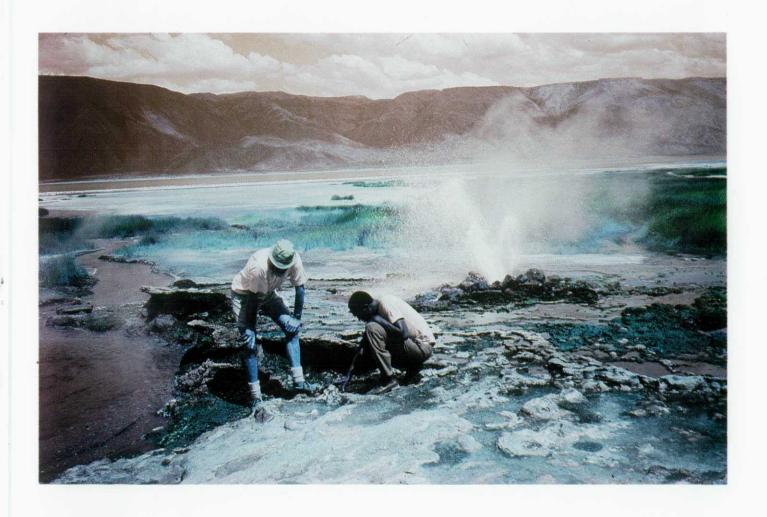
Geothermics and hydrogeology of the southern part of the Kenya Rift Valley with emphasis on the Magadi–Nakuru Area



Research Report SD/89/1 Hydrogeology Series



British Geological Survey

# RESEARCH REPORT SD/89/1

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D J Allen, W G Darling and W G Burgess

# BRITISH GEOLOGICAL SURVEY

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This report was prepared for the Overseas Development Administration

Cover illustration
Project staff examining hot
springs at Lake Bogoria

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#### **FOREWORD**

This report summarizes the findings of the hydrogeological component of the British Geological Survey (BGS)/Ministry of Energy and Regional Development (MERD) contribution to the Kenya Rift Valley Geothermal Project. This is a bilateral technical co-operation project between the Government of the United Kingdom - represented by the Overseas Development Administration (ODA) - and the Government of Kenya (GOK). Assistance by the Government of the UK was designed to fit within the framework of a larger United Nations Development Programme (UNDP)/GOK project whose objectives were to explore for geothermal energy in the Rift Valley between the Silali crater in the north and the Tanzanian border in the south.

During the project, which lasted from 1985 to 1988, fieldwork and hydrogeological data record collection were initially carried out by W.G. Burgess of BGS in co-operation with MERD scientists Messrs. Mariita, Nyaga, Odondi and Ouma. Subsequent work in Kenya was undertaken by D.J. Allen and W.G. Darling of BGS, assisted by Mr Ndogo of MERD. Sample analyses were undertaken mainly by staff at the BGS laboratories at Wallingford (and elsewhere as noted in the text). Data interpretations were made by the authors. The work was carried out under the general supervision of Dr. M.C.G. Clarke (Project Leader), and Dr. R.L. Johnson (Regional Geologist, Africa and the Middle East).

The report fully supersedes ten interim reports (listed in the References) which have been issued at intervals since December 1985. All analyses given in the previous reports are presented in this summary document.

In general the physical hydrogeological and hydrogeochemical investigations carried out during the project are described separately in this report (Chapters 4 and 5). However in the cases of the Olkaria and Magadi regions the large quantity of data made it more appropriate to consider the areas individually (Chapters 6 and 7). A summary of the conclusions of the study is presented in Chapter 8.

The work described in this report was carried out on behalf of ODA. The results may be used to aid formulation of Government policy but do not in themselves represent Government policy. They are presented in a format agreed between ODA and BGS. The views and judgements expressed are those of the British Geological Survey and do not necessarily represent those of ODA.

This report presents the results of hydrogeological and hydrogeochemical studies in the Kenya Rift Valley as part of the British Geological Survey (BGS)/Ministry of Energy and Regional Development (MERD) contribution to the Kenya Rift Valley Geothermal Project.

The objective of these studies was to provide a greater understanding of the location, nature and movement of the thermal waters in the Rift and of the cool ambient waters recharging the thermal fields. In the study the physical hydrogeology of the Rift was investigated to provide basic information concerning regional groundwater occurrence and flow patterns. The chemistry of both thermal and ambient waters was studied in order to understand the nature and origin of the thermal waters and to further explain groundwater mixing patterns.

Physical hydrogeological data were collected over a region of the Rift Valley from the Tanzanian border in the south (Figure 2.1) to Nakuru in the north and extending to the groundwater divides on the bounding rift escarpments. Information from 600 boreholes in this area was abstracted from records and supplemented by data collected in the field. The types of data collected included lithological information, hydraulic data and borehole constuction details.

Analysis of these data has shown that on a regional scale the Rift Valley between Lakes Nakuru and Magadi broadly exhibits the hydrogeological features expected of a Valley-interfluve system, with lateral groundwater flows from the Rift escarpments to discharge areas on the Rift floor and axial groundwater flows away from the Rift floor culmination at Lake Naivasha. This model is modified by the presence of the major Rift faults, which act as barriers to lateral flow, leading to longer, deeper, flow paths, and by the grid faulting in the Rift floor which tends to align flow paths within the Rift along its axis.

The permeabilities of the volcanic rocks underlying the Rift Valley are generally poor. Aquifers are normally found in fractured or reworked volcanics and are usually confined. Aquifer properties at depths exceeding 250 metres are virtually unknown except in the Olkaria geothermal field where low permeabilities (around 5 millidarcies) are found. Preliminary modelling studies carried out during the project suggest that rocks at depth elsewhere in the rift may also have low permeabilities.

Preliminary water balance estimates from the Naivasha catchment suggest that subsurface flow from Lake Naivasha is directed predominantly to the south, and that the quantity of discharge is greatly in excess of the geothermal discharge of the Olkaria power station. It is therefore considered unlikely that geothermal abstraction affects the level of the lake.

Fluid samples for hydrochemical analysis were taken from 129 sites ranging from the Silali area in the north (Figure 2.1) to Lake Magadi in the south. Samples were taken both from thermal sources (geothermal boreholes, fumaroles and thermal springs) and non-thermal sources (water boreholes, springs, lakes and rivers). In addition samples of rainfall were taken for isotopic analysis, and fumarole fluid samples collected by a UNDP project were

analysed.

These analyses have enabled the model of the regional flow systems to be substantially improved. In particular the mixing between subsurface discharge from Lake Naivasha and rift-wall waters has been shown using stable isotope techniques, and Naivasha water has been traced as far south as Suswa volcano and to the north as far as Lake Elmenteita. The analysis of geothermal fluids from Eburru, Olkaria, Longonot and Suswa has led to the conclusion that all the fluids can be explained in terms of a mixing series between Rift wall water and water from Lake Naivasha, and there is no evidence of a unique deep thermal water.

Two thermal areas - Olkaria and Magadi - were examined in some detail during the study. At Olkaria the results support the conclusion of other workers that the present wellfield is situated somewhat to the south of a thermal upflow. Other thermal upflows at Eburru and Longonot are implied from gas analyses. There are indications at Olkaria that short flow paths may be involved, and that the system may be quite old. At Magadi it is concluded that the thermal springs are formed by a two-component mixing series, probably with a local heat source, and that the hot end member is at a temperature of 100-130°C.

The main conclusions of this study are that the geothermal areas at Eburru, Olkaria-Domes, Longonot, Suswa and Magadi are individual geothermal fields with local heat sources giving rise to separate convective cells in which the geothermal fluids originate as mixtures of ambient groundwaters and lakewater (or groundwater and river water in the case of Magadi). It is recommended that further investigation concentrates on the main areas of upflow, at Olkaria-Domes, Eburru and Longonot.

#### **ACKNOWLEDGEMENTS**

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. 1

#### 1 INTRODUCTION

The purpose of this study was to investigate the hydrogeology of a section of the Rift Valley with particular reference to its geothermal character. The study examined in detail an area between Lake Nakuru in the north and Lake Magadi in the south (Figure 2.1), with emphasis on the Naivasha catchment. In addition chemical sampling was undertaken as far north as Silali and as far west as Homa Bay, and rainfall samples were collected over an even larger area.

The ultimate objective of a study such as this is the production of a conceptual model of the major systems of groundwater flow in the Rift Valley. These can broadly be classified as cold or ambient water systems, which are driven by topographic head gradients, and hot water systems, driven principally by head gradients resulting from the density differences between hot and cold fluids.

The cold water systems can be studied by standard hydrogeological techniques which involve the construction of piezometric maps from water level data (mainly derived from boreholes), and the assessment of the hydraulic properties of the aquifer (normally obtained from pumping tests). In the Rift Valley these techniques are restricted by the lack and poor quality of such data, but by making certain assumptions valuable insight can be obtained into directions and likely amounts of flow. In addition to the physical data, chemical and isotopic data are important in helping to identify possible recharge areas, mixing patterns and residence times of groundwaters, which in turn are used to correct and improve the physical model.

Geothermal systems are unlikely to be penetrated by boreholes (unless geothermal exploration boreholes have been drilled) and the geochemical investigation of the thermal fluids therefore assumes a greater importance. Indeed in the reconnaissance stage of exploration (before surface geophysical techniques are employed) geochemistry is by far the most valuable tool in determining the hydrodynamic nature of a geothermal system, providing information such as the nature of the geothermal fluid, temperatures at depth, mixing processes and likely areas of upflow.

By combining the model of the cold water systems (derived mainly from physical data) with that of the geothermal systems (deduced essentially from chemical data) the relationship between the two can be studied. This enables questions about the origin of the geothermal fluids, areas of recharge to and discharge from the geothermal fields, and availability of recharge to the exploited fields to be addressed.

The structure of the report reflects the above approach. The initial sections are concerned with the physical hydrogeology of the study area, and in the main these are concerned with ambient water flows. The section on geochemistry deals in detail with geothermal manifestations, as well as ambient water chemistry. The geothermal field at Olkaria and the geothermal manifestations at Magadi have warranted detailed investigations and accordingly are treated separately.

The concluding discussion is essentially a broad summary of the conclusions reached in the preceding sections of the report.

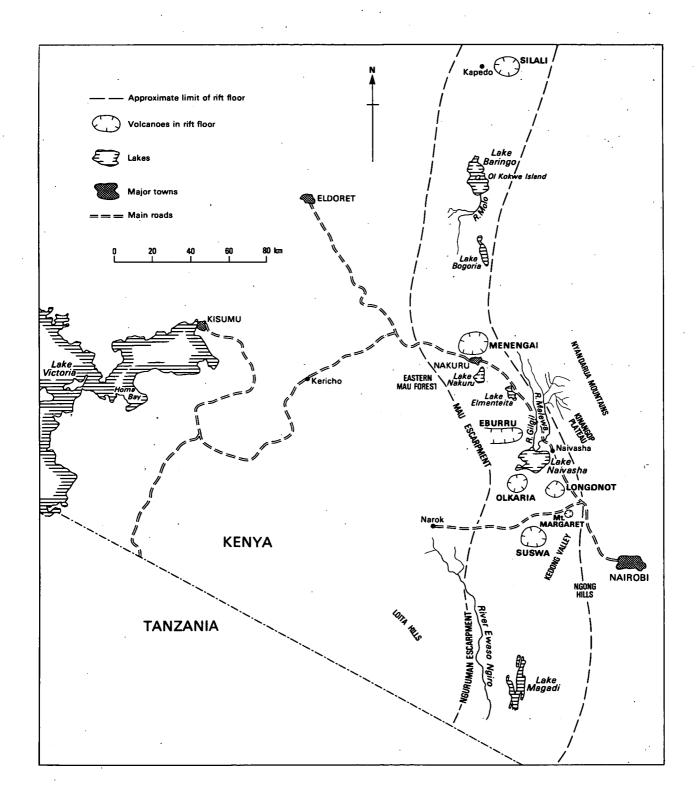


Figure 2.1 Location map

#### 2 PHYSIOGRAPHY AND SURFACE HYDROLOGY

### 2.1 Nakuru - Longonot

The Rift Valley in the area between Lake Nakuru and Longonot volcano (Figures 2.1 and 4.1) is bounded by the Mau Escarpment in the west, rising to 3000 m, and the Nyandarua - Kikuyu Escarpment in the east with a maximum elevation of 3999 m. The central Rift is further bounded by relatively high fault scarps and intervening plateaux on either side, notably the Rongai Plain (1800 to 2000 m) and the Eburru Forest (2400 to 2670 m) in the west and the Bahati Escarpment (2100 to 2400 m) and the Kinangop Plateau (2100 m) in the east, (although the Kinangop Plateau is strictly speaking a shelf rather than a plateau). The Ol Bolossat Plain (2300 m) lies between the Nyandarua Mountains and the Bahati Escarpment and forms a northward extension of the Kinangop Plateau.

The floor of the Rift Valley culminates near Lake Naivasha (1880 m). To the north are Lakes Elmenteita (1780 m) and Nakuru (1760 m). All three lakes lie in basins of internal drainage. To the south of Lake Naivasha Longonot volcano rises to 2780 m and Menengai crater (2280 m) lies to the north of Lake Nakuru. A series of smaller volcanic hills further disrupts the valley floor between Olkaria (2434 m) south-west of Lake Naivasha, and Lake Elmenteita, either side of Eburru mountain. A prominent gorge, Ol Njorowa (Hell's Gate) runs south from Lake Naivasha separating Olkaria from the lower slopes of Longonot.

In terms of surface water hydrology the area containing Lakes Nakuru and Elmenteita can be considered separately from that occupied by Lake Naivasha.

### 2.1.1 Nakuru - Elmenteita Area

Lake Nakuru (which is separated from Lake Elmenteita by a low topographic divide) lies at the northern boundary of the study area, in a graben between Isirkon (2097 m) to the east and the Mau Escarpment to the west. Menengai rises to the north of the lake, and the high ground of the Mau and Eburru Forests lies to the south. The lake is alkaline and saline (sodium - bicarbonate type) as a result of evaporation and is recharged by rainfall, surface runoff and groundwater.

The rivers Njoro, Larmudiac, Makalia, and Nderit drain from the Mau Escarpment towards Lake Nakuru, but most of the flow is lost as groundwater recharge before the lake is reached. Of these rivers the Makalia and Njoro are normally perennial (McCann, 1972). The Ngosur (a permanent stream) and several minor streams flow from the Bahati uplands westwards towards Lake Nakuru, although none of them reaches the lake.

Lake Elmenteita is, like Lake Nakuru, recharged by direct precipitation, from shallow aquifers and by surface runoff. The Meroni, Mbaruk and Kariandusi streams (which flow from the Bahati Escarpment) reach the lake, but only after most of their discharge has been lost to shallow aquifers.

#### 2.1.2 Naivasha Area

The Naivasha catchment is separated from the Nakuru - Elmenteita catchment mainly by the Eburru volcanic pile which is linked to the Mau Escarpment by a ridge at an altitude of around 2600 m. Between Eburru and the Bahati Escarpment the surface drainage divide runs via Gilgil along a culmination of the Rift floor at an altitude of approximately 2000 m.

South-west of the drainage divide the Gilgil and Malewa Rivers, both of which are perennial, provide much of the recharge to Lake Naivasha. The Gilgil River has its headwaters high in the Bahati Forest and drains parts of the eastern slopes of the Bahati Escarpment. These slopes also provide some of the tributaries of the much larger Malewa River. Most of the discharge of the Malewa River however, at least in its upper reaches, derives from the western slopes of the high Nyandarua Range from tributaries which initially flow north-west, and then turn south-west as they drain the Ol Bolossat Plain (a shallow asymmetrical graben lying to the east of the Bahati Escarpment). Further downstream the Malewa is joined by the Turasha River which is also perennial and drains the north Kinangop Plateau via deeply-incised tributaries.

On the west side of the Naivasha catchment the main river draining the Mau Escarpment is the Marmonet, which flows towards the lake but fails to reach it, instead recharging the alluvium of the Ndabibi Plain. Similarly none of the numerous seasonal streams which incise the Eburru Ridge reaches Lake Naivasha.

To the south of Lake Naivasha the surface water divide runs from the Mau Escarpment in the west, via Olkaria and Longonot to the Kinangop Plateau and finally to the Nyandarua Mountains. Surface drainage in this region (at least at the lower altitudes) is limited, only the River Karati providing perennial flow in its upper reaches.

### 2.2 Longonot - Magadi

The southern part of the Rift Valley is bounded in the west by the Nguruman and Mau escarpments. In the south-east a series of scarps eastwards from the Nkama Plain mark the boundary of the Rift, which is more clearly defined by the Kikuyu Escarpment at the latitude of Mt. Suswa. The Nguruman Escarpment descends from a height of 1950 m via the Kirikiti Platform at 1350 m to the Rift Valley floor at 900 m in the extreme west, from where the valley floor descends by a series of ridge and trough faulted escarpments to 590 m at Lake Magadi in the centre of the Rift. The Mau Escarpment reaches a height of 2375 m to the north-west of Suswa, and the Kikuyu Escarpment 2400 m to the east.

The Rift Valley floor is divided into many sub-parallel ridges and troughs trending approximately NNE, a physiographic expression of the recent grid faulting. The valley floor slopes southwards with a gradient of approximately 1:100 from Lake Naivasha to Lake Magadi and the surfaces of the fault blocks dip similarly gently southwards. At the latitude of Lake Magadi there are six main troughs: the Ewaso Ngiro Plain, the Embaash (Koordiya) plain, the Magadi central trough, the Olkeri Plain, the Koora Plain, and the Nkama (Kuenia) Plain.

The only perennial river in the Rift in this sector is the Ewaso Ngiro River, which has built out an extensive alluvial fan several kilometres onto the Ewaso Ngiro Plain. The river rises in the Ol Pusimoru Forest to the west of the Mau Escarpment and its tributaries drain the south-western slopes of the escarpment, from around the latitude of lake Naivasha southwards. The river initially flows south-east, then turns south, passing to the west of Lake Magadi and to the east of the Nguruman Escarpment, where it is joined by tributary streams draining the escarpment. The Ewaso Ngiro River finally discharges into the Engare Ngiro swamp at the north end of Lake Natron, to the south of the present project area.

All the troughs are bounded by fault escarpments and are generally alluvium-filled discrete basins of internal surface drainage. The Magadi trough at its southern, deepest, end is filled by the alkaline Lakes Magadi and Little Magadi. The Toroka River drains the Kajiado Escarpment in the east into the Nkama depression, and Olkeju Ngiro drains the Koora trough via Oltepesi and the northern slopes of Olorgasailie. Further north the Ewaso Kedong drains from the Kikuyu Escarpment to the east of Suswa volcano.

There is no surface drainage to, nor any outlet from, Lake Magadi. A number of springs and seepages which feed the lake occur around its margin, some of which have a significantly elevated temperature (maximum 86°C at the northern extremity of Little Magadi). As a result of extreme evaporation Lake Magadi has developed some of the most concentrated brines to be found in the alkaline saline lakes of the Rift Valley, and a layer of Trona (crystalline carbonates of sodium) covers the surface.

A number of isolated volcanic centres are located in this area of the Rift, notably Ol Doinyo Nyoke (1169 m), Olorgasailie (1760 m), Ol Esayeti (1950 m) and Suswa (2356 m). Of these the youngest and least eroded are Ol Doinyo Nyoke in the south and Suswa in the north.

# 2.3 Rainfall

Rainfall in the study area is concentrated into the two rainy seasons of October-November and March-May. Within the Rift mean annual rainfall is low, ranging from 430 mm at Magadi through 627 mm at Naivasha to 981 mm at Nakuru, with most of the region experiencing an average of about 750 mm (Met. Dept. data 1931-1980). The average maximum daily temperature at Magadi is 35°C (minimum 23°C), while at Naivasha, near the culmination of the Rift, it is 25°C (minimum 9°C).

Relative humidity is low throughout the Rift (less than 75% at Naivasha, less than 60% at Magadi) and potential evaporation (1600 to 1800 mm) greatly exceeds annual rainfall. Monthly averaged potential evaporation at Naivasha exceeds rainfall by a factor of 2 to 8 for every month except April when potential evaporation still exceeds rainfall except in the wettest of years. The same figures are not recorded for Magadi where the excess of evaporation over rainfall must be considerably greater. However individual storms in the two rainy seasons can be extremely heavy and in areas of permeable material some recharge is probable.

On the Rift escarpments rainfall values are much higher ranging up to around 1250 to 1500 mm annually (McCann 1974). Also evapotranspiration rates at these altitudes are lower at about 1400 mm per year, and much less during the rainy seasons.

#### 2.4 Geothermal Manifestations

Geothermal manifestations in the area between Lake Nakuru and Lake Magadi consist of hot and altered ground, fumaroles and hot springs. The most active thermal areas are mainly those associated with the volcanic centres at Eburru, Olkaria, Longonot and Suswa. In these areas fumaroles - often lying on fault lines - are common, although thermal springs are rare. This is in part because the volcanic centres occupy high ground and are therefore in hydrological recharge areas. Hot springs associated with these areas are found (though infrequently) in topographically lower regions such as to the north of Eburru and in Njorowa Gorge to the south-east of Olkaria. The

natural heat discharge from Olkaria has been estimated as 376~MW, and from Eburru as 130~MW (Glover, 1972).

The only important thermal area which is not associated with a volcanic centre (and where there are no fumaroles) is at Lake Magadi. Here the hot and warm springs surrounding the Lake discharge an estimated 250 MW (Crane, 1981). Elsewhere thermal springs are infrequent and usually occur near the Rift margins. These springs are often associated with faulting and do not reach elevated temperatures.

#### 3 GEOLOGY

In the study area the Rift Valley is mainly composed of a succession of late Tertiary and Quaternary volcanics with, in some areas, intervening lacustrine beds and alluvium principally of reworked volcanic debris. Pre-Cambrian Basement rocks are postulated to underlie this volcano-sedimentary succession at or below sea-level. The topography of the basement is uncertain and is the subject of continuing geophysical research.

The Rift is defined by the major Pliocene boundary faults of the Nguruman and Mau Escarpments in the west, and the Kikuyu, Nyandarua and Bahati Escarpments in the east. In the south-east the boundary of the Rift is less well defined, there being a succession of smaller escarpment faults with intermediate faults between them. The main fault scarps range from 300 to 1600 m in height, are en echelon in plan, and form a complex graben 60 to 70 km wide, reducing to 17 to 35 km by fault offsets and steps. The volcanic succession on the flanks of the Rift Valley is over 2000 m thick in places, and the succession in the Rift floor is considered to be significantly thicker than this, perhaps reaching 3000 to 4000 m (Baker, Mohr and Williams, 1972).

A dense system of Middle and Upper Pleistocene grid faulting within the Rift dissects the graben floor and step-fault platforms. These faults are sub-parallel to the main Rift faults, reach densities of two or three per kilometre and normally have throws of less than 150 m (Baker, Mohr and Williams, 1972). The Rift floor faults are locally obscured by late Quaternary volcanic piles, such as Longonot and Suswa, and by lower and middle Pleistocene sediments around Magadi and between Naivasha and Nakuru.

The oldest rocks found in the study area are Archean Basement gneisses which outcrop near to the summit of the Nguruman Escarpment in the south-west (Baker, 1958). These are overlain by Pliocene basalts, which also occur beneath a cover of younger volcanics along parts of the rift floor. Several volcanoes of Pliocene age appeared along the sides and floor of the developing Rift and examples in the project area are; the Nyandarua (Aberdare) Range, composed of basalts, phonolites, trachytes and mugearites, and the Olorgesailie, Ol Esayeti and Ol Esakut volcanoes to the south-west of Nairobi which are composed of basalts, trachytes, phonolites and nephelinites. The Ngong volcano, also to to south-west of Nairobi contains melanephelinites, basanites and phonolites (Baker, Williams, Miller and Fitch, 1971).

Plio-Pleistocene trachyte lavas and ignimbrites occupy nearly all the floor of the central and southern Rift in Kenya and occur in places on the marginal plateaux. The lower part of the group consists of trachytic tuffs with prominent ignimbrite units which are best exposed on the Bahati and Kinangop Escarpments on the eastern side of the Rift (Thompson and Dodson, 1963). Further east ash flows of this age are found on the flanks of the Nyandarua Range and elsewhere.

West of the Rift Plio-Pleistocene ignimbrites form most of the Mau Range and extend northward (Baker, Williams, Miller and Fitch, 1971). On the Rift floor trachyte and some basalt occur within the ignimbrite succession.

In the Magadi area the extensive plateau trachytes represent the upper part of the group (Baker, 1958), and these extend onto the eastern side of the Rift to form the Limuru trachytes west of Nairobi. On the Kikuyu Escarpment and in the Kijabe area trachytic flows and pyroclastics are interbedded (Thompson, 1964).

A late Quaternary phase of mainly trachyte caldera eruptions occurred along the floor of the Rift Valley and is represented in the study area by the large central volcanoes of Suswa and Longonot, which date from the middle Pleistocene and comprise phonolite, alkaline trachyte and rhyolite lavas and extensive pyroclastics. Also included in this phase of activity are the basaltic cinder cones, rubbly lavas and tuff rings of the Elmenteita region, the Eburru volcanic pile (heavily mantled with pyroclastics but with phonolite and trachyte reported [Thompson and Dodson, 1963]) and the highly comenditic lavas of the Olkaria area.

Sedimentary deposits are mainly found in the central southern and northern parts of the project area. In the south a thin layer of lake beds (the Oloronga beds), mainly reworked volcanic debris with thicknesses of up to 15 m, overlie the plateau trachytes and preceded the extensive grid faulting which determines the present day topography. Succeeding Middle Pleistocene sediments include the Olorgasailie lake beds of diatomaceous clays and the fine silts and clays of the Ewaso Ngiro basin, sediments of the Kedong Valley (predominantly clays and fine sandstones with poorly sorted conglomerate), and the silicified clays of the earliest Magadi lake. Subsequent minor faulting disturbed these sediments and was followed in the Magadi area by extensive lacustrine deposition (the High Magadi beds) to a level 12 m above the present lake surface, and by further sedimentation in the Ewaso Ngiro basin (Baker, 1958). At Magadi deposition of the Evaporite Series is thought to mark the onset of alkaline spring activity, which continues to the present day.

In the northern part of the project area Lower Middle Pleistocene sediments (mainly subaqueously deposited pyroclastics) have been found in the Kinangop scarp and in the Njorowa Gorge (Thompson and Dodson, 1963). There are also diatomaceous sediments of Upper Middle Pleistocene age east of Lake Elmenteita. However the most widespread sediments were deposited during the Gamblian Pluvial period towards the end of the Pleistocene and cover much of the Rift floor between Lake Naivasha and the northern boundary of the project area.

During this period relatively stable conditions existed in the area and extensive lacustrine deposits were laid down and subsequently partly eroded. Three lake levels have been recorded and it was only during the first maximum of the Gamblian Pluvial that the lake occupying the Naivasha basin joined that occupying the Nakuru basin , when the respective lake levels were 122 m and 220 m higher than at present. The Gamblian lake deposits are composed of volcanic ash, silts, clays and a few bands of diatomite. They are tectonically relatively undisturbed and have a maximum recorded thickness of 33 m (Thompson and Dodson, 1963).

#### 4 HYDROGEOLOGY

### 4.1 Introduction

### 4.1.1 Scope of the Study

In general the permeability of rocks in the Rift Valley is low, although there is considerable local variation. Aquifers are normally found in fractured volcanics, or along the weathered contacts between different lithological units. These aquifers are often confined or semi-confined and storage coefficients are likely to be low. In addition aquifers with relatively high permeabilities are found in sediments covering parts of the Rift floor (particularly around Lake Naivasha). Such aquifers are often unconfined and will have relatively high specific yields. Tectonic movements of the Rift Valley have important effects on aquifer properties, both on a small scale by creating the local fracture systems which comprise many aquifers, and on the large scale by forming regional hydraulic barriers or shatter zones of enhanced permeability.

Knowledge of the hydrogeology of the Rift Valley varies considerably over the project area (between Lake Nakuru and Lake Magadi) and depends primarily on the distribution of water supply boreholes. Around Lake Naivasha for example over 100 boreholes have been drilled since the 1930's, whereas less than 20 boreholes have been drilled in the Rift floor between Longonot volcano and Lake Magadi - a distance of nearly 100 km.

Another limitation is that boreholes can strictly only provide information concerning groundwater conditions within the drilled depth of the borehole, and in the case of the Rift Valley boreholes this usually implies depths of less than 250 m (an important exception is the Olkaria geothermal field where borehole depths exceed 1 km). This means that to a large extent the hydrogeology of the Rift Valley at depths relevant to the recharge of geothermal fields (several kilometres) has to be inferred from information such as piezometric and chemical data. In particular the degree of connection between aquifers intercepted by boreholes on the Rift sides, and those at depth beneath the Rift is poorly known

In this study borehole data have been used in two main ways. Firstly they have been used to construct a piezometric map of the Rift Valley - vital in attempting to examine regional flow systems. Secondly an attempt has been made to identify variations in aquifer properties with rock type, and with depth. After examining the effects of structure, a semi-quantitative assessment of the regional flows which may contribute to the deep geothermal systems has been made.

#### 4.1.2 Previous Work

General accounts of the hydrogeology of the project area are given in the reports of the Geological Survey of Kenya. Particularly relevant reports are; No. 78 covering the area from Gilgil to beyond the northern boundary of the area (McCall, 1967), No. 55 covering the Longonot-Gilgil area (Thompson and Dodson, 1963), No. 43 covering the Kijabe and Kinangop areas (Thompson, 1964), and No. 42 covering the Magadi area (Baker, 1958). In addition Ministry of Works Technical Report No. 3 discusses groundwater conditions in the Nakuru area (McCall, 1957).

Hydrogeological reports with specific reference to geothermal energy studies in the Rift Valley in areas north of Longonot were prepared as part of a

previous UN study (McCann, 1972 and 1974), and similar investigations have recently been completed to the north of the present project area (Geotermica Italiana, 1987). Several papers and reports have been published which are relevant to the hydrogeology of the Rift Valley in the project area, and these are mentioned in the appropriate sections of this report.

## 4.2 Data Collection and Data Base Construction

The geological and topographic variations of the Rift Valley both have important consequences for water occurrence and movement. Water flows in the direction of decreasing head, and in general this implies flow down a topographic gradient. Therefore given the overall surface geometry of the Rift in the project area as a wide trough, sloping axially to the north and south away from a culmination at Naivasha, groundwater may be expected to flow from the sides of the Rift towards the centre and axially towards the north and south, away from Naivasha. However the geological complexity of the area, both in terms of lithology and structure, influences this simple intuitive picture substantially, and in order to attempt any quantitative assessments about groundwater location and flow, data concerning head gradients, permeabilities, porosities and flow boundaries must be obtained.

In the Rift such data can only be obtained from boreholes (and from infrequent springs) and must be collected over the area which influences the groundwater systems. In practice this means examining an area bounded by the groundwater divides of the Nguruman and Mau Escarpments to the west, and the Nyandarua, Kikuyu and minor escarpments to the east.

The resulting survey of borehole data covers 32 sheets of the 1:50,000 scale topographic map series, and extends from Lake Nakuru in the north to Lake Magadi in the south, and from Njoro in the west to the outskirts of Nairobi in the east.

All borehole data were obtained from the Ministry of water development (MWD) in Nairobi. At MWD borehole positions and numbers are marked on 1:50,000 scale maps. Details of lithology, well construction, water strikes and levels, and pumping test data are held on file.

Data for 596 boreholes were abstracted from MWD records. The density of borehole data varies considerably; most boreholes are in the north and east of the project area, with very few in the south and west. Data for most boreholes in the Nakuru-Magadi region of the Rift were abstracted; the exceptions were generally where borehole density was high, when a representative sample was taken.

Data were initially copied from the files and were subsequently entered into a computer data base at Wallingford, listings of which are given in Appendices 1 to 5.

Appendix 1 shows basic borehole data. The boreholes are listed in order of borehole number (for the majority of boreholes which have a "C" prefix this is also, in general, a chronological listing). The grid reference and borehole altitude were obtained by reference to the borehole position marked on the relevant 1:50,000 scale map held at MWD (this information is not normally given in the MWD files). Where the borehole was dry the rest water altitude is shown as a maximum value.

Appendix 2 lists borehole completion data such as depth, diameter and the depth to which plain casing extends below ground level. Aquifer lithology, where known, is taken from the driller's log.

Appendix 3 gives water strikes and water levels. Normally one water strike and a final rest water level were recorded, but multiple strikes and levels are not uncommon.

Appendix 4 shows borehole productivity data. Most boreholes which struck water were pumped and a borehole yield noted. Often (particularly recently) data concerning discharge rate and drawdown are recorded in the MWD files, enabling specific capacity to be calculated, and values are given in the Appendix. Also included are notes concerning features of borehole productivity such as high temperature, production of steam, or whether the borehole was dry.

Appendix 5 is included as an aid to locating particular boreholes. Boreholes are listed in order of increasing values of Grid Easting, and for a particular value of Easting are arranged in order of increasing values of Northing.

# 4.3 Water Level Data and the Piezometric Map

## 4.3.1 Data Reliability and Map Construction

A problem with collecting hydrogeological data in the Rift Valley is that so few wells have access for water level measurements, either because a piston pump is installed or because the borehole is blocked. Therefore water levels are taken from borehole records. These data refer to the levels at the time of well completion, which is a period spanning over 50 years for boreholes in the project area. This introduces errors in defining piezometric contours, because of the seasonal and longer term variations in groundwater levels.

The scale of such errors may be found by comparing borehole water levels at the time of completion with levels measured recently. Table 4.1 shows this for boreholes of various ages in the project area. The recent values were measured as part of a thermal gradient survey carried out by G. Batticci as part of the recent UN Geothermal Project (G. Batticci, pers. comm.).

Table 4.1 indicates differences in water level between original and recently-measured levels ranging from zero to 107 and 124 m. However the higher figures are unreliable, the first (borehole C2388) because the 1955 level does not take into account a perched water level (given in brackets), and the second (borehole C1726) because both the original and recent water levels are uncertain. The remaining twelve values range between zero and 39 m with all but one value below 20 m. While these differences are not insignificant, such temporal variations are small when compared with the large spatial variation in surface topography and water table geometry encountered in the Rift, and can therefore be ignored when groundwater movement on the scale of the Rift is considered. They cannot however be ignored if local small-scale effects are examined.

Other errors are introduced into piezometric map construction by using borehole rest water levels which may represent a local averaging of several piezometric surfaces where different aquifers are intersected by a borehole. Again the importance of such errors depends on the scale considered.

The scale chosen for the piezometric map of the project area (Figure 4.1) was

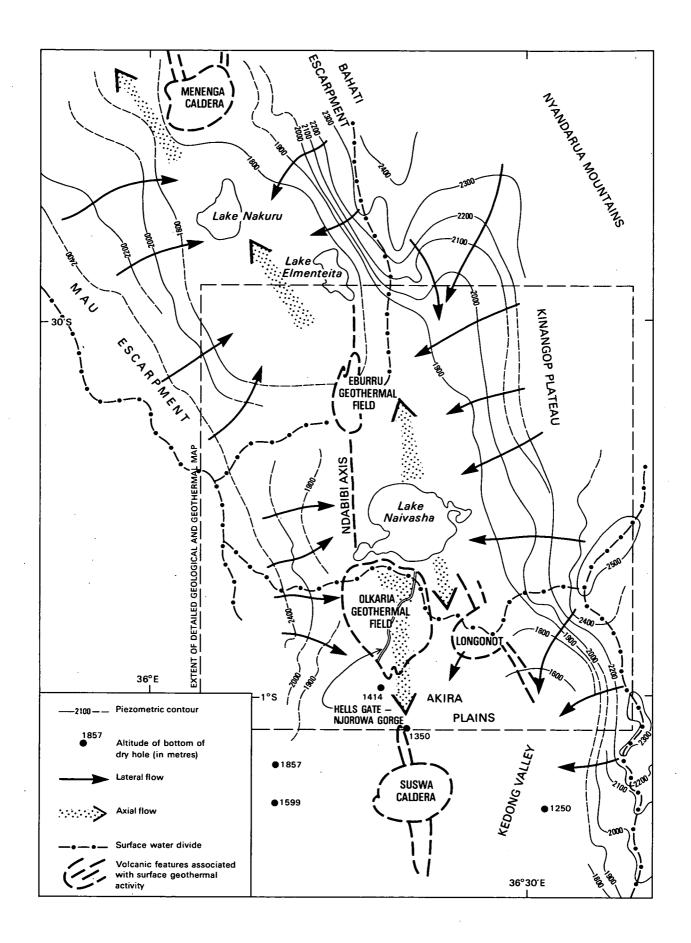


Figure 4.1 Piezometric Map of the Project Area.

Table 4.1 Borehole water level comparisons.

|             | ORIGINAL W                     | ATER LEVEL                             | RECENT W          | ATER LEVEL*                            |  |
|-------------|--------------------------------|--|-------------------|--|--|
| Well<br>No. | Borehole<br>completion<br>date | Borehole<br>rest water<br>level<br>(m) | Date <sub>.</sub> | Borehole<br>rest water<br>level<br>(m) | Water level<br>change<br>(recent-original) |
| C1391       | 31/3/51                        | 111.0                                  | 29/1/86           | 95                                     | - 15.0                                     |
| C1726       | 31/3/51                        | ?259.2                                 | 26/9/85           | ?135                                   | ?-124.2                                    |
| C2109       | 16/12/53                       | 42.0                                   | 11/9/85           | 43.9                                   | 1.9  |
| C2358       | 25/3/55                        | 265.0                                  | 12/10/85          | 225.6                                  | - 39.4                                     |
| C2388       | 4/6/55                         | ?241.7                                 | 10/9/85           | 134.5                                  | ?-107.2                                    |
| C2813       | 14/4/58                        | 41.5                                   | 13/9/85           | 24.4                                   | - 17.1                                     |
| C3397       | 23/8/66                        | 108.0                                  | 1/2/86            | 107.7                                  | - 0.3                                      |
| C3677       | 25/2/68                        | 15.2                                   | 13/2/86           | 19.7                                   | 4.5  |
| C4143       | -/-/76                         | 172.0                                  | 25/3/86           | 173.0                                  | 1.0  |
| C6271       | -/-/84                         | 34.6                                   | 1/2/86            | 34.6                                   | 0  |
| C6056       | 29/1/85                        | 13.8                                   | 31/1/86           | 14                                     | 0.2  |
| C6290       |                                | 197                                    | 20/9/85           | 197                                    | 0 .  |
| C6300       | 9/3/83                         | 132.9                                  | 25/9/85           | 133.4                                  | 0.5  |
| M001        | -/-/85?                        | 155                                    | 14/2/86           | 155                                    | 0  |

 $<sup>\</sup>star$  Recent water levels measured by G Battici, UN Geothermal Project.

1:250,000 with a contour interval of 100 m (with variations depending on the data quality). At this scale the regional flow systems which may contribute to geothermal recharge can be well represented, while the effects of errors such as those discussed above can be minimised. Piezometric contours have been drawn using the borehole water level data, and spring data obtained from the 1:50,000 and 1:250,000 topographic map series. Where such data are scarce local topographic variations have been used as a guide to contour geometry. Surface water divides have been drawn with reference to the topographic maps.

# 4.3.2 Analysis of the Piezometric Map

In general the map shows the features expected of a valley/interfluve system, with groundwater flowing from elevated recharge areas to low-lying discharge areas, the flow occurring both laterally and longitudinally according to the Rift geometry. In the following discussion the different sub-catchments are considered separately.

#### Nakuru-Elmenteita

Lakes Nakuru and Elmenteita lie a little to the north-west of the culmination of the Rift floor (between Naivasha and Gilgil). Groundwater gradients and therefore flows in this area are generally directed towards the lakes, with some flow away from the area to the north-west. In more detail, groundwater flows north-east from the Mau Escarpment, south-west from the Bahati Escarpment and northwards from Eburru. It is also probable that there is some southerly flow from Menengai towards Lake Nakuru. However at depth it is likely that flow occurs to the north-west away from the Nakuru-Elmenteita catchment towards the lower-lying area around Lake Bogoria.

#### Naivasha

This is the most important catchment in the project area in terms of present and near-future geothermal development. It is also the most complex hydrogeologically, because while it is lower than the Rift escarpments it is at a culmination of the Rift floor.

