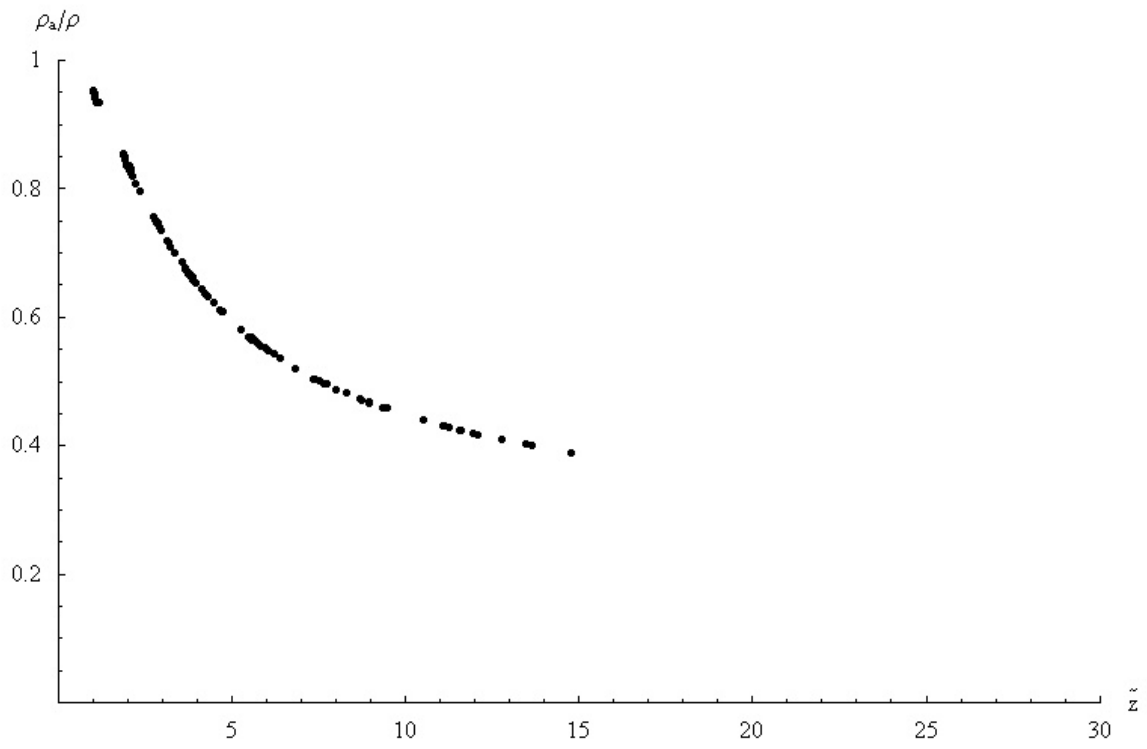


Figure 7: Dependence of apparent resistivity on depth-of-investigation for Gradient arrays.