Flows towards Lake Naivasha from the Mau Escarpment and the Kinangop Plateau are unambiguous and some of the groundwater from the western side of the Rift must eventually form part of the discharges at Olkaria and Eburru. However the longitudinal flows in this area are more difficult to assess.

To the north of Naivasha the surface water divide runs approximately east-west through Eburru, and then north through Gilgil. However there is no evidence that a groundwater divide follows this route, because the piezometric surface has an uninterrupted fall from Lake Naivasha, around the east side of Eburru, towards Lake Elmenteita, indicating flow in this direction.

The configuration of groundwater contours around Eburru is uncertain because boreholes drilled at Eburru have encountered steam. It is probable that while shallow groundwaters on the south side of Eburru move locally towards Naivasha, deeper flows are substantially northwards.

Around Lake Naivasha itself the groundwater level is between approximately 1880 and 1890 m, i.e. roughly that of the lake itself. East and west of the lake the groundwater contours rise, indicating flow towards the lake, while to the south they remain at about the same level as far as the latitude of

the Longonot/Olkaria complex.

South of this region the piezometric surface drops by several hundreds of metres. Indeed its position is unknown because the few boreholes drilled between Longonot and Suswa have all proved to be dry, or have produced steam. The data do indicate a fall of at least 450 m in piezometric level over a distance of around 10 km (i.e. a gradient of at least 0.05 m/m). At depth a north-south pressure gradient of 11 bars/km has been reported in the Olkaria geothermal field (Bodvarsson and others, 1987) which corresponds to a freshwater head gradient of 0.1 m/m.

Groundwater certainly flows away from Lake Naivasha because the lake water is fresh, even though the lake has no outlet and lies in an area of high evaporation. The position of the lake, at a culmination of the Rift floor, suggests flow both to the north and to the south (i.e. a groundwater divide runs east-west in the vicinity of the lake). As discussed above, northerly flow may occur both via Gilgil and under Eburru (but see Section 5.3). Southerly flow must also occur, following the hydraulic gradient, but the high values of the gradient suggest that values of permeability in the Olkaria-Longonot region are low. Values for subsurface discharge in the Naivasha area are discussed in Section 4.6.

#### Longonot-Magadi

A surface water divide runs east-west through Olkaria and Longonot but appears to have little effect on the southerly flow of groundwater from Naivasha. Between Longonot and Lake Magadi groundwater flows from the sides of the Rift towards the centre, and southwards along the Rift towards Magadi. The unknown, but very deep position of the piezometric surface in the Suswa area suggests that flow from the sides of the Rift in this area is limited, and it is very likely that the major Rift faults act as low permeability barriers to flow across the Rift. For example borehole C4971 in the Rift to the east of Suswa encountered no water at a depth of 300 m, corresponding to a maximum water level altitude of 1250 m, whereas less than 10 km to the east, on the side of the Rift, the piezometric surface is between 100 m and 200 m below the surface, at an altitude of 1900-2000 m.

Between Suswa and Lake Magadi water level data are very sparse, but the limited evidence indicates the expected flow down the topographic gradient, i.e. southwards from Suswa, south-east from Narok, south-west from the Ngong area and east from the Nguruman Escarpment, with all flows eventually coinciding in the topographic low around Lake Magadi. From hydraulic evidence there is no way of distinguishing which of these flows contributes the most to the thermal springs at Lake Magadi, but the nearby Nguruman Escarpment would seem to be a likely source because of the substantial hydraulic head gradient which it could provide.

# 4.4 Aquifer Properties

# 4.4.1 Specific Capacity, Transmissivity and Hydraulic Conductivity

Very little information is available concerning the variation in aquifer properties between the various rock types of the Rift Valley. The main reason for this is that the standard hydrogeological field test to determine aquifer transmissivity - a carefully monitored pumping test with observation wells - has not been undertaken when water wells have been drilled. (The Olkaria wells form a special case and will be considered later). In general, after water wells have been drilled they have been test-pumped for a few hours in

order to obtain a well yield. In some cases recovery data have been recorded, but for the majority of wells only a yield, or a yield and a pumped water level at equilibrium have been noted. (While theoretically equilibrium conditions are never attained in confined conditions, in practical terms drawdowns often increase at very low rates after a short period of pumping). Where yield and equilibrium drawdown data are available then specific capacities (yield/drawdown) can be calculated, and these are given in Appendix 4. Where drawdowns were too small to be registered a nominal maximum value of 0.2 m has been used (it is assumed that drawdowns greater than this would have been noticed). The calculated values of specific capacities in these cases are therefore probably minima.

The specific capacity of a well depends primarily on the transmissivity of the aquifer. Other factors which influence specific capacity are well losses and partial penetration, but in general, variations in specific capacity are paralleled by variations in transmissivity. In certain circumstances, namely if the pumped well has no well losses and fully penetrates an extensive confined aquifer which is homogeneous and isotropic then transmissivity can be derived from specific capacity by using the Thiem equation (Thiem, 1906) with the extra assumption that the radius of influence of the well is 300 m. (This value need not be exact because it appears as a logarithm in the equation).

Thus

$$T = \frac{43.20}{\pi s} \ln[300/r_{w}] \tag{1}$$

Where

 $T = Transmissivity (m^2/d)$ 

Q = Discharge rate (1/s)

s = Drawdown at equilibrium (m)

 $r_w = Well radius (m)$ 

Equation 1 has been applied to all cases where the specific capacity and the well radius are known. In a few cases the well radius is unknown and for these the Logan approximation has been used (Logan, 1964).

$$T = 105.4Q/s$$
 (2)

where all symbols have the same meaning as before

Naturally the strict validity of equation 1 is questionable for many if not most of the boreholes for which specific capacity data are available (and this is true to an even greater extent for equation 2). While most of the boreholes are at least partially confined (water strikes and rest water levels often differ greatly), factors such as partial penetration and anisotropy are likely to be common. Some idea of the validity of the equation may be obtained by comparing the predicted variation of transmissivity with specific capacity with values derived from carefully monitored (albeit single well) pumping tests. Figure 4.2, using data from McCann (1974) indicates that the correlation is, in general, good.

Transmissivity values may be converted to values of hydraulic conductivity if the thickness of the producing interval is known. An estimate of this thickness may be obtained by assuming that it corresponds to the distance between the main water strike and the bottom of the borehole. This estimate

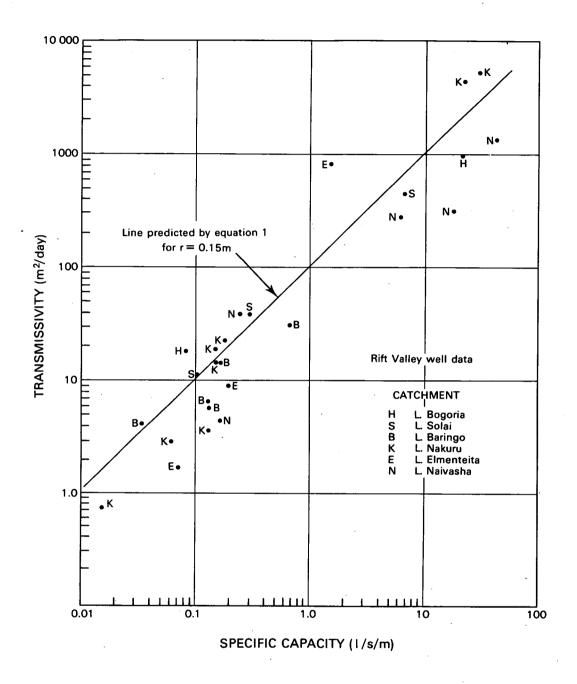


Figure 4.2 Variation of Transmissivity with Specific Capacity.

of aquifer thickness will tend to be an over-estimate, because it takes no account of the non-producing intervals within the aquifer, and therefore it will tend to lead to an under-estimate of hydraulic conductivity.

Values of estimated transmissivity and hydraulic conductivity are given in Appendix 6. It must be stressed that these values - particularly the hydraulic conductivities - should be regarded as semi-quantitative only, because of the assumptions on which they are based. They are useful because they enable the hydraulic properties of one area to be compared to another, providing an insight into the relative merits of different rock types as aquifers.

4.4.2 Variations in Aquifer Properties over the Rift

#### Introduction

Borehole data taken from areas of the Rift which can be represented by particular rock types have been examined using the search facility of the data base and the results are detailed below.

The Rift Floor in the Naivasha-Nakuru Area

The sediments of the Naivasha-Nakuru region are penetrated by numerous wells which provide water to the various towns and settlements in the region. The relatively large amount of data available therefore enables the hydrogeological properties of the Lake deposits to be examined in a series of small areas.

### Lake Naivasha Area

Details of 100 boreholes around Lake Naivasha have been used in the data base. These penetrate Gamblian sediments and underlying Middle Pleistocene volcanics and sediments. Boreholes within an area bounded by Eastings 1900 and 2150 and between Northings 99050 and 99300 are considered, and this area is further subdivided into four quadrants termed NW Naivasha, NE Naivasha, SW Naivasha, and SE Naivasha by Easting 2050 and Northing 99150.

#### N.W Naivasha

This area extends from the west bank of the Gilgil River around the lower slopes of Eburru to the Ndabibi Plain and the western shore of Lake Naivasha to a point approximately 1 km north of Crater Lake. Details of 26 boreholes are held on the data base, of which the majority lie within 5 km of the lake shore. Borehole depths range between 10 m (C2356) and 213 m (C4499) and drilling logs indicate that aquifers are composed predominantly of fractured lavas and pyroclastics.

The average values of yield, specific capacity, estimated transmissivity and estimated permeability for this area are given in Table 4.2. While there is no universally accepted method of averaging permeability data many workers prefer the geometric mean where aquifer permeability varies laterally (Warren and Price, 1961; Bennion and Griffiths, 1966) and this mean has therefore been used for specific capacity, estimated transmissivity and estimated permeability data, with the arithmetic average shown in brackets. In the following discussion "mean" refers to the geometric mean and "average" refers to the arithmetic mean.

The data show this region to have good aquifer properties. Only one well in

Average aquifer characteristics of selected areas and lithologies from borehole data. (Figures in brackets are arithmetic means) Table 4.2

| Total<br>No.<br>boreholes   | 35                    | 22          | 17          | 56          | 12                  | 31                | 25                | 32               | Ξ            | 48                         | 23             | 43                       |
|---|-----------------------|-------------|-------------|-------------|---------------------|-------------------|-------------------|------------------|--------------|----------------------------|----------------|--------------------------|
| No.<br>dry<br>boreholes   | 0                     | 0           | 0           | 0           | _                   | 2                 | _                 | വ                | က            | 4                          | 2              | 4                        |
| Geometric<br>mean<br>estimated<br>permeability<br>m/d                 | 12(33)                | 20(114)     | (961)       | 148(818)    | 1.4(3.9)            | 2(7)              | 1.2(3.7)          | 0.8(5)           | 0.1(0.2)     | 1.1(35)                    | 1(10)          | 1.1(22)                  |
| Geometric<br>mean<br>estimated<br>transmissivity<br>m <sup>2</sup> /d | 307(1170)             | 502(3082)   | 297 (940)   | 1601 (5308) | 78(143)             | 32(261)           | 14(47)            | 14(106)          | 4(5)         | 20(325)                    | 22(174)        | 20(119)                  |
| Geometric<br>mean<br>specific<br>capacity<br>1/s/m                    | 2.8(11.6)             | 4.6(29.2)   | 2.7(8.7)    | 14.9(52.6)  | 0.7(1.3)            | 0.3(2.4)          | 0.1(0.4)          | 0.2(0.9)         | 0.03(0.04)   | 0.2(2.6)                   | 0.2(1.6)       | 0.2(1.1)                 |
| Arithmetic<br>mean<br>borehole<br>yield<br>1/s                        | 9.3                   | 4.4         | 5.4         | 6.4         | 2.6                 | 1.9               | 3.4               | 1.8              | 1.9          | 2.1                        | 1.3            | 1.7                      |
| Lithology   | Sediments + volcanics | =           | =           | =           | =                   | =                 | Tuffs             | =                | Pyroclastics | Trachyte                   | Pyroclastics   | =                        |
| Area  | NE Naivasha           | SE Naivasha | SW Naivasha | NW Naivasha | Naivasha-Elmenteita | Elmenteita-Nakuru | Bahati Escarpment | Kinangop Plateau | S Kinangop   | E Suswa Rift<br>Escarpment | Mau Escarpment | Mau Forest<br>(W Nakuru) |

the area was found to be dry - C4499, which is not included in the averaging procedure - and the average yield is 6 1/s. The mean specific capacity of 14.9 1/s/m is the highest of any region examined in the study area and this is reflected in the high values for estimated transmissivity and hydraulic conductivity.

#### N.E Naivasha

This area stretches from the right bank of the Gilgil River around the north-eastern shore of Lake Naivasha to Crescent Island, and includes Naivasha Township, where most of the boreholes are situated. Thirty-five borehole records in the area were examined, ranging in depth from 26 m (C2117) to 128 m (C4155). Drillers'logs commonly show the aquifer as consisting of 'sand and gravel' (reworked volcanics) or 'lake sediments' with a few references to pyroclastics. None of the boreholes are dry and productivities are generally good with yields averaging 9 l/s and specific capacities averaging 3 l/s/m (Table 4.2). The estimated mean transmissivities and hydraulic conductivities are less than in the N.W Naivasha area, but are nevertheless high when compared with other areas of the Rift. The permeability estimate for this area of 12 m/d is of the order which would be expected for clean sands (Freeze and Cherry, 1979).

#### S.E Naivasha and S.W Naivasha

The S.E Naivasha area extends from Crescent Island around the S.E shore of Lake Naivasha between the lake shore and the lower slopes of Longonot to the southernmost point of the lake. The S.W Naivasha area lies to the west and includes the Kongoni settlement, part of the Ndabibi plain and Crater Lake. Details of 22 boreholes in the S.E Naivasha area and 17 boreholes in the S.W Naivasha area are included in the data base, with most of the boreholes clustered around the lake shore. Borehole depths in the S.E area range from 25 m (C4989) to 183 m (C1279), and in the S.W area from 31 m (C2636) to 152 m (C2863). In both areas boreholes penetrate lake sediments and volcanics. Average borehole yields for both areas are similar at around 5 l/s, and slightly lower than those for the N.W and N.E Naivasha areas and there are no dry wells. There is some evidence that specific yields and transmissivities are higher in the S.E area than in the S.W (Table 4.2) but the data are too few to permit further interpretation.

Boreholes around Lake Naivasha are on average the most productive in the project area - a fact noted by Thompson and Dodson (1963) who suggested that the cause was the shallow water table and the use of more efficient pumps in these boreholes. That this is not the case is shown by the high values of specific capacity (a factor independent of rest water level or pump efficiency) which are found in the Naivasha area (Table 4.2). It is likely however that the proximity of a recharge boundary in the form of the lake accounts to some extent for the high specific capacities, but only for those wells in the immediate vicinity of the lake, because production tests normally last for less than one day. In the N.W Naivasha area, for example, which is characterised by the highest values of specific capacity, many of the boreholes are close to the lake and may therefore be affected by a recharge boundary. However boreholes at some distance from the lake also have high specific capacities (e.g. boreholes C2522, C2706, C2813 and C4499 which has the highest value in the area) and it is concluded that the permeability of the Lake Naivasha area is higher than that of the rest of the Rift in the project area.

#### Naivasha-Elmenteita

Twelve boreholes have been drilled in the Rift Valley floor between Naivasha township and Elmenteita, in an area defined by Eastings 1950-2130 and Northings 99300-99470. Borehole depths vary between 61 m (C3929) and 264 m (C2388) with aquifers mainly occurring in sand and silt deposits. (One borehole near to the eastern margin of the Rift (C2076), to the north of Gilgil encountered water at 65.5°C). Table 4.2 shows that the average yield of these boreholes, at around 2.5 l/s, is approximately half of boreholes further south, and specific capacities are greatly reduced - although only four values can be determined. It is likely that the lower permeability is due to the smaller grain size of these deposits.

### Elmenteita-Nakuru

Thirty-one boreholes have been drilled in the floor of the Rift Valley between Lake Nakuru and Lake Elmenteita (in an area defined by Eastings 1700-1950 and Northings 99350-99600). Water bearing rocks in this region include surface sediments, pyroclastics and lavas. Borehole yields are similar to those of the Naivasha-Elmenteita region (c. 2 l/s) and specific capacities are also comparable, of the order of 1 l/s/m. Two dry wells were drilled in the area, corresponding to a failure rate of 7%.

# Rift Margins

### Bahati Escarpment

Data from 25 boreholes (one of which was dry) drilled in the Pliocene Tuffs forming the Bahati Escarpment, between Eastings 1854-2049 and Northings 99600-99800, shows them to be less permeable than the Rift Floor deposits. The mean specific capacity is only 0.1 l/s/m (Table 4.2) and estimated mean transmissivities and permeabilities are about half those determined for the Rift Valley floor to the west. (Borehole yields are similar to those in the Rift Valley Floor between Lakes Nakuru and Elmenteita, but the comparison is misleading because larger drawdowns are incurred on the escarpment). Limited data suggest that aquifers are often found where the tuffs are fractured and weathered.

# Kinangop Plateau and Kikuyu Escarpment

Details have been obtained of 32 boreholes drilled in the Kinangop Tuffs forming the Kinangop Plateau, in an area defined by Eastings 2175-2400 and Northings 99150-99300. Table 4.2 indicates that the aquifer properties of these tuffs are similar to those of the Bahati Tuffs to the north, with low values of specific capacity, estimated transmissivity and estimated hydraulic conductivity. Borehole yields are low and a significant proportion of boreholes (16%) proved to be dry. Most water-bearing material comprises weathered tuffs and sediments.

To the south of this area, details of 27 boreholes on the south Kinangop Plateau and the Kikuyu Escarpment (in an area defined by Eastings 2225-2400 and Northings 99040-99150) have been examined. These boreholes which mainly penetrate pyroclastics generally have poor aquifer properties, with specific capacities normally less than 0.05 l/s/m, and the estimated mean hydraulic conductivity is around 0.1 m/d. Three dry wells are recorded in this area, corresponding to 11% of the total.

#### Rift Escarpment east of Suswa

An area defined by Northings 98550-98850 and Eastings 2300-2400 (and Easting 2450 north of Northing 98650) was selected to examine boreholes drilled in the Limuru Trachyte. Records of 48 boreholes in this area are held on the data base, and these indicate the aquifer properties to be similar to those of the Kinangop tuffs and Bahati tuffs, with a mean specific capacity of  $0.2\ l/s/m$  and with a mean estimated hydraulic conductivity of around  $1\ m/d$ . Four boreholes (8%) were dry. Drillers logs indicate that the main aquifer potential lies in weathered zones and fractures.

#### Mau Escarpment

Data from 23 boreholes drilled in the Mau Pyroclastics, in an area to the west of Naivasha defined by Eastings 1500-1900 and Northings 99100-99350, have been examined. Five (22%) of the boreholes were dry when drilled and the remainder have in general low specific capacities and estimated transmissivities and hydraulic conductivities (Table 4.2). In fact the aquifer properties shown by these rocks are very similar indeed to those of the Kinangop Tuffs across the Rift Valley. This is not unexpected because both formations are of similar age and lithology (Thompson and Dodson, 1963).

#### Mau Forest slopes

To the west of Lake Nakuru the lower slopes of the Mau Escarpment comprise mainly Recent and Quaternary pyroclastics and pumice. The aquifer properties of these materials were investigated in an area bounded by Eastings 1500-1660 and Northings 99550-99700. Table 4.2 indicates that the aquifer characteristics of these formations are similar to those of the Mau pyroclastics, with aquifers mainly consisting of weathered volcanics. Four boreholes (9% of the total) were dry.

### Conclusions

The above survey is necessarily confined to areas where enough boreholes have been drilled to enable a reasonable estimate of average aquifer properties to be obtained. In practice this has meant that most of the Rift margins south of Suswa, and all the Rift floor south of Longonot cannot be examined because of poor data coverage. The best-known area is the Rift floor around Lake Naivasha, and it is here that the most productive wells are found. Borehole yields in this area are usually in excess of 3 1/s and mean specific capacities are around 3 1/s/m. The highest permeabilities in the area are to the north-west of the lake where the geometric mean specific capacity is 15 1/s/m. While to some extent these values may be attributed to recharge from the lake it is evident that the sediments and volcanics which underlie this region have a substantially higher permeability than elsewhere in the project area.

Further north permeability falls, probably as a result of a decrease in sediment size, and in the area between lakes Nakuru and Elmenteita borehole yields fall to around 2 1/s and the mean specific capacity is only 0.3 1/s/m.

On the sides of the Rift the permeability is in general lower than that of the Rift floor. There is a fair degree of regional uniformity in the aquifer properties of the various rock types, although those obtained from individual boreholes may vary greatly. In particular the pyroclastics covering the Mau Escarpment and the north Kinangop Plateau have very similar properties with borehole yields of around 1 l/s and geometric mean specific capacities of

0.2 l/s/m. The Bahati Escarpment tuffs and Limuru trachytes also appear to have similar hydraulic properties to the Mau pyroclastics. Only the pyroclastics of the south Kinangop Plateau and the Kikuyu Escarpment differ markedly, with lower specific capacities.

The estimated values of transmissivity shown in Table 4.2 mimic the variations in specific capacity from which they were calculated. Estimates of hydraulic conductivity are more variable, but support the conclusions reached from the specific capacity variations, and in addition suggest values for use in regional modelling. The geometric mean hydraulic conductivity of rocks bordering the Rift is estimated to be of the order of 1 m/d on the basis of the estimates in Table 4.2. This increases slightly for the Rift floor between Naivasha and Nakuru, and is approximately one order of magnitude greater for the sediments and volcanics around Lake Naivasha, and up to two orders of magnitude greater to the north-west of the lake (with some of the increase being apparent and caused by the proximity of the lake). The very large estimated permeability of the north-west Naivasha area suggests that grid faults may significantly contribute to flows in this area.

These values of hydraulic conductivity are only rough estimates, but they are reasonable for large volumes of fractured, partly-weathered rock (Freeze and Cherry, 1979). However they are only valid for the depth of rock penetrated by the boreholes, which is typically less than 200 m. At depth, where weathering ceases and where fissure apertures are reduced by overburden stress the hydraulic conductivity will be less, as discussed below.

# 4.4.3 Aquifer Properties of rocks at depth

The only deep boreholes drilled in the Rift are those in the Olkaria geothermal field, (the hydrogeology of which is discussed in Section 6.1). The permeability of the reservoir rocks at Olkaria is low, and recent modelling of the Eastern Olkaria borefield has produced values of intrinsic permeability of  $7.5 \times 10^{-15}$  m² for the steam zone (700-800 m approximately) and  $4 \times 10^{-15}$  m² for the underlying liquid-dominated zone (Bodvarsson and others, 1987). In the commonly-used oil industry notation these values correspond to 7.5 millidarcies (mD) and 4 mD respectively. The average value of intrinsic transmissivity of the reservoir is also low, with values ranging between 1 and  $5 \times 10^{-12}$  m³. The effective porosity of the liquid-dominated zone is estimated to be 2% on average, with spatial variations of 0.25-5%. In terms of well response the reservoir behaves as a dual porosity system, with both fracture and matrix porosity and permeability.

As a result of the poor transmissivity the flow rates from the Olkaria wells are low, with the average well producing only 6 kg/s of steam, which is the equivalent of 2.5  $MW_{\bullet}$  (Bodvarsson and others, 1987).

Translated into cold water (20°C) terms for comparison with the water borehole values these figures indicate hydraulic conductivity and transmissivity values of around  $3x10^{-3}$  m/d and 1-4 m<sup>2</sup>/d respectively.

The values are significantly lower than those obtained for most water boreholes throughout the Rift, which is expected in view of the depth of the geothermal reservoir. However it is not known how representative these values are of permeabilities elsewhere in the Rift because the geothermal reservoir is in an unusual environment where mineral alteration, dissolution or deposition can enhance or reduce rock permeability.

In the absence of other deep wells in the Rift a preliminary estimate of

permeability at depth has been made by calculating the transit times of groundwater flows for a range of permeabilities and comparing these with age data from groundwater samples obtained by radioisotope analysis.

An analytical model has been used (developed by J.Barker of B.G.S) which considers steady state flow below an irregular water table in a two-dimensional vertical section of an aquifer between vertical no-flow boundaries (interfluves or valley bottoms) and above a horizontal no-flow boundary. In addition to the geometry of the water table and the positions of the boundaries the model requires that the hydraulic conductivity (horizontal and vertical) and the porosity be known and constant throughout the section. The model calculates the heads around the boundaries and at any point within the section, and fluxes at the water table, using a 'Biem' analytical technique. In this study the model was also used to trace flow paths within the section and to calculate transit times.

The section chosen lies across the Rift north of Naivasha (Figure 4.3). The line was selected to pass through boreholes C1404 and C4178 from which <sup>14</sup>C ages have been obtained. The uncorrected <sup>14</sup>C ages of waters from these boreholes are of the order of 1000 years, but these are upper limits (Section 5.5) and the average ages are considered to be much less, possibly only of the order of 100 years.

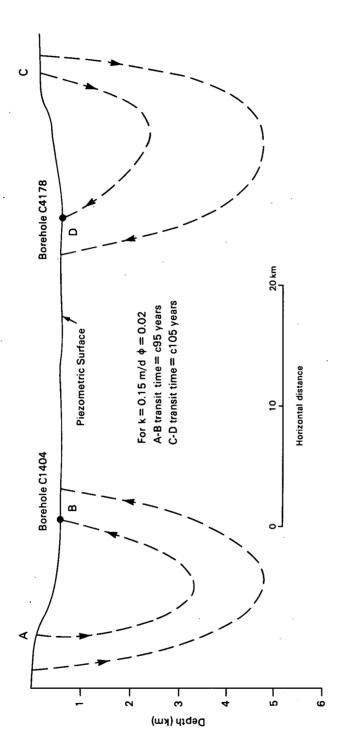
Head data from the model were obtained from the piezometric map and various combinations of hydraulic conductivity and porosity data were used. Figure 4.3 shows flow paths which are relevant to the two boreholes for an isotropic system. The model results indicate that if a porosity of 2% is chosen (similar to that found at Olkaria) then, to obtain an age of around 100 years a hydraulic conductivity of 0.15 m/d must be used, whereas for an age of 1000 years the relevant value is 0.015 m/d.

These estimated values of hydraulic conductivity values are 5-50 times larger than the value obtained for the Olkaria geothermal field, but they should be regarded as maxima. This is because the model assumes that the waters found in the boreholes originate on the sides of the Rift; whereas there are several chemical indications (discussed in Section 5) that these waters have an essentially local origin. If the well-waters indeed have a mainly local origin then the small component of Rift-wall groundwater which reaches the wells is presumably significantly older than the local waters (for it is unlikely that Rift-wall waters could move via deep flowpaths to the Rift centre so rapidly as to be younger than local groudwaters and yet arrive in undetectably small quantities). Hence the modelled hydraulic conductivities of the deep aguifers are likely to be be less than the range In conclusion, this simple model therefore suggests that the given above. average hydraulic conductivity of rocks at depth under the Rift Naivasha area is probably much less than 0.1 m/d and may in fact be of order of 0.001 m/d as at Olkaria (although this is speculative).

## 4.5 Structure

The structure of the Rift Valley and in particular the major marginal Rift faults and the system of grid faulting on the Rift floor undoubtedly have a substantial effect on the groundwater flow systems of the area.

In general faults are considered to have two effects on fluid flow. They may facilitate flow by providing channels of high permeability, or they may prove to be barriers to flow by offsetting zones of relatively high permeability. The hydraulic role of faults is a subject which is poorly understood because



Section across the Rift showing possible flow paths.

Figure 4.3

there is often little direct evidence that a particular fault behaves in a particular way. On the whole faults are more commonly thought of as hydraulic barriers in cold groundwater systems where horizontal flows predominate, whereas in geothermal systems where vertical flows are more important they are often considered to provide conduits for flow. However care is needed to avoid invoking either property without evidence.

In the Rift Valley the main direction of faulting is along the axis of the Rift, and this has a significant effect on flows across the Rift. It is apparent from the high hydraulic gradients which are developed across the Rift escarpments that the effect of the major faults is to act as zones of low permeability. This is particularly true of the Bahati Escarpment and the escarpment to the east of Suswa. Water flowing in the weathered zones (which are often old land surfaces and therefore sub-horizontal) and fractures of the pyroclastics and lavas forming these Rift escarpments is forced to flow downwards by the faults, and in the case of the escarpment east of Suswa the fault permeability is so low that the piezometric surface in the Rift Valley is considerably below the Rift floor.

The effects of Rift faulting appear to be less in the Kinangop Plateau area where the piezometric contours are more widely spaced, and limited borehole evidence from the Mau Escarpment to the west of Naivasha suggests that flows towards the lake are not greatly affected. Borehole data are very limited on the west side of the Rift south of Longonot, but dry boreholes to the west of Suswa indicate that Rift faulting may inhibit lateral flows in this area.

Flows along the Rift are likely to be strongly affected by the substantial amount of grid faulting of the Rift floor. The effect of these faults is to channel flow along the axis of the Rift, either because the faults are open and act as conduits, or if they are infilled because they provide permeability barriers to lateral flow. A microseismic study of the Rift valley concluded that the grid faults, unlike the escarpment faults, are quite active (Tobin, Ward and Drake, 1969) which suggests that they are open. Alternatively in a recent study of the Olkaria area (Ogoso-Odongo, 1986) it was stated that faults in the Olkaria region acted as barriers, diverting southerly flow from Eburru to the south-west, towards Suswa; however the evidence for such behaviour is slim. Within the Olkaria geothermal field no evidence has been found of hydraulic barriers (Bodvarsson and others, 1987).

In summary the effect of faulting is to cause groundwater flows from the sides of the Rift towards the centre to follow longer flow paths reaching greater depths, and to align flows within the Rift along its axis.

### 4.6 Regional Groundwater Flows in the Longonot-Eburru Area

## 4.6.1 Introduction

The Naivasha catchment between Longonot and Eburru is in a hydrogeologically complex environment (as noted in Section 4.3.2), receiving water from direct precipitation and from the Rift flanks - either as stream flow or subsurface flow - and discharging groundwater to the north and south. The geothermal fields at Olkaria and Eburru lie at the southern and northern edges of the Naivasha catchment and the recharge of these fields is therefore intimately connected with subsurface flows within (or more precisely out of) the catchment.

Attempts to quantify groundwater flows in the Naivasha catchment comprise two

types; water balance studies, and applications of Darcy's Law of groundwater flow on a regional scale. These are considered below.

### 4.6.2 Water Balance Studies

A water balance approach has been used by McCann (McCann, 1972 and 1974) in an attempt to assess the water available for recharging deep aquifers and geothermal systems in several of the Rift catchments. McCann's method involved the determination of the ratio of orographic precipitation to potential evapotranspiration. A correlation (based on studies of semi-arid basins in the United States) between this ratio and the ratio of recoverable water to potential evapotranspiration, was then assumed, which enabled the quantity of recoverable water to be calculated.

For the Naivasha catchment McCann calculated a total precipitation of  $2761 \times 10^6 \text{ m}^3/\text{y}$ . Of this he calculated that  $2507 \times 10^6 \text{ m}^3/\text{y}$  evaporated (from Lake Naivasha, swamps and the surrounding catchment) leaving  $254 \times 10^6 \text{ m}^3/\text{y}$  as outflow from the catchment.

The problem with this type of calculation is that the evaporation rate is so high in the Rift valley that any errors in its estimation or in the estimation of rainfall result in large errors in the calculated value of recharge. For example, in the above calculation the resulting value of recharge is only 9% of the initial precipitation, and combined errors in estimated precipitation and evaporation could easily equal this amount. In the case of recharge from Lake Naivasha alone however different methods can be used to assess the water balance in order to provide a comparison. Subsurface flow from Lake Naivasha

It has long been recognised that subsurface flow from Lake Naivasha must occur, because the lake water is fresh even though the lake has no surface outlet and lies in an area of high evaporation. Examples of attempts to quantify discharge from the lake are given below.

### Physical model

McCann (1974) used a water balance method to estimate groundwater recharge from the lake. Water inflows to a combined lake and swamp area of 203 km² were assumed to comprise direct precipitation of  $132 \times 10^6$  m³/y and gauged streamflow of  $248 \times 10^6$  m³/y. Output from the lake was considered to take the form of evaporation of  $346 \times 10^6$  m³/y (at a potential rate of 1700 mm/y) and groundwater recharge, which was therefore calculated to be  $34 \times 10^6$  m³/y. This figure for recharge is likely to be an under-estimate, as McCann points out, because the stream inflow is a minimum value (some flows were not gauged). McCann's recharge value agrees well with that previously obtained by Sikes (1935), who determined a figure of  $43 \times 10^6$  m³/y using a similar water balance method.

### Isotopic model

Panichi and Tongiorgi (1974) used isotopic data from influent waters and lake water to model the groundwater recharge from the lake. The method relates the (oxygen) stable isotopic composition of the lake to that of influent water for a given ratio between inflow and evaporation rates and for a given value of relative humidity. The model also requires knowledge of the fractionation factor between liquid and vapour and the isotopic composition of atmospheric vapour; the relationship between these quantities and humidity was determined

by the authors by reference to Lake Elmenteita.

Therefore if the isotopic compositions of the influent waters and the lake are known, and if the evaporation rate is known, then the inflow rate to the lake can be calculated for a given humidity. The difference between inflow and evaporation rates is therefore presumed to be equal to the recharge from the lake.

Panichi and Tongiorgi derive a value of  $250 \times 10^6$  m³/y for groundwater recharge by this method. They argue that this figure agrees well with McCann's but this is based on a misreading of his work; McCann arrives at a similar value of  $254 \times 10^6$  m³/y, but for the entire catchment, his figure for lake recharge alone is  $34 \times 10^6$  m³/y as discussed above.

If however the isotopic balance method is used with isotopic data obtained during the present project different values are found. Panichi and Tongiorgi used a  $\delta^{10}$ O value of +4.6% for Lake Naivasha water, whereas an average value of +6.1% was obtained in the present study (samples 24,76). Also they used a  $\delta^{10}$ O value of -4% for water influent to the lake. While this does appear to be appropriate for the precipitation in the area, the volume of precipitation over the lake is only around 35% of the total inflow (McCann, 1974). Most of the inflow to the lake is in fact provided by the Rivers Gilgil and Malewa, which, arising in the high Rift Escarpments to the east, have a much lighter isotopic composition (a  $\delta^{10}$ O value of -9% was determined for the River Malewa [sample 79]). it is therefore estimated that an average  $\delta^{10}$ O value of -7% should be used to represent all waters influent to the lake.

Using these new stable isotope values, and the humidity range of 0.7-0.8 suggested by Panichi and Tongiorgi, values of 1.01-1.15 are obtained for the ratio of inflow to evaporation. For an evaporation of  $346 \times 10^6$  m<sup>3</sup>/y from the lake and marginal swamps (McCann, 1974) this corresponds to a recharge range of  $4-52 \times 10^6$  m<sup>3</sup>/y, a value which encompasses the McCann, and Sikes, estimates.

### Chloride balance

A third approach to the problem is a chemical balance using an ion such as chloride which is conserved in the groundwater system. Chloride values of the lakewater are recorded as varying between 7 ppm and 28 ppm (Glover, 1972) but the upper values were found only in the small south-western bay; most values vary between 7 ppm and 10 ppm, with an average of 8.6 ppm (5 values). For the whole lake, including the SW bay, a mean value of 10 ppm is assumed.

The inflow from the Malewa and Gilgil rivers has an estimated chloride concentration of 2-3 ppm (Glover, 1972) and an average of 2.5 ppm is assumed. The chloride concentration of rainfall in the area is unknown, but is unlikely to exceed 1 ppm. The total annual chloride input to the lake is therefore estimated to be  $7.5 \times 10^8$  grams of chloride (using McCann's figures for precipitation and river flow) and the recharge necessary to remove this amount is  $7.5 \times 10^7$  m<sup>3</sup>/y.

### Discussion

All three of these methods rely on assumptions in which there may be significant errors; for example they all assume that the volume of the lake is essentially unchanging when this is known to be untrue - although such changes occur only slowly. Also the methods all rely on McCann's calculations of evaporation or inflow, or both, and none of them takes into account the unknown groundwater additions to the lake from the sides of the Rift. However

the range of estimates is small enough to suggest that a mean value of  $50 \times 10^6$  m³/y may be taken for the subsurface recharge from Lake Naivasha, with an estimated error of  $\pm 40 \times 10^6$  m³/y.

The significance of this figure is that it sets a minimum value for the total recharge to aquifers over the whole of the Naivasha catchment. Thus while McCann's figure of  $254 \times 10^6$  m³/y cannot be accepted with any confidence, the total recharge value must be at least that from the lake alone i.e. of the order of  $50 \times 10^6$  m³/y.

### 4.6.3 Regional flows

Estimates of the quantities of flow on a regional scale out of the Naivasha catchment can be attempted if certain assumptions are made concerning regional head gradients and permeabilities.

Southward flows from the Naivasha area

In Section 4.3.1 it was established that a north-south groundwater gradient of at least 0.05 m/m exists over the Olkaria-Longonot area, and over Olkaria field itself the gradient has been measured as 0.1 m/m. latter gradient is accepted and if the estimated hydraulic conductivity of the Olkaria geothermal field  $(3x10^{-3} \text{ m/d} - \text{Section 4.4.3})$  is taken to represent that across the Rift (with a width of 25 km), and assuming flow to occur to a depth of 5 km (below which depth fissures are unlikely to be open) then the southerly flow at depth from the Naivasha catchment is estimated to be 14x10° m³/y. To this figure must be added the amount of southerly flow in shallow aquifers. The hydraulic conductivity of rocks at relatively shallow depths (to around 500 m - the depth of the caprock) in the Olkaria-Longonot area is unknown, but if it is taken to be between 0.1 m/d and 1 m/d i.e. similar to the Rift-wall rocks then, assuming the same hydraulic gradient and a saturated thickness of 300 m (that is, assuming the average depth to the water table to be 200 m) then the shallow component of southerly flow is estimated to be between  $27 \times 10^6$  m<sup>3</sup>/y and  $270 \times 10^6$  m<sup>3</sup>/y.

The above figures are very crude, being based on very rudimentary data, but they do indicate the order of magnitude of southerly flows from the Naivasha catchment, and suggest that the shallower aquifers may form a significant conduit for southerly flow.

Northerly flows from the Naivasha area.

McCann (1974) estimated a northerly flow of  $39 \times 10^6$  m³/y from the Naivasha catchment towards the Elmenteita catchment (on the basis of a transmissivity of 1000 m²/d). Data from the present study (Table 4.2) suggest values of transmissivity of less than 100 m²/d to the drilled depth of boreholes between Naivasha and Elmenteita, suggesting transmissivities of the order of 500 m²/d for shallow aquifers (to around 500 m, assuming water tables to be near the surface). If a mean groundwater gradient of 0.004 m/m is taken (from the piezometric map) and assuming the width of the Rift to be 15 km an estimate of  $11 \times 10^6$  m³/y is obtained for shallow northerly flow. Deep northerly flow (i.e between 500 m and 5 km) over the same cross-section is estimated as  $0.3 \times 10^6$  m³/y, assuming the same permeability as at Olkaria.

#### 4.6.3 Discussion

The implication of the above rough analysis is that much of the subsurface outflow from the Naivasha catchment flows to the south, via Olkaria-Longonot

towards Suswa, and eventually towards Magadi (although there is little evidence that such water ever reaches Magadi in an identifiable form).

In terms of relative flow amounts to the north and south, the most important, and least known value is the hydraulic conductivity of relatively shallow material beween Longonot and Suswa. If the higher value of the range given above is taken, the the total flow out of the Naivasha catchment is estimated to be around  $295\times10^6$  m³/y - a figure which agrees reasonably well with McCann's estimate of  $250\times10^6$  m³/y - of which around 20% is lake recharge. Less than 5% of this total would flow north, and of the southerly flow only 5% would occur at depth.

If the lower estimate of hydraulic conductivity is taken, then the total estimated recharge value is  $52 \times 10^6$  m<sup>3</sup>/y, virtually all of which could be lake recharge. Here northerly flow would account for about 20% of the flow from the catchment, and of the southerly flow around 25% would be at significant depths.

Concern has been expressed about the possible effect of geothermal production on the level of Lake Naivasha. According to Bodvarsson and others (1987) the average well at Olkaria produces about 6 kg/s of steam, equivalent to around 2.5 MW<sub>e</sub>. Therefore in order to produce 45 MW<sub>e</sub> the present wellfield discharges approximately 100 kg/s of steam, equivalent to a liquid discharge rate of  $3x10^6$  m³/y. This is only a small proportion of even the minimum estimated total natural southerly flow from the Naivasha area (41x10<sup>6</sup> m³/y). It is therefore considered that any effect of present or proposed geothermal production on lake levels is likely to be masked by the effects of natural rainfall variations over the catchment.

#### 5 GEOCHEMISTRY

### 5.1 Geochemical Sampling and Analysis

# 5.1.1 Sampling

The locations of all BGS - sampled sites are given in Appendix 7, which provides additional information on these and various UNDP sites. Water samples intended for chemical analysis were filtered through a 0.45µ Millipore filter under wellhead or hand pump pressure. Two 30ml Sterilin sample tubes were filled at each site, one being acidified with a drop of concentrated HCl (primarily to stabilise cations) and the other left unacidified to preserve original chloride and bicarbonate as far as possible. When hot springs were sampled a third 30ml water sample was collected, diluted ten times by distilled water to prevent silica from precipitating.

Samples for O and H stable isotope analysis were collected in 30ml glass bottles with neoprene-lined caps (McCartney type). Waters for  $\delta^{13}\text{C}$  measurement of dissolved inorganic carbon (DIC) were collected in 250ml glass bottles and usually precipitated in the field with alkaline BaCl $_2$  solution.

Samples for tritium analysis were collected in 500ml glass bottles. Radiocarbon analysis entailed the collection of two 60 litre water samples in aspirators at most sites except those with high bicarbonate, when one was sufficient. Field precipitation with alkaline BaCl<sub>2</sub> was carried out with FeSO<sub>4</sub> added to speed up flocculation where necessary. The resulting pairs of carbonate precipitates were eventually bulked in 2.5 litre polythene bottles.

Gas samples for chemical and isotopic analyses were collected from geothermal wells, fumaroles and one water well in 125ml glass bulbs with side septa. Steam from the geothermal wells and fumaroles was condensed through a stainless steel coil immersed in cold water to permit the collection of these samples.

Samples for inert gas ratio and helium isotope ratio measurement were collected in copper tubes clamped at each end. Samples were collected in dissolved or gaseous form, the latter with or without a condensing coil, depending on the sampling technique used.

#### 5.1.2 Measurement

Measurements of pH, temperature and sometimes Eh and alkalinity were made at the time of sampling. Eh measurements require flowing, air-free water, and these conditions were not always possible to fulfil. All other measurements were carried out in the UK. Chemical analysis (at BGS Wallingford) was by plasma emission spectrophotometry for cations and non-halides, and automated colorimetry for halides.

Stable isotope analysis was carried out at BGS Wallingford by mass spectrometry of  $\rm H_2$  produced by reduction of water by zinc (for  $\delta^2 \rm H$ ), and of  $\rm CO_2$  produced by equilibration with water (for  $\delta^{18}\rm O$ ), acid decomposition of precipitated bicarbonate ( $\delta^{13}\rm C$  DIC) or from geothermal sources after cryoseparation and drying ( $\delta^{13}\rm C$   $\rm CO_2$ ). Gas ratio measurements were made by gas chromatography using thermal conductivity and flame ionisation detectors.

Tritium measurements were made by the DSIR Institute of Nuclear Sciences, New Zealand employing pre-distillation, electrolytic enrichment and liquid scintillation counting. Radiocarbon was measured by the NERC Radiocarbon Laboratory by counting benzene after conversion from  ${\rm CO_2}$  liberated by acid from  ${\rm BaCO_3}$  precipitated in the field (see above); this work was supervised by Dr D D Harkness.

Inert gas samples were measured at the University of Bath by static mass spectrometry. Helium isotope ratios were also determined by mass spectrometry after suitable preparation; this work was carried out at the University of Cambridge. We are grateful to Mr M J Youngman and Dr J N Andrews (Bath) and Ms E Griesshaber and Prof. R K O'Nions (Cambridge), both for measuring the samples and for discussing interpretation of the results.

### 5.2 Water Chemistry

5.2.1 Non-thermal and Slightly Thermal Waters: Suswa to Nakuru.

This section deals with most of the waters sampled between Suswa and Nakuru. The only high-temperature waters in this area were collected from the Olkaria area, and these, together with samples from the Ol Njorowa (Hell's Gate) Gorge, are treated in Section 6 of this report.

The waters sampled fall into two main classes: modified and unmodified. The latter category includes waters whose chemical composition is derived from normal water-rock interaction at moderate temperatures, while the former comprises waters which possess evaporated or thermal components.

Results are reported in Table 5.1 and their areal distribution plotted in Figures 5.1a to 5.1g. Most unmodified groundwaters tend to be associated with the eastern and western Rift walls, i.e. sites 25-27, 85, 87, 90-92, 96, 100 and 101. The major element chemistry of these waters is summarised in Table 5.2, from which it is apparent that the waters are of sodium bicarbonate type with a relatively high silica content. The analyses are typical of igneous terrains, where dissolution of minor carbonate provides the main anion,  $HCO_3$ . Table 5.15 shows that all waters are oversaturated with respect to SiO2, but most have not yet reached calcite saturation. Only trace amounts of chloride and sulphate minerals are present in these rocks, hence the low amounts of these ions, and the relatively low total dissolved solids (TDS), averaging 365 mg/l. While much lower TDS values are known from groundwater in igneous rocks in temperate climates, the higher TDS in these waters is attributed in most cases to the high ambient temperature obtaining in the Rift Valley rather than to long residence time or particularly deep circulation.

Waters of similar composition are seen in some wells on the Rift floor - for example sites 37, 39, 82, 95 and 118, and it is considered that these waters too are the product of rainfall followed by limited water-rock interaction. When the major constituents of both categories are plotted against chloride, reasonably linear relationships are seen (Figures 5.2a to 5.2g), leading to the conclusion that simple dissolution of rock is proceeding except for Si, which reaches early saturation. There is no evidence that waters are mixing with those from another hydrochemical 'facies', for example a chloride-rich, calcium-depleted thermal water. Even in the case of the slightly thermal springs and boreholes this seems to be the case; a plot of Na temperature maintains a basic relationship (Figure 5.3a) though Si varies little (Figure 5.3b) for the reasons given above. Simple increases in solutes are observed to take place with rise in temperature, presumably both because of the increased temperature and because these waters have taken more time to circulate, though radioisotope data suggests that these time differences are not great (Section 5.5).

Chemical and stable isotope data for all water samples collected in the Rift Valley during the present study.

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Chemical and stable isotope data for all water samples collected in the Rift Valley during the present study. Table 5.1 (contd)

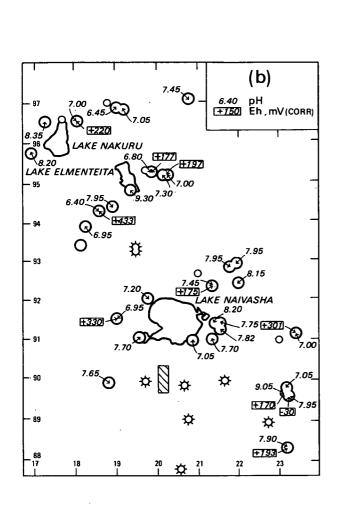
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| Ø                               | α.       | 0.018                                   | 00.0<br>9.0<br>20.0   | 7.14       | 2.53<br>2.06         | 7.12   | 70.7<br>7.78   | 0.95<br><.02    |     | 0.05        | 0.14   | -:<br>-       | 0.03  |
| samples study.                  | Li       | 0,16                                    | 0.27                  | 1.09       | 0. <b>66</b><br>0.52 | 1.16   | 1.05   | <.01<br>0.016   |     | 0.53        | 0.43   | 960.0         | 0.089 |
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| and stable<br>in the Rif        |          | 0                                       | 713.                  | 183        | 108<br>334           | ç<br>• | 183<br>172   | 0<br>187        |     | 1120<br>653 | 1100   | 989           | 989   |
| Chemical collected              |          | 0.5                                     | ) H /                 | ; ·        |                      | ,      | · ·  | <br>            |     | 1.4<br>3.3  | 6.4  | <del>1</del>  | 18    |
|                                 | Ca       | 5.4                                     | 10.8                  |            | 0.0<br>2.0           |        |  | •               |     | 40<br>41.6  | 85.  | 13            | 38    |
| Table 5.1 (contd)               | ×        | 67                                      | 31<br>27              | 118        | 40<br>37             | 47     | 532  | <.7<br>15       |     | 48<br>32.   | 79   | 30            | 87    |
| Table                           | Na       | 97                                      | 379<br>379<br>30      | 584<br>584 | 265<br>398           | 486    |  | 3.2<br>68       |     | 400<br>199  | 403  | 386           | 187   |
| •                               | Site No. | 105                                     | 108                   | 110        | 1111                 | 113    | 115  | 116<br>118      | 119 | 121         | 123<br>124   | 127           | 129   |

## **KEY**

- Well or spring water, full chemistry
   Other sites, stable isotopes only
   Fumaroles, condensate or gas
- 85 Value measured
  Site number [shown on (a) only]
- Olkaria Hell's Gate area

10Km UTM Grid 37S shown



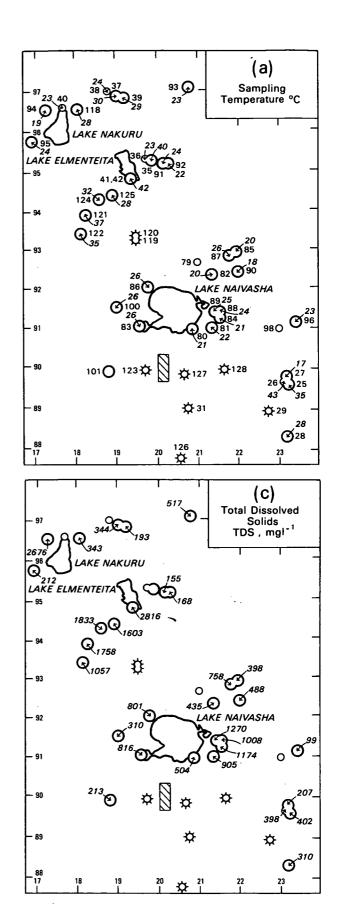


Figure 5.1a-c Maps of sampling, chemical and isotopic data from the Suswa-Nakuru sector.

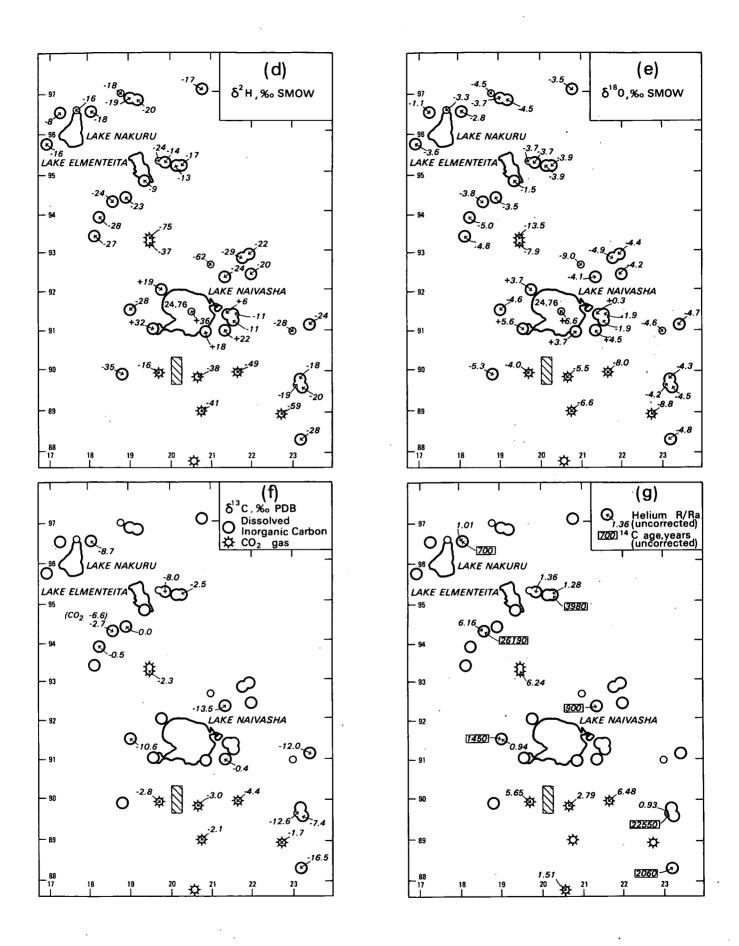


Figure 5.1d-g Maps of sampling, chemical and isotopic data from the Suswa-Nakuru sector.

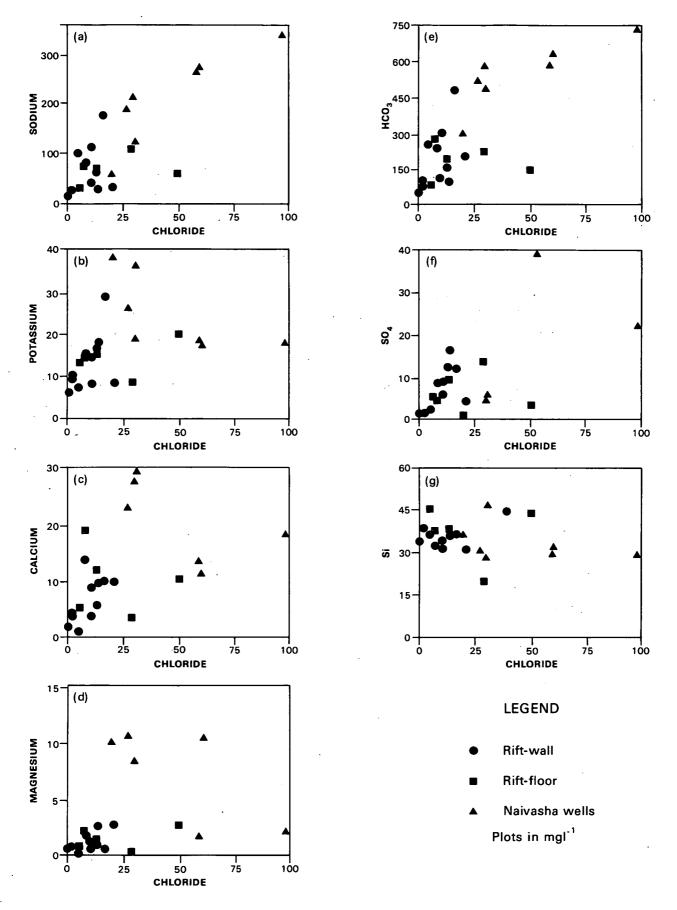


Figure 5.2a-g Plots of major ions versus chloride for unmodified Rift-wall and Rift-floor groundwater, and for wells with a large proportion of water from Lake Naivasha.

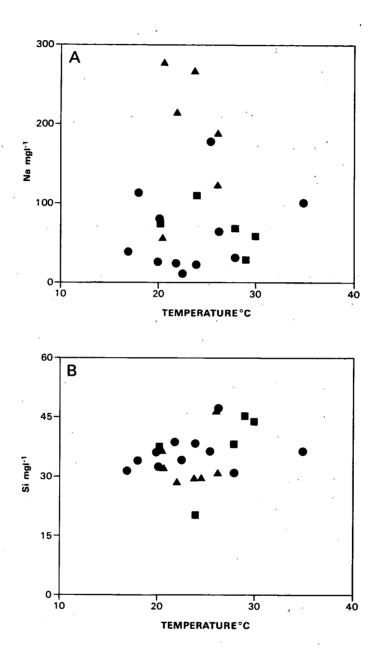


Figure 5.3a-b Plots of sodium and silica versus sampling temperature for unmodified Rift-wall and Rift-floor groundwater, and for wells with a large proportion of water from Lake Naivasha.

■ Rift floor

Naivasha wells

Rift wall

Other properties of these waters, such as pH and Eh (oxidation potential) measurements, do not conflict with the picture of unevolved groundwater obtained from the solutes. Figure 5.1b shows that pH is similar for most of these waters, with a very few exceptions such as the alkaline Kijabe springs (27), and averages 7.5 pH units which is typical of dilute bicarbonate waters. Eh values were recorded at comparatively few sites (Figure 5.1b), but they all indicate that the waters are oxidising in character. Temperatures range from 18°C (90) to 43°C (27), but (as already stated) there are no grounds on the basis of water chemistry for believing that the warmer waters are cooled or diluted high temperature waters.

It is likely that the compositional range of the waters described above (Table 5.2) is typical of shallow waters from the Rift wall and floor for considerable distances north and south of the Suswa-Nakuru sector. Supporting evidence comes from the BGS data in the Magadi area and from the MERD data in the Bogoria area.

Modified waters can be divided into those north and south of the Eburru massif. The southern group are all relatively close to Lake Naivasha; the furthest is some 6 km away. Seven wells were sampled (80, 81, 83, 84, 86, 88 and 89) and the average and range of analyses for major elements are given in Table 5.3. If the average analysis is compared with the mean for Rift-wall groundwaters it can be calculated that the average concentration increase is by a factor of 3.4, and that most of the ions have a similar ratio to chloride in both groups (Figures 5.2a to 5.2g). Only silica differs from this pattern, and this can be attributed to its abundance in the rocks: a similar solubility limit has been reached in both groups (Table 5.15).

The rather consistent increase in concentration in the Naivasha wells can plausibly be linked to evaporation in the lake, as Glover (1972) noted. Stable isotope results (Section 5.3) are very diagnostic of this process and confirm that the Naivasha wells contain up to 80% of lakewater. It is assumed that the lake is recharged by a combination of river and groundwater in the northeast, which then undergoes evaporative concentration before eventually discharging to the south and perhaps north of the lake, which lies at the culmination of the Rift floor. Thus mixing between lakewater and shallow groundwater would occur along flowpaths away from the lake, giving rise to the chemical and isotopic properties of the Naivasha group of well waters. There is no evidence that the well waters are linked in any way to possible outflows from Olkaria or Eburru.

Waters sampled to the north of Eburru in the modified category include four wells between the massif and Lake Elmenteita (121, 122, 124 and 125), a warm spring complex at the southern end of Elmenteita (41/42), and a well to the northwest of Lake Nakuru (94). The remainder of sampling points in this area are considered to be unmodified groundwaters.

The sample from site 94 is best explained by considering it to be outflow from the highly saline Lake Nakuru, though much diluted by fresher water from the sides of the Rift (Section 5.3.3). The well has an ambient temperature (Table 5.4) which effectively rules out the possibility that it is some kind of thermal outflow perhaps flowing towards the lake. Although Lake Nakuru is highly saline and therefore typical of a closed basin lake, the possibility of a small amount of flow out to the northwest does exist on piezometric grounds (Section 4.3.2). In the next section it is noted that no traces of Nakuru-type water are seen in wells to the north of Nakuru.

Table 5.2

Range of concentrations and average major ion values for unmodified Rift-wall waters.

| Ion              | average value | range  |
|------------------|---------------|--------|
|                  | mgl-1         | mg1-1  |
|                  |               |        |
| Na               | 61            | 11-177 |
| К .              | , 13          | 1-29   |
| Ca               | 8             | 1-19   |
| Mg               | 1.5           | 0-3    |
| HCO <sub>3</sub> | 190           | 44-476 |
| C1 ·             | 13            | 1-50   |
| SO <sub>4</sub>  | 7             | 1-12   |
| $SiO_2$          | 71            | 22-101 |

Table 5.3

Range of concentrations and major ion values for wells containing a large proportion of water from Lake Naivasha.

| Ion              | average value<br>mgl <sup>-1</sup> | range<br>mgl <sup>-1</sup> |  |  |
|------------------|------------------------------------|----------------------------|--|--|
| Na               | 208                                | 56-275                     |  |  |
| K                | 25                                 | 17-38                      |  |  |
| Ca               | 27                                 | 11-52                      |  |  |
| Mg               | 9                                  | 2-28                       |  |  |
| HCO <sub>3</sub> | 543                                | 297-626                    |  |  |
| C1               | 47                                 | 20-100                     |  |  |
| SO <sub>4</sub>  | 18                                 | 0-48                       |  |  |
| SiO <sub>2</sub> | 71                                 | 61-100                     |  |  |

Table 5.4 Chemistry and isotopic composition of water from the 'Badlands' wells and warm springs of Lake Elmenteita.

| •                                    |      |      |      |      |       |
|--------------------------------------|------|------|------|------|-------|
| Property                             | 122  | 121  | 124  | 125  | 41-42 |
| Temperature, °C                      | 35   | 37   | 32   | 28   | 42    |
| рН                                   | -    | 7.0  | 6.4  | 8.0  | 9.2   |
| Na, mgl-1                            | 199  | 400  | 403  | 386  | 917   |
| K, mgl-1                             | 32   | 48   | 64   | 30   | 33    |
| Ca, mgl-1                            | 42   | 40   | 58   | 13   | 13    |
| Mg, mgl-1                            | 3    | 1    | 5    | 14   | 0     |
| HCO <sub>3</sub> , mgl <sup>-1</sup> | 653  | 1120 | 1100 | 998  | 1230  |
| C1, mgl-1                            | 13   | 14   | 55   | 78   | 425   |
| SO <sub>4</sub> , mgl <sup>-1</sup>  | 9    | 9    | 17   | 22   | 75    |
| $SiO_2$ , $mgl^{-1}$                 | 106  | 126  | 131  | 66   | 123   |
| TDS, mgl-1                           | 1057 | 1758 | 1833 | 1603 | 2816  |
| δ <sup>2</sup> Η, °/ <sub>00</sub>   | -27  | -28  | -24  | -23  | -9    |
| δ <sup>18</sup> 0, °/ <sub>00</sub>  | -4.8 | -5.0 | -3.8 | -3.5 | -1.5  |

|                      | Average Olkaria<br>thermal water | Average Naivasha<br>well water | 41-42 | Indicated lakewater contribution to 41-42 |  |  |
|----------------------|----------------------------------|--------------------------------|-------|---|--|--|
| Na/Cl                | 0.98                             | 4.4                            | 2.2   | 35%                                       |  |  |
| HCO <sub>3</sub> /C1 | 0.36                             | 11.6                           | 2.9   | 23%                                       |  |  |
| SO <sub>4</sub> /Cl  | 0.14                             | 0.38                           | 0.18  | 17%                                       |  |  |

The sequence of sites running northeast from well C431 (122) to the Elmenteita springs (41 and 42) is interesting as it presents the only opportunity (apart from fumaroles) of looking at the remnants of a geothermal outflow in the Suswa to Nakuru sector of the Rift. All the wells exceed the unmodified Rift-wall type of composition in terms of dissolved constituents (Table 5.4), and it is known from <sup>3</sup>He/<sup>4</sup>He measurements at site 124 (Section 5.6.2) that a high temperature upflow must ultimately be responsible for the chemistry of much of the water flowing north from Eburru. Because of the curved disposition of these sites in relation to the Eburru volcanic centre, they all lie at about the same distance from the centre (around 13 km). There is an increase in TDS values from about 1000 mg/l in the southwest to nearly 3000 mg/l at the warm springs, with chloride increasing at the expense of bicarbonate and sulphate, though bicarbonate remains the dominant anion.

The increase in TDS to the northeast does not necessarily imply a greater outflow contribution. Taking the average Olkaria thermal water composition to represent that of the Eburru upflow, and the average composition of the wells close to Lake Naivasha to represent northward subsurface flow from Lake Naivasha, it can be seen from comparisons of the ratios of major constituents to chloride that some 30% or so of lakewater mixing with thermal water could be responsible for the compositions seen in the warm springs at the southern end of Lake Elmenteita (Table 5.4). Close support is given by the stable isotopic results (Section 5.3.3) which imply a lakewater contribution of between 30-35%.

To the southwest of the springs the wells suggest a much smaller or totally absent lakewater contribution - indeed the slight increase in heavy isotopes might simply be due to steam loss from the underlying groundwater. However, study of the ratio of constituent ions to chloride for all five sites does imply that a dilution series is involved and that the isotope results can probably be taken at face value.

In view of the low chloride contents measured in the wells it may be doubted that they are truly representative of primary outflow from Eburru. The high bicarbonate values suggest that they may be the result of condensation of  $\mathrm{CO}_2$  and associated gases into what is basically a Rift-wall type of water on the basis of stable isotopes. It is shown elsewhere (Section 5.3.4) that Eburru upflow water is probably very similar in isotopic terms to Rift-wall water, and therefore mixing or steam heating involving shallow and thermal waters in the Eburru outflow area is unlikely to show up isotopically. However, the likelihood that the well waters are of secondary composition is not supported by the high  $\mathrm{SiO}_2$  and Li results, particularly from sites 121 and 122.

Nevertheless, if the wells are considered to be secondary manifestations of thermal outflow from Eburru, then the low temperatures of the waters and the lack of evidence of secondary steam production in the 'badlands' area is an indication that the quantities of cold, shallow groundwater flowing from the Rift wall are of sufficient volume to 'quench' steam boiling off the thermal outflow. Only where the outflow water itself is ascending towards the southern end of Lake Elmenteita and mixing with water flowing north from Lake Naivasha does the shallow groundwater temperature become higher.

If, however, the  $SiO_2$  and Li results are given weight then it must be assumed that the Eburru upflow water is considerably lower in chloride than the thermal fluid at Olkaria. To some extent this is likely, as the Eburru system is considered on isotopic grounds to derive from the low-chloride

Rift-wall water rather than the higher-chloride lakewater which feeds Olkaria. In this case it must be assumed that there is only a small upward leakage of outflow water on its journey north to Lake Elmenteita. The result appears to be a ternary mixing system between Rift-wall water, thermal outflow and Lake Naivasha water.

Despite the differences between these two models, it is clear that there must be outflow north from Eburru and also underflow from Lake Naivasha. These two sources combine to account for the apparent water supply deficiency in the Elmenteita basin noted by McCann (1972).

### 5.2.2 Surface, Thermal and Non-Thermal Waters: Nakuru to Silale.

The rather limited number of samples collected and analysed by the BGS-MERD team from this area has been supplemented by 11 samples collected between northern Lake Bogoria and Nakuru by two MERD staff members (Messrs M. Arusei and J. Wambugu) as part of their MSc course work at Leeds University, where the samples received chemical analysis. Isotopic analysis of these samples was performed at BGS Wallingford and the results are considered in Section 5.3.5 of this report.

chemistry results are presented in Tables 5.1 and Figures 5.4a to 5.4.d. Major element chemistry is now considered. Nakuru and Bogoria concentrations resemble those measured in the Suswa-Nakuru sector for waters believed to have originated as rainfall on the Rift wall or In fact stable isotopic measurements suggest that the higher floor. groundwater in this area is mainly from the Rift floor rather than wall, otherwise the waters are similar in character with the ranges of Na 37-174, K 4.7-22, Ca 1.0-20, Mg 0.1-3.8, Cl 4.2-13, SO<sub>4</sub> 2-20 and HCO<sub>3</sub> 187-322 mg/l. Though there is a considerable drop in altitude between Lake Nakuru and Lake Bogoria (some 770 m) there is no geochemical evidence of flow out of Lake Nakuru to the north. Samples collected from wells or springs a few km from Lake Bogoria (i.e. B1, B4 and B7) are generally similar to those further south in their chemistry and suggest that, like these samples, they are derived from local rainfall. It is presumed that groundwater flow in the general area must be directed towards Lake Bogoria, which has the very high salinity associated with closed or almost closed basin lakes. shores of the lake two boiling springs were sampled (B2 and B3). chemistry of these springs suggests locally-derived groundwater which has been drawn into a CO2-rich geothermal upflow. The concentration ratios are similar to those measured at the warm spring at the southern end of Lake Elmenteita (see previous section) and the total TDS value is about 1.5 times The Elmenteita springs are some 15 km north of the Eburru upflow, their presumed source, but issue at only about 40°C compared to the boiling temperatures of the Bogoria springs. This suggests that the Bogoria springs are much closer to their upflow and may be rapidly cooling by adiabatic rather than conductive processes; the apparent steam loss identified from stable isotopic measurement supports this (Section 5.3.5). The silica and alkali geothermometers give temperatures of below 150°C for the Bogoria springs; such temperatures at depth seem too low in view of the vigorous boiling of the springs. This implies that upflow is being modified by a cooler inflow at some stage. Isotopic evidence (Section 5.3.5) points to a small amount of lakewater contamination but suggests that steam heating is involved; on this basis the lakewater could be contributing at various levels in the thermal circulation. Equally, non-thermal 'fresh' groundwater could be responsible for the erroneous performance of the geothermometers, though in view of the relatively high salinity of the boiling springs this is

Table 5.5

Chemistry and isotopic composition of samples collected by MERD personnel in the Lake Bogoria area.

| 6180             | -2.8         | -0.7 | -0.5 | -3.2           | -3.1 | -3.3 | -2.7         | -2.5 | -2.8        | -2.7 | -2.8  |
|------------------|--------------|------|------|----------------|------|------|--------------|------|-------------|------|-------|
| 62H              | -12          | ۳    | -2   | <del>1</del> . | -14  | -15  | -10          | -13  | -19         | 91.  | -14   |
| TDS              | 533          | 4443 | 5083 | 687            | .991 | 847  | 260          | 558  | 394         | 327  | 612   |
| SiO2             | 06           | 111  | 137  | . 58           | 70   | 51   | 80           | . 84 | . 19        | 7.0  | 86    |
| \$0¢             | <del>-</del> | 57   | 52   | 20             | 9    | 9    | <del>-</del> | =    | 16          | 7    | 20    |
| C1               | 20           | 280  | 400  | 11.8           | 16.5 | 78   | 11.8         | 5.2  | 21          | 4.2  | 26    |
| HCO <sub>3</sub> | 278          | 2645 | 2787 | 283            | 671  | 542  | 325          | 322  | 195         | 195  | 283   |
| Mg               | 1.7          | 07.0 | 0.16 | 3.8            | 40   | 7.5  | 1.0          | 2.8  | <del></del> | 2.5  | 0.10  |
| Ca               | 6.4          | 1.4  | 0.7  | 8.9            | 67 . | 14.3 | 4.5          | 19.6 | 6.3         | 11.6 | 1.0   |
| ×                | 10           | 12   | 37   | 10             | 11   | 56   | 10           | 22   | <b>1</b>    | 4.7  | 10    |
| Na               | 117          | 1336 | 1669 | 93             | 121  | 169  | 117          | 91   | 84          | 37   | . 174 |
| Нd               | 8.9          | 8.7  | 9.3  | 7.6            | 7.7  | 8.1  | 6.3          | 6.9  | 7.5         | 7.4  | 9.8   |
| Temp<br>°C       | 37.0         | 93.5 | 96.4 | 34.5           | 29.4 | 42.9 | 37.7         | 29.2 | 33.2        | 38.5 | 36.9  |
| SITE             | B1           | B2   | B3   | B4             | B5   | B6   | B7           | M1   | M2          | M3   | 7W    |

NOTE: Chemical analyses carried out at Leeds University by M Arusei and J Wambugu of the M.E.R.D.

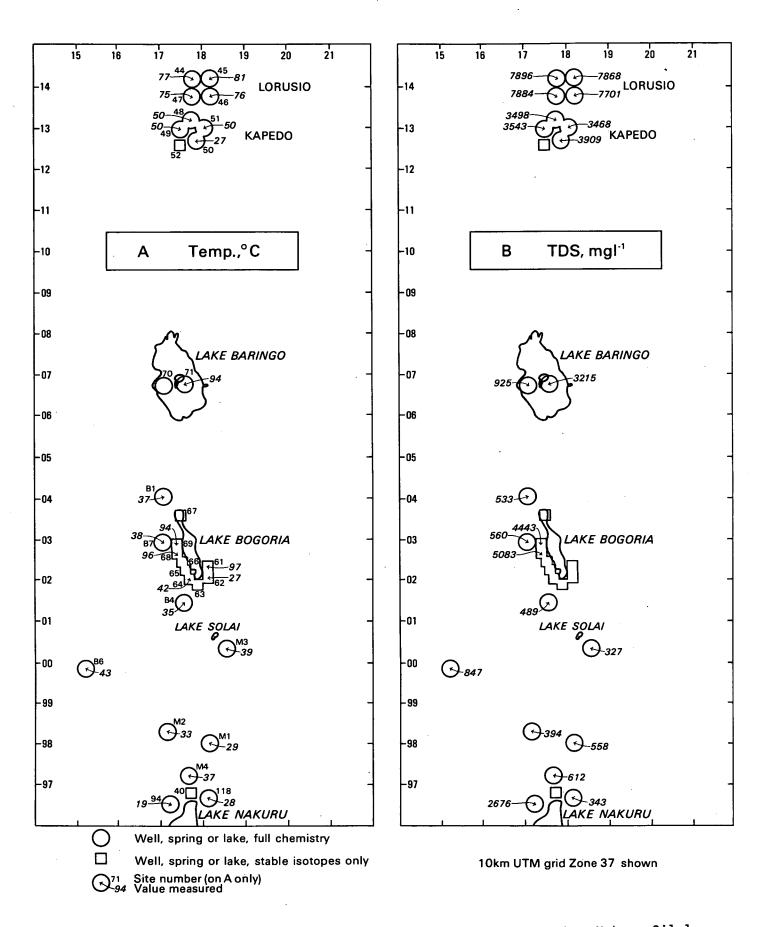


Figure 5.4a-b

Maps of chemical and isotopic data for the Nakuru-Silale sector ('M' and 'B' numbers relate to samples collected by MERD).

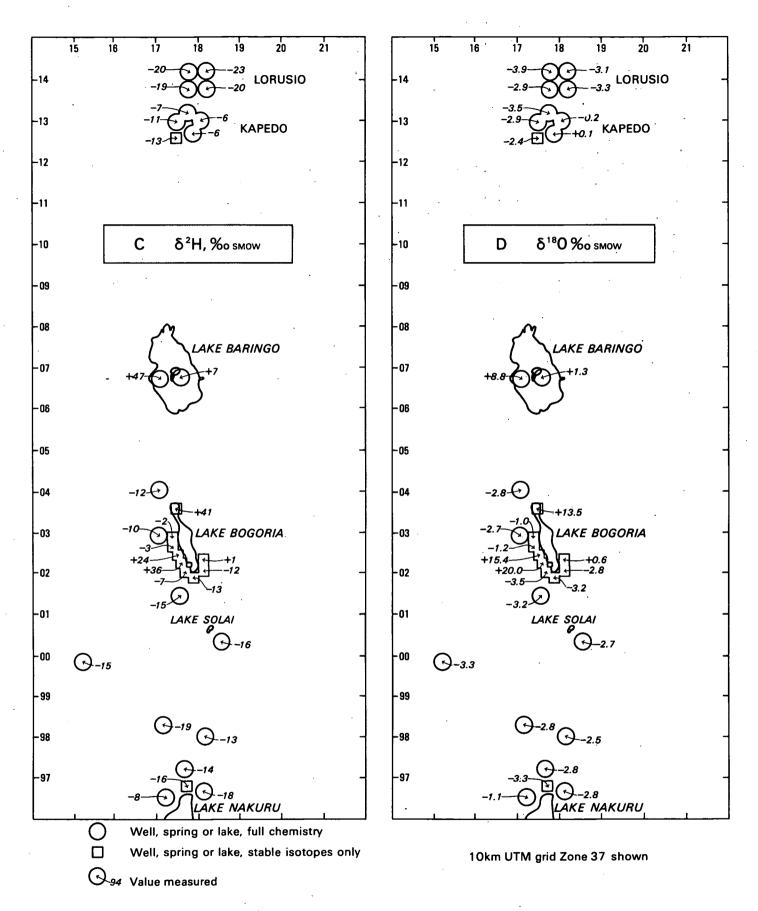


Figure 5.4c-d Maps of chemical and isotopic data for the Nakuru-Silale sector ('M' and 'B' numbers relate to samples collected by MERD).

perhaps less likely. Geotermica Italiana (1987) proposed a ternary mixture of thermal water, lakewater and another water component, the origin of which was not altogether clear from their isotopic evidence. Their mixing models suggested the maximum temperature at depth to be about 190°C, while gas and isotopic geothermometers gave results in excess of 200°C. The few data considered here cannot confirm these results quantitatively, but qualitatively their similarity to the Eburru outflow and to some extent the Olkaria fluid suggests that such temperatures may well be correct.

At Lake Baringo, samples were collected from a boiling spring on the central island of Ol Kokwe, and from the lake. Analyses are given in Table 5.1 and shown in Figures 5.4a to 5.4d. The spring water is almost four times higher in TDS than the lake and therefore, as Glover (1972) pointed out, is most unlikely to be the result of steam heating of lakewater. Its chemistry is typical of other high temperature thermal waters further south in the Rift for example there is a strong resemblance to the Olkaria fluid (e.g. very similar Cl/SO<sub>4</sub> ratios) except that there is much more bicarbonate, which implies condensation of CO<sub>2</sub> at shallow depths. Stable isotope results indicate that the boiling springs probably contain a proportion of lakewater mixed with the original groundwater presumed to feed the system. Silica and alkali geothermometers (Table 5.14) show temperatures in excess of 175°C, and it is concluded from this that lakewater must be entering the system before or during heating; if lakewater were mixing at shallow depths interference with the geothermometers would tend to result, as is apparently the case at Lake Bogoria.

Two groups of hot springs north of Lake Baringo were sampled. The results (Table 5.1, Figures 5.4a-d) show that the waters are not dissimilar in element ratios, but that the Lorusio group is twice as high in TDS and contains proportionately higher amounts of HCO<sub>3</sub>. Silica and alkali geothermometers give rather similar temperatures at depth for each group in the range 120-150°C. Since the Lorusio group is hotter and more concentrated in TDS, it is tempting to consider that the Kapedo group is the result of dilution of the Lorusio water, but isotopic measurements make this explanation inplausible and imply a separate origin (Section 5.3.5).

The Kapedo springs are similar in chemical composition and amount to the Ol Kokwe spring water, though in terms of Na/K ratio and  $\rm SiO_2$  content are different enough to affect geothermometry results. The spread of values of elements between the various springs is probably a consequence of evaporation/steam loss (Section 5.3.5). In spite of the similarity to the Ol Kokwe spring the isotopic signatures are much closer to the meteoric line and do not suggest that Lake Baringo water penetrates this far north in recognisable form, thus contradicting the admittedly tenuous evidence from  $\rm C_2H_6/CH_4$  ratios (Section 5.6.1).

### 5.2.3 conclusions

The consideration of chemical data, particularly from the relatively well-sampled Naivasha-Nakuru sector of the Rift Valley reveals that on the whole large-scale mixing of high temperature thermal outflow with 'fresh' Rift-wall water does not occur where it can be directly sampled. Few ambient or slightly warm well or spring waters show any evidence of mixing, although the basalt 'badlands' north of Eburru are an exception. Otherwise thermal outflows often appear very close to lakes — i.e. in low-lying discharge areas. (Lake Naivasha is an exception because it is itself recharging, and the outflows from the neighbouring Olkaria-Domes-Longonot area, or the Suswa area, have not been detected). The association of hot or

boiling springs with low-lying lakes has led to the belief that there could be a general body of thermal water underlying the Rift over a large area (Mahon, 1972). Certainly there is a similarity between the chemistry of many of the hotter thermal springs as far north as Lorusio. However stable isotope evidence (Section 5.3.3 et seq.) tends not to support this conclusion. Instead the general chemical resemblance is more likely to be due to separate convective systems in rather similar lithologies (in geochemical terms) aided by the copious flux of CO<sub>2</sub> in the Rift Valley (Bailey, 1980).

### 5.3 Stable Isotopes - Water.

#### 5.3.1 Introduction

Oxygen ( $^{18}O/^{16}O$ ) and hydrogen ( $^{2}H/^{1}H$ ) isotope ratios are calculated with reference to Vienna Standard Mean Ocean Water (SMOW) and are presented in Table 5.1. They were measured on rainfall, surface water, groundwater and fumarole steam condensates.