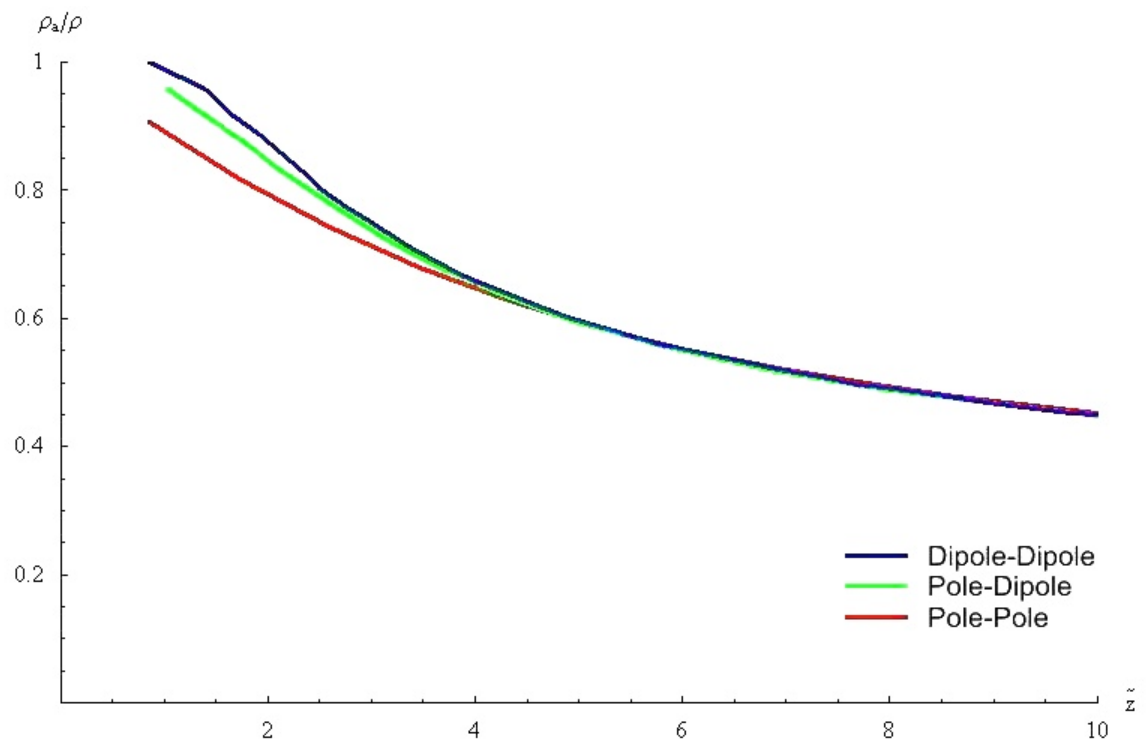


Figure 8: Dependence of apparent resistivity on depth-of-investigation for Pole-Pole (red), Pole-Dipole (green) and Dipole-Dipole (blue) arrays.

By examining Fig. 8, one can see that for $\tilde{z} < 4-5$ m there is an advantage to using Pole-Dipole over Pole-Pole, and a further advantage to using Dipole-Dipole over Pole-Dipole. This is likely to be due to differences in the sensitivity distributions of the different array types. The sensitivity distribution of a given configuration depends on where the current flows in the surrounding region. Since the electric field of a dipole decreases more rapidly with distance than that of a pole, the current will flow closer to the measurement line for configurations containing dipoles than for configurations containing poles. Therefore, we would expect short Dipole-Dipole configurations to be less sensitive to the presence of the rail than corresponding Pole-Pole or Pole-Dipole configurations.

It is likely that the effect on ERT measurements made at the GCR site will not be as severe as those simulated here. This is because there will be a non-zero contact resistance between the rail and the ground. Figure 9 shows the effect of varying the contact resistance, which is proportional to the dimensionless parameter $c = 1/(gpr_c)$, where r_c is the model cylinder radius.