### 5.3.2 Rainfall in the Rift: Magadi to Lodwar.

Counterpart staff distributed sample bottles to 21 rainfall stations throughout the Kenya Rift Valley in January/February 1986. The station locations are given in Appendix 7 and range from Magadi in the south to Lodwar near Lake Turkana in the north.

The stable isotope characteristics of the samples were determined at Wallingford using the methods of Darling et al. (1982).  $\delta^{18}$ O and  $\delta^{2}$ H values are given in Table 5.6 and are plotted on Figure 5.5. Data from three rainfall samples taken in 1985 are also included in the figure. Least squares linear regression analysis was used to identify the line

$$\delta^2 H = 5.56 \, \delta^{18} O + 2.04 \, (r^2 = 0.88)$$
 (3)

through the data. In addition lines were fitted separately to data for the smaller and larger rainfall events to check for bias (such as that related to the 'amount effect' (Dansgaard, 1964) or to possible evaporation from rain collectors), but none was found.

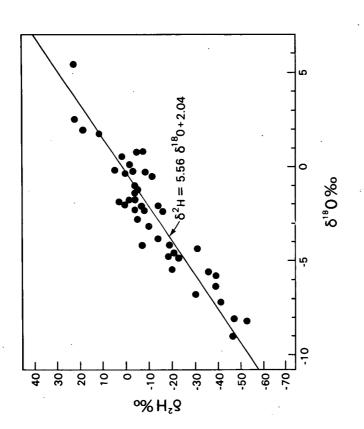
Equation 3 has a smaller slope than that of the world meteoric line proposed by Craig (1963) with a slope of 8; this is probably because rain over the Rift Valley evaporates somewhat as it falls. A regression calculated for 80 Rift Valley groundwaters from Magadi to Silale (Figure 5.6) gave a slope very similar to that defined by rainfall:

$$\delta^2 H = 5.49 \, \delta^{18} O + 0.08 \, (r^2 = 0.81)$$
 (4)

This suggests that the rainfall line, though based on sampling over a limited period of time, is likely to be reasonably accurate. Additional support is provided by studies outside the Rift: in the Chyulu Hills of southeast Kenya the following relationship was observed for 35 samples (BGS unpublished data):

$$\delta^2 H = 5.68 \, \delta^{18} O + 6.04 \, (r^2 = 0.89)$$
 (5)

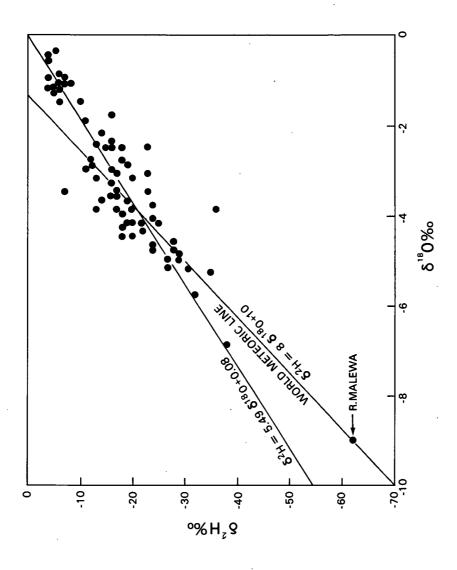
This indicates that rather low meteoric gradients are found in southern Kenya as a whole and are not confined to rainfall in the Rift Valley.



Delta-diagram of rainfall stable isotope data from collection stations in the Magadi- Silale sector.

Figure 5.5

| STATION | COORDINATES    | ALTITUDE | DATE              | RAINFALL | $\delta^2 H$ | δ180   |
|---------|----------------|----------|-------------------|----------|--------------|--------|
|         |                | (m)      |                   | (mm)     | . •/•        | o SMOW |
| 1       | AH 99 91       | 600      | 21.3.86           | 16.3     | -7           | +0.8   |
| •       | ,, ,,          |          | 31.3.86           | 2.6      | +22          | +5.4   |
| 2       | BJ 16 26       | 600      | 21.3.86           | 8.4      | -8           | -0.3   |
|         |                |          | 7.4.86            | 11.4     | -14          | -2.1   |
| 3       | BJ 37 37       | 1000     | 18.3.86           | 3.2      | +12          | +1.7   |
| ,       | 7D 40 30       | 4000     | -                 | -<br>?   | -<br>-10     | -3.2   |
| 4       | ZP 18 30       | 1800     | 6.4.86            | :<br>?   | -64          | -10.2  |
| 5       | 7D 20 00       | 1000     | 10.4.86           | 14.3     | -04<br>+5    | -0.2   |
| 3       | ZP 20 80       | 1900     | 5.3.86<br>11.4.86 | 6.6      | -30          | -6.8   |
| 6       | ZQ 16 36       | 2760     | 18.4.86           | 21.5     | -47          | -9.0   |
| O       | 2Q 10 30       | 2700     | 20.4.86           | 22.2     | -18          | -4.8   |
| 7       | BJ 31 98       | 2200     | 7.3.86            | 8.4      | -39          | -5.8   |
| ,       | DJ 31 30       | 2200     | 23.4.86           | 7.6      | -36          | -5.6   |
| 8 .     | AK 42 21       | 2550     | 10.3.86           | 8.8      | -4           | -2.3   |
| 0 .     | AR 42 21       | . 2330   | 22.4.86           | 49.0     | -23          | -4.9   |
| 9       | BK 14 20       | 1920     | 10.3.86           | 22.2     | -7           | -4.2   |
| 9       | DK 14 20       | 1920     | 10.4.86           | 16.1     | -39          | -6.4   |
| 11      | BK 02 45       | 2000     | 12.4.86           | 4.2      | -3           | -0.3   |
| 11      | DR 02 43       | 2000     | 23.4.86           | 34.7     | -53          | -8.2   |
| 12      | AK 73 69       | 1850     | 20.3.86           | 2.0      | -4           | -1.4   |
| 12      | AR 73 07       | 1030     | 18.4.86           | 11.0     | - <b>5</b>   | -1.3   |
| 13      | BJ 41 79       | 2340     | 21.3.86           | 13.7     | -14          | -3.9   |
| 13      | 50 41 75       | 2540     | 23.4.86           | 18.4     | -41          | -7.2   |
| 14      | ZR 04 04       | 2100     | 18.3.86           | 23.3     | 0            | -2.0   |
| • •     |                | 2.00     | ?                 | ?        | +3           | -1.9   |
| 15      | AL 72 29       | 1150     | 20.3.86           | 10.7     | +2           | +0.5   |
|         | 112 12 27      |          | 10.4.86           | 39.7     | -11          | -0.5   |
| 16      | ZR 30 06       | 1550     | 18.3.86           | 8.0      | -20          | -5.5   |
|         |                | ,,,,,,   | 4.7.86            | 25.0     | -5           | +0.7   |
| 17      | AL 76 38       | 1000     | 10.4.86           | 17.0     | -19          | -4.2   |
|         |                |          | 20.4.86           | 19.2     | -5           | -2.8   |
| 18      | ZR 05 54       | 2050     | 7.3.86            | 10.1     | -4           | -1.8   |
| -       |                |          | 10.4.86           | 16.8     | -47          | -8.1   |
| 19      | AM 69 05       | 900      | 7.3.86            | 16.1     | -1           | +0.1   |
|         |                |          | 22.3.86           | 5.4      | 0            | -0.4   |
| 20      | BM 43 21       | 2000     | 18.3.86           | 4.4      | -31          | -4.4   |
|         |                |          | 21.4.86           | 10.2     | -16          | -2.4   |
| 21      | 35°40'E 2°23'1 | 088 1/2  | 5.3.86            | 32.3     | -7           | -2.2   |
|         |                |          | 7.3.86            | 23.3     | -1           | -1.8   |
| 22      | 35°36'E 3°07'1 | N 550    | 4.3.86            | 28.9     | +19          | +1.9   |
|         |                |          | 24.4.86           | 33.4     | -21          | -4.6   |
|         |                |          |                   |          |              |        |



Delta-diagram of stable isotope data from unmodified groundwaters in the Magadi-Silale sector.

Figure 5.6

However, rather depleted water from the Malewa River which rises in the Nyandarna Mountains is seen to fall on the world meteoric line. This implies that the modifying influeces are restricted to lower altitudes, as might be expected.

Altitude and Latitude Effects.

The high topographic relief of the Kenya Rift Valley makes it likely that significant variations with altitude in the mean isotopic composition of rainfall will occur. This was investigated for the rainfall samples by plotting  $\delta^{18}\mathrm{O}$  vs height and  $\delta^{2}\mathrm{H}$  against height. Taking height as the controlled variable in each case a least squares regression line was fitted to the data sets giving:

$$\delta^{18}O = -0.0029 \text{ x altitude (m)} + 1.99$$
 (6)

$$\delta^2 H = -0.0148 \text{ x altitude (m)} + 10.82$$
 (7)

The values of the coefficients of determination for equations 6 and 7 are 0.32 and 0.24 respectively, indicating significant scatter in the data. It is thought that this is largely caused by the limited number of samples obtained from each station. Individual rainfall events at a given station can give widely differing isotopic results, as shown in Table 5.6, because evaporation and temperature effects will be different for different rainfall events. Many samples from a given station would however be expected to have isotopic compositions which fall around a mean, dependent mainly on the altitude.

The change in  $\delta^{18}$ O is estimated as -0.29% (i.e. decrease) for every 100 m of This compares favourably with values obtained ascent from equation 6. elsewhere; i.e. -0.2% for Sweden, -0.4% (French Alps), (Czechoslovakia), -0.26% (Nicaragua), -0.18% (Cameroon), -0.16% (Greece) (Figures quoted in Darling and Lardner, 1985). Few studies of deuterium variation with height are available but it is assumed that if the figure for oxygen is accepted, then the estimated variation of -1.5% per 100 m for  $\delta^2$ H from equation 7 can also be accepted because of the close correlation between  $\delta^2$ H and  $\delta^{18}$ O described by equation 3.

The possible effect of latitude on the isotopic characteristics of the rainfall samples has been examined by plotting the isotopic variation with height for samples from the southern (Nairobi and Narok 1:250,000 maps), central (Nyeri and Kisumu maps), and northern (Rumuruti, Eldoret, Maralal and Turkana maps) areas respectively. This showed some evidence of a decreasing trend in the amount of isotopic variation with height changes from south to north, with the central area falling most closely on the line described by equations 6 and 7. However the coefficients of determination were low, and the hypothesis of a latitude dependent effect is regarded as inadequately supported by the available data. Also there was no evidence of a systematic variation in isotopic composition from one side of the Rift to the other.

## 5.3.3 Surface and Low Temperature Groundwater: Suswa to Nakuru.

In this area a typical stable isotope value for groundwater from the side of the Rift is -28%  $\delta^2$ H, -4.8%  $\delta^{18}$ O, which is similar to values measured on the Kinangop plateau (Figures 5.1d and 5.1e). Slightly lighter Rift-wall waters were measured (up to -35%  $\delta^2$ H, -5.3%  $\delta^{18}$ O) in a few places, but there is no evidence of the highly depleted isotopic compositions presumed to exist in the Nyandarua (Aberdare) Mountains to the northeast and which are measured in

the main river (River Malewa) feeding Lake Naivasha. The implication is that the mountains are drained chiefly by surface water whose depleted composition is masked by the high evaporation acting on Lake Naivasha, the local sump for surface drainage.

The typical Rift-wall composition of -28%  $\delta^2 H$ , -4.8%  $\delta^{18}$ O does not accord particularly well with the isotope-altitude relationships propounded in the previous section, but these are necessarily tentative and probably more important as relative indicators of altitude. In this sector of the Rift unmodified meteoric water appears to range from -35% to about -18%  $\delta^2 H$ , an altitude difference of some 700 m. The corresponding  $\delta^{18}$ O range is -5.3 to -3.5% suggesting a difference of 600 m.

In contrast to the well waters on or near the side of the Rift, lakewaters are highly enriched in heavy isotopes owing to the great potential for evaporation. While lakes Elmenteita and Nakuru are discharge areas within an almost closed drainage basin, Lake Naivasha is a source of recharge to the Rift and provides a very effective tracer for axial groundwater movement. The typical Naivasha composition is +35%  $\delta^2 H$ , +6.6%  $\delta^{18} O$ , and it is possible to draw contours (where there are sufficient well data) showing the approximate percentage of lakewater in the mixing series between lakewater and groundwater (Figure 5.7). If certain assumptions about the production of fumarole steam are made it is possible to infer groundwater compositions beneath thermal centres; while these data have been added to Figure 5.7 their calculation is explained in the next section.

Most of the groundwater sampled in this part of the Rift can be explained in terms of unmodified rainfall or of rainfall mixed with lakewater. no evidence for a third source of water with thermal characteristics (for instance with a pronounced  $\delta^{18}$ O shift) underlying the area at depth. greatest mixing effects are demonstrated in the wells close to Lake Naivasha, which have an obvious lakewater contribution . Since the lake is on the topographic culmination of the Rift floor, discharge to both north and south may be expected. Unfortunately well data are concentrated on the east and west sides of the lake, and the only strong indication of the presence of lakewater elsewhere (apart from high-temperature geothermal sources) comes from the warm springs near the southern end of Lake Elmenteita some 30 km to These suggest a 30% contribution from Lake Naivasha. northeast of the lake the River Malewa debouches into a swamp which ultimately must recharge the lake, and there is accordingly no evidence of heavily-evaporated water here. While the influence of the lake is seen up to 6 km away SSE of the lake, data from the western side suggest that there is very little flow to the west.

The warm springs at the southern end of Lake Elmenteita show evidence of water from Naivasha, as already mentioned. A few kilometres to the northeast and southwest of the springs typical Rift-wall water compositions of -24%  $\delta^2 H$  are seen (36 and 124). The flow of (already considerably diluted) lakewater to the north therefore passes through a relatively narrow constriction at this point. Beyond this well data are sparse, and the effects of discharge at the northwest end of Lake Elmenteita of considerably enriched water would in any case obliterate evidence of Naivasha water. Although Lake Nakuru is assumed (like Elmenteita) to be extremely enriched in heavy isotopes, there are only limited signs of this in wells to the northwest of the lake. The implication of this is that flow out of this basin is very small and most water is lost by evaporation. Alternatively, if there is a greater flow to the northwest from the lake it is being rapidly diluted by a comparable amount of flow from the sides of the Rift (particularly from the west).

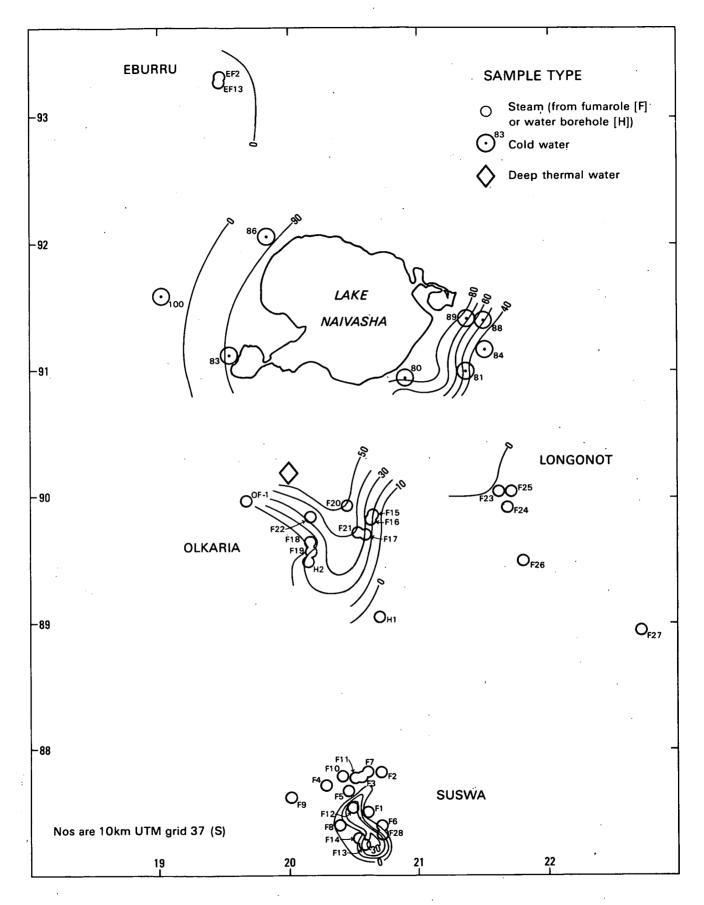


Figure 5.7 Contour map showing the contribution of Naivasha lakewater to groundwater in the Suswa-Eburru sector, based on geochemical evidence from wells, springs and fumaroles. Contours are in percent lakewater.

#### 5.3.4 Thermal Waters: Suswa to Eburru.

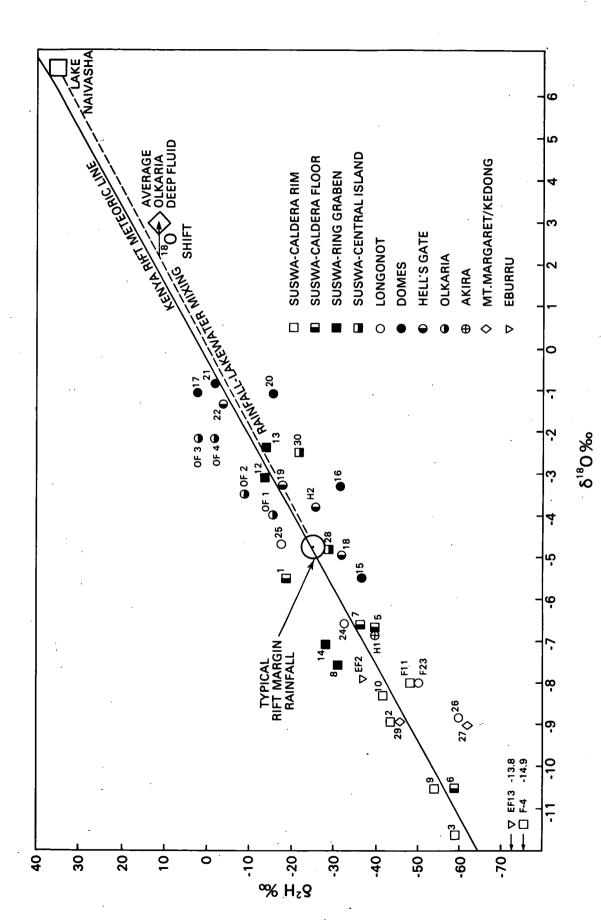
Steam condensate from fumarolic discharges on Suswa, Longonot Domes, Olkaria, Eburru and surrounding areas was collected for analysis, much of it by Dr. H. Armannsson of the UNDP. (Site details are provided in Appendix 7) Deep thermal fluid was sampled from some of the wells in the E. Olkaria geothermal field which, although only a small area on the maps in Figures 5.1d and 5.1e, is of extreme importance as the only location in this part of the Rift where the total geothermal fluid can be sampled.

The geochemistry of Olkaria-Hell's Gate area is dealt with in greater detail in Section 6.2, but the total fluid compositions from the wells are plotted together with steam condensates from all fumaroles on Figure 5.8. The steam condensate samples form an elongate group, parallel to the meteoric line for the Rift, and covering a large range, approximately -1 to -15%  $\delta^{10}$ O. There is no sign of a conspicuous  $\delta^{10}$ O shift in the fumarole results or the Olkaria thermal fluid.

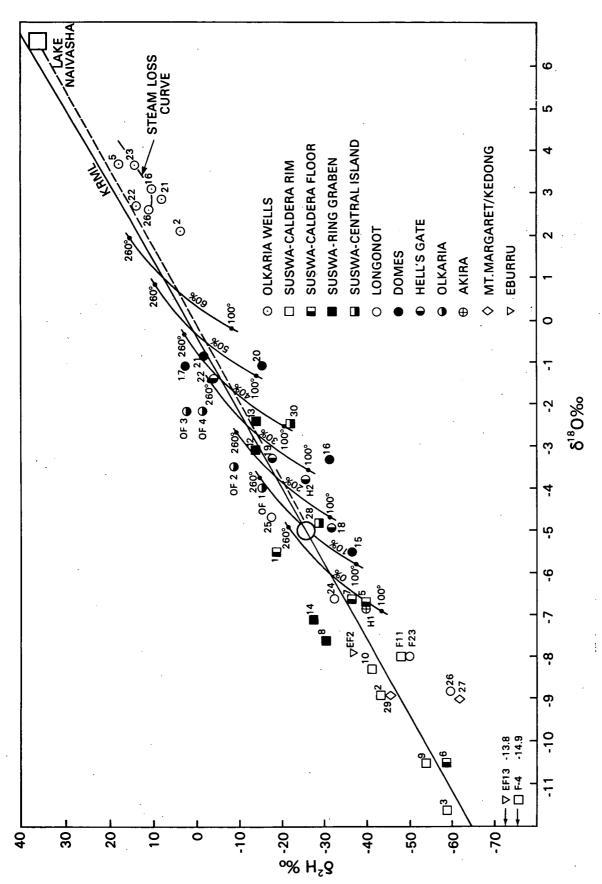
On the basis of the steam results it is proposed that most, if not all, of the fumarole condensates are products of steam separation from a mixing series between Naivasha lakewater (+36%  $\delta^2 H$ , +6.6%  $\delta^{18} O$ ) and Rift-wall groundwater (-30%  $\delta^2 H$ , -5.0%  $\delta^{18} O$ ). This situation may be slightly complicated by a small  $\delta^{18} O$  shift (maximum 1.5%) suggested by the Olkaria results.

To demonstrate this hypothesis, Figure 5.9 shows a  $\delta$ - plot of all steam samples together with theoretical lines formed by primary steam separation from various dilutions of lakewater with Rift-wall water allowing for a small (1%)  $\delta^{18}$ O-shift. The resulting temperature ranges (100-260°C) form parallel curves with a gradient somewhat steeper than the KRML, and several of the fumarole groups form dispositions sub parallel to these calculated lines e.g. Longonot, Hell's Gate and Suswa caldera floor - suggesting that the interpretation may be justified. Samples lying outside the primary steam range are likely to be caused by local conditions - for example the fumaroles from the Eastern Olkaria wellfield appear to derive from steam heated groundwater, and the more depleted waters from Suswa may be the result of steam condensation, a process considered by Darling and Armannsson (in In addition, the primary steam envelope would itself be subject to possible local dilution effects and small variations in  $\delta^{\text{1S}}\text{O}$  shift.

The steam data from each region are now considered in terms of the lakewater mixing model. Starting with Eburru, the most northerly high-temperature manifestation in this sector of the Rift, it can be seen on Figure 5.9 that the samples obtained from EF2 lie beyond the influence of lakewater. implies that water from Naivasha does not flow beneath Eburru during its passage northwards. Eburru EF2 shows some evidence of local dilution effects, but the presence of He and H2 in the accompanying gases confirm that the steam is basically primary and derived from local Rift-wall groundwater. This is confirmed by the outflow from Eburru which affects the chemistry of wells at sites 121, 122, 124 and 125. These waters have a basic Rift-wall isotopic composition but their chemistry is clearly the result of thermal processes - they contain for example high silica, lithium and bicarbonate, as well as having a high gas content (mainly CO<sub>2</sub>) and a <sup>3</sup>He/<sup>4</sup>He ratio similar to EF2 (Table 5.11). EF13, on the other hand, is highly depleted in heavy isotopes and can only easily be explained by a large degree of steam condensation below surface. The very low gas content of this fumarole (Z. W. Muna, pers. comm.) tends to confirm that it is not unmodified primary steam.



data Delta-diagram of fumarole condensate stable isotope from the Suswa-Eburru sector. Figure 5.8



steam production from a groundwater-lakewater mixing series. The curves show the percentage of lakewater Fumarole stable isotope data shown in relation to primary contributing to steam. Figure 5.9

The fumaroles in the Olkaria and Hell's Gate area are treated in more detail with the Olkaria wellfield in Section 6.2, but all show the influence of lakewater to a greater or lesser extent. In the Domes area east of Hell's Gate, the fumaroles generally show compositions suggesting more than 30% lakewater in the thermal fluid. The Longonot crater fumaroles (F23-25) on the other hand imply little or no lakewater at depth, while the fumarole on the southern slopes of the volcano (F26) and those of the eastern part of the valley beyond, Mt. Margaret (F27) and Kedong (F29) suggest that no lakewater reaches these areas.

The Suswa area has four different zones: caldera rim, caldera floor, ring graben and central island, and this zonation is partly reflected in the condensate stable isotope results (Figure 5.9). In general only samples from the ring graben and central island show evidence of lakewater content, with F8 and F14 showing evidence of steam heating. A small hot spring (56°C) the ring graben was recently discovered (M C G Clarke, pers. comm.) which yielded a result of -25%  $\delta^2$ H, -4.5%  $\delta^{18}$ O. This composition probably represents the residual water remaining after the steam heating responsible for F8 and F14, and implies that local rainfall on Suswa meets ascending steam as it percolates downwards. Caldera rim and floor samples are general depleted and are probably the results of local dilution processes and/or (especially in the case of the most depleted samples) condensation processes; it is known from gas analyses (Section 5.6) that at least some of the rim fumaroles contain a component of air.

The fumarole data have been added to the contour map of lakewater dilution based on well water analyses (Figure 5.7). The fumarole data suffer some disadvantages (assumptions of origin, probable large variations in depth and tortuosity of routes to the surface) but by and large provide a plausible picture of southward flow from Lake Naivasha, perhaps largely confined in width to the E. Olkaria-Domes area but large enough in volume to form up to 30% of the water beneath parts of Suswa. The fumaroles of the Suswa caldera floor and rim are on the direct path of this supposed flow to the south, yet show few signs of direct derivation from the flow. Either the steam has been much modified by dilution and/or condensation as discussed above, or perhaps less likely, a strong flow of Rift-wall water is entering the system from the west.

Owing to the lack of opportunities to sample water or steam south of Suswa it is impossible to say how far towards Lake Magadi the influence of Naivasha water may extend. Inasmuch as 30% lakewater could be present 30 km south of Naivasha it may be assumed that recharge from the Rift walls will have diluted lakewater beyond recognition at perhaps 50 km south of the lake, so that it would be impossible to identify the influence of Naivasha water on Lake Magadi, some 100 km away.

In summary, it has been demonstrated that most fumarole isotope ratios can be explained by production of steam (suitably modified in certain cases) from a mixing series between Rift-wall meteoric water and evaporated water from Lake Naivasha. No evidence of any deeper reservoir of singular composition has been seen, and it appears that oxygen shifting of the dimensions commonly seen in other geothermal systems does not exist. It should be remembered that  $\delta^{18}O$  shifting is dependent on a combination of residence time, initial rock and water  $\delta^{18}O$  values and the porosity of the system(s). Not enough is yet known about rock  $\delta^{18}O$  ratios to comment on the rather low  $\delta^{18}O$  shifts.

The conclusions of this report regarding the significance of fumarole

isotopes are broadly similar to those of Armannsson (1987b) in that he proposed mixing between unmodified Rift-wall water and a deep thermal water of an evaporated origin. Isotope data reported here (Section 6.2) have shown that Olkaria must be considered to be part of the general hydrothermal system in the area, and that Lake Naivasha is therefore the source of this evaporated water.

5.3.5 Surface, Thermal and Non Thermal Waters: Nakuru to Silale.

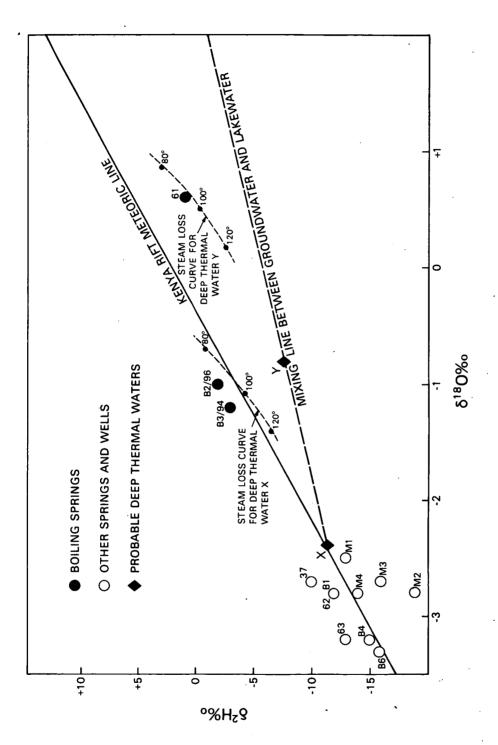
Various thermal and associated waters were sampled from the Nakuru area to a point some 170 km further north near the Silale volcanic centre. Stable isotope results are given in Tables 5.1 and 5.5 and are shown in Figures 5.4c and 5.4d.

As discussed in the previous section, there appears to be comparatively little outflow from the almost closed basin of Lake Nakuru. Between this lake and Lake Bogoria to the north, groundwater stable isotope values are similar to those from the valley floor further south and average -16%  $\delta^2$ H, -2.9%  $\delta^{18}$ O. Despite the fact that some of these waters are slightly thermal (up to 43°C, Figure 5.4a) they probably all represent unmodified Rift-floor rainfall with the thermal waters similar in provenance to the Kariandusi warm spring (35).

At Lake Bogoria itself a wide variation in stable isotopes is seen, ranging from unmodified Rift-floor recharge through boiling springs to highly evaporated lakewater. Figure 5.10 shows the various waters plotted on a delta-diagram. Non-thermal or slightly thermal waters cluster round the local Rift meteoric line at about -13%  $\delta^2 H$ , -2.8%  $\delta^{10}$ 0 and are presumably derived from local recharge in the hills around the lake, The three boiling springs sampled have rather heavier compositions, whereas the lakewater itself is extremely enriched in heavy isotopes due to the large amount of evaporation taking place from the closed basin.

It was suggested by Glover (1972) that slightly thermal water underlying the general area reacts both with ascending steam and with lakewater, while Geotermica Italiana (1987) postulated a ternary mixing model involving local groundwater, thermal water and lakewater. The few data reported here do not support the steam heating model, but neither do they prove the ternary mixing Although the three boiling springs do not lie directly on a dilution between the regional cool springs and the extremely evaporated lakewater, their position is consistent with steam loss from points along this line (Figure 5.10). To this extent the contention that lakewater is involved is likely to be correct (and indeed the situation of the boiling springs on the lakeshore makes this very likely) but there is no evidence that steam with a different isotopic composition is playing a part in the It appears from the isotopic evidence that regional shallow groundwater could be suitable as a source for the thermal fluid, and that the somewhat enriched isotopic compositions seen in the boiling springs are due more to steam separation than to a lakewater contribution. isotopic evidence from these results for the slightly heavier thermal water invoked by Geotermica Italiana (1987), which could probably only come from a source like Lake Baringo. While subsurface flow counter to the general dip of the Rift floor to the north in this area cannot be ruled out, it is This is not to rule out the possibility of the boiling springs being the product of a complex mixing process between shallow groundwater, thermally modified groundwater and lakewater - Section 5.2.2.

Lake Baringo is a 'freshwater' lake which in view of the lack of surface



Delta-diagram of stable isotope data from groundwaters, thermal waters and lakewater of the Lake Bogoria region.

Figure 5.10

outflow must have a considerable subsurface egress. In this respect it may be compared to Lake Naivasha, though unlike that lake outflow is likely to be restricted to a northerly direction. Only two sites were sampled at the lake - a boiling spring on the central, remnant volcanic cone island of Ol Kokwe, The results are shown on a delta-diagram in and the lakewater itself. Figure 5.11. It can be seen that the lakewater is highly evaporated, to a much lesser extent than the stagnant Lake Bogoria. The boiling spring on the central island lies on a direct dilution line between the local shallow groundwater (presumed to be similar to that of the Bogoria area) the lakewater, and might therefore be assumed to be the product of heating a mixture of both waters by steam. However as demonstrated by the results considered in Section 5.2.2 (and pointed out by Glover, 1972), the boiling spring contains a much higher TDS content than the lakewater and cannot therefore be the result of steam heating of lakewater. In spite of this it seems clear that the boiling spring is related to lakewater in some way: the isotopic content of the spring water is too enriched to be simply the result of steam loss from thermal water derived from shallow Rift-floor recharge. It appears that any mixing between lakewater and shallow groundwater must take place in the deep geothermal system, with the upflow into the central island being largely unaffected by the lakewater, however unlikely this may seem at first sight.

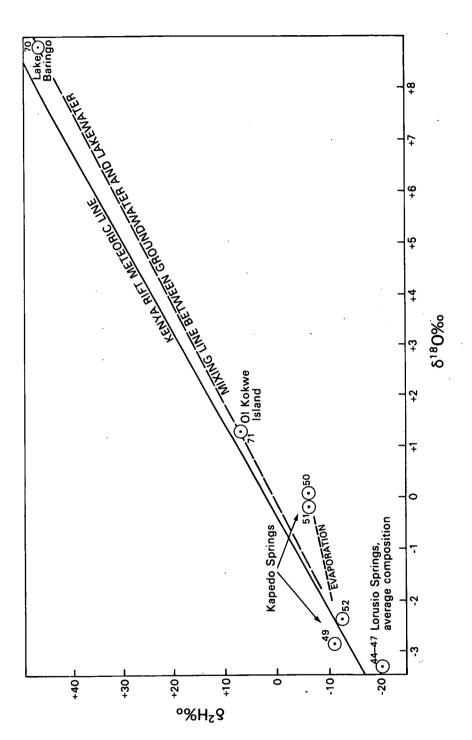
Subsurface discharge from Lake Baringo to the north should be detectable in wells, springs and perhaps fumaroles north of the lake, though only sites at Kapedo and Lorusio were sampled. These sites are some 50 and 60 km away respectively, and by analogy to the Naivasha outflow little evidence of lakewater would be likely to remain. Although two of the Kapedo group of springs show enriched isotope values (Figure 5.11) these are not on the dilution line between presumed local groundwater and lakewater, and instead are more likely to represent evaporative enrichment from the local groundwater.

The Lorusio springs are hotter than the Kapedo springs, and the average isotopic composition is shown in the delta-diagram in Figure 5.11. It is apparent that it is slightly lighter than any of the Kapedo group and may therefore be derived more from the Rift wall than the floor. Though the two groups of springs are relatively close to each other it is unlikely that Kapedo is diluted Lorusio water; not only is it difficult to see what the positive end member could be, but it would also imply a southerly flow, which is contrary to the general flow direction in this part of the Rift. On these grounds therefore it is considered that the two groups are unrelated manifestations.

# 5.4 Stable isotopes - carbon

Differences in the  $^{13}\text{C}/^{12}\text{C}$  ratio relative to that of the Pee Dee Belemnite (PDB) zero standard were measured on dissolved inorganic carbon (DIC) precipitated from water as  $\text{BaCO}_3$ , or directly on  $\text{CO}_2$  gas. Results are reported in Table 5.7.

Most samples were collected from the Suswa-Nakuru sector of the Rift and the distribution of sampling points is shown in Figure 5.1f). In this area quite a large variation in  $\delta^{13}$ C DIC is seen, ranging from around 0 to -16.5%. The isotopic value of DIC depends primarily on the values of soil CO<sub>2</sub>, rock carbonate, and amount and temperature of water-rock contact. The interpretation of  $\delta^{13}$ C DIC can therefore be complicated in areas such as the Rift where crustal CO<sub>2</sub> is present in considerable amounts (Bailey 1980).



Delta-diagram of stable isotope data from thermal waters and lakewater of the Lake Baringo region.

Figure 5.11

Table 5.7 Carbon stable isotope data for Rift Valley water and gas samples.

| Site No. | Site Name                | δ <sup>13C</sup> DIC | δ <sup>13</sup> CCO <sub>2</sub> | δ <sup>180</sup> C0 <sub>2</sub> |
|----------|--------------------------|----------------------|----------------------------------|----------------------------------|
|          |                          | 100                  | PDB                              | % SMOW                           |
| 25       | Viinha DVA               | 7 4                  |                                  |                                  |
| 25<br>26 | Kijabe RVA<br>Kijabe Spr | - 7.4<br>-12.6       |                                  |                                  |
| 26<br>28 | Mayer's Fm               | -12.6<br>-16.5       |                                  |                                  |
| 26<br>29 | Mt Margaret*             | -10.5                | -1.7                             | +34.4                            |
| 31       | Akira H-1*               |                      | -1.7<br>-2.1                     | +32.8                            |
| 35       | Kariandusi Spr           | - 8.0                | -2.1                             | +32.0                            |
| 53       | Bala Springs             | - 0.0<br>- 1.7       |                                  |                                  |
| 57       | Bala Springs             | - 2.3                |                                  |                                  |
| 74       | Magadi NW                | + 0.9                | •                                |                                  |
| 75<br>75 | Oltopesi                 | - 7.4                |                                  |                                  |
| 81       | C567                     | - 0.4                |                                  |                                  |
| 82       | C4178                    | -13.5                |                                  |                                  |
| 92       | Kanyamwi Fm              | - 2.5                |                                  |                                  |
| 96       | Kinangop P65             | -12.0                |                                  |                                  |
| 100      | C1404                    | -10.6                |                                  |                                  |
| 104      | Hell's Gate seep 2       | -11.0                |                                  |                                  |
| 110      | Olkaria OW2              | -10.2                | -2.7                             | +41.9                            |
| 111      | Olkaria OW26             | - 4.8                | -2.4                             | +42.5                            |
| 112      | Olkaria OW22             | - 7.5                |                                  |                                  |
| 114      | 01karia OW23             | - 5.1                |                                  |                                  |
| 115      | 01karia OW21             | - 7.1                |                                  |                                  |
| 116      | 01karia OW5              | -14.6                |                                  |                                  |
| 118      | Nakuru No. 7 (Lanet)     | - 8.7                |                                  |                                  |
| 119      | Eburru EF-2              |                      | -2.3                             | +36.3                            |
| 121      | C431                     | - 0.5                |                                  |                                  |
| 123      | W Olkaria fumarole       |                      | -2.8                             | +37.2                            |
| 124      | Soysambu DEL             | - 2.7                | -6.6                             | +37.1                            |
| 125      | C1990                    | 0.0                  |                                  |                                  |
| 127      | Domes F-15*              |                      | -3.0                             | +35.7                            |
| 128      | Longonot F-23            |                      | -3.5                             | +29.5                            |
| UNDP 51  | Longonot F-23            |                      | -4.4                             | +29.5                            |
| UNDP 44  | Suswa F-28               |                      | -3.7                             | +36.6                            |
| UNDP 43  | Suswa F-12               |                      | -3.2                             | +37.8                            |
|          |                          |                      |                                  |                                  |

 $C_{DIC}$  = dissolved inorganic carbon C and  $O_{CO_2}$  = carbon dioxide

<sup>\* =</sup> samples collected by UNDP

In Section 5.5 two possible rock carbonate values are considered for modelling purposes, with a value of -5% being chosen as the more likely value owing to the presence of carbonatitic volcanism in the Rift. carbonatite samples from the Homa Bay area to the west of the Rift had  $\delta^{13}$ C values of -3.0. -4.2 and -8.2% respectively, so a figure of -5% is a Assuming soil zone carbon dioxide to have a value of reasonable compromise. about -26%, a minimum  $\delta^{13}$ C value after stoichiometric dissolution would be around -15.5%. One sample, from Mayer's Farm (28) is close to this value at -16.5%, which tends to confirm the young age of this water. Other samples indicating only small amounts of post-dissolution 13C exchange are seen on the eastern flanks of the Rift (Kijabe warm spring, Kinangop P65 - sites 27 and 96) or in wells which appear to derive their water from the flanks, such as Ndabibi (100) in the west and Naivasha C4178 (82) in the east. Slightly heavier  $\delta^{13}C$  DIC values are seen at lower altitudes, perhaps because the waters are slightly warmer and able to exchange 13C more readily (though the Kijabe warm spring on the Rift flank (26) does not show such exchange while the RVA well (25), which is cooler, does).

All these waters could be the product of dissolution of rock carbonate by soil-derived  $CO_2$  followed by isotope exchange or incongruent solution. Other Rift waters are significantly heavier in  $\delta^{13}C$  DIC. In the case of a site like C567 (81) this is attributed to the high proportion of lakewater present in the well:  $\delta^{13}C$  in lakewater tends to become heavier with the loss of CO<sub>2</sub> accompanying evaporation, which can be seen from Table 5.15 to have caused calcite to rise to saturation level. This may also be the explanation for the positive  $\delta^{13}$ C DIC from the Magadi N.W. lagoon springs (74, Section For sites like the 'badlands' wells (121,124 and 125) and the Bala springs of the Homa Bay area (53 and 57) magmatic CO2 of about -3% is probably playing an important role in the carbon isotope systematics, tending to drive  $\delta^{13}C$  DIC towards zero or even positive values because of the positive CO2-DIC fractionation at lower temperatures. In the case of site 124, where both CO and DIC were measured, the amount of fractionation (3.9%) was exactly as predicted for the sampling temperature (Table 5.8). Site 125 appears to posess the greatest contribution from magmatic CO2 of the three 'Badlands' wells sampled.

At Olkaria, the only other location where both  $\delta^{13}C$  CO<sub>2</sub> and  $\delta^{13}C$  DIC were measured, equilibrium between the two phases was not well established according to the calculated separation temperatures (Table 5.8). This may be because of insufficient time for re-equilibration to occur between reservoir and wellhead, though neither OW2 or OW26 appear to be in equilibrium at reservoir temperatures (Section 6).

Carbon dioxide in the Suswa-Nakuru part of the Rift has a  $\delta^{13}C$  of -3% with a standard deviation of 0.7. These may be typical volcanogenic values, but are not always associated with volcanic centres; cold  $CO_2$  'mofettes' are known from the Rift and beyond - for example two wells at Meru, east of Mt. Kenya, each gave a  $\delta^{13}C$  value of -3.5%. This tends to confirm the idea of a pervasive  $CO_2$  flux having a deep crustal origin over a wide area (Bailey, 1980), and indicates that a  $\delta^{13}C$  of around -3% is not an infallible indicator of thermal activity. One methane-containing sample (from Eburru) was analysed for its  $\delta^{13}C$  content - see Section 5.7.3.

The carbon stable isotope results can be summarised as follows. They provide a measure of the approach to equilibrium, if any, of DIC and rock carbonate, which can be broadly related to a combination of residence time and temperature, and which is essential for radiocarbon modelling purposes. They discriminate between 'normal' waters and those being affected by injection of

Radiocarbon uncorrected and WATEQF-ISOTOP modelled Rift Valley groundwater ages, with equilibrium  $\delta^{13} \text{C}$  CO2 values.

# 14C CORRECTED AGES IN YEARS

| $\delta^{13}C_{r} = 0.6^{13}C_{r} = -5$       | $8 = IHd$        | . †   | 16405 8249 | 1     | MODERN | 1     | ı<br>! | 1    | ļ .  | 1     | 1            | MODERN | MODERN | MODERN |       | 1     |      | 1    | ı    | 1    | 1     | MODERN     | į.   | MODERN     |      | = dissolved inorganic carbon | measured CO <sub>2</sub> value | calculated equilibrium CO <sub>2</sub> value | rock carbonate value |    |
|---|------------------|-------|------------|-------|--------|-------|--------|------|------|-------|--------------|--------|--------|--------|-------|-------|------|------|------|------|-------|------------|------|------------|------|------------------------------|--------------------------------|--|----------------------|----|
| $\delta^{13}C_{r} = 0  \delta^{13}C_{r} = -5$ | $$ $pH_{I} = .5$ | 1     | 9136 4823  | 1     | MODERN | ſ     | 1      | i i  | . 1  | ı     | ı            | MODERN | MODERN | MODERN | ı     | i     |      | ı    | 1    | 1    |       | 700 MODERN | ı    | 26190 8388 |      |                              | <b>11</b>                      | II   | II                   | -1 |
| 813C <sub>CO2</sub> eq                        |                  | -18.2 | -14.2      | -18.8 | -23.7  | -15.9 | -6.2   | 9.9- | -8.2 | -16.5 | -8.9-        | -20.9  | -8.9   | -16.6  | -17.6 | -9.7  | -4.1 | 6.9- | -4.5 | -6.5 | -14.0 | -14.8      | -6.1 | 9.9-       | -6.4 |                              |                                |  |                      |    |
| 813CCO2                                       | · °/oo PDB       | 1     | ı          | i     | ı      | 1     | 1      | 1    | ı    | ı     | ı            | 1      | ı      | ı      | ı     | -2.7  | -2.4 | i    | I    | ı    | i     | t          | 1    | 9.9-       |      |                              |                                |  | -                    |    |
| 813CDIC                                       |                  | -12.6 | -7.4       | -12.6 | -16.5  | -8.0  | -1.7   | -2.3 | 6.0+ | -7.4  | <b>4.</b> 0- | -13.5  | -2.5   | -10.6  | -11.0 | -10.2 | -4.8 | -7.5 | -5.1 | -7.1 | -14.6 | -8.7       | -0.5 | -2.7       | 0.0  |                              | ern carbon                     |  | n system pH          |    |
| Unc. Age                                      | Yrs              | i     | 22500      | ı     | 2060   | ı     | ı      | 1    | ı    | ı     | 1            | 006    | 3980   | 1450   | 1     | 1     | ı    | 1    | ı    | ı    | ı     | 200        | ı    | 26190      |      | activity                     | percent modern                 | uncorrected                                  | initial open system  |    |
| A14C  | PMC              |       | 6.2        | ı     | 9.87   | 1     | 1      | ı    | ı    | ı     | 1            | 91.4   | 62.8   | .0.98  | 1     | ı     | ì    | ı    | l    | ı    | ı     | 94.7       | 1    | 4.0        | 1    | A = a                        | PMC = F                        | Unc = u                                      | $pH_{I} = i$         |    |
| SITE  |                  | 16    | 25         | 27    | 28     | 35    | 53     | 99   | 74   | 7.5   | 81           | 82     | 92     | 100    | 104   | 110   | 111  | 112  | 114  | 115  | 116   | 118        | 121  | 124        | 125  |                              |                                | •  |                      |    |

crustal  $CO_2$  or evaporation. Fractionations between the various carbon species are potential geothermometers, but their use appears to be rather circumscribed.

# 5.5 Radioisotopes

### 5.5.1 Carbon-14

The radiocarbon content of groundwater was measured at 7 representative sites (Figure 5.1g). It was considered that an indication of groundwater age would be of use as a check on the flow rates deduced from physical modelling of groundwater movement. The uncorrected ages shown on Figure 5.1g are calculated on the basis of simple  $^{14}\text{C}$  decay and take no account of addition of 'dead' carbon to the system. In general this addition comes from the dissolution of 'dead' rock carbonate phases by 'active' carbon dioxide produced in the soil zone; if rock and dissolved inorganic carbon  $\delta^{13}\text{C}$  values are known or assumed, corrections to the groundwater 'age' can be attempted. Several correcting methods are available - in this case WATEQF-ISOTOP was used.

Table 5.8 shows the results of running WATEQF-ISOTOP with two initial pH values, 5 and 8, and using two different rock carbonate  $\delta^{13}$ C values. In each case soil zone CO2 is assumed to have been -25% PDB. Normally rock carbonate is assumed to be marine-derived and to have a  $\delta^{13}C$  of about 0%. This was used as a starting point to run the ISOTOP model, but in the Rift Valley a marine derivation for carbonate phases is unlikely. In view of the carbonatitic volcanism associated with the Rift, the model was run with a rock carbonate value of -5% PDB, a typical carbonatite value. In most cases the resulting ages are modern, irrespective of starting conditions. exceptions to this are from the DEL well on the Soysambu Estate and the Rift Valley Academy (124 and 25). Both these wells have a high bicarbonate content, especially the DEL well, and it is probable that the apparent ages are an artefact caused by the addition to the carbonate system of large amounts of crustal CO2. Dissolved CO2 from the DEL well was measured for 13C content and the value, -6.6% PDB, was in exact agreement with the ISOTOP calculated equilibrium for the measured DIC  $\delta^{13}$ C of -2.7% PDB. In reality these two waters are likely to be very much younger than the modelled ages, and by analogy with wells in similar positions within the Rift, e.g. Ndabibi C1404 (100) and Mayers Farm (28), are probably largely modern.

### 5.5.2 Tritium

The tritium content of representative groundwater was determined at Rift Valley sites (Table 5.9). In all cases except Lanet (Nakuru No. 7 W.S. well, site 118) values were well below 1 TR, suggesting that there is a negligible contribution from thermonuclear tritium and that accordingly the waters must be at least 25 years old. The slightly higher <sup>3</sup>H figure for Lanet can be compared with the <sup>14</sup>C value which gave the youngest uncorrected age of any of the Rift samples.

# 5.5.3 Implications of the radioisotope data

Sites where radiocarbon and/or tritium were measured were selected on the basis of their value in identifying groundwater flow paths. Thus radiocarbon samples were taken in the western side of the Rift floor at the Ndabibi and Soysambu estates (100 and 124), the central part of the Rift at Naivasha C4178 and Nakuru No. 7 (82 and 118) and the eastern flanks at Mayers Farm, Kijabe RVA and Kanyamwi Farm (28, 25 and 92). Mayers Farm and Kijabe RVA

Table 5.9 Tritium content of groundwaters from the Suswa-Nakuru sector of the Rift Valley.

| Site No. | Site Name           | Temp, <sup>O</sup> C | рН    | TR    | ± σ  |
|----------|---------------------|----------------------|-------|-------|------|
| 25       | Kijabe RVA          | 35                   | 7.95  | 0.09  | 0.14 |
| 28       | Mayer's Fm          | 28                   | 7.90  | 0.00  | 0.17 |
| 35       | Kariandusi          | 39                   | 6.6   | 0.34  | 0.16 |
| 82       | Naivasha C4178      | 20                   | 7.45  | 0.05  | 0.15 |
| 92       | Kanyamwi Fm         | 24                   | 7.30  | 0.34  | 0.16 |
| 96       | Kinangop P65        | 23                   | 7.00  | -0.01 | 0.14 |
| 100      | Ndabibi C1404       | 26                   | 6.95  | 0.34  | 0.17 |
| 101      | Kokot, Maiella      | -                    | 7.65  | 0.42  | 0.15 |
| 110      | Olkaria OW2         | 34*                  | 6.23* | 0.19  | 0.14 |
| 111      | Oklaria OW26        | 34*                  | 6.05* | 0.27  | 0.16 |
| 118      | Nakuru No. 7, Lanet | 28                   | 7.00  | 1.64  | 0.16 |
| 124      | Soysambu DEL        | 32                   | 6.40  | 0.15  | 0.15 |

TR = tritium ratio (1 TR  $\equiv$  1 atom of  $^{3}$ H in  $10^{18}$  atoms  $^{1}$ H)

<sup>\* =</sup> cooled water phase from wellhead separator

might particularly be expected to be associated with deep seated faults, and Nakuru No. 7 is situated on a prominent N-S lineation on the valley floor, but none of these sites indicates long residence times (except perhaps for a small component) once radiocarbon corrections have been made. Conversely, tritium measurements show that in places where rapid flow might have been expected, especially perhaps at the Kokot water collection gallery (101), water was of pre-thermonuclear age.

The radioisotope measurements therefore suggest that there are no slow, deeply circulating groundwater flow paths playing a significant role in the hydrogeology of this part of the Rift Valley. A small contribution from deeper groundwater cannot however be entirely ruled out by the radioisotope evidence.

### 5.6 Gases

# 5.6.1 CO<sub>2</sub> and permanent gases (excluding inert gases)

During the investigations in the Rift Valley, gas samples were collected for  $\delta^{13}C$  analysis. Most of these samples were taken from fumaroles and wells between Suswa and Nakuru, though samples were also drawn from gaseous springs at Bala (on the Lake Victoria arm of the Rift), Lorusio (in the Rift Valley north of Lake Baringo), and the Meru area ESE of Mt. Kenya. While the isotopic results are discussed elsewhere in this report, the opportunity to carry out permanent gas analysis was taken and the results are presented in Table 5.10.

Excluding gases derived from the atmosphere, either originally or by entrainment or contamination, crustally-derived CO2 dominates all samples, usually with CH4 in second place, albeit at a much lower level. and/or He are present, methane lies in third place. The low molecular weight gases diffuse very easily; the detection of both H2 and He is taken as evidence of close proximity to a strong upflow, as at Eburru and Longonot, where the volcanic origins of the gas are confirmed by the helium isotope In the case of the Lorusio spring only H2 is present; as a very similar H<sub>2</sub>/CO<sub>2</sub> ratio to those of Eburru and Longonot is observed it may be that the springs are close to an upflow, though at a distance which allows The <sup>3</sup>He/<sup>4</sup>He ratio was not measured for Lorusio and escape of helium. therefore cannot offer confirmation. At Bala He rather than H2 was present the He R/Ra value (next section) was not elevated much above the atmospheric level though total He was very high.

In the absence of  $\rm H_2$ , He and  $\rm H_2S$  (which was not measured) methane may be the best evidence of proximity to upflow (Armannsson, 1987a) and, by implication, deep fluid temperature. The results support this in a qualitative way, with for example Mt. Margaret (29), a relatively cool thermal area, having a much lower  $\rm CH_4/CO_2$  ratio than Eburru (119), which most other data suggest is a high temperature area. The shortcomings of  $\rm CH_4/CO_2$  as a geothermometer are however apparent (Section 5.7.2).

The ratio  $C_2H_6/CH_4$  may be an index of a lakewater contribution, as discussed elsewhere in this report with relevance to the Olkaria area. In the Naivasha area the decline in  $C_2H_6/CH_4$  is roughly in the order northern East Olkaria > West Olkaria > Domes > southern East Olkaria > Eburru > Longonot > Suswa, i.e. fairly consistent with increasing distance from the lake. The high ratio for the DEL well water (site 124) is likely to be an artefact of measurement at low concentrations, but Lorusio and Bala have apparently genuinely high  $C_2H_6/CH_4$  ratios and it may be worth noting that Lorusio has

Composition of fumarole, well and spring gas samples, excluding inert gases.

|                            |                      | 8             | as compc                             | sition   | :<br>:<br>:<br>: | !            | ratios  | ios by weig       | ght   |
|----------------------------|----------------------|---------------|--------------------------------------|----------|------------------|--------------|---------|-------------------|---|
| SITE NO                    | CO <sub>2</sub>      | %<br>%        | C <sub>2</sub> H <sub>6</sub><br>vpm | H<br>%   | He %             | æ ₩          | CH4/CO2 | $H_2/CO_2$ x 10-3 | C <sub>2</sub> H <sub>6</sub> / CH <sub>4</sub> |
| 29/F-27<br>31/H-1<br>44-47 | 57.7<br>27.9<br>66.6 | 0.092         | 7.5                                  | nd<br>nd | חק<br>חק         | 42.2 71.9    | 0.58    | 0                 | 10<br>7.0                                       |
| 53-54                      | 44.0                 | 0.32          | . * .                                | g pr     | 0.93             | 54.8         | 2.6     | )<br>• I          | <br>  |
| 110                        | 40.3                 | 0.6/          | 9.5                                  | nd<br>nd | 말                | 59.0<br>51.8 | 0 +     | l i               | 0.6<br>6.6                                      |
| 119                        | 78.9                 | 4.6           | 5.0                                  | 1.7      | 0.5              | 14.3         | 21.     | 0.98              | 0.20  |
| 123<br>124                 | 74.4                 | 0.37          | 0.5                                  | 담임       | 말                | 25.3<br>25.7 | 0.0     | 1 1               | 5.b<br>94.                                      |
| 1:26<br>127                | 10.2                 | 3 vpm<br>0.13 | nd<br>2.5                            | nd       | nd               | 89.8         | 0.01    | 1 1               | 3,6   |
| 127/F15<br>128             | 12.6                 | 0.06          | 0.0                                  | 멸.       | ng c             | 87.4         | 7.7     | , ,               | 3.1   |
| 128/F-23                   | 44.4                 | 0.30          | 0.5                                  | 06.0     | 0.34             | 54.0         | 2.5     | 0.92              | 0.31  |
| F-7                        | 24.6                 | 0.45          | 0.5                                  | pu       | pu               | 75.0         | 6.7     | 1                 | 0.21  |
| F-12                       | 25.9                 | 0.085         | pu                                   | nd       | pu               | 74.0         | 1.2     | 1                 | 1   |
| F-28                       | 0.99                 | 0.41          | <del>.</del> 0                       | pq       | pq               | 33.6         | 2.3     | 1                 | 0.46  |
| K-1                        | 35.8                 | 0.010         | pu                                   | nd       | pu               | 64.2         | 0.10    | 1                 | 1   |
| K-2                        | 39.5                 | 12 vpm        | pq                                   | pu       | pu               | 8:09         | 0.01    | t                 | ì   |

<sup>\*</sup> Sample also contained 3 vpm C<sub>3</sub>H<sub>8</sub>

R = residual gases including  $N_2$ , Ar,  $H_2S$  and possibly  $O_2$  nd = not detected Samples with F, H and K prefixes collected by Dr H Armannsson of the UNDP. been believed to derive its water ultimately from Lake Baringo (though see Sections 5.2.2 and 5.3.5), while Bala is close to the edge of Lake Victoria. By contrast the Meru (Chogoria) springs which cannot be supplied by lakewater have very low  $CH_4$  values and undetectable  $C_2H_6$ .

# 5.6.2 Helium and Inert Gases

Helium isotope ratios

The ratio <sup>3</sup>He/<sup>4</sup>He was measured for 13 samples from the Suswa-Nakuru sector of the Rift and on one sample from the Bala springs on the edge of Lake Victoria. This latter sampling point had been chosen because a gas sample collected in 1985 indicated a high total helium content. Results are reported (Figure 5.1g, Table 5.11) in the conventional form of R/Ra, where R denotes the <sup>3</sup>He/<sup>4</sup>He ratio of the sample and Ra the <sup>3</sup>He/<sup>4</sup>He of air which effectively remains constant. Also shown in Table 5.11 are the He and Ne contents of each sample: He/Ne is a sensitive indicator of air contamination because the level of crustal neon is very much lower than that of air. Providing the amount of air contamination is small, a correction can be made to the original R/Ra value (Table 5.11). This was first proposed by Craig et al (1977) and takes the form:

$$(R/Ra)c = \frac{(R/Ra)(x-1)}{x-1}$$

where

 $x = \frac{\text{He/Ne(sample)}}{\text{He/Ne(air)}} \frac{\text{BNe}}{\text{BNe}}$ 

(R/Ra)c = corrected R/Ra

BNe and BHe = Solubility coefficients for appropriate temperature

The results show that two samples possess helium contents essentially derived from air (Ndabibi C1404 and Nakuru No. 7, sites 100 and 118). While sampling procedures cannot be ruled out as causing this, other samples appear to have been satisfactorily collected using identical techniques. If accepted as genuine, the results tend to support the radioisotopic indications that these samples are very young waters which have largely conserved atmospheric inert gas ratios.

The remaining samples mostly have R/Ra values >1, indicating the presence of excess mantle helium to a greater or lesser extent. Samples collected as gas from fumaroles and geothermal wells tend to have the highest levels (corrected R/Ra values of 5.6-6.7 for Eburru, Longonot and Olkaria) but one water well (Soysambu DEL site 124) possesses a value in this range. Conversely two fumaroles, Suswa F3 and Domes F15 (126 and 127), have lower R/Ra values, though gas analyses suggest that these fumaroles have substantial amounts of entrained atmospheric gases which may be diluting any <sup>3</sup>He component.

The main significance of <sup>3</sup>He/<sup>4</sup>He ratios within this sector of the Rift is that they do not show much evidence of transport of mantle helium up the deep faults presumed to exist at the sides of the Rift; for example Kanyamwi Farm well C570 and Kijabe Warm Spring (92 and 27) have values close to atmospheric, though the Kariandusi warm spring (35) does have an elevated level (but see next section for further comments on Kijabe). Instead the high levels are all associated with volcanic centres except for the Soysambu

|                                | Ne content<br>P/cm <sup>3</sup><br>STP/g | 4.52 × 10 8<br>1.45 × 10 7<br>2.29 × 10 7<br>3.03 × 10 7<br>1.59 × 10 7<br>1.59 × 10 7<br>1.59 × 10 7<br>1.59 × 10 7<br>1.26 × 10 6<br>3.98 × 10 6<br>3.98 × 10 6<br>3.98 × 10 6  |
|--------------------------------|--|---|
|                                | He content cm³ ST                        | 5.43 × 10 <sup>-8</sup> 2.86 × 10 <sup>-7</sup> 1.08 × 10 <sup>-7</sup> 2.26 × 10 <sup>-8</sup> 3.48 × 10 <sup>-8</sup> 1.22 × 10 <sup>-8</sup> 2.94 × 10 <sup>-6</sup> 5.16 × 10 <sup>-6</sup> 5.96 × 10 <sup>-6</sup> 5.96 × 10 <sup>-6</sup> |
| es of the                      | (R/Ra)c                                  | 0.896<br>2.947<br>1.434<br>1.323<br>0.871<br>5.694<br>5.694<br>5.623<br>6.262<br>6.521<br>6.556   |
| s and gases                    | ×  | 5<br>85<br>85<br>85<br>1.6<br>383<br>429<br>0.9<br>14<br>17<br>32   |
| ratios in groundwaters         | R/Ra                                     | 0.928<br>1.359<br>1.446<br>1.281<br>0.938<br>5.682<br>5.711<br>1.005<br>6.243<br>6.156<br>6.156<br>6.482  |
| ratios in                      | Sample<br>Type                           | ZZZZGUZGUZGGG   |
| Helium isotope<br>Rift Valley. | Site Name                                | Kijabe RVA Kariandusi Spr Bala Springs Kanyamwi Fm Ndabibi C1404 Olkaria OW2 Olkaria OW26 Nakuru No. 7, Lanet Eburru EF-2 Olkaria W. field Soysambu DEL Suswa F-3 Domes F-15 Longonot F-23  |
| Table 5.11                     | Site No.                                 | 26<br>35<br>53<br>100<br>110<br>111<br>124<br>126<br>127  |

 $R/Ra = \frac{3H/^4H}{3H/^4H}$  sample (R/Ra)c = R/Ra corrected for air contamination X = correction factor (see text)

G = gas (fumarole or geothermal well)

W = water (well or spring)

(samples measured at the University of Cambridge by Ms E Griesshaber)

DEL well (124), which on various grounds can be linked to outflow from the Eburru centre.

On a wider scale the He isotope ratios indicate an approach to a mid-ocean ridge basalt (MORB) type composition with R/Ra values typically of 8-9. Such values and higher have been measured in Ethiopia and a hot-spot origin attributed to the values in excess of 9 (Craig et al, 1977). The R/Ra values associated with Eburru, Longonot and Olkaria are consistent at around 6, suggesting that they share the same local crustal reservoir; whether or not there is a gradual enrichment northwards along the Rift towards MORB values may be answered by the next phase of the Geothermal Project.

As already mentioned, the total helium content of the Bala spring on the edge of Lake Victoria is very high ( $2.86 \times 10^{-3}$  cc He/cc total gases). The R/Ra value of 1.446 indicates that there has either been some concentration of air-derived inert gases containing minor enrichment in  $^3$ He (and the Ne content is high) or, that any radiogenic ( $^4$ He) and mantle ( $^3$ He) additions are largely balancing out in proportional terms. Similar gas compositions and concentrations are known from southern Africa (K O'Nions, pers. comm.).

### Inert gases

Measurement of concentrations of inert gases were made on seven well waters, two warm spring waters and seven fumaroles. Results are presented in Tables 5.12(a) and (b) as volumes (STP) of gas per volume of water or gas as appropriate and in Table 5.13 as various ratios.

When the dissolved gas results are plotted in the form of argon versus neon content and xenon versus krypton content (Figure 5.12a), it can be seen that the inert gas ratios are wholly consistent with an atmospheric origin and, apart from one sample showing depletion, can be used to attempt estimates of recharge temperature. As with other gases, the amount of each inert gas in solution is controlled by the air temperature at the point of recharge. Providing water does not undergo significant heating below surface, amounts of inert gas in solution should be preserved at the sampling point, enabling calculation of recharge temperature (Mazor, 1977). However, amounts of gas in solution also depend on air pressure, and this will vary with recharge Because in the present case this is not known, a gas ratio rather than volume approach has been used here. Gas partition coefficients (Wilhelm et al., 1977) are independent of pressure and in theory permit calculation of recharge temperatures without knowing initial pressures, which in turn allows some conclusions about recharge altitude to be drawn.

Using neon as a reference, tentative temperatures for argon, krypton and xenon have been calculated (Table 5.12a) for all sites except 124 (DEL), where original gas ratios have been disturbed by the influx of geothermal gases (Table 5.13). As the ratio approach is cruder than the volume method, agreement between the three temperature sets is not good, but when the averaged figures are considered they serve as an indicator of relative if not absolute average recharge heights. Of the five sites giving plausible temperatures (25, 28, 91, 96 and 118), the temperature range is about 7°C. With a maximum temperature lapse rate of 0.6°C per 100 m, this would correspond to an altitude range of the order of 1200 m. Altitudes based on the premise of essentially local recharge to Nakuru No. 7 (118) are shown in Figure 5.13 and suggest that the highest sampling point, Kinangop P65 Intermediate wells obtains its water from an average altitude of 3200 m. obtain water from between 150 to 400 m above the sampling point. The results from Naivasha 4178, Ndabibi C1404 and Kariandusi warm spring cannot be

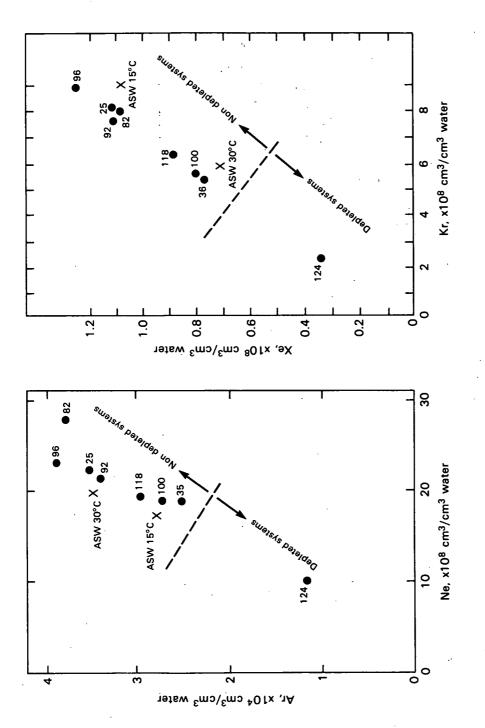
Table 5.12a Inert gas contents (cm $^3$ /cm $^3$  H $_2$ 0 at STP) and calculated recharge temperatures for selected groundwaters.

| Site No. | Site Name<br>Temp Altitude                    | He × 10 <sup>-8</sup> | Ne × 10 <sup>-7</sup> | $\begin{array}{c} \text{Ar} \times 10^{-8} \\ \text{Ar/Ne} \times 10^{-3} \\ \text{t}_{r} \end{array}$ | Kr × 10 <sup>-8</sup><br>Kr/Ne<br>t <sub>r</sub> | Xe x 10 <sup>-8</sup><br>Xe/Ne<br>t <sub>r</sub> |
|----------|---|-----------------------|-----------------------|--|--|--|
| 25       | Kijabe RVA<br>35°C 2500 m                     | 64.3                  | 1.64                  | 2.60<br>1.59<br>21.8   | 5.98<br>0.365<br>16.2                            | 0.86<br>0.053<br>13.7                            |
| 28       | Mayer's Farm<br>28°C 2100 m                   | 3.67                  | 1.47                  | 2.25<br>1.53<br>24.0   | 4.97<br>0.338<br>19.9                            | 0.70<br>0.048<br>17.5                            |
| 35       | Kariandusi Spring<br>39 <sup>0</sup> C 2300 m | 5.47                  | 1.43                  | 1.94<br>1.35<br>>30  | 4.16<br>0.291<br>28.1                            | 0.58<br>0.041<br>24.1                            |
| 82       | Naivasha 4178<br>21°C 1900 m                  | 6.18                  | 2.47                  | 3.38<br>1.37<br>>30  | 7.09<br>0.287<br>>30                             | 0.97<br>0.039<br>25.6                            |
| 92       | Kanyamwi Farm<br>27 <sup>o</sup> C 2300 m     | 5.16                  | 1.64                  | 2.60<br>1.59<br>21.8   | 5.87<br>0.358<br>17.1                            | 0.84<br>0.051<br>14.6                            |
| 96       | Kinangop P65<br>21 <sup>0</sup> C 2600 m      | 5.69                  | 1.67                  | 2.83<br>1.70<br>17.9   | 6.42<br>0.384<br>13.9                            | 0.91<br>0.055<br>12.4                            |
| 100      | Ndabibi C1404<br>21°C 2100 m                  | 3.61                  | 1.47                  | 2.11<br>1.44<br>28.4   | 4.53<br>0.308<br>25.1                            | 0.62<br>0.042<br>22.4                            |
| . 118    | Nakuru No. 7<br>28 <sup>0</sup> C 2000 m      | 3.34                  | 1.53                  | 2.29<br>1.50<br>25.4   | 5.03<br>0.329<br>21.2                            | 0.69<br>0.045<br>19.5                            |
| 124      | Soysambu DEL<br>32°C 1900 m                   | 143                   | 0.87                  | 1.05<br>-<br>-   | 2.12   | 0.30   |

 $t_{\mathbf{r}}$  = calculated recharge temperature,  $^{\mathrm{o}}\mathrm{C}$ 

5.12b Inert gas contents  $(cm^3/cm^3 gas)$  of selected fumaroles.

| Site No. | Site Name     | He × 10 <sup>-5</sup> | Ne x 10 <sup>-7</sup> | Ar × 10 <sup>-4</sup> | Kr × 10 <sup>-8</sup> | Xe × 10 <sup>-8</sup> |
|----------|---------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 53       | Bala Spring   | 1270                  | 3.65                  | 30.9                  | 22.4                  | 3.09                  |
| 110      | Olkaria OW2   | 4.07                  | 0.15                  | 0.10                  | 0.15                  | <del>-</del>          |
| 111      | Olkaria OW26  | 3.07                  | 122                   | 56.4                  | 69.8                  | 7.09                  |
| -119     | Eburru EF-2   | 5.52                  | 0.30                  | 0.35                  | 0.73                  | 0.11                  |
| 123      | Olkaria West  | 2.00                  | 0.21                  | 0.26                  | 0.53                  | 0.10                  |
| 126      | Suswa F-3     | 2.58                  | 74.9                  | 34.5                  | 43.1                  | 3.64                  |
| 127      | Domes F-15    | 2.57                  | 61.8                  | 30.9                  | 35.6                  | 3.27                  |
| 128      | Longonot F-23 | . 0.75                | 28.4                  | 12.0                  | 14.0                  | 1.45                  |



Plots of argon versus neon and xenon versus krypton contents of selected groundwaters in the Suswa-Nakuru (Diagram after air saturated water. sector. ASW Mazor, 1977). Figure 5.12a

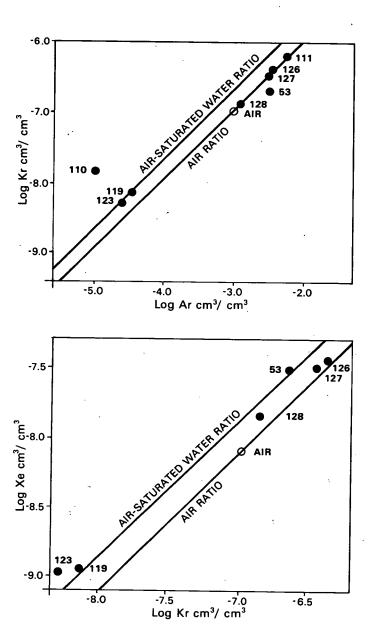


Figure 5.12b Plots of krypton versus argon and xenon versus krypton contents of gases mainly collected from fumaroles.

Table 5.13 Dissolved gas ratios from mass spectrometric measurement of selected groundwaters.

| Site No. | Site Name      | Sample Type | e Type 40Ar/3<br>ratio |          | N <sub>2</sub> / | Ar<br>±  | CO <sub>2</sub><br>ratio | /Ar  |
|----------|----------------|-------------|------------------------|----------|------------------|----------|--------------------------|------|
|          |                |             |                        | <u> </u> |                  | <u> </u> | ; Iatio                  |      |
| 25       | Kijabe RVA     | Water       | 294.1                  | 1.3      | 37.8             | 0.2      | 20.9                     | 1.5  |
| 28       | Mayer's Farm   | Water       | 294.1                  | 1.0      | 39.9             | 0.2      | 97.3                     | 1.3  |
| 35       | Kariandusi Spr | Water       | 295.4                  | 0.5      | 49.8             | 0.7      | 93.3                     | 1.2  |
| 53       | Bala Spring    | Gas         | 846.0                  | 35.3     | 22.5             | 0.7      | 155.0                    | 1.0  |
| 82       | Naivasha C4178 | Water       | 296.4                  | 2.2      | 42.4             | 0.2      | 62.5                     | 1.1  |
| 92       | Kanyamwi Farm  | Water       | 294.9                  | 2.0      | 39.3             | 0.2      | 41.3                     | 1.5  |
| 96       | Kinangop P65   | Water       | 296.8                  | 0.9      | 39.1             | 1.0      | 61:0                     | 3.7  |
| 100      | Ndabibi Cl404  | Water       | 297.6                  | 0.8      | 57.9             | 0.4      | 39.2                     | 0.9  |
| 110      | Olkaria OW2    | Gas         | 304.4                  | 7.7      | 43.2             | 8.2      | 86.0                     | 7.0  |
| 111      | Olkaria OW26   | Gas         | 247.1                  | 21.0     | 66.9             | 4.8      | 60.0                     | 5.0  |
| 118      | Nakuru No. 7   | Water       | 293.7                  | 1.3      | 40.2             | 1.3      | 35.5                     | 0.7  |
| 119      | Eburru EF-2    | Gas         | 303.4                  | 3.5      | 23.2             | 2.0      | 46.0                     | 7.0  |
| 123      | Olkaria West   | Gas         | 261.4                  | 26.5     | 35.2             | 6.4      | 223.0                    | 15.0 |
| 124      | Soysambu DEL   | Water       | 297.0                  | 2.7      | 35.2             | 0.3      | 972.0                    | 87.0 |
| 126      | Suswa F-3      | Gas         | 293.1                  | 2.9      | 87.8             | 2.5      | 11.0                     | 1.0  |
| 127      | Domes F-15     | Gas         | 291.3                  | 0.3      | 88.0             | 0.7      | 16.0                     | 1.0  |
| 128.     | Longonot F-23  | Gas         | 278.7                  | 0.7      | 77.8             | 0.4      | 10.0                     | 1.0  |

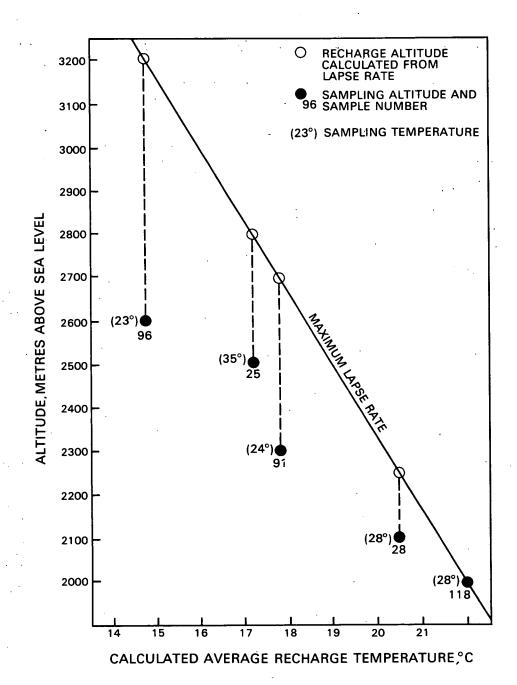


Figure 5.13 Plot of inert gas-derived recharge temperatures versus sampling altitude for selected groundwaters in the Suswa-Nakuru sector compared to temperature lapse rate.

interpreted in the same way. In the case of Kariandusi subsurface heating may have disturbed the ratios of the inert gases, otherwise sampling problems are likely to be responsible for the dubious results.

For free gas samples, plots of Kr content vs Ar content and Xe content versus Kr content are shown in Figure 5.12(b). They indicate that the gases were probably all originally derived from meteoric water, but that contamination has affected some samples (111, 126-128). In the case of OW 26 and F 23 (111, 128) this probably occurred during sampling or storage, but there is other evidence from gas measurements (see above) that the Suswa and Domes fumaroles F-3 and F-15 (126 and 127) may already have had air The Bala sample was collected from a bubbling pool, where it is entrained. sometimes difficult to avoid some air contamination (cf Kariandusi spring, However,  $N_2/Ar$  at Bala is <u>lower</u> than water (Table 13), presumably due to high 40Ar (see below), which indicates that this alone is responsible for the shift from the ASW (air saturated water) line. This is confirmed by the Xe vs Kr plot which shows that the Bala sample is consistent with an ASW The ratio Kr/Xe suggests a recharge temperature of 10°C, and while origin. this ratio seems liable to underestimate temperatures by 10° or so, it does imply that this water has not been subjected to boiling at any stage, and is unlikely to be coooled outflow from a high-temperature geothermal system. This is in agreement with the chemical geothermometers (5.7.1).

The inert gas results also provide other information. They confirm that the Soysambu DEL well (124) has large amounts of helium and carbon dioxide in solution and also indicate that helium is enhanced in the Kijabe RVA well (25). A warm spring near to this particular well had a He/He index close to that of air, so possibly radiogenic He is offsetting a He contribution. However, examination of the AOAr/HA ratio (Table 5.13) indicates that in every case but one the value is comparable to that in air, 295.6 (Nier, 1950), and that therefore there is very little production of the radiogenic AOAr isotope which usually accompanies He production. The exception, Bala (53), is high in AOAr which implies that radiogenic He is offsetting an otherwise high R/Ra value to result in the observed R/Ra of 1.4 (5.6.2).

# 5.6.3 Implications of the gas data

The non-inert gas data in this report are all collected from thermal manifestations and are only interpreted in a qualitative way: presence of He and  $\rm H_2$  is indicative of proximity to an upflow, while the ratio  $\rm C_2H_6/CH_4$  may be a measure of lakewater input to a hydrothermal system. Quantitative interpretation of gas data from the Suswa, Longonot and Domes areas has been provided by Armannsson (1987b)

The inert gas and helium isotope data however have relevance to both thermal and non-thermal hydrogeology. There appears to be little evidence of the enhancement of radiogenic He and Ar isotopes which usually occurs in waters with long residence times. In this respect the data support the conclusion of <sup>14</sup>C measurement. Where high helium is encountered it appears to be due to close association with volcanic centres. There is from the work so far no clear indication that mantle helium is encountered in association with deep faulting. The recharge temperatures gained from consideration of amounts of inert gases in solution show a tendency for recharge to be more local at lower altitudes, the reverse of what might be expected. It is unlikely (at least in the cases where inert gases indicate sensible temperatures) that waters have circulated to great depths and have then cooled again during travel to the surface as this would have upset the inert gas ratios.