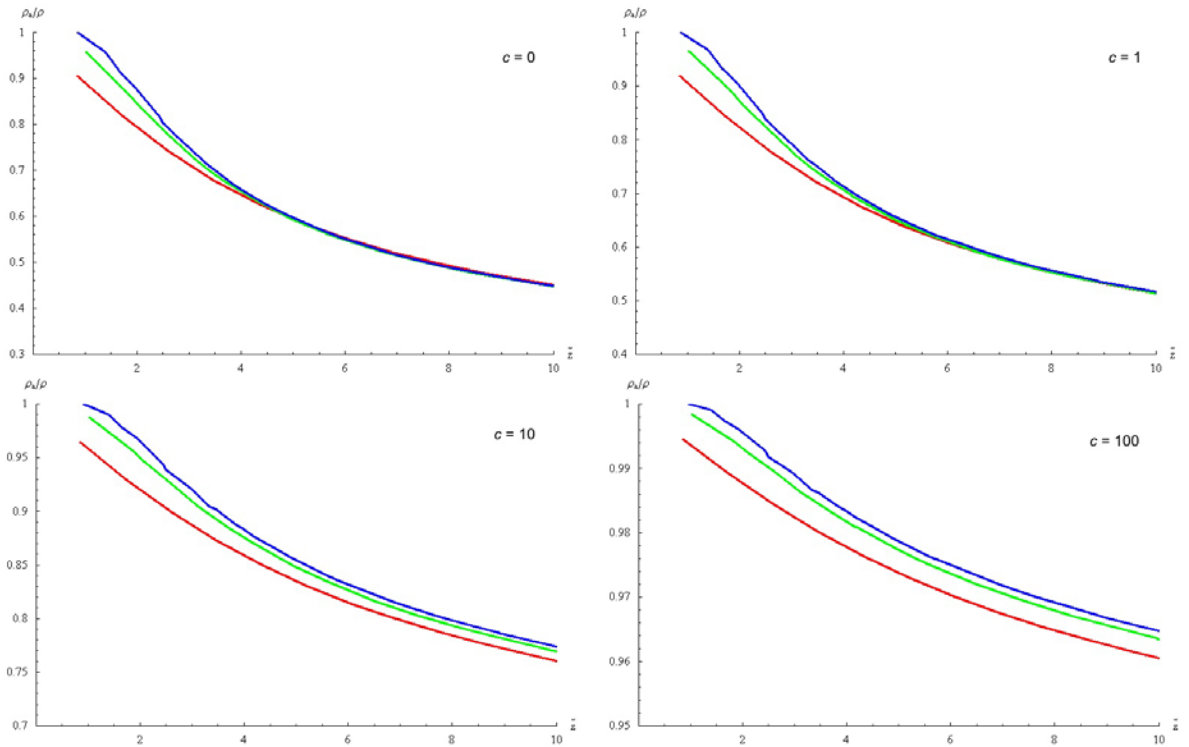


Figure 9: Dependence of apparent resistivity on depth-of-investigation for Pole-Pole (red), Pole-Dipole (green) and Dipole-Dipole (blue) arrays, and $c = 0$ to $c = 100$. Note that the vertical scale of each graph is different.

Figure 9 indicates that, whatever the contact resistance of the rail, the Dipole-Dipole array is affected the least, and is therefore the best choice. It also shows that, for larger contact resistances, the superiority of the Dipole-Dipole configuration is reduced in magnitude, but extends to greater depths-of-investigation.

3 Conclusion

The effects of a conductive rail track on apparent resistivity measurements made along the direction parallel to it have been investigated using a simple semi-analytical model. As expected,

the apparent resistivity is reduced by the presence of the rail. It was found that all commonly used ERT array configurations are affected to a similar degree. However, there are small advantages to be gained by using configurations containing dipoles (close pairs of current and / or potential electrodes). Consequently the configuration that is influenced least by the rail is the Dipole-Dipole type, and therefore this is recommended for use when conducting ERT surveys parallel to rail lines. The reduction in apparent resistivity is more pronounced at greater depths of investigation, and this effect may manifest itself as a decrease in resistivity with depth in any resulting ERT image. In general, the severity of the effect on the apparent resistivity data depends on the contact resistance between the rail and the ground, and is this more pronounced if the contact resistance is low. Making a quantitative assessment of the degree of influence of the rail for a known measured contact resistance should be possible, but this would require further work. It is recommended that an additional procedure be included in field operations to measure the rail-ground contact resistance so that its effect on the ERT surveys can be evaluated. This is particularly relevant to resistivity monitoring programmes that include a series of repeat surveys to assess the effects of long-term seasonal changes.

4 References

The references listed below are held in the Library of the British Geological Survey at Keyworth, Nottingham. Copies of the non-confidential references may be purchased from the Library subject to the current copyright legislation. Confidential reports cannot be released without the written permission of the client.

- DAHLIN, T, AND ZHOU, B. 2004. A numerical comparison of 2D resistivity imaging with 10 electrode arrays. *Geophysical Prospecting*, Vol. 52, 379-398.
- EDWARDS, L S. 1977. A modified pseudosection for resistivity and IP. *Geophysics*, Vol. 42, 1020-1036.
- WAIT, J R. 1983. Resistivity response of a homogeneous earth with a contained vertical conductor. *IEEE Transactions on Geoscience and Remote Sensing*, Vol. GE-21, 109-113.