Various SiO<sub>2</sub> and alkali cation geothermometers calculated for all Rift Valley water samples.

| NA/K<br>B=0            | 2212114683847723237<br>2009772833387723237<br>300997728333877277   | 330.1<br>450.8<br>185.1 | 512.2<br>153.6<br>52.7<br>281.3<br>325.0  | 9.8891 | 464.9<br>398.3<br>408.2      | 375.6 | 437.0 | 93.6           | 777<br>78.7<br>775.5<br>77.8<br>64.3<br>64.3  |
|------------------------|--|-------------------------|---|--------|------------------------------|-------|-------|----------------|---|
| MGCOR                  | 183.5  | 96.2                    | 82.7<br>155.3<br>88.0<br>75.5             | 190.6  | 139.0<br>53.9<br>55.0        | 117.6 | 181.2 |                | 140.3<br>145.1<br>128.4   |
| CA<br>PACES            | 382.5<br>4286.5<br>4186.0<br>3399.4<br>4123.4<br>4123.4<br>387.8<br>371.1<br>387.8   | 65.8<br>21.1<br>98.9    | 65.0<br>101.1<br>98.6<br>56.7<br>45.5     | 67.2   | 61.8<br>36.2<br>31.7         | 52.5  | 6.09  | 269.9<br>245.8 | 155.4<br>151.2<br>164.3<br>148.2<br>146.1<br>133.3  |
| NA/K/<br>B=1/3         | 199555<br>199555<br>199555<br>1996<br>1996<br>1997<br>1997<br>1997<br>1997<br>1997<br>1997   | 221.0<br>215.9<br>185.7 | 261.9<br>180.3<br>121.6<br>210.3<br>211.5 | 357.4  | 248.6<br>229.3<br>230.1      | 241.2 | 252.1 | 188.0<br>191.2 | 171.2<br>171.8<br>170.2<br>172.0<br>155.2<br>155.0  |
| IN DEG C<br>B=4/3      | 888888937<br>8904448888894<br>8888444888888888888888888  | 115.7<br>50.8<br>147.9  | 118.7<br>175.8<br>142.1<br>123.2          | 110.2  | 109.3<br>97.3<br>94.3        | 137.7 | 129.8 | 401.6<br>364.1 | 344.9<br>345.5<br>347.7<br>350.2<br>275.6<br>251.2  |
| RMOMETERS,<br>LC CRIST | 0807738888888888773897<br>080777877777777777777777777777777777   | 89.5<br>7.9 ·           | -10.4<br>72.7<br>42.2<br>65.5<br>64.5     | 1.8    | 54.1<br>46.0<br>53.2         | 82.9  | 84.7  | 99.6           | 73.6<br>722.1<br>722.1<br>722.1<br>71.4<br>6.3  |
| OTHE<br>CA<br>CHA      | 97.6<br>1001.0<br>1001.0<br>1001.0<br>1003.7<br>1114.4<br>1114.4<br>1111.9<br>1101.9<br>73.3<br>73.3<br>74.7<br>89.2   | 112.4<br>22.5<br>97.7   | 2.6<br>93.8<br>60.1<br>85.8<br>84.7       | 15.9   | 73.2<br>64.2<br>72.2         | 105.1 | 107.1 | 123.7<br>122.1 | 94.7<br>93.1<br>93.1<br>86.7  |
| GE<br>SILI<br>QZ       | 126.8<br>129.9<br>129.9<br>129.9<br>129.9<br>131.9<br>1004.8<br>1004.8<br>1006.0<br>119.3  | 140.0<br>57.0<br>126.9  | 37.6<br>123.4<br>92.5<br>116.2<br>115.2   | 9.05   | 104.7<br>96.4<br>103.7       | 133.6 | 135.3 | 150.0<br>148.6 | 124.2<br>123.1<br>122.8<br>122.7<br>122.7<br>117.0  |
| AMPHS                  | 25.52<br>112.26<br>100.44<br>100.11<br>100.11<br>100.11<br>100.11<br>100.11<br>100.11<br>100.11<br>100.11<br>100.11<br>100.11  | 19.5<br>-51.5<br>7.8    | -67.0<br>-22.0<br>-1.7<br>-2.5            | -56.7  | -11.6<br>-18.8<br>-12.5      | 13.7  | 15.2  | 28.6<br>27.3   | 4444461   |
| LOG<br>PCO2            | 11 11111111111111111111111111111111111   | 9.56-                   | 22322<br>22357<br>61557                   | -3:2   | -3.0                         | -1.2  | -2.0  | 9.00           | 0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0. |
| SIO2<br>MG/L           | 00000000000000000000000000000000000000   | 105.2<br>16.7<br>82.8   | 9.4<br>77.4<br>40.6<br>67.2<br>65.9       | 13.9   | 53.0<br>44.3<br>52.0         | 93.7  | 7.96  | 124.7<br>121.9 | 78<br>76.1<br>75.9<br>76.9<br>68.0  |
| D DATA<br>TDS<br>MG/L  | 34499<br>339609<br>371956<br>371956<br>381518<br>473961<br>473960<br>47360<br>47360<br>47360<br>47360<br>47360<br>47360<br>47360<br>47360<br>47360<br>47360<br>47360<br>47360<br>47360 | 315<br>71<br>615        | 303<br>366<br>379<br>174<br>279           | 96     | 135<br>261<br>251            | 301   | 148   | 3107<br>2312   | 7559<br>7412<br>7086<br>7489<br>3307<br>3238<br>3647  |
| MEASURED<br>Ph         | 9 000000000000000000000000000000000000   | 8.00<br>8.80<br>8.80    | 7.90<br>7.95<br>9.05<br>7.90              | 7.91   | 7.85<br>7.25<br>7.07<br>6.78 | 97.9  | 7.03  | 9.29<br>9.13   | 7.75<br>7.67<br>7.50<br>7.95<br>8.13<br>8.13  |
| TEMP                   | 000188778887788888<br>0001890099099094<br>000189009909999999999999999999999999999  | 25.7<br>21.5            | 35<br>43.3<br>16.9<br>7.9                 |        | 240.00                       |       |       | . ທີ່ຜູ້ເ      | 277.77.00<br>817.00<br>27.00<br>27.00<br>27.00  |
| SITE NO.               | 1264000000000000000000000000000000000000   | 20<br>22<br>22<br>23    | 22265<br>2876<br>2876<br>2876             | 302    | 724335<br>724335             |       | 0 6 C | 3510<br>7510   | 1444440<br>0400000000000000000000000000000  |
| <b>⊢</b>               | 110041000000000000000000000000000000000  | 221<br>221<br>231       | 28765<br>28765<br>28765                   | 385    | , w w w w w                  | 200   | 000   | 7577           | 24654<br>2464<br>2464<br>2464   |

Table

|                  | NA/K<br>B=0                           | 70.3  | 332.7<br>332.7<br>332.7<br>333.7<br>331.5                            |      | 162.3<br>112.3<br>60.8<br>56.0    | 5561<br>567<br>567<br>567<br>567<br>567<br>567<br>567<br>567   |
|------------------|---------------------------------------|-------|--|------|-----------------------------------|--|
| ted              | MGCOR                                 | 142.4 | 168.9<br>151.5<br>52.0<br>53.2                                       |      | 57.0                              | 1118<br>155.66<br>135.66<br>134.6 6.66<br>15692.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20<br>1656.20  |
| calculated       | CA<br>PACES                           | 133.6 | 88:3<br>2245:3<br>2245:3<br>205:5<br>149:0<br>149:0                  |      | 101.6<br>157.3                    | 262<br>262<br>262<br>263<br>263<br>263<br>263<br>263   |
|                  | NA/K/CA<br>B=1/3 PA                   | 153.6 | 135.7<br>173.8<br>170.6<br>154.1<br>158.8<br>206.0<br>206.1<br>206.1 |      | 178.6<br>197.0<br>126.2<br>201.0  | 2772<br>2775<br>2776<br>2776<br>2776<br>2776<br>2776<br>2776   |
| thermometers     | IN DEG C<br>B=4/3                     | 254.9 | 2214<br>5514<br>5712<br>8712<br>800.25<br>800.25                     |      | 154.8<br>383.3<br>142.0<br>1045.2 | 11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>1102<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>11022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022<br>1022 |
| on geo<br>mples. | EOTHERMOMETERS,<br>ICA<br>CHALC CRIST | 73.8  | 63.9<br>67.7<br>64.2<br>64.2<br>61.1<br>-7.8<br>101.7                |      | 31.0<br>125.4<br>36.0<br>73.7     | 286846887468964640<br>2862794688964689640<br>28627968968964689640  |
| cat<br>er s      | OTHERMC<br>CA<br>CHALC                | 6.46  | 84.0<br>88.1<br>88.3<br>84.3<br>80.9<br>5.4<br>126.1<br>-8.1         | •    | 47.7<br>152.6<br>53.3<br>94.8     | 94<br>98<br>98<br>98<br>98<br>98<br>98<br>98<br>98<br>98<br>98<br>98<br>98<br>98   |
| رة <b>ج</b> رق   | SILIO<br>QZ                           | 124.4 | 1114.5<br>1118.3<br>1116.8<br>111.7<br>1252.1<br>27.2                |      | 81.0<br>175.1<br>86.2<br>124.3    | 11112<br>1112<br>1112<br>112<br>112<br>112<br>112<br>113<br>113  |
| 02 and<br>ft Val | AMPHS                                 | 5.6   | -3.000.1<br>-4.52.9<br>-7.30.8<br>-7.30.8<br>-7.30.8<br>-7.30.8      | ·    | -31.7<br>-271.9<br>5.5<br>5.5     | 111120447777774<br>11117777777777777777777777777   |
| us SiG           | LOG<br>PCO2                           | -1.7  | 1011181187   | •    | 10.5                              | 24444444444444444444444444444444444444   |
| Vario<br>for a   | SIO2<br>MG/L                          | 78.7  | 2001<br>2001<br>2001<br>2001<br>2001<br>2001<br>2001<br>2001         |      | 31.0<br>186.1<br>35.1<br>75.3     | C0800000000000000000000000000000000000   |
| contd)           | DATA<br>TDS<br>MG/L                   | 3251  | 22328<br>319618<br>24092<br>22046<br>20987<br>2 3148<br>2 3036       |      | 910<br>3128<br>2013<br>45172      | 212<br>3672<br>3633<br>328<br>328<br>1574<br>1639<br>1739<br>174<br>176<br>176<br>176  |
| 5.14 (cc         | MEASURED<br>PH                        | 8.12  |  | 9.00 | 8.94<br>7.00<br>.00               | 77777777887978879797<br>974788197218948209199<br>403193877080874014833   |
| Table g          | TEMP                                  | 50.0  | 878666   |      | 255.<br>343.7<br>62.5<br>8        | 00000000000000000000000000000000000000   |
|                  |                                       |       |  |      |                                   |  |

Various SiOs and alkali cation deothermometers Table 5.14 (contd)

|   | 99.0  | -i 6. v                 | 278.6<br>236.9<br>180.1          | 227.<br>24.             | 292.5         | 208.3<br>245.4 | 243.7<br>162.1 | 318.2 |
|---|-------|-------------------------|----------------------------------|-------------------------|---------------|----------------|----------------|-------|
| •   | 158.8 | 275.8<br>133.0          |                                  |                         | 153.2         | 189.8<br>156.4 | 164.8          | 57.8  |
| •   |       | 0.0                     | 204.4<br>134.0<br>143.8          | -100                    | 51.2          | 64.2<br>50.5   | 56.8<br>94.1   | 9.49  |
| ulated  | 161.9 | 292.1<br>157.2<br>182.2 |                                  | നന്ത്                   | 213.8         | 200.4<br>203.6 | 213.9<br>185.6 | 233.0 |
| ers cald  | 211.2 | 80.29                   | 489.8<br>358.6<br>403.5          | 76.9                    | 123.7         | 167.7<br>136.0 | 169.8<br>181.8 | 156.7 |
| and aikail cation geotnermometers calculated<br>Valley water samples. | 98.1  | 000                     | 214.3<br>197.9                   | നനത                     | യഗ            | 100.2<br>89.7  | 102.3<br>64.9  | 82.0  |
| on geor<br>imples.  | 122.0 | 99.7                    | 119.8<br>253.7<br>234.9          | 252.8<br>252.3<br>259.4 | -17.0<br>96.6 | 124.4<br>112.7 | 126.7<br>85.2  | 104.0 |
| ull cati<br>ater sa   | 148.5 | 28.                     | 139.2<br>141.6<br>231.2<br>219.6 | 300.                    | . O           | 150.6<br>140.3 | 152.6<br>115.6 | 132.6 |
| ind aika<br>alley'n   | 27.2  |                         | 25.5<br>134.9<br>119.2           |                         |               | 29.1<br>19.7   | 31.0<br>-2.2   | 12.8  |
| Si02 a<br>Rift V  |       |                         |                                  | 000<br>000              |               | -0.8           | -0.3           | -1.2  |
| Various<br>for all  | 121.9 | 85.                     | 145.5<br>117.9<br>534.7<br>453.5 | 30.<br>28.<br>60.       |               | 126.2<br>105.7 | 130.5<br>66.3  | 92.0  |
|   | 655   |                         | 1590<br>1590<br>676<br>1091      | 200                     |               | 1632<br>950    | 1702<br>1541   | 868   |
| able 5.14 (conta)   |       |                         | 202                              | 6.20<br>6.20<br>6.20    | .0.           | 6.95           | 6.40           | 7.00  |
| - a<br>- a<br>- a<br>- a<br>- a<br>- a<br>- a<br>- a<br>- a<br>- a    | 19.6  | 4466                    | 72.0<br>152.0<br>159.0<br>157.0  | 8 m %                   | <br>7.        | 37.1<br>30.0   | 32.4<br>27.8   | 25.0  |
|   |       |                         |                                  |                         |               |                |                |       |

The foregoing evidence (particularly the <sup>3</sup>He/<sup>4</sup>He and inert gas radioisotope data) points to the fact that there is no sign shown by groundwaters of mixing with a deep, long residence component, except at Bala. Only groundwaters closely associated with volcanic centres (e.g. at 124) show large He enhancement, and even this seems to be caused by volcanic gas inflow rather than long residence of water.

# 5.7 Geothermometry

### 5.7.1 Water chemistry

These geothermometers involve consideration of the effect of temperature either on solubility of a species (normally a form of silica) or on the amount of exchange of various cations (the alkali and alkaline earth metals). In older rocks and at temperatures above 150°C quartz is likely to be the controlling mineral phase for the silica geothermometer, but in rocks of Rift age below 150°C control is likely to be by cristobalite or chalcedony. original basic alkali geothermometer of Na/K (White 1965), which assumes cation exchange with alkali feldspar, has been supplemented by versions including Ca and Mg (Truesdell 1975, Fournier and Potter 1979) and a correction for low temperature waters (Paces 1975). Table 5.14 shows the results of nine geothermometer calculations based on these various premises for all the Rift Valley Geothermal Project samples for which appropriate chemical data exist. These are now discussed with reference to the various sectors of the Rift studied during the project - Magadi, Suswa-Nakuru, north of Menengai, and north eastern margins of Lake Victoria.

The Magadi hot springs have surface temperatures of up to 85°C and TDS values rising to over 40,000 mgl<sup>-1</sup> (Section 7). As a consequence of the highly alkaline chemistry of the springs the simple Na/K geothermometer gives unrealistically low temperatures, while low levels of Ca and Mg make use of the corrected versions inappropriate. (Indeed most of the more obviously thermal waters in the Rift are low in Ca and Mg as a consequence of various mineral controls.) Of the SiO<sub>2</sub>-based geothermometers, amorphous silica can be ruled out, as it can be in the whole of the Rift. Cristobalite gives results often little different from the sampling temperatures, but both chalcedony and quartz give reasonably steady temperatures well in excess of sampled temperatures which suggests that these warm springs have a single source at a temperature between 100°C and 130°C variously affected by cooling Two boreholes between Magadi and Suswa and/or mixing processes (Section 7). Oltepesi and Mosiro (22 and 129) - have medium TDS waters of ambient temperature which on chemical and isotopic grounds show little evidence of a thermal origin. The lowest temperatures suggested by geothermometers for the sites are 76°C (cristobalite) and 58°C (Mg corrected respectively, but it seems unlikely that these well waters have ever reached such temperatures. The same is probably true for most of the groundwaters in the Suswa-Nakuru sector of the Rift (with the obvious exception of the Olkaria-Hells Gate area, which is considered separately) where for most of the waters the alkali geothermometers are excessive and even the silica-based ones are rather high. It is unlikely, for example, that borehole waters of ambient temperature (i.e. around 20°C) in the vicinity of Lake Naivasha have been raised to over 65°C then cooled again during their passage from recharge Such waters are characterised by low TDS values, virtually precluding mixing with thermal components. The chemical geothermometers are therefore also unconvincing in this sector of the Rift, with the exception of the wells north of Eburru and the warm spring on the edge of Lake Elmenteita (121-125 and 41-42) which are considered on other grounds to have a thermal component.

The sampled waters of the Bogoria-Silale area are generally hot (up to boiling) and the quartz and  $CO_2$ -corrected alkali geothermometers suggest a source for Kapedo and Lorusio waters at a temperature of 120-160°C, probably at the lower end of this range. The boiling spring of Ol Kokwe Island in Lake Baringo (71) yields a higher-temperature set of results of which quartz and  $CO_2$ -corrected alkali geothermometers agree well (about 175°C) though cristobalite at 152°C is also plausible.

The Bala hot springs of the Homa Bay area of northeast Lake Victoria range in temperature from 35°C to 75°C. Only the quartz geothermometer gives a credible temperature range, 112°C to 118°C. The appropriate Na/K/Ca geothermometer gives a rather high temperature.

Various factors affect the performance of geothermometers. Steam separation can affect silica concentrations, owing to adiabatic rather than conductive cooling, but this is only likely to apply to large, vigorously boiling springs, which are uncommon in the Rift. More importantly, amounts of silica in cooler Rift groundwaters may be raised to levels in excess of cristobalite or chalcedony equilibrium concentrations by release of silica from alteration of silicate minerals, eg by influx of  $\mathrm{CO}_2$  (Fournier, 1981). The ubiquity of of  $\mathrm{CO}_2$  in the Rift (Bailey, 1980) is consistent with this interpretation. As mentioned earlier the alkali geothermometers can be affected by high Mg contents, but this element is almost always present at very low levels in Rift Valley groundwaters.

The overall impression given by the geothermometer results is that those based on cations must be used cautiously in the Rift Valley. Of the silica-based geothermometers, quartz and chalcedony appear to be useful for hot springs, but for cooler waters, although chalcedony is the least oversaturated SiO<sub>2</sub> species (Table 5.15) and therefore theoretically most likely to tend towards the actual maximum temperature achieved at depth, it still produces temperature estimates which appear to be excessive. In this respect cristobalite is more reasonable, although it also often appears to overestimate temperatures at depth.

# 5.7.2 Gas geothermometers

These depend on temperature-controlled gas-mineral equilibria being achieved in the reservoir(s) which feed the fumarole, well or spring. Various versions exist, some using single gases and some gas ratios (Arnorsson and Gunnlaugsson, 1985). Carbon dioxide, hydrogen and hydrogen sulphide are the most suitable gases to use for geothermometry because the reactions controlling them seem to approach equilibrium over a large temperature range, but  $\rm H_2$  and  $\rm H_2S$  are often only present (if at all) below detection limit in Rift Valley fumarole gases. Methane, although usually second only to  $\rm CO_2$  as a 'geothermal' gas, is more loosely related to reservoir temperatures owing to departures from the controlling reactions (Arnorsson and Gunnlaugsson 1985), the main one of which may be the Fischer-Tropsch reaction between  $\rm CO_2$  and molecular  $\rm H_2$ .

Armannsson (1987b) dealt with the application of gas geothermometers to the Suswa, Longonot and Domes areas. This study has used the  $\rm CO_2/H_2$  geothermometer to estimate temperatures at depth, but this has been possible at only two sites (Table 5.16). Methane/carbon dioxide ratios from these and other sites have been applied to the theoretical  $\rm CH_4/CO_2$  - temperature curve of Ellis and Giggenbach presented in Glover (1972). The results are also given in Table 5.16.

|      |            |              |        |           |           |           | •         |
|------|------------|--------------|--------|-----------|-----------|-----------|-----------|
| SITE | CHALCEDONY | CRISTOBALITE | QUARTZ | CALCITE   | MAGNESITE | NAHCOLITE | MAGADIITE |
| 24   | +0.027     | +0.149       | +0.616 | -0.383    | -1.056    | -4.516    | _         |
| 25   | +0.516     | +0.558       | +0.960 | -1.001    | -1.622    | -4.366    | -1.808    |
| 26   | +0.032     | +0.057       | +0.446 | -0.682    | -0.965    | -4.639    | -4.207    |
| 27   | +0.666     | +0.747       | +1.180 | -1.883    | -2.400    | -4.955    | -3.025    |
| 28   | +0.526     | +0.582       | +0.616 | -0.165    | -1.056    | -4.889    | -2.250    |
| 37   | +0.660     | +0.713       | +1.123 | -1.659    | -2.224    | -4.750    | -2.212    |
| 39   | +0.684     | +0.739       | +1.151 | -1.611    | -2.456    | -5.264    | -1.728    |
| 41   | +0.393     | +0.415       | +0.801 | +0.026    | -0.643    | -3.070    | 0.026     |
| 80   | +0.687     | +0.760       | +1.187 | -0.358    | -1.070    | -4.420    | -1.925    |
| 81   | +0.558     | +0.627       | +1.051 | +0.328    | -0.226    | -3.591    | -2.360    |
| 82   | +0.702     | +0.775       | +1.203 | +0.396    | -1.403    | -4.368    | -1.857    |
| 83   | +0.540     | +0.600       | +1.017 | +0.291    | -0.047    | -3.733    | -1.992    |
| 84   | +0.624     | +0.697       |        | -0.011    |           | -3.468    | -1.935    |
| 85   | +0.637     | +0.710       | +1.138 | -0.052    | -0.984    | -4.348    | -1.790    |
| 86   | +0.728     | +0.788       | +1.205 | +0.077    | -0.194    | -3.949    | -1.076    |
| 87   | +0.624     | +0.689       | +1.104 | +0.150    | -1.075    | -3.773    | -1.159    |
| 88   | +0.548     | +0.614       | +1.035 | +0.091    | -0.821    | -3.515    | -2.224    |
| 89   | +0.533     | +0.597       | +1.017 | +0.729    | -0.213    | -3.321    | -1.861    |
| 90   | +0.683     | +0.761       | +1.193 | -0.030    | -1.260    | -4.087    | -1.499    |
| 91   | +0.667     | +0.732       | +1.153 | -1.616    | -2.356    | -5.382    | -2.129    |
| 92   | +0.696     | +0.766       | +1.191 |           | -2.662    | -5.286    |           |
| 93   | +0.742     | +0.809       | +1.231 | -0.262    |           | -4.348    | -1.009    |
| 94   | +0.607     | +0.684       | +1.115 | +0.301    |           | -2.675    | -1.386    |
| 95   | +0.382     | +0.447       | +0.868 | -0.410    |           | -4.283    | -3.250    |
| 96   | +0.634     | +0.703       | +1.126 | -2.478    | -2.963    | -5.926    | -2.939    |
| 97   | +0.780     | +0.848       | +1.271 | -1.899    | -2.511    | -4.965    | -1.843    |
| 99.  | +0.539     | +0.601       | +1.018 | +0.158    | -0.244    | -4.247    | -3.389    |
| 100  | +0.926     |              | +1.470 | -1.746    | -2.676    |           | -1.551    |
| 101  | +0.810     | +0.907       | +1.354 | -1.727    | -2.406    | -5.135    | -2.308    |
| 104  | +0.893     | +0.968       | +1.397 | -2.276    | -3.029    |           | -1.331    |
| 108  | +0.700     | +0.767       | +1.190 | -0.720    | -1.524    |           | -1.842    |
| 109  | +0.444     | +0.419       | +0.766 | -1.396    |           |           | -0.919    |
| 110  | +0.996     | +1.093       | +1.540 | -3.203    |           | -4.067    | -0.233    |
| 111  | +1.652     | +1.750       | +2.197 | -3.035    | -4.161    | -4.091    | +3.913    |
| 112  | +1.581     | +1.678       |        |           |           | -3.442    | +3.369    |
| 113  | +1.649     | +1.747       | +2.194 | -3.500    | -4.526    | -4.160    | +4.144    |
| 114  | +1.649     | +1.745       | +2.191 | -2.917    | -3.948    | -3.797    | +3.895    |
| 115  | +1.673     | +1.770       | +2.217 | -3.320    | -4.044    | -3.750    | +4.166    |
| 118  | +0.621     | +0.678       | +1.092 | -1.019    | -1.974    | -4.587    | -2.231    |
| 121  | +0.714     | +0.752       | +1.150 | +0.163    | -1.205    | -3.185    | -0.467    |
| 122  | +0.948     | +1.045       | +1.492 | -0.357    | -1.594    | -3.441    | -1.117    |
| 124  | .+0.779    | +0.826       | +1.233 | -0.298    | -1.323    | -3.153    | -0.787    |
| 125  | +0.530     | +0.587       | +1.001 | +0.488    | +0.540    |           | -1.662    |
| 129  | +0.888     | +0.985       | +1.432 | -0.445    | -0.905    | -3.518    | -1.364    |
|      |            |              |        | - · · · • |           |           |           |

NOTE: Saturation Index = log

Values within the range  $\pm$  0.10 are saturated, otherwise + is supersaturated and - is undersaturated.

Table 5.16 Gas geothermometer temperatures for fumaroles in the Suswa, Longonot, Olkaria-Domes and Eburru sector of the Rift Valley.

| SITE NO  | LOCALITY                     | t CO <sub>2</sub> / H <sub>2</sub> | t CO <sub>2</sub> /CH <sub>4</sub> | t CO <sub>2</sub> |
|----------|------------------------------|------------------------------------|------------------------------------|-------------------|
| 29/F-27  | Mt. Margaret                 |                                    | 330                                | 423               |
| 31/H-1   | Akira Ranch                  | -                                  | 314                                | 246               |
| 44-47    | Lorusio Springs <sup>2</sup> | 246                                | 338                                | · -               |
| 53-54    | Bala Springs 2               | ·<br><del>-</del>                  | 314                                | _                 |
| 110      | Olkaria OW2                  | <del></del>                        | 308                                | -                 |
| -111     | Olkaria OW26                 | . <del>-</del>                     | 322                                | -                 |
| 119      | Eburru EF-2                  | 256                                | . 296                              | _                 |
| 123      | W. Olkaria                   | <u>-</u>                           | 400                                |                   |
| 124      | Soysambu DEL 2               | -                                  | 319                                | _                 |
| 126      | Suswa, rim                   | -                                  | 384                                | 324               |
| 127      | Domes                        | -                                  | 313                                |                   |
|          |                              |                                    |                                    | 316               |
| 127/F-15 | Domes                        | -                                  | 320                                |                   |
| 128      | Longonot, crater             | 256                                | 311                                |                   |
|          |                              |                                    | ٠.                                 | 409               |
| 128/F-23 | Longonot, crater             | 255                                | 315                                | ·                 |
| F-7      | Suswa, caldera floor         | _                                  | 307                                | 303               |
| F-12     | Suswa, ring graben           | _                                  | 324                                | 298               |
| F-28     | Suswa, central island        | ·<br>-                             | 316                                | 370               |
| K-1      | Meru, Chogoria               | _                                  | 315                                |                   |
| K-2      | Meru, Chogoria               | -                                  | 383                                | -                 |

Figures from Armannsson (1987b) for directly-calculated CO<sub>2</sub> geothermeter.

Samples with F, H and K prefixes collected by Dr H Armannsson of the UNDP.

<sup>2</sup> Gas samples collected from water

While the  ${\rm CO_2/H_2}$  geothermometer gives apparently plausible results for Longonot and Eburru, the  ${\rm CH_4/CO_2}$  temperatures seem too high. Arnorsson and Gunnlaugsson (1985) warn that these cannot necessarily be interpreted as equilibrium temperatures preserved from greater depths.

## 5.7.3 Isotope geothermometers

Various isotope fractionations can in principle yield information on temperatures at depth. The fractionation of water can itself reveal information on boiling temperatures if certain assumptions are made; this subject has been dealt with in passing in Section 5.3. Differences between  $\delta^{18}$ O values in steam condensate and accompanying  $CO_2$  from fumaroles could also be used since isotopic exchange ceases in the vapour phase, but rapid re-equilibration at condensation temperatures can only be prevented with sophisticated sampling techniques such as cryotrapping. Another possible geothermometer is the fractionation of  $\delta^{13}$ C between DIC and  $CO_2$  gas, but since this requires a sample of liquid from which to obtain the DIC the exercise is usually academic. However, it may be noted that at the Soysambu DEL well (site 124) the  $\delta^{18}$ O  $CO_2$ -H<sub>2</sub>O and  $\delta^{13}$ C DIC- $CO_2$  equilibria are in exact agreement with the measured temperature (Table 5.8).

Other geothermometers which have been used in geothermal systems elsewhere are the  $\rm H_2-H_2O$  (Arnason, 1977) and the  $\delta^{13}C$   $\rm CO_2-CH_4$  fractionation (Hulston, 1977). Insufficient sample volumes were collected to attempt isotopic measurement of  $H_2$  or  $CH_4$  except at Eburru, where a  $\delta^{13}C_{CH4}$  was measured on a sample from site 119. This gave the very enriched result of -6.7% which indicates a very high temperature and may be incorrect, though it is worth noting that samples collected previously from Eburru fumaroles unexpectedly high  $\delta^{13}C_{CH4}$  values averaging -14.7% corresponding measured  $\delta^{13}C_{CO2}$  values to temperatures of around 500°C (Glover, 1972). However the  $\delta^{13}C_{CO2-CH4}$  geothermometer may not be universally applicable, depending as it does on the attainment of equilibrium for the Fischer-Tropsch reaction mentioned above - for example, at Olkaria this geothermometer indicates temperatures well in excess of 300°C (Glover, 1972), subsequent well drilling has yielded fluid of significantly In view of the strong indications from stable isotopes that temperature. water from Lake Naivasha reaches Olkaria and perhaps some of the other high temperature areas in the Suswa-Eburru zone, the presence of biogenic methane produced from organically-rich lake water cannot be excluded. would upset any isotopic geothermometer on the Fischer-Tropsch equilibrium.

# 5.7.4 Geothermometers - Summary

The application of chemical geothermometers to ambient and warm groundwaters in the Rift Valley is often inappropriate. Most ambient groundwaters are local and will not have been raised to much higher temperatures or mixed with thermal waters during their travel, but many give excessive alkali and Si geothermometer temperatures, for reasons explained above. In hot springs and geothermal wells, however, both alkali and quartz temperatures are plausible unless, such as Magadi, local conditions are such that the Na/K/Ca geothermometer is rendered useless.

There are however comparatively few opportunities for sampling hot water in the Rift - most areas of thermal upflow appear as fumarolic discharges. The gas geothermometers are potentially useful here, though the ratio types,  ${\rm CO_2/H_2}$  and  ${\rm CO_2/H_2S}$ , which are perhaps easiest to measure accurately, cannot often be applied because of the scarcity of  ${\rm H_2S}$  and  ${\rm H_2}$  in Rift fumarole

gases.  $CH_4/CO_2$  ratios, though available for all gases, are a rather unreliable geothermometer both on account of the controlling reactions and the possibility of a biogenic component. The straightforward  $CO_2$  geothermometer may be the most universally applicable one in the Rift, though Armansson (1987a) points out that cold  $CO_2$  wells exist inside and outside the Rift where the  $CO_2$  geothermometer cannot sensibly be applied. This is despite the indications from carbon isotope measurements that all the  $CO_2$  has a similar origin.

particularly Isotope fractionations are by and large not geothermometers. Oxygen and hydrogen isotope fractionations between liquid and vapour phases only indicate the temperature of separation, which in fumaroles can be much cooler than reservoir temperature. The CH4-CO2 isotope from the same problems as the geothermometer suffers CH<sub>4</sub>/CO<sub>2</sub> geothermometer. Other potential isotope geothermometers require difficult collection techniques (eg  $\delta^{18}$ O liquid -  $CO_2$ gas) or collecting large amounts of gas (eg  $\delta^2$ H liquid -  $H_2$  gas) and may only serve to indicate separation temperatures.

# 6.1 Hydrogeology of the Olkaria Geothermal Field

Geothermal exploration at Olkaria started in the 1950's, and the first exploration well was drilled in 1956, followed by a second well in 1958. However these wells failed to produce steam and exploration drilling was abandoned until the 1970's when several successful wells were drilled (Noble and Ojiambo, 1975).

During the last decade production drilling has been carried out at Olkaria, and a 45 MW $_{\circ}$  power station has been constructed in the eastern part of the field. By early 1987 34 wells had been drilled at Olkaria, of which 25 are in the East Olkaria production field which covers an area of approximately 2 km $^2$ . Well depths generally range from 1000 m to 1600 m with the deepest well reaching 2484 m (Bodvarsson and others, 1987).

The stratigraphic sequence in the area comprises subhorizontal intercalated rhyolite, trachyte and basalt lavas with thin pyroclastic beds (Browne, 1981). A thick trachyte extends from 200 m to 400 m below which basalts and rhyolites predominate to 900 m. At greater depths trachytes form the main rock type (Bodvarsson and others, 1987).

A basaltic caprock between 500 m and 700 m is thought to confine the geothermal reservoir at Olkaria. A steam zone, between 50 m and 100 m thick at a pressure of 3.5 MPa and with a temperature of 240°C underlies the caprock. Below the steam zone is a liquid-dominated reservoir which follows a boiling point for depth relationship with a temperature of 300°C at a depth of 1500 m (Bodvarsson and others, 1987). Above the caprock are shallow aquifers containing cool saline waters.

Zones of high permeability (feed zones) exist both in the steam zone and in the underlying liquid-dominated reservoir. These are few in number with normally one major feed in the feed zone and one or two in the liquid zone. There is no good correlation between rock type and permeability although it has been suggested that the pyroclastics may be more permeable (Browne, 1981). Permeability values are discussed in Section 4.4.3.

The East Olkaria field shows a substantial north-south pressure gradient of 1.1 MPa/km from which it has been inferred that an upflow zone exists to the north of the present field (Bodvarsson and others, 1987). Well temperature measurements (Haukwa, 1986) and the distribution of epidote (Browne, 1981) also indicate that the hottest, upwelling part of the field is to the north. Southerly flow beneath the caprock may then have created the steam zone by phase separation (Grant and Whittome, 1981). In a recent interpretation of reservoir hydrology (Barnett and others, 1987) it has been suggested that a major fault running east-west across the field - the Olkaria Fault - acts as a conduit for hot upwelling fluid, and that at shallow levels the upflow is perturbed by cooler fluids associated with a major north-south structure, the Ololbutot Fault.

In recent years exploration drilling has discovered extensions of the field to the west and north. Wells in the west Olkaria field have in general lower temperatures than those in the east, but they have encountered mainly liquid (and therefore their mass output is potentially higher). Permeability values in this area are similar to those in the east (Haukwa, 1984).

# 6.2 Geochemistry

The Olkaria geothermal field has already been mentioned as the only locality in the Rift where deep thermal fluid can be sampled, and as such has provided useful information, particularly isotopic, about flow southwards from Lake Naivasha. In addition to this larger scale picture, the relatively high density of sampling points in the eastern wellfield and the Hell's Gate (Ol Njorowa) Gorge permits closer analysis of the relationship between the wellfield and possible outflow in the gorge.

Figures 6.1a to 6.1l show plans of sampling sites in the wellfield (oblongs) and gorge (circles) with chemical and isotopic values indicated. apparent that there are changes in chemical and isotopic species, and also that there are similarities and dissimilarities in various species between the wellfield and gorge sampling sites. While the geochemistry of the Olkaria geothermal field has been investigated in considerable detail by other workers (Arnorsson et al, in prep.), a brief description of the changes across the wellfield is now given . Total dissolved solids (TDS) rise north to south from 676 to 1590 mg/l, an increase of some 2.4 times. ions show fairly even increases of this order, except for SO4 which increase but is low in the southernmost well (OW2),  $\mbox{HCO}_3$  which rises again, and Si which is constant except for a lower level This general increase in TDS content across the eastern wellfield from north to south fits the regional model of southerly flow from Lake Naivasha deduced from isotopic evidence: water at the southern end of the wellfield has been in residence longer than water in the north and has thus had more time reaction with the reservoir rock at high temperature. Clearly the water has achieved supersaturation in some species before others; silica values hardly change across the wellfield. Isotopic changes across the wellfield are not (Figures 6.1i and 6.1j). The southernmost well (OW2) comparatively depleted, and if this represents a local dilution effect it may also explain the drop in Si and SO<sub>4</sub> already noted above. Otherwise, variations between wells may be due to steam loss (a loss curve from OW26 shown in Figure 5.9), though is more likely to be due to a combination of variable water-rock  $\delta^{18}$ O shifting and local dilution. If the total fluid compositions are considered to derive from mixing of Rift-wall groundwater and Naivasha water, a 55 to 75% lakewater contribution is suggested.

The relationship of the three northern Hell's Gate (Ol Njorowa) water sampling points to the geothermal field seems fairly straightforward. The only sample from the western side of the gorge (107) has a very high TDS (>2000 mg/l) and most probably represents natural outflow or artificial effluent from the field. Although the temperature of this manifestation is only 32°C, the enrichment in dissolved solids is probably due to steam loss/evaporation. Sites 108 and 109, on the eastern side of the gorge opposite the wellfield, have a chemistry much closer to wellfield values which suggests that they are sampling relatively unmodified outflow. The higher TDS level in 109 shows that evaporation is likely to have occurred which, as for site 107, is likely to be related to steam heating because SO<sub>4</sub>/Cl ratios are higher than in the deep fluids. Simple evaporation would tend to cause isotopic enrichment, and 109 with a higher TDS and temperature is accordingly slightly heavier than 108.

South of these sites, on the eastern side of the gorge, four sampling sites possess stable isotopic values similar to those from the wellfield. In terms of chemistry, however, these sites are very much lower in TDS which implies that they are not directly derived from deep fluid. Instead they are probably the result of condensation of steam which was separated from an

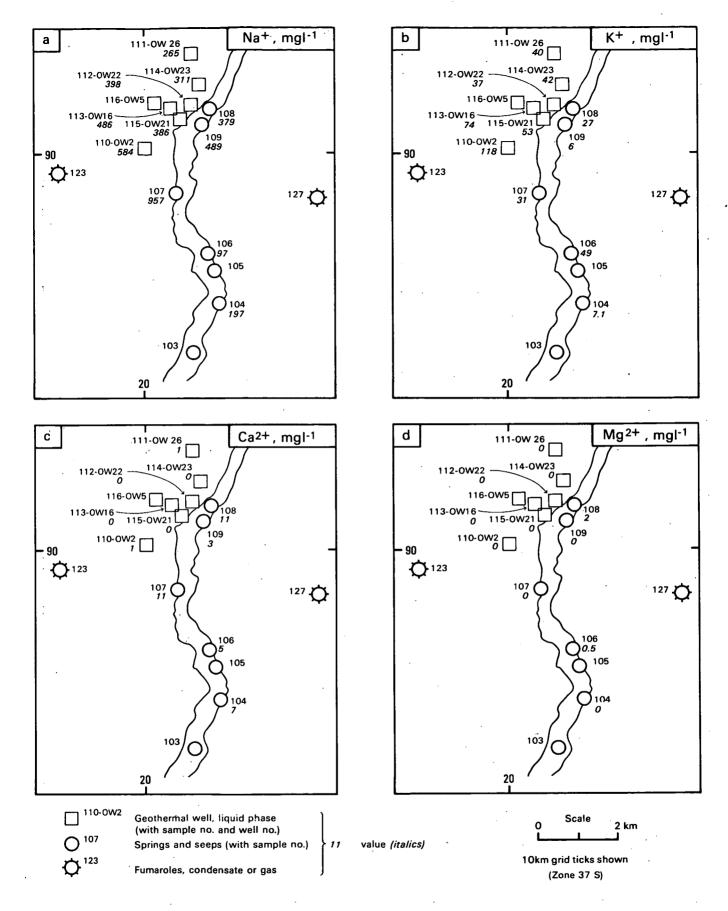


Figure 6.1a-d Maps of chemical and isotopic data for the Olkaria-Ol Njorowa (Hell's Gate) geothermal area.

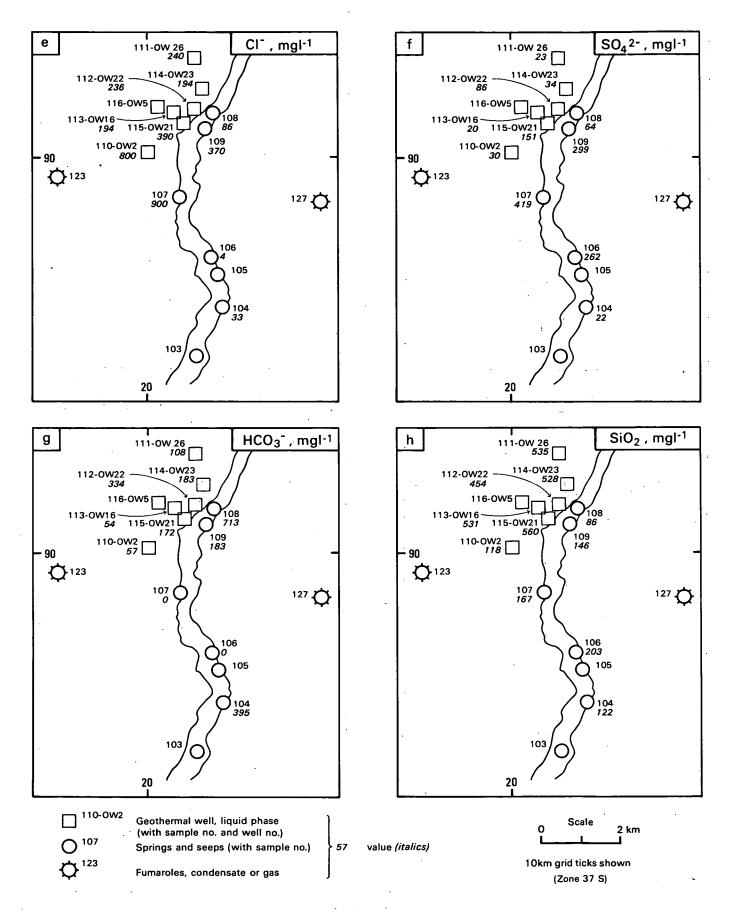


Figure 6.1e-h Maps of chemical and isotopic data for the Olkaria-Ol Njorowa (Hell's Gate) geothermal area.

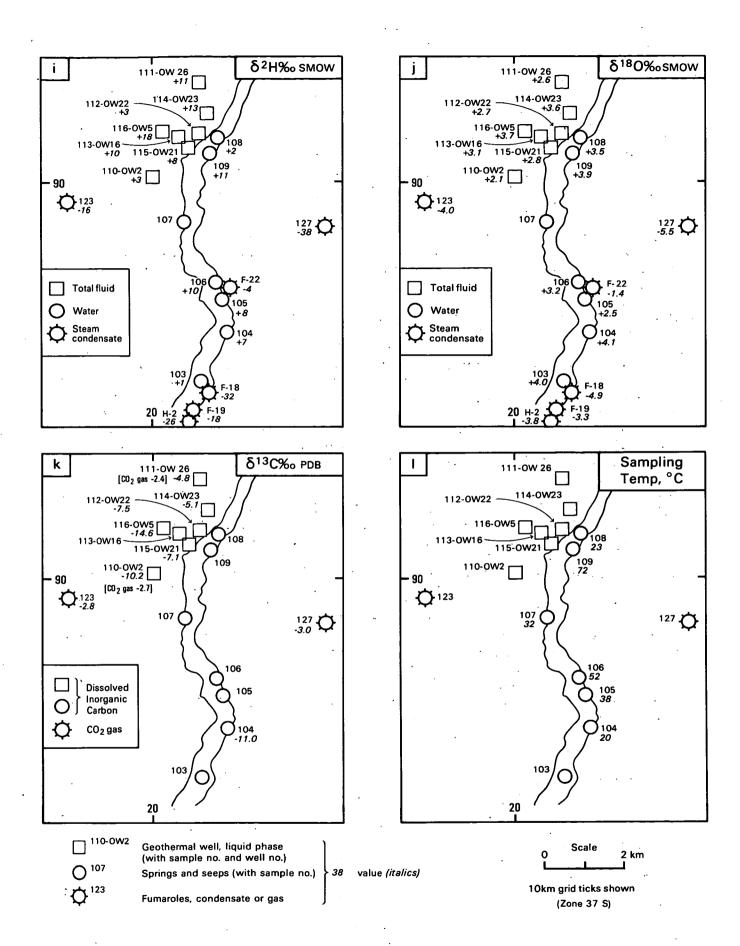


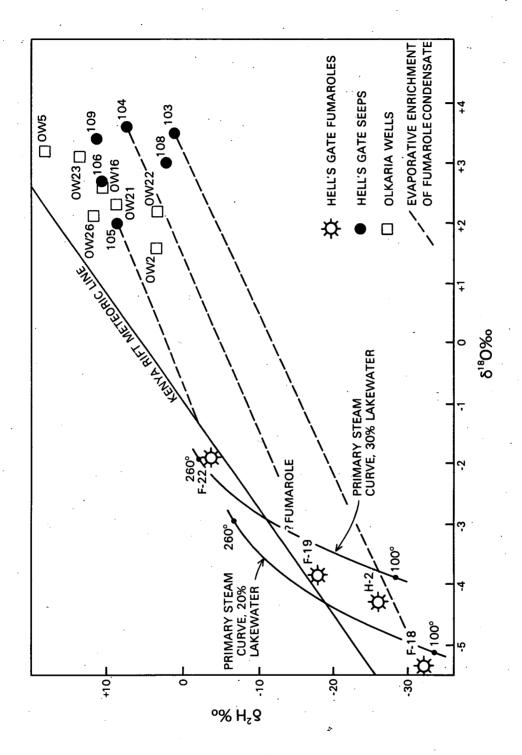
Figure 6.1i-1 Maps of chemical and isotopic data for the Olkaria-Ol Njorowa (Hell's Gate) geothermal area.

Olkaria-type deep fluid which is undergoing progressively greater dilution with Rift-wall water as it flows to the south. In some cases the sampled springs or seeps are clearly associated with nearby fumaroles while in others the connection with a steam source is less obvious, but similar mechanisms seem to apply in each case. The end result is that although sites 103-106 have similar isotopic values to the wellfield and sites 108 and 109, they are actually produced from lighter waters. Figure 6.2 shows the primary steam line for a 20% lakewater component. This line passes near F18, F19 and H2, suggesting that their steam shares a common origin. Site 103 appears to result from surface (or near-surface) condensation of F18, and an evaporative slope connects the fumarole with the seep. Similarly sites 105 and 106 are associated with F22 along a trend of similar gradient, while the fumarole itself lies near the 30% lakewater primary steam line. Site 104, which is situated about halfway between F18 and F22, has no obvious steam source, but an evaporative line sub-parallel to the other two would suggest that the source is around 25% lakewater, in accordance with the progressive southward dilution.

Fumaroles 01 to 03 were sampled in the wellfield itself. These samples lie outside the range of likely primary steam composition (Figure 5.9) and are probably the consequence of steam heating of cooler, more diluted lakewater overlying the Olkaria reservoir with values of about 0%  $\delta^2$ H, 0%  $\delta^{18}$ O. A fumarole in the western Olkaria field could possibly be related to this process but may alternatively be a product of primary steam separation from a more dilute reservoir. In view of the major north-south fault (Ololbutot) dividing the eastern and western wellfields the latter is a tempting conclusion, but more western wellfield fumarole and/or wellfield data are required to confirm or refute this interpretation.

Carbon isotope ratios show a steady depletion in  $\delta^{13}$ C DIC southwards across the geothermal field (Figure 6.1k). On the other hand, CO2 gas from OW2, OW26, F15 and the western Olkaria fumarole already referred to are remarkably similar ( $\delta^{13}$ C -2.4 to -3.0% PDB). Although HCO<sub>3</sub> and CO<sub>2</sub> may almost be in isotopic equilibrium for OW26, indicating a temperature of about 200°C, they are completely out of equilibrium for OW2. This is unlikely to be a result of sampling technique; the fact that  $\delta^{13}C$  DIC depletion is steady, δ<sup>13</sup>Cco<sub>2</sub> values remain constant and bicarbonate concentration does not correlate with  $\delta^{13}$ C depletion suggests that the explanation lies elsewhere. Changes in the δ<sup>13</sup>C of well CO<sub>2</sub> in other geothermal fields have been attributed to the precipitation of calcite caused by near-well boiling conditions. discussed below, there is no evidence for this occurring in the Olkaria wells on the basis of the water chemistry presented here, and in any case  $\delta^{13}$ C CO<sub>2</sub> does not appear to change. In addition there is no reason why this should affect the  $\delta^{13}$ C CO<sub>2</sub>-DIC equilibrium, which would be expected to re-establish In the absence of further data the itself during transit to the surface. question remains open

Gas samples were collected from OW2 and OW26 and results are given in Table 5.10. The geothermometric aspects of these gas samples are considered in Section 5.7.2 of this report, where it is suggested that the presence of a large percentage of lakewater in the Olkaria reservoir could be responsible for a proportion of the methane measured in the gases. Such biogenic methane would render unreliable chemical and isotopic geothermometers based on inorganic thermal  $CH_4$ . The ethane values from OW2 and OW26 appear to indicate a lakewater rather than a thermogenic origin: OW26 has the highest  $C_2H_6/CH_4$  ratio of any gas sample collected while OW2, situated downflow, is lower. By contrast a very strong upflow like Longonot F23 (indicated by the presence of He and  $H_2$ ) has a low  $C_2H_6/CH_4$  ratio. On this rather tenuous



Delta-diagram of stable isotope data from the Olkaria-Ol Njorowa (Hell's Gate) geothermal area. Figure 6.2

evidence, the West Olkaria fumarole sampled may have a larger lakewater contribution than its H and O isotopic values suggest.

The lack of readily detectable He or  $\rm H_2$  at Olkaria suggests that the wells are further from an upflow than for example the Longonot crater fumarole F23 or the Eburru fumarole EF2.

Chemical geothermometers give good results for the Olkaria wellfield. is reasonable agreement for most wells between the quartz and Na/K results. Samples from five wells give an average temperature of 255°C for quartz, and The results can be compared with the average 240°C for Na/K (Table 5.14). main feed temperature of eight (unidentified) Olkaria wells of 242°C In the same report, CO<sub>2</sub> geothermometry results were (Armannsson, 1987b). reported averaging 245°C, and it was assumed that calcite was a primary control of CO2 concentrations. The WATEQF-calculated saturation indices (Table 5.15), though not as ideal for high temperature geothermal systems as some specific codes, suggest that it is indeed the case. Calcite, although undersaturated, is the major carbonate phase, though not so very much in excess of magnesite and nahcolite. This undersaturation of calcite may be a consequence of cooling by conduction, or perhaps limited dilution, after upflow. The wells do of course show supersaturation with respect to quartz and, it is interesting to note, magadiite - a sodium silicate mineral, NaSi<sub>7</sub>O<sub>13</sub>(OH)<sub>3</sub>.3H<sub>2</sub>O, first identified by Eugster (1970) in the Lake Magadi area.

Tritium results from OW2 and OW26 are identical within measurement error, averaging 0.23 TR (Table 5.9). This level implies either that inflow has been in transit for at least 40 years, or that it is older than this but has a small amount of thermonuclear tritium (i.e. post 1954) as a result of leakage from the surface. Alternatively the <sup>3</sup>H content might result from the decay of <sup>6</sup>Li, though this process is probably of most significance in granitic rocks (Andrews and Kay, 1982).

Helium isotope ratios of corrected R/Ra values 5.69 and 5.83 (Table 5.11) were noted for OW2 and OW26. The values are close to those of Longonot F23 and Eburru EF2 and are probably derived from the same local crustal reservoir. The fact that they are slightly lower than the volcanic upflows is presumably due to the fact that they are not directly situated over the local Olkaria upflow. A very similar R/Ra value of 5.62 was noted for the West Olkaria fumarole sampled. While this does not necessarily imply that the western wellfield is intimately linked to the eastern, it does suggest a similar proximity to an upflow. The Domes fumarole F15 gave a lower R/Ra value of 2.92 - this may suggest increasing distance from an upflow, but gas analyses indicate that air entrainment could have affected the ratio.

#### Olkaria Area - Conclusions.

Geochemical indications are that flow across the eastern wellfield is taking place from north to south. While it should be borne in mind that the chemistry of the water fraction will not be identical to that of total fluid at depth in the reservoir (due to steam and gas separation), the data serve to indicate a general rise in solutes across the wellfield presumably due to increasing amounts of water-rock interaction and perhaps steam loss. The TDS of the fluid is however low by the standards of many other geothermal fields, which may suggest a relatively short flow path and/or residence time, though the latter is constrained as to its lower limit by the tritium data. Chemical geothermometers give reliable results where they can be compared with well-bottom temperatures.

Water stable isotopes indicate a decreasing lakewater contribution to the deep fluid in a southerly direction. They also show that only a limited  $\delta^{18}$ O shift is presently occurring: this implies a system of some antiquity where rock is approaching isotopic equilibrium with original water values after a large amount of throughflow. The alternative explanation, a younger but very 'wet' geothermal system seems less likely from the preliminary interpretation of the local water balance presented in this report. Core material obtained from some Olkaria wells will be subjected to stable isotope analysis to see what light can be shed on the field's history.

Gas data suggest that eastern Olkaria is not situated directly over an upflow since He and  $\rm H_2$  are only present at lower concentrations. Although the R/Ra values are relatively high these are not infallible indicators of proximity to upflow - for example the DEL well (site 124) on the Eburru outflow has a very similar R/Ra to EF2, even though it is situated some 10 km away.

The relationship between  $\delta^{13}CCO_2$  and  $\delta^{13}CDIC$  is problematic, but the hydrocarbon gas ratios appear to confirm that substantial amounts of lakewater are present at Olkaria.

#### 7.1 Introduction

As a result of extreme evaporation of the alkaline lake brine (Na+,  $HCO_3^{2-} + CO_3^{2-}$  type; salinity 290 000 mg/l), Lake Magadi contains a deposit of crystalline trona up to 40 m thick (Jones and others, 1977). This is composed of crystalline carbonates of sodium (principally sodium sesquicarbonate [Na<sub>2</sub>CO<sub>3</sub>.NaHCO<sub>3</sub>.2H<sub>2</sub>O]) which is dredged by the Magadi Soda Company and treated before being calcined in large kilns to produce soda ash.

The lake is fed by groups of alkaline springs with temperatures varying between 34°C and 86°C which occur at several points around the periphery of the lake (Figure 7.1, adapted from Baker, 1958). In general the hottest springs are the most dilute and occur in the north, and the cooler more saline springs are found to the south of the lake. The values of discharge of the springs are very variable. Some are only seepages rising in the mud and shingle of the lake shore (for example those at Bird Rock). Others such as the main hot springs feeding Little Magadi are much larger, with flows of several litres/second.

According to Baker (1958) most springs issue from scree at the base of the fault escarpments bounding the lake and nearly all the spring waters then find their way into the stagnant lagoons that border the main trona bed at lake level. During and immediately after the rainy seasons the lagoons are connected with the shallow brine body covering the lake surface (Jones and others, 1977). This brine body vanishes during the dry seasons exposing a porous but firm trona deposit. As a result of the economic and scientific importance of Lake Magadi a number of studies have been carried out, usually aimed at determining the origin of the solutes forming the trona. These attempts have naturally included studies of the springs bordering the lake and it is therefore pertinent to review them where they bear on the origin and nature of the hot springs.

#### 7.2 Origin of the Hot Springs - Previous Work

Early ideas concerning the origin of the springs are discussed by Baker (1958). He considers three hypotheses, namely Parkinson's, Stevens' and the re-circulation hypothesis.

Parkinson's hypothesis (1914) was that the spring water is of juvenile origin. The water, he suggested, contains magmatic  $\mathrm{CO}_2$  and reacts with the sodium silicates in the lavas through which it passes, forming sodium carbonate and silica. This hypothesis may be dismissed on the basis of the isotope evidence which proves the water to be meteoric in origin - although the chemical reaction suggested is valid.

Gregory in 1921 (cited in Baker, 1958) raised the possibility that the lake was an evaporating pan in which trona, leached from adjacent lavas by percolating waters was deposited, but he rejected the idea in favour of Parkinson's hypothesis.

Stevens (1932) concluded that the greater part of the lake salts at Magadi must be derived from spring solutes and he suggested that the constancy of the carbonate/chloride ratio in the springs implied a common source for them all, which he considered to be a large body of 'mother liquor' at depth. Later, in 1951, Guest and Stevens, having estimated the flows of the springs (by considering the rate of lake evaporation) concluded that the rate of

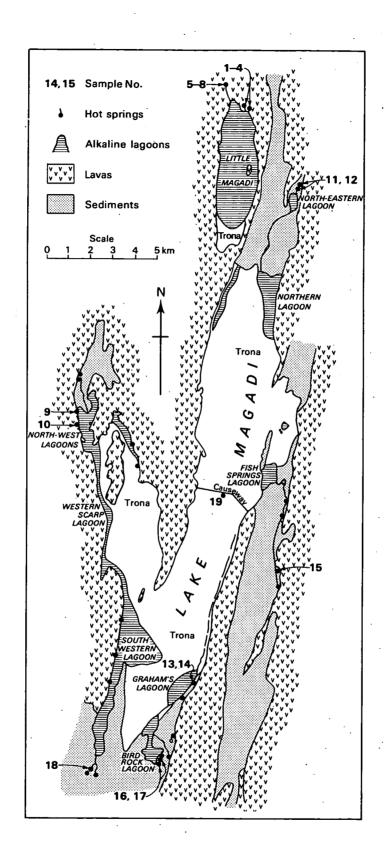


Figure 7.1 Location map of the Magadi hot springs.

solute addition to the lake was too great to account for its age (Guest and Stevens, 1951). They therefore reasoned that a proportion of the lake liquor must recirculate, with heavy liquor descending and becoming mixed with ascending hot spring water.

Bakers own hypothesis (1958) was that groundwater in the Rift Valley leaches salt from igneous silicates over a large area. These salts become concentrated by repeated evaporation of lake water, and re-leaching in the numerous pans between fault escarpments in the southern Rift Valley. Such waters would ultimately accumulate as alkaline groundwater in the Magadi basin at the lowest point in the Rift Valley, and would provide trona by evaporation of the spring waters.

More recently Eugster and others have proposed a detailed model for brine evolution at Magadi involving evaporative concentration as the main process for solute acquisition (Eugster, 1970; Jones, Eugster and Rettig, 1977; Eugster, 1980).

The basis for the model is that, according to Eugster, the Na/Cl ratios of stream waters on the sides of the Rift are similar to those of groundwaters, and for the springs bordering the lake. Eugster therefore proposes that the increase in solute concentration observed between the peripheral streams and the lake brines is principally a result of surface evaporation, and can be followed by using NaCl as a tracer (assuming that NaCl remains in solution until very late in the concentration process). Eugster argues that constituents such as Ca, Mg, HCO<sub>3</sub> and CO<sub>2</sub>, SiO<sub>2</sub> and K which are not concentrated to the same degree as NaCl are lost during brine evolution, chiefly by precipitation (or in the case of CO<sub>2</sub>, by degassing).

The main mechanism for evaporative concentration proposed by Eugster is the dissolution of efflorescent crusts. These crusts are formed either by the evaporation of runoff, or by capillary evaporation of shallow groundwater. Once formed, only the more soluble constituents of the crusts are dissolved by subsequent contact with dilute rainwater. Thus for example, NaCl and  $\rm Na_2CO_3$  dissolve, while calcite, magnesium calcite, dolomite silica and silicates remain.

Eugster's postulated circulation system "involves inflow from dilute rim streams descending into the Rift Valley and ephemeral runoff within the valley floor feeding local dilute groundwater bodies. It also stipulates the presence of a hot saline groundwater body at some depth within the trachyte lavas [under Lake Magadi]. This body is inferred from the constancy of the spring temperatures over 40 years" (Eugster, 1980).

In order therefore to arrive at the various spring concentrations, composition and temperatures Eugster postulates three sources which are mixed in different proportions for each spring: shallow groundwater (cold, dilute), deep groundwater (hot, saline) and recirculated surface brine (cold, more saline, high pH). The solutes in all three sources originate ultimately by evaporative concentration.

Recently Hillaire-Marcel and Casanova (1987) have used Eugster's model and with the addition of isotopic data have attempted to identify the different types of water in the model. The authors obtained  $\delta^2 H$  and  $\delta^{18} O$  values for the lake, for several of the surrounding springs, and for local precipitation.

Hillaire-Marcel and Casanova found a linear relationship between the  $\delta^2 H$  and

 $\delta^{18}\mathrm{O}$  values for the springs and the interstitial lake brine which indicated evaporation. By regressing this line to the World Meteoric Line they obtained an intersection value which they considered to represent the value of deep thermal water. This value is significantly depleted isotopically with respect to the average value for present day recharge and, the authors suggest, represents recharge during the last humid episode in Kenya. This period was determined by Hillaire-Marcel and Casanova as 12000-10000 years BP from stromatolite dating, when the lake level was significantly higher than at present.

A study by Crane (1981) has concentrated more on the geothermal aspects of the springs. She compiled thermal, seismic and rainfall data collected over periods of up to 60 years and attempted to correlate spring temperature variation with volcanic, tectonic and meteoric activity.

Crane found that the southern cooler springs have a rapid temperature response to rainfall fluctuations over several decades. She concluded that these springs therefore have a shallow source and, following Eugster's model, that they therefore recirculate lake brines rapidly.

No such relation between temperature and rainfall was evident for the northern springs leading Crane to conclude that these arise from a deep-seated saline water body. She did however attribute temperature variations in the northern springs partially to volcanic activity in Tanzania and suggested that this inferred a greater hydraulic connection with the Rift to the south than with the north. Other temperature variations were postulated by Crane to have been caused by local seismic activity affecting circulation patterns.

The total heat output of the Magadi region was estimated by Crane to be around 900 MW, based on aerial infra-red measurements.

Additional hydrochemical work in the Magadi area was carried out by Glover (1972) who favoured an origin for the springs as locally steam-heated groundwater, and a limited number of stable isotopic analyses (mainly  $\delta^{10}$ ) have been reported by Panichi and Tongiorgi (1974) and Bwire-Ojiambo (1984).

## 7.3 Sampling.

Samples for chemical and isotopic analysis were taken from all the main groups of springs and from several of the minor groups, as shown in Figure 7.1. Samples 1-4 and 5-8 were taken from two groups of hot springs to the north-east and north respectively of Little Magadi. These groups contain the hottest springs found around Lake Magadi, with temperatures of up to  $85.3^{\circ}$ C. Flow rates of individual springs range up to an estimated 6 l/s. The springs are mainly associated with fault scarps, and some occur within the lagoon.

Samples 9 and 10 were taken from a series of springs and seeps spread over a distance of over a kilometre to the west of the North-West Lagoons. The temperature of the sampled springs, 45°C, was significantly lower than that of the Little Magadi springs and flow rates were also lower, ranging up to 2 1/s for individual springs.

Samples 11 and 12 were obtained from a group of three springs and seep zones on the east side of a small graben to the north of the North-East Lagoon. Spring temperatures were intermediate to the previous groups at  $65-67^{\circ}\text{C}$  and spring discharges totalled 5 l/s.

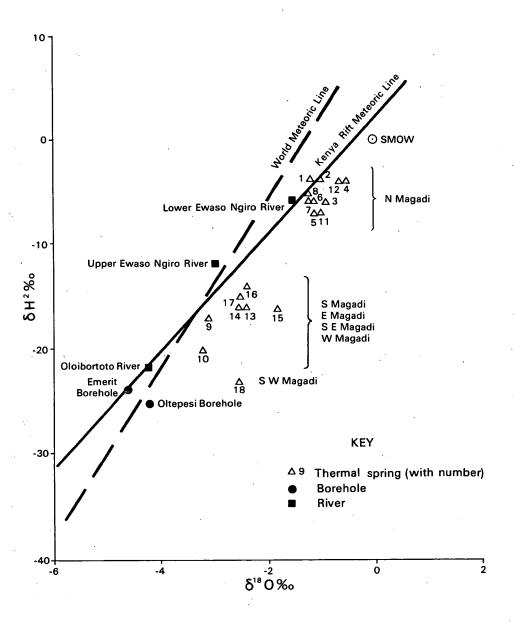


Figure 7.2 Stable isotope characteristics of waters in the Magadi area.

A small spring group on the edge of Graham's Lagoon producing water at 38-39.5°C was sampled (samples 13 and 14), as was a group of springs further north with low discharge rates and the lowest temperatures recorded - 34°C (sample 15).

At the southern end of Lake Magadi by the Bird Rock Lagoon, a group of seeps and small springs (flow rates less than 1 l/s) with temperatures of  $40.5\text{-}40.8^{\circ}\text{C}$  were sampled (samples 16 and 17). To the west sample 18 was taken from a powerful set of springs with an estimated total discharge of 100 l/s and a temperature of  $45.3^{\circ}\text{C}$ .

Finally a sample of lake liquor was taken from a point near the causeway (sample 19).

In addition to springs and lakewater samples were taken from the Ewaso Ngiro and Oloibortoto rivers to the west (samples 20,21,32) and from boreholes at Oltepesi and Emerit, about 40 km to the NE of Magadi.

#### 7.4 Isotopic Characteristics.

Isotopic determinations ( $\delta^{18}$ O,  $\delta^{2}$ H) are listed in Table and illustrated in Figure 7.2, which includes for reference the standard World Meteoric Line of Craig (1963) and the Kenya Rift Meteoric Line determined previously (Section 5.3).

Ambient water samples.

Three samples from rivers near to Magadi are shown in Figure 7.2. Two of the samples were taken from the Ewaso Ngiro River which is the only perennial river in the area; one sample was from the upper reaches of the river, near Narok, and the other was taken where the river reaches the Ewaso Ngiro plain at the base of the Nguruman Escarpment. The slope of 4.3 between the two samples' isotopic compositions (Figure 7.2) suggests that evaporation has occurred between the upper and lower reaches of the river, and this is supported by the higher concentration of solutes found in the lower sample.

Thermal springs.

The isotopic characteristics of the thermal springs (Figure 7.2) fall mainly into two groups. The northern, hotter springs from the north shores of Little Magadi and the North-Eastern Lagoon form a tight cluster about the local meteoric line, with an average value of -5%  $\delta^2$ H and -1%  $\delta^{18}$ O (samples 1-8, 11-12). The cooler spring groups of the North-West Lagoon (samples 9-10) and the spring groups to the east and south east of the lake (samples 13-17) form a looser, more isotopically more depleted cluster near the meteoric line with an average vale of around -17%  $\delta^2$ H, -2.5%  $\delta^{18}$ O. Sample 18, taken from a powerful warm spring at the southern end of the lake may not form part of this second cluster, being slightly more depleted in deuterium and enriched in  $^{18}$ O.

Many thermal waters throughout the world exhibit a significant increase in  $\delta^{19}\mathrm{O}$  as a result of interaction with silicates or carbonates at depth, an effect known as the 'oxygen shift'. However the Magadi spring samples show very little evidence of any shift and in fact the hottest springs fall closest to the meteoric line whereas these would be expected to be the most shifted. Hillaire-Marcel and Casanova (1987) suggest that the oxygen shift has indeed occurred, but that isotopically depleted  $\mathrm{CO}_2$ , associated with the carbonatitic volcanism of the Oldoingo Lengai volcano to the south of Magadi,

has mixed with the springwaters and has resulted in depletion by isotopic exchange. However, while it is true that the waters around Magadi are CO<sub>2</sub>-rich, the above hypothesis is unnecessary and unproven. Apart from the unlikelihood of waters being shifted away from the meteoric line and then fortuitously back onto it (in the case of the hottest springs) the quantities of CO<sub>2</sub> required to exchange with the springwaters would be enormous. A similar explanation is that little or no shift has occurred, probably because flow paths and groundwater residence times of the springwaters are too short for exchange to occur.

Another possible mechanism which may have affected the isotopic compositions of the springwaters is evaporation, such as the trend suggested by Hillaire-Marcel and Casanova (1987) and discussed in Section 7.2. In general terms it is possible that all values which lie to the right of the Kenya Rift Meteoric Line on Figure 7.2, may indeed lie on an evaporative trend even though they are close to the meteoric line. This is because the Kenya Meteoric Line is itself a reflection of evaporative effects, which is why it departs from the World Meteoric Line.

However the data do not support Hillaire-Marcell and Casanova's contention that all the springs lie on an evaporative trend because the most enriched samples (which would be expected to be the most evaporated) lie closest to the local meteoric line. Also the cooler springs, which according to Hillaire-Marcel and Casanova have mixed with recirculated (and therefore highly evaporated) lake brines should therefore be further along the evaporation trend than the hot brines, which they are not.

Eugster's hypothesis concerning spring evolution depends on evaporation for solute concentration but this is not supported by a plot of  $Cl^-$  v.  $\delta^{18}O$  (Figure 7.3) which shows that an increase of salinity of three orders of magnitude is not accompanied by any isotopic enrichment. However his hypothesis is not rejected by such data if the re-dissolution of evaporites by meteoric waters is postulated as the dominant mechanism for brine concentration.

In summary, the hottest springs appear to represent unaltered meteoric water, and their tight clustering indicates that they have not mixed substantially with waters of different composition. This in turn suggests that their original source had a similar isotopic composition to the springs. Such a source is apparent in the Lower Ewaso Ngiro River, which has an isotopic composition which is very similar to those of the hot springs (in fact it is very slightly depleted with respect to the spring isotopes, but this difference could be accounted for by a small amount of evaporation). The river flows along the base of the Nguruman Escarpment approximately 20 km to the west of Lake Magadi and is perennial. The postulated recharge mechanism would therefore be via the river alluvium on the Ewaso Ngiro plain.

#### Lake water.

The enrichment of  $\delta^{18}O$  of the lake brines at Magadi is not accompanied by enrichment in  $\delta^2H$  to give the usual evaporative gradient. This is because of the extreme salinity of the brines (approximately 300,000 mg/l) which causes a reversal of the isotopic gradient to occur, leading to a reduction in  $\delta^2H$  (Gat, 1980).

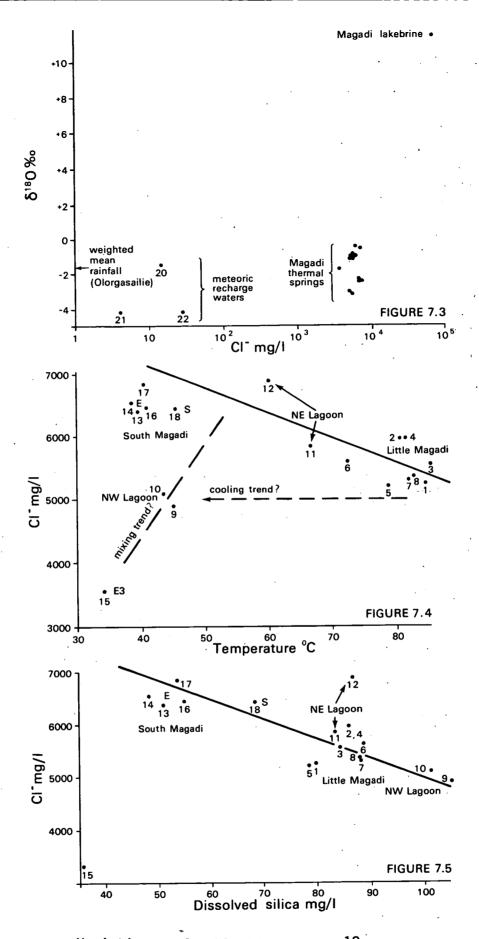


Figure 7.3 Variation of chloride with  $\delta^{18}0$  for Magadi water samples. Figure 7.4 Variation of chloride with temperature for Magadi spring samples. Variation of chloride with silica for Magadi spring samples.

## 7.5 Hydrochemistry.

The springs around Lake Magadi are alkaline Na-HCO<sub>3</sub> brines with chloride a subordinate anion and a salinity range of 30,000 mg/l to 40,000 mg/l. Their hydrochemistry has been described in some detail by Jones and others (1977).

With three exceptions the present data show a direct inverse relationship between dissolved chloride Cl<sup>-</sup>, and discharge temperature (Figure 7.4). Sample 15 is interpreted as a local spring at ambient temperature unrelated to the thermal system. This linear relationship between Cl<sup>-</sup> and temperature implies that the Magadi springs discharge a mixture of two components. A thermal relatively less saline component appears to mix in varying proportions with a cooler saline component prior to discharge. Samples 9 and 10 which do not appear to conform with this view may be on a cooling trend or a mixing trend.

The dependence of silica solubility on temperature controls the levels of  $SiO_2$  in solution above about  $100^{\circ}C$  and dissolved  $SiO_2$  is commonly preserved in solution on subsequent cooling or mixing. A plot of dissolved chloride versus silica (Figure 7.5) supports the inverse mixing relationship and suggests that the NW lagoon springs have cooled on ascent (i.e. they have the highest silica concentrations).

Additional support for the mixing hypothesis comes from a linear relationship between temperature and lithium, sodium and potassium. Overall chemical evidence suggests that a low temperature component with relatively low concentrations of lithium and potassium and higher concentrations of chloride and sodium (and to some extent sulphate) mixes with a thermal component with the inverse properties.

#### 7.6 Discussion

Lake Magadi lies at the lowest point of the southern Kenya Rift Valley and is therefore the point to which all groundwaters in the Rift from Lake Naivasha southwards are directed. This in turn means that the region is a discharge area and a terminus for solutes leached from the rocks composing the Rift by circulating groundwaters, and the presence of evaporites and saline springs in the area is therefore to be expected, as discussed by Baker (1958).

Various attempts have been made to explain more precisely the mechanism for solute concentration and trona formation, and by far the most detailed and most widely accepted in the literature is that of Eugster and others, based on evaporative concentration.

Eugster's hypothesis hinges on the assumption that Na/Cl ratios remain constant from marginal streams to lake brines. This assumption is well supported by data for the sequence from springs to trona formation; but there are few data for the sequence from marginal streams through groundwaters to springs. Eugster proposes surface and capillary evaporation and dissolution of efflorescent crusts as mechanisms of evaporative concentration (Eugster, 1980). The results of the present study indicate that if Eugster's hypothesis is to be accepted only the dissolution of efflorescent crusts by meteoric waters is a possible mechanism for solute concentration.

Of greater importance to the present study, however are Eugster's proposals, supported by Hillaire-Marcel and Casanova (1987) and Crane (1981), regarding the sources of the waters supplying the Magadi thermal springs. Eugster proposes two cool components (Section 7.2) mixing with the thermal component

and Crane cites evidence that the cool meteoric component is a relatively shallow system. Data from the present study, however, indicate essentially a two-component mixing series, with one cool saline end-member and a hot less saline end-member. Also, whereas one of Eugster's cool components is recirculated lake brine the present study indicates that the cool end-member shows little of the evaporation that characterises the true lake brines. On the other hand the interstitial lake brines are so saline (with chloride contents ranging between 37000 mg/l and 96000 mg/l [Eugster, 1980]) that the ratio of groundwater to lakewater would be high to obtain the salinity of the warm springs (c. 7500 mg/l). Eugster's model and the two component mixing model are not necessarily incompatible therefore if a body of ambient groundwater, with a salinity of around 7500 mg/l chloride, is postulated to exist in the sediments underlying the lake formed by a mixture of meteoric water and either recirculated lakewater or perhaps dissolved evaporites.

Some evidence for the existence of a saline groundwater body is that a borehole drilled to 297 m encountered brines with a salinity of 20000 mg/l chloride in the lavas beneath the lake (Eugster, 1980). This borehole was stated as being artesian (i.e. indicating upward flow within the lavas towards some discharge area) but no temperature data were given.

The third and geothermally significant component of Eugster's spring model is the proposed hot saline groundwater body with a composition similar to the hottest springs at Little Magadi (i.e. with a chloride content of around 5000 mg/l and a TDS of around 30000 mg/l). Eugster's evidence for such a body is the constancy of spring temperatures and chemistry over several decades. Paradoxically Crane (1981) presents data of <u>variations</u> in spring temperature over several decades but concludes that as the hot spring temperatures do not vary with changes in rainfall then they must originate in a deep reservoir.

Data from the present study support Eugster's hot spring source. The chemical data suggest a single end-member source for the hot springs and the clustering of the isotopic data indicate that the hottest springs have not mixed significantly with other waters and therefore represent the hot end-member of the mixing series. If this is so then Silica geothermometry may be used to estimate the temperature of the springs at depth (other cation geothermometers cannot be used because of the origin of the solutes). Table 5.14 shows that these temperatures are low, never reaching 150°C. (The highest temperatures estimated by silica geothermometry are in fact those for the two NW Lagoon samples, which do not fall in the same isotope cluster on Figure 7.2 as the other hot springs, for reasons which are unknown).

An alternative interpretation of the data is raised by Mahon's (1972) suggestion that much of the Rift is underlain by a hot body of water containing a few hundred parts per million of chloride. This view was based on similarities in the chemistry of fluids at Olkaria and hot springs further north near lakes Elmenteita, Bogoria and Baringo. If it were assumed that a hot end-member of the Magadi mixing series existed with a chloride content of 450 mg/l (similar to that found at Olkaria) then this body of water would, from Figure 7.4, have a temperature slightly in excess of 200°C. There is however no direct evidence for any such water in the Magadi area and the hypothesis is regarded as unlikely.

The best indications of the likely source of the Magadi thermal water are provided by the stable isotope data. These show (Figure 7.2) that the water is meteoric but more enriched than the sampled groundwaters (although these were obtained from a significant distance to the north-west). From the

available data, the most likely source is the Ewaso Ngiro River which runs along the base of the Nguruman Escarpment some 25 km to the west of Lake Magadi. In this area the Ewaso Ngiro River has undergone some evaporation and is somewhat enriched isotopically, compared with its headwaters. Figure 7.2 shows that its isotopic composition is in fact very close to that of the northern Magadi hot springs and the very small difference in composition could readily be attributed to further evaporation and some mixing with local groundwaters. (Mixing could also explain the displacement of the NW Lagoon springs from the main hot spring cluster).

It has sometimes been suggested that the Magadi hot springs could have their origin in the groundwater recharge from Lake Naivasha, but this may be refuted on two accounts. Firstly the hot spring stable isotope data show no connection with the highly enriched samples obtained from Lake Naivasha. Secondly isotopic evidence from groundwaters around Lake Naivasha indicates that the lakewater becomes significantly diluted by mixing with local groundwaters within a short distance of the lake, and dilution would increase as the lakewater flowed south. Therefore, while some lakewater may eventually reach the Magadi springs, it would be so diluted as to be unrecognisable.

A more pertinent question therefore is whether the Magadi hot springs have their origin in the mix of waters flowing from the north, or from essentially local sources such as the Ewaso Ngiro and the Nguruman Escarpment, and in the absence of other data the isotopic evidence favours a local origin. The lack of an oxygen isotope shift in the hot springs also suggests a local origin by implying a short contact time between water and rock, and therefore a short flow path. The postulated recharge mechanism would therefore be via the river alluvium of the Ewaso Ngiro plain to the west of Lake Magadi.

The short distance between recharge and discharge areas suggests a convective cell driven by a local heat source probably to the west of Magadi, of unknown origin.

In conclusion, the Magadi hot springs appear to derive from a hot, saline groundwater body with a temperature of between 100-150°C. Recharge is considered to be provided by the lower Ewaso Ngiro River and local groundwaters derived from the sides of the Rift, with cold waters percolating through the river alluvium and underlying volcanics and rising, after being heated, via active grid faults around Lake Magadi. The heat source for the springs is probably local and lies to the west of Lake Magadi. Although the heat output of the springs is significant (estimated as greater than 250 MW from their discharge, and 900 MW from infra-red analysis) the low indicated reservoir temperature would rule out the use of the resource for electrical power generation unless binary systems were to be considered.

Finally it is suggested that further geothermal research in the Magadi area should include shallow borehole drilling to the north of Magadi in order to identify the characteristics of fluid flowing from the north, and geophysical work/borehole drilling to the west of Little Magadi to attempt to identify the postulated thermal upflow in this area.

#### 8 CONCLUSIONS

On a regional scale the Rift Valley between Lakes Nakuru and Magadi broadly exhibits the hydrogeological features expected of a Valley-interfluve system with lateral groundwater flows from the Rift escarpments to discharge areas on the Rift floor, and axial groundwater flows away from the Rift floor culmination at Lake Naivasha. This model is modified by the presence of the major Rift faults, which act as barriers to lateral flow, leading to longer, deeper, flow paths, and by the grid faulting in the Rift floor which tend to align flow paths within the Rift along its axis.

The permeabilities of the volcanic rocks underlying the Rift Valley are generally low, although there is considerable local variation. normally found in fractured or reworked volcanics, or along the weathered contacts between different lithological units. The highest values of permeability are found in the reworked volcanics composing the sediments of the Naivasha area, where the specific capacities of wells often exceed 3 l/s/m and where estimated hydraulic conductivities of greater than 10 m/d In the Rift floor to the north, where the sediment size decreases, borehole specific capacities fall, to around 0.3 1/s/m in the Elmenteita-Nakuru area (leading to an estimated average ' hydraulic conductivity of 2 m/d). On the Rift escarpments the permeabilities of the different rock types are uniformly low. Mean borehole specific capacities and estimated hydraulic conductivities range from 0.03 l/s/m and 0.1 m/d for the South Kinangop Pyroclastics to 0.2 l/s/m and 1.1 m/d for the Rift Escarpment Trachyte to the east of Suswa and the Mau Forest pyroclastics.

These figures are only applicable to the drilled depths of the boreholes, normally less than 250 m. Below this depth permeabilities will fall, mainly as a result of the closure of fissures by overburden stresses. The only available data for permeability at depth are from the Olkaria Geothermal Field where values of around 5 mD have been found, equivalent to a cold water hydraulic conductivity of about  $3\times10^{-3}$  m/d. Simple modelling in the present study has suggested an upper limit of 0.1 m/d for rocks at depth in the Naivasha area.

Preliminary estimates of subsurface flows from the Naivasha catchment suggest that the amount contributed by Lake Naivasha is around  $50 \times 10^6$  m³/y (which is 20% of the total recharge estimated by a previous water balance study). Flow to the south via relatively shallow aquifers (i.e. at depths of less than about 500 m) may be the most significant route for water flow from the catchment, accounting for perhaps 50% to 90% of the total.

Chemical data obtained during the present study have enabled the model of the ambient flow systems to be refined. Stable isotope determinations on samples of rainfall taken over a wide area have enabled an isotopic meteoric line for the Rift to be constructed which is similar to the trend for ambient and slightly thermal groundwaters. In addition an approximate correlation of isotopic composition with height has been found. This correlation suggests that much of the groundwater in the Naivasha-Nakuru area is relatively local in origin, particularly at lower altitudes according to the inert gas data. Such an interpretation is supported by modern radiocarbon ages and the lack of enhancement in radiogenic inert gases. The implication is that deep components of flow are not important in the shallow hydrology of the Rift floor, and therefore supports the contention that permeabilities at depth are low.

The most important result of the chemical analyses with regard to ambient

(and geothermal) water flows in the Study Area of the Rift is the tracing of water from Lake Naivasha using stable isotope data. River water entering the Lake has a very depleted composition indicative of its origin at high altitudes (principally in the Nyandarua Mountains). Meteoric water entering the lake directly has a less depleted composition similar to that of However the lake itself is highly enriched by virtue of the intense evaporation to which it is subjected. Enriched lakewater flowing both to the north and to the south can therefore be detected in groundwater and geothermal fluid samples by stable isotope analysis. By this method it has been shown that Lake Naivasha water flows northwards via Gilgil - but not apparently under Eburru - at least as far as Lake Elmenteita, where it estimated to form 30% of the discharge of warm springs bordering the lake. To the south a component of Naivasha lakewater has been detected as far but there is no evidence that it reaches Lake Magadi in identifiable form.

The interpretation of geochemical analyses of geothermal fluids from Eburru, Olkaria, Longonot and Suswa has led to the important conclusion that all the fluids can be explained in terms of a mixing series between Rift-wall meteoric water and water from Lake Naivasha and that there is no evidence of a unique deep thermal water. At Eburru, analysis of fumarole condensates and gases indicates that the steam is basically primary and is derived from local Rift-wall groundwater; well and spring-waters to the north of Eburru show evidence of outflow of geothermal fluids in this direction. At Olkaria the wellfield shows evidence of a 55-75% lakewater component mixing with Rift-wall groundwater; fumaroles in the Domes area further east indicate a smaller but significant (>30%) lakewater contribution, and fumaroles in Longonot crater, east of the Domes, show only traces of lakewater. Longonot and Mt. Margaret, fumaroles show no evidence of lakewater influence. The Suswa area shows evidence of lakewater, but only in fumaroles in the ring graben and central island (where however a substantial contribution - 30% of lakewater has been detected).

Further south, at Magadi, the hot springs are considered to derive from a hot saline groundwater body, whose origin lies in a mixture between recharging waters from the lower Ewaso Ngiro River and local groundwaters. No evidence of the presence of Naivasha lakewater has been found.

To the north, basic geochemical sampling of the Lake Bogoria and Lake Baringo thermal systems tends to confirm that lakewater mixing is involved, although at Baringo this appears to take place in an unexpected manner. The Kapedo and Lorusio springs north of Lake Baringo are not obviously affected by subsurface outflow from the lake

There is no evidence in any of the geothermal fluids sampled of a  $\delta^{18}O$  shift of the magnitude commonly seen in other geothermal systems. This could be due to rapid transit times, or to equilibration of rock and water  $\delta^{18}O$  values, but too little is yet known of rock  $^{18}O/^{16}O$  values to understand which process is involved.

Gases in the geothermal fluids are dominated by crustally-derived  ${\rm CO_2}$  usually followed by  ${\rm CH_4}$  - although at a much lower level. (There is also evidence of a pervasive  ${\rm CO_2}$  flux over much of the Rift which is unrelated to specific geothermal fields). The presence of He and H<sub>2</sub> - regarded as indicators of upflow conditions - has been confirmed at Eburru and at Longonot. High  $^3{\rm He}/^4{\rm He}$  ratios, taken to represent evidence of the transport of mantle helium, are found at Eburru, Longonot and Olkaria. The ratio of  ${\rm C_2H_6/CH_4}$  may be an index of lakewater contribution to groundwaters and geothermal fluids

and is found to vary with distance from Lake Naivasha, thus supporting the mixing model.

The use of chemical geothermometers in the Rift has met with variable success. In the Olkaria geothermal field quartz, alkali and gas geothermometers give plausible temperatures. However in the other thermal areas there are few opportunities to sample hot water, and the gas geothermometers are often problematic; the ratio types commonly cannot be used because of the scarcity of  $\rm H_2$  and  $\rm H_2S$  in fumarolic gases. At Magadi the highly alkaline nature of the springs precludes the use of the alkali geothermometers, although those based on quartz seem to be reliable. Ambient or slightly thermal waters elsewhere in the study area often give excessive indications of temperature which are unsupported by other evidence.

Two thermal areas, Olkaria and Magadi were examined in some detail during the study. At Olkaria the results support the conclusion of other workers that the present wellfield is situated somewhat to the south of a thermal upflow. Also there are indications that short flow paths may be involved, and that the system may be quite old. At Magadi it is concluded that the thermal springs are formed by a two-component mixing series, probably with a local heat source, and that the hot end member is at a temperature of 100-130°C.

With regard to the warm springs found at various points along the Rift margins, there is no indication that these are anything other than local phenomena associated with Rift faults and result from deep groundwater circulation under ambient geothermal gradients. The geothermal potential of these springs is therefore low.

In summary, the main conclusions of this study are that the geothermal areas at Eburru, Olkaria-Domes, Longonot, Suswa and Magadi are individual geothermal fields where local heat sources set up convective cells which circulate fluids which originate as mixtures of ambient groundwaters and Naivasha Lakewater (or in the case of Magadi, probably a mixture of groundwater and recharging river water). There is no evidence of a deep thermal fluid pervasive over large areas of the Rift - chemical similarities between geothermal fluids from different areas are caused by similar groundwaters reacting with similar rock types. Thermal areas north of Nakuru (Bogoria, Baringo, Kapedo and Lorusio) though sampled in much less detail during this study, are considered to have a fundamentally similar mode of origin.

It is also tentatively concluded from the limited available data that recharge into the Naivasha catchment should be ample to sustain production from geothermal fields bordering the catchment - however a thorough water balance study would be needed to be certain of this. Further south, groundwater conditions around Suswa are virtually unknown, and therefore the availability of recharge is speculative. There are indications however of at least some hydraulic connection with the Naivasha catchment.

It is recommended therefore that future exploration should concentrate on areas where high temperatures and thermal upflow conditions are expected, and present data suggest that these are to be found principally at Eburru, Olkaria, Longonot and probably Suswa. Magadi appears to have limited potential in view of the low temperatures indicated - although the heat output from the area is high. Areas of outflow from the fields, that is to the north of Eburru and to the south of Olkaria, Longonot and Suswa are not expected to possess significant geothermal potential, nor are areas between the fields.

## **General References**

- Andrews, J.N. and Kay, R.L.F. 1982. Natural production of tritium in permeable rocks. Nature, 298, 361-363.
- Armannsson, H. 1987a. Geochemistry of steam in the Suswa and Longonot geothermal areas. Technical Report. Project KEN/82/002. United Nations Department of Technical Co-operation for Development.
- Armannsson, H. 1987b. Studies on the geochemistry of steam in the Suswa and Longonot areas and water in the Lake Magadi, Kedong Valley and Lake Turkana areas, Rift Valley, Kenya. Final Technical Report. Project KEN/82/002. United Nations Department of Technical Co-operation for Development.
- Arnason, B. 1977. The hydrogen and water isotope thermometer applied to geothermal areas in Iceland. Geothermics, 5, 125-151.
- Arnorsson, S. and Gunnlaugsson, E. 1985. New gas geothermometers for geothermal exploration calibration and application. Geochimica et Cosmochimica Acta, 49, 1307-1325.
- Bailey, D.K. 1980. Volcanism, Earth degassing and replenished lithosphere mantle. Philosophical Transactions Royal Society London, A297, 309-322.
- Baker, B.H. 1958. Geology of the Magadi Area. Report Geological Survey of Kenya 42.
- Baker, B.H., Mohr, P.A. and Williams, L.A.J. 1972. Geology of the Eastern Rift System of Africa. Geological Society of America Special Paper 136. 67 pp.
- Baker, B.H., Williams, L.A.J., Miller, J.A. and Fitch, F.J. 1971. Sequence and geochronology of the Kenya Rift volcanics. Tectonophysics, 11, 191-215.
- Bennion, D.W. and Griffiths, J.C. 1966. A stochastic model for predicting variations in reservoir rock properties. Transactions American Institute of Mining Engineers, 237, 9-16.
- Bodvarsson, S., Pruess, K., Stefansson, V., Bjornsson, S. and Ojiambo, S.B. 1987. East Olkaria Geothermal Field, Kenya. 1: History Match With Production and Pressure Data Decline. Journal of Geophysical Research, 92, No. B1, 521-539.
- Browne, P.R.L. 1984. Subsurface stratigraphy and hydrothermal alteration of the eastern section of the Olkaria Geothermal Field, Kenya. Proceedings 6th New Zealand Geothermal Workshop, Auckland, N.Z., 33-41.
- Bwire-Ojiambo, S. 1984. Isotope hydrogeochemistry of Lakes Elmenteita and Naivasha catchment areas. Unpublished paper to Olkaria review meeting, Nairobi December 1984, 8 pp.

- Craig, H. 1963. In "Nuclear Geology on Geothermal Areas", (E.Tongiorgi, ed.), 17-53. Consiglio Nazionale della Richerche, Lab. di Geol. Nucl. Pisa.
- Craig, H. Lupton, J.E. and Horowitz R.M. 1977. Isotopic geochemistry and hydrogeology of geothermal waters in the Ethiopian Rift Valley. Scripps Institute of Oceanography. Reference Number 77-14, University of California, San Diego.
- Crane, K. 1981. Thermal variations in the Gregory Rift of southern Kenya. Tectonophysics, 74, 239-262.
- Dansgaard, W. 1964. Stable isotopes in precipitation. Tellus 16, 436.
- Darling, W.G. and Armannsson, H. 1989. Stable isotopic aspects of fluid flow in the Krafla, Namafjall and Theistareykir geothermal systems of north-east Iceland. Chemical Geology 76, No. 3/4.
- Darling, W.G., Bath, A.H. and Brunsdon, A.P. 1982. Revised procedures for the measurement of <sup>2</sup>H/<sup>1</sup>H and <sup>18</sup>O/<sup>16</sup>O in water samples. BGS Hydrogeology Group Stable Isotope Technical Report No. 16.
- Darling, W.G. and Lardner, A.J. 1985. The effect of altitude on the stable isotope composition of rainfall in the Balquhidder research catchments. BGS Hydrogeology Research Group Stable Isotope Technical Report No. 27.
- Eugster, H.P. 1970. Chemistry and origin of the brines of Lake Magadi, Kenya. Mineralogical Society of America Special Paper 3, 215-235.
- Eugster, H.P. 1980. Lake Magadi, Kenya, and its précursors. In "Developments in Sedimentology", 28, Hypersaline brines and evaporitic environments. Editor, A. Nissenbaum. Elsevier.
- Fournier, R.O and Potter R.W. 1979. Magnesium correction to the Na-K-Ca chemical geothermometer. Geochimica et Cosmochimica Acta, 43,1543-1550.
- Freeze, R.A. and Cherry J.A. 1979. Groundwater. Prentice-Hall. 604 pp.
- Geotermica Italiana Srl. 1987. Geothermal Reconnaissance Survey in the Menengai-Bogoria Area of the Kenya Rift Valley. Final Draft Report Part IV Hydrogeology. TCD CON 7/85 KEN 82/002.
- Glover, R.B. 1972. Chemical characteristics of water and steam discharges in the Rift Valley of Kenya. Unpublished Report to the UNDP, 56 pp.
- Grant, M.A. and Whittome, A.J. 1981. Hydrology of Olkaria Geothermal Field.

  Proceedings 3rd New Zealand Geothermal Workshop, Auckland N.Z.,
  125-129.
- Haukwa, C.B. 1984. Recent measurements within Olkaria East and West Fields.

  Paper for Kenya Power Company Scientific and Technical Review
  Meeting, 13 pp.
- Haukwa, C.B. 1986. Interpretation of well measurements for exploration

- areas and reservoir changes in Olkaria East Field. Paper for Kenya Power Company Scientific and Technical Review Meeting, 11 pp.
- Hillaire-Marcel, C. and Casanova, J. 1987. Isotopic hydrology and paleohydrology of the Magadi (Kenya) Natron (Tanzania) basin during the late Quaternary. Palaeogeography, Palaeoclimatology, Palaeoecology, 58, 155-181.
- Hulston, J.R. 1977. Isotope work applied to geothermal systems at the Institute of Nuclear Sciences, New Zealand. Geothermics, 5, 89-96.
- Jones, B.F., Eugster H.P. and Rettig, S.L. 1977. Hydrochemistry of the Lake Magadi basin, Kenya. Geochimica et Cosmochimica Acta. 44, 53-72.
- Logan, J. 1964. Estimating transmissibility from routine production tests of water wells. Groundwater, 2, No. 1,35-37.
- Mahon, W.A.J. 1972. The general geochemistry of the Rift Valley of Kenya,
  Lake Baringo to Lake Magadi, and the geochemistry of Olkaria,
  Eburru and Lake Hannington geothermal prospects. Technical Review
  Meeting Report. United Nations Geothermal Resources Exploration
  Project.
- Mazor, E. 1977. Geothermal tracing with atmospheric and radiogenic noble gases. Geothermics, 5, 21-36.
- McCall, G.J.H. 1957. Geology and groundwater conditions in the Nakuru area.

  Ministry of Works (Hydraulic Branch) Technical Report No. 3.
- McCall, G.J.H. 1967. Geology of the Nakuru-Thompson's Falls-Lake Hannington area. Report Geological Survey of Kenya 78.
- McCann, D.L. 1972. A preliminary hydrogeologic evaluation of the long-term yield of catchments related to the geothermal prospect areas in the Rift Valley of Kenya. Unpublished U.N Report. 23 pp.
- McCann, D.L. 1974. Hydogeologic investigation of the Rift Valley catchments. Unpublished U.N Report. 47 pp.
- Nier, A.O. 1950. A redetermination of the relative abundances of the isotopes of carbon, nitrogen, oxygen, argon and potassium. Physics review, 77, 789.
- Noble, J.W. and Ojiambo, S.B. 1975. Geothermal exploration in Kenya. Second U.N. Symposium, Development and use of Geothermal Research, San Francisco, California, U.S.A., 189-204.
- Ogoso-Odongo, M.E. 1986. Geology of the Olkaria geothermal field. Geothermics, 15, No. 5/6, 741-748.
- Paces, T. 1975. A systematic deviation from the Na-K-Ca geothermometer below 75 C and above  $10^{-4}$  atm  $P_{\rm CO2}$ . Geochimica et Cosmochimica Acta, 39, 541-544.
- Panichi, C. and Tongiorgi, E. 1974. Isotopic study of the hot water and steam samples of the Rift Valley, Kenya. Unpublished report to the U.N.D.P, 56 pp.

- Parkinson, J. 1914. The East African Trough in the neighbourhood of the soda lakes. Geographical Journal, 44, 33-49
- Sikes, H.L. 1935. Notes on the Hydrology of Lake Naivasha. Journal of The East Africa and Uganda Natural History Society, 13, 74-89.
- Stevens, J.A. 1932. Lake Magadi and its alkaline springs. Unpublished report to the Magadi Soda Co. Ltd., Kenya.
- Thiem, G. 1906. Hydrologische Methoden. Gebhardt, Leipzig. 56 pp.
- Thompson, A.O. 1964. Geology of the Kijabe Area. Report Geological Survey of Kenya 67.
- Thompson, A.O. and Dodson, R.G. 1963. Geology of the Naivasha area. Report Geological Survey of Kenya 55.
- Tobin, D.G., Ward P.L. and Drake C.L. 1969. Microearthquakes in the Rift Valley of Kenya. Geological Society of America Bulletin, 80, 2043-2046.
- Truesdell, A.H. 1975. Geochemical techniques in exploration. <u>In</u> Proceedings of the Second United Nations Symposium on the development and use of Geothermal Resources, 1, 53-86.
- Warren, J.E. and Price, H.S. 1961. Flow in heterogeneous porous media.

  Journal Society of Petroleum Engineers, 1, 153-169.

# BGS Internal Reports in Chronological Order

- Burgess, W.G. 1985. Report on a visit 22 October to 30 November 1985. Report WD/OS/85/31
- Burgess, W.G. 1986. Report on a visit 17 March to 26 April 1986. Report WD/OS/86/4.
- Burgess, W.G. 1986. Hydrogeology and geothermics of the Magadi-Longonot Sector. Report WD/OS/86/5.
- Burgess, W.G. 1986. Notes on the groundwater conditions in the Longonot-Nakuru Sector of the Rift Valley. Report WD/OS/86/6.
- Allen, D.J. 1986. Report on a visit 11-17 October 1986.
- Allen, D.J. and Darling W.G. 1987. Interpretation of fluid sample analyses from Magadi-Silale area. Report WD/OS/87/3
- Allen, D.J. 1987. Report on a visit 10 March to 3 April 1987. Report WD/OS/87/8.
- Allen, D.J. 1987. Report on a visit 18 May to 30 May 1987. Report WD/OS/87/14.
- Allen, D.J. and Darling W.G. 1987. Hydrogeology progress Report, March-August 1987. Report WD/OS/87/16.

Darling, W.G. 1987. Report on a visit 28 April to 28 May 1987. Report WD/OS/87/12.

# APPENDICES

# APPENDIX 1 - GENERAL BOREHOLE DATA

| BOREHOLE<br>NUMBER | EASTING      | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--------------------|--------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| 0001C              | 2263         | 99149          | 143/3          | 2450                         | 2317                         | 16/05/85                       |
| C0054              | 2094         | 99264          | 133/2          | 1910                         | 1895                         | 27/10/39                       |
| C0057              | 2187         | 99111          | 133/4          | 2088                         | <1994                        | 27/10/39                       |
| C0059              | 1799         | 99411          | 133/1          | 1880                         | 1776                         | 03/12/39                       |
| C0079              | 1798         | 99413          | 133/1          | 1880                         | 1784                         | 25/04/33                       |
| C0092              | 2191         | 99108          | 133/4          | 2118                         | <1960                        | 31/12/39                       |
| C0107              | 1563         | 99607          | 118/4          | 2261                         | <2186                        | -/12/30                        |
| C0108              | 1392         | 99694          | 118/4          | 2480                         | 2460                         | -/12/30                        |
| C0115<br>C0131     | 2038<br>1391 | 98844          | 147/2          | 1600<br>2480                 | <1350<br>2467                | 17/07/41<br>04/10/40           |
| C0131<br>C0132     | 1391         | 99697<br>99693 | 118/4<br>118/4 | 2480                         | 2467<br>2464                 | 14/10/40                       |
| C0152              | 1793         | 99685          | 119/3          | 1861                         | 1813                         | 19/11/41                       |
| C0164              | 1555         | 99598          | 118/4          | 2332                         | 2313                         | 23/12/41                       |
| C0165              | 1818         | 98719          | 147/1          | 2030                         | <1875                        | 10/04/47                       |
| C0202              | 1567         | 99595          | 118/4          | 2320                         | 2282                         | 26/11/42                       |
| C0204              | 1795         | 99684          | 119/3          | 1860                         | 1834                         | 30/10/42                       |
| C0205              | 1582         | 99625          | 118/4          | 2195                         | 2091                         | 14/12/42                       |
| C0208              | 1548         | 99651          | 118/4          | 2292                         | <2092                        | 24/01/43                       |
| C0210              | 2092         | 99094          | 133/4          | 1910                         | 1895                         | 15/02/43                       |
| C0211              | 1587         | 99615          | 118/4          | 2220                         | 2130                         | 18/02/43                       |
| C0214              | 1657         | 99674          | 118/4          | 1880                         | 1825                         | 28/02/43                       |
| C0220<br>C0223     | 1589<br>1574 | 99563<br>99554 | 118/4<br>118/4 | 2300<br>2406                 | 2267<br>2353                 | 24/04/43<br>26/05/43           |
| C0223              | 1567         | 99567          | 118/4          | 2367                         | 2304                         | 17/06/43                       |
| C0231              | 2143         | 99198          | 133/2          | 1896                         | 1887                         | 06/07/43                       |
| C0258              | 1536         | 99662          | 118/4          | 2228                         | 2173                         | 21/03/43                       |
| C0261              | 1767         | 99337          | 133/1          | 2120                         | 2049                         | 31/07/43                       |
| C0264              | 2272         | 99034          | 134/3          | 2580                         | 2437                         | 24/08/43                       |
| C0266              | 1836         | 99418          | 133/1          | 1880                         | 1776                         | 10/09/43                       |
| C0288              | 1440         | 99684          | 118/4          | 2220                         | 2138                         | 19/02/44                       |
| C0295              | 2157         | 99260          | 133/2          | 2000                         | 1962                         | 17/07/43                       |
| C0306<br>C0307     | 1724         | 99625          | 119/3          | 1780                         | 1761                         | 28/06/44<br>04/08/44           |
| C0307              | 1723<br>1802 | 99637<br>99678 | 119/3<br>119/3 | 1780<br>1880                 | 1770<br>1813                 | 17/05/47                       |
| C0321              | 2084         | 99724          | 119/3          | 2360                         | 2337                         | 03/12/43                       |
| C0376              | 1456         | 99673          | 118/4          | 2411                         | 2374                         | 05/09/45                       |
| C0379              | 1443         |                | 118/4          | 2257                         | <2257                        | 21/09/45                       |
| C0381              | 2434         | 97868          | 161/3          | 1650                         | 1627                         | 03/10/45                       |
| C0407              | 2327         | 98695          | 148/1          | 2140                         | 2002                         | 01/05/46                       |
| C0408              | 1790         | 99685          | 119/3          | 1885                         | 1788                         | 24/04/47                       |
| C0416              | 2355         | 98723          | 148/1          | 2140                         | 2073                         | 03/06/46                       |
| C0417              | 1971         | 99679          | 119/4          | 2480                         | 2341                         | 08/06/46                       |
| C0419              | 1680         | 99619          | 119/3          | 1970                         | 1840                         | 24/05/46                       |
| C0423<br>C0429     | 1472<br>1889 | 99687<br>99431 | 118/4<br>133/1 | 2280<br>1840                 | 2216<br>1768                 | 03/11/45<br>22/06/46           |
| C0429              | 1828         | 99389          | 133/1          | 1940                         | 1781                         | 27/04/40                       |
| C0440              | 2353         | 98613          | 148/3          | 2020                         | 1974                         | 11/07/46                       |
| C0451              | 2390         | 97883          | 161/3          | 1520                         | 1476                         | 28/08/46                       |
| C0456              | 1944         | 99552          | 119/4          | 1860                         | 1813                         | 05/08/46                       |
| C0457              | 2110         | 99354          | 133/2          | 2000                         | 1973                         | 31/08/46                       |
| C0458              | 2124         | 99331          | 133/2          | 1928                         | 1891                         | 22/08/46                       |
| C0463              | 1464         | 99557          | 118/4          | 2760                         | 2747                         | 06/09/46                       |
| C0465              | 2087         | 99374          | 133/2          | 1960                         | 1919                         | 19/09/46                       |

| BOREHOLE<br>NUMBER | EASTING      | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--------------------|--------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| C0466              | 1911         | 99165          | 133/3          | 1940                         | 1891                         | 26/09/46                       |
| C0467              | 2156         | 99142          | 133/4          | 1960                         | 1877                         | 11/10/46                       |
| C0468              | 2090         | 99257          | 133/2          | 1910                         | 1893                         | 10/10/46                       |
| C0485              | 1636         | 99646          | 118/4          | - 2087                       | 2023                         | 11/11/46                       |
| C0510              | 1847         | 98788          | 147/1          | 2040                         | <1875                        | 28/02/47                       |
| C0511              | 1847         | 98732          | 147/1          | 1770                         | <1599                        | 07/02/47                       |
| C0531<br>C0533     | 2146<br>1846 | 99196<br>99364 | 133/2<br>133/1 | 1920<br>1990                 | 1904<br>1784                 | 29/05/47<br>30/05/47           |
| C0553              | 2375         | 99219          | 134/1          | 2560                         | 2472                         | 10/7/30-                       |
| C0562              | 2109         | 99116          | 133/4          | 1900                         | 1877                         | 25/06/47                       |
| C0563              | 1959         | 99106          | 133/4          | 1900                         | 1893.                        | 23/07/47                       |
| C0567              | 2139         | 99098          | 133/4          | 1955                         | 1899                         | 18/06/47                       |
| C0570              | 2022         | 99552          | 119/4          | 2340                         | 2310                         | 03/08/47                       |
| C0572              | 2228         | 99138          | 134/3          | 2220                         | 2010                         | 29/08/47                       |
| C0579              | 2013         | 99103          | 133/4          | 1900                         | 1878                         | 13/09/47                       |
| C0580              | 2142         | 99146          | 133/4          | 1925                         | 1879                         | 06/09/47                       |
| C0581              | 2002         | 99098          | 133/4          | 1900                         | 1877                         | 12/07/47                       |
| C0582              | 2119         | 99125          | 133/4          | 1895                         | 1881                         | 07/07/47                       |
| C0605<br>C0624     | 2381<br>1538 | 97887          | 161/3<br>118/4 | 1500<br>2236                 | 1378<br>2175                 | 20/09/47<br>22/01/48           |
| C0624<br>C0628     | 2107         | 99654<br>99148 | 133/4          | 1900                         | 1854                         | 08/10/47                       |
| C0631              | 1975         | 99208          | 133/4          | 1910                         | 1883                         | 17/11/47                       |
| C0633              | 2317         | 99074          | 134/3          | 2670                         | 2506                         | 17/06/85                       |
| C0634              | 2349         | 99126          | 134/3          | 2600                         | 2561                         | 15/01/48                       |
| C0648              | 1549         | 99671          | 118/4          | 2217                         | <1988                        | 09/03/48                       |
| C0651              | 2345         | 99316          | 134/1          | 2580                         | <2419                        | 10/3/48                        |
| C0655              | 1516         | 99674          | 118/4          | ^ 2174                       | 2098                         | 04/03/48                       |
| C0665              | 1456         | 99704          | 118/4          | 2280                         | 2143                         | 08/04/48                       |
| C0667              | 2111         | 99145          | 133/4          | 1904                         | 1881                         | 15/10/47                       |
| C0670<br>C0677     | 1803<br>2389 | 99676<br>99233 | 119/3<br>134/1 | 1850<br>2610                 | 1798<br><2427                | 21/05/48<br>28/05/48           |
| C0677              | 2390         | 99233          | 134/1          | 2590                         | 2557                         | 02/05/48                       |
| C0678              | 2268         | 99193          | 134/1          | 2520                         | <2410                        | 12/06/48                       |
| C0692              | 2269         | 99189          | 134/1          | 2520                         | 2362                         | 26/06/48                       |
| C0699              | 2371         | 99198          | 134/1          | 2520                         | 2444                         | 02/07/48                       |
| C0703              | 2328         | 99092          | 134/3          | 2650                         | 2565                         | 10/07/48                       |
| C0704              | 1964         | 99285          | 133/2          | 2469                         |                              | 21/04/48                       |
| C0705              | 1965         | 99296          | 133/2          | 2440                         | <2394                        | 26/04/48                       |
| C0706              | 1966         | 99294          | 133/2          | 2460                         | <2400                        | 29/04/48                       |
| C0707              | 1966         | 99290          | 133/2          | 2480                         | 1014                         | 07/05/48                       |
| C0719<br>C0729     | 1803<br>2125 | 99676<br>99039 | 119/3<br>133/4 | 1880<br>2050                 | 1814<br>1890                 | 18/09/49<br>30/09/48           |
| C0729 ·            | 1816         | 99668          | 119/3          | 1870                         | 1809                         | 12/10/48                       |
| C0732              | 2019         | 99405          | 133/2          | 2042                         | 1849                         | 26/06/48                       |
| C0741              | 1643         | 99470          | 118/4          | 2320                         | 2278                         | 21/10/48                       |
| C0745              | 1574         | 99606          | 118/4          | 2240                         | 2145                         | 05/11/48                       |
| C0780              | 2268         | 99185          | 134/1          | 2540                         | 2358                         | 18/08/48                       |
| C0783              | 1721         | 99406          | 133/1          | 2180                         | 2089                         | 27/11/48                       |
| C0804              | 2079         | 99702          | 119/4          | 2360                         | 2318                         | 23/12/48                       |
| C0805              | 1698         | 99688          | 119/3          | 1870                         | 1757                         | 00/12/48                       |
| C0811              | 2474         | 98029          | 161/3          | 1760                         | 1742                         | 30/01/49                       |
| C0813              | 1851         | 99621          | 119/3          | 1900                         | 1779                         | 08/03/49                       |
| C0814<br>C0822 .   | 2200         | 99243<br>99621 | 133/2<br>119/3 | 2179<br>1900                 | 2136<br><1762                | 23/02/48<br>00/11/48           |
| C0822 .            | 1844<br>2416 | 97788          | 172/1          | 1640                         | 1503.                        | 07/03/49                       |
| C0836              | 1823         | 99650          | 119/3          | 1890                         | 1821                         | 12/04/49                       |

|     | BOREHOLE<br>NUMBER | EASTING                   | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|-----|--------------------|---------------------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| (   | C0839              | 2435                      | 98563          | 148/3          | 1880                         | 1855                         | 29/12/48                       |
|     | C0845              | 1759                      | 99415          | 133/1          | 1920                         | 1794                         | 09/04/49                       |
|     | C0855              | 1665                      | 99703          | 119/3          | 1954                         | 1771                         | 00/14/49                       |
|     | C0858              | 1831                      | 99598          | 119/3          | 1882                         | 1766                         | 07/05/49                       |
| - ( | C0869              | 1841                      | 99615          | 119/3          | 1900                         | 1769                         | 01/06/49                       |
| - 4 | C0870              | 2014                      | 99720          | 119/4          | 2620                         | 2542                         | 02/03/49                       |
|     | C0872              | 2076 <sup>-</sup>         | 99718          | 119/4          | 2400                         | 2352                         | 02/04/49                       |
|     | C0875              | 2408                      | 97759          | 172/1          | 1540                         | 1467                         | 31/05/49                       |
|     | C0882              | 1696                      | 99702          | 119/3          | 1929                         | 1769                         | 11/05/49                       |
|     | C0910              | 2097                      | 99081          | 133/4          | 1940                         | 1927                         | 28/05/49                       |
|     | C0916              | 1598                      | 99595          | 118/4          | 2140                         | 2022                         | 23/06/49                       |
|     | C0921<br>C0939     | 1508                      | 99595          | 118/4          | 2500<br>2127                 | 2402<br>2001                 | 06/04/49<br>19/09/49           |
|     | C0939<br>C0946     | 2204 <sup>°</sup><br>2236 | 99171<br>99216 | 133/2<br>134/1 | 2330                         | 2001                         | 06/07/49                       |
|     | C0947              | 2124                      | 99121          | 134/1          | 1905                         | 1881                         | 17/05/49                       |
|     | C0953              | 1629                      | 99518          | 118/4          | 2300                         | 2206                         | 06/08/49                       |
|     | C0965              | 1986                      | 99386          | 133/2          | 1950                         | <1767                        | 12/10/49                       |
|     | C0984              | 1478                      | 99696          | 118/4          | 2240                         | 2200                         | 04/10/49                       |
|     | C0994              | 2355                      | 99136          | 134/3          | 2580                         | 2537                         | 23/11/49                       |
| (   | C1000              | 2331                      | 99147          | 134/3          | 2600                         | 2475                         |                                |
|     | C1001              | 1705                      | 99589          | 119/3          | 1958                         | <1714                        | 16/12/49                       |
|     | C1007              | 2364                      | 99139          | 134/3          | 2560                         | 2537                         | 08/12/49                       |
|     | C1013              | 2258                      | 99201          | 134/1          | 2520                         | 2355                         | 15/12/49                       |
|     | C1013              | 2258                      | 99201          | 134/1          | 2520                         | 2355                         | 15/12/49                       |
|     | C1019              | 2015                      | 99630          | 119/4          | 2440                         | 2277                         | 03/12/49                       |
|     | C1021<br>C1027     | 1453<br>1754              | 99663<br>99468 | 118/4<br>119/3 | 2403<br>1810                 | 2382<br>1731                 | 31/12/49<br>04/01/50           |
|     | C1027              | 2278                      | 99263          | 134/1          | 2480                         | <2343                        | 18/11/49                       |
|     | C1023              | 1444                      | 99668          | 118/4          | 2414                         | 2379                         | 04/02/50                       |
|     | C1043              | 2059                      | 99557          | 119/4          | 2260                         | 2125                         | 17/03/50                       |
|     | C1051              | 2294                      | 99190          | 134/1          | 2560                         | 2400                         | 15/03/50                       |
|     | C1062              | 1975                      | 99194          | 133/2          | 1900                         | 1989                         | 16/03/50                       |
|     | C1063              | 1984                      | 99203          | 133/2          | 1900                         | 1890                         | 23/03/50                       |
|     | C1080              | 1805                      | 99657          | 119/3          | 1870                         | 1763                         | 17/05/50                       |
|     | C1082              | 1812                      | 99667          | 119/3          | 1870                         | 1810                         | 17/05/50                       |
|     | C1082              | 2017                      | 99627          | 119/4          | 2530                         | 2470                         | 17/05/50                       |
|     | C1089              | 1560                      | 99705          | 118/4          | 2149                         | <1905                        | 17/05/50                       |
|     | C1112              | 2365                      | 99283          | 134/1          | 2780                         | <2628                        | 29/09/49                       |
|     | C1125<br>C1126     | 1626<br>2365              | 99636<br>98545 | 118/4<br>148/3 | 2100<br>2020                 | 2015<br>1816                 | 24/06/50<br>28/07/50           |
|     | C1126              | 1625                      | 99425          | 132/2          | 2520                         | 2510                         | 15/06/51                       |
|     | C1161              | 2242                      | 99024          | 134/3          | 2160                         | 1965                         | 03/03/50                       |
|     | C1250              | 1853                      | 99629          | 119/3          | 1910                         | 1761                         | 07/12/50                       |
|     | C1259              | 2420                      | 98413          | 148/3          | 1820                         | 1811                         | 02/12/50                       |
|     | C1265              | 2226                      | 99108          | 134/3          | 2240                         | <1995                        | 19/12/50                       |
|     | C1277              | 2388                      | 99188          | 134/1          | 2520                         | 2451                         | 02/10/50                       |
| (   | C1279              | 2142                      | 99072          | 133/4          | 2000                         | 1878                         | 26/10/50                       |
|     | C1281              | 2094                      | 99104          | 133/4          | 1900                         | 1876                         | 08/11/50                       |
|     | C1287              | 1883                      | 99488          | 119/3          | 1815                         | 1764                         | 01/12/50                       |
|     | C1294              | 2413                      | 98410          | 148/3          | 1840                         | 1831                         | 19/01/51                       |
|     | C1325<br>C1356     | 1481<br>2112              | 99691<br>99121 | 118/4<br>133/4 | 2270<br>1895                 | 2180<br>1883                 | 10/03/51<br>21/03/51           |
|     | C1356              | 1996                      | 99631          | 133/4          | 2460                         | 2313                         | 24/03/51                       |
|     | C1361              | 2059                      | 99553          | 119/4          | 2280                         | 2094                         | 13/11/54                       |
|     | C1362              | 1644                      | 99666          | 118/4          | 2040                         | 1865                         | 14/04/51                       |
|     | C1374              | 1814                      | 99667          | 119/3          | 1875                         | 1814                         | 26/05/51                       |

| BOREHOLE<br>NUMBER | EASTING      | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--------------------|--------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| C1379              | 2064         | 99646          | 119/4          | 2380                         | 2344                         | 01/05/55                       |
| C1383              | 1828         | 99489          | 119/3          | 1845                         | 1790                         | 10/05/51                       |
| 1390               | 2329         | 97909          | 161/3          | 1420                         | <1249                        | 06/03/51                       |
| 1391               | 2369         | 97893          | 161/3          | 1480                         | 1369                         | 31/03/51                       |
| 1394               | 1797         | .99416         | 133/1          | 1880                         | 1790                         | 21/05/51                       |
| 1402               | 2072         | 98910          | 133/4          | 1710                         |                              | 21/04/51                       |
| 1404               | 1902         | 99153          | 133/3          | 1940                         | 1882                         | 04/03/50                       |
| 425                | 2235         | 99019          | 134/3          | 2120                         | 1859                         | 13/06/51                       |
| .434               | 1855         | 99704          | 119/3          | 1960                         | 1923                         | 14/02/51                       |
| 1436               | 1860         | 99713          | 119/3          | 1980                         | 1935                         | 28/02/51                       |
| 1464               | 1972         | 99180          | 133/2          | 1888                         | 1880                         | 10/03/50                       |
| 475                | 2278         | 99078          | 134/3          | 2600                         | 2539                         | 07/07/51                       |
| .482               | 2139         | 99166          | 133/4          | 1894                         | 1880                         | 23/06/51                       |
| 1483               | 2157         | 99257          | 133/2          | 1974                         | 1943                         | 25/06/51                       |
| 486                | 2159.        | 99129          | 133/4          | 1974                         | 1963                         | 13/07/51                       |
| 487                | 2156         | 99126          | 133/4          | 1974                         | 1883                         | 18/07/51                       |
| 488                | 2180         | 99223          | 133/2          | 2088                         | 2012                         | 23/07/51                       |
| 491                | 1626         | 99634          | 118/4          | 2120                         | 2035                         | 28/07/51                       |
| 499                | 2349         | 97803          | 161/3          | 1400                         | <1271                        | 27/07/51                       |
| .503               | 2239         | 99019          | 134/3          | 2140                         | 1879                         | 22/08/51                       |
| 504                | 1404         | 99714          | 118/4          | 2380                         | 2289                         | 12/08/51                       |
| 523                | 2253         | 97658          | 172/1          | 1340                         | <1208                        | 07/09/51                       |
| 524                | 2009         | 98951          | 133/4          | 1737                         |                              | 12/06/51                       |
| 525                | 2000         | 98903          | 133/4          | 1631                         | <1414                        | 21/07/51                       |
| 535                | 1701         | 99708          | 119/3          | 1950                         | 1773                         | 28/09/51                       |
| 545                | 1621         | 99411          | 132/2          | 2520                         | 2514                         | 03/10/51                       |
| 558                | 1802         | 99680          | 119/3          | 1900                         | 1775                         | 26/10/51                       |
| 559                | 2181         | 98278          | 160/2          | 990                          | 906                          | 27/10/51                       |
| 584                | 1801         | 99513          | 119/3          | 1804                         | 1786                         | 14/11/51                       |
| 585<br>602         | 1581         | 99582          | 118/4          | 2280                         | 2271                         | 25/01/51                       |
| 502<br>514         | 2302         | 99053          | 134/3          | 2680                         | 2530                         | 31/10/51                       |
| 625 ·              | 2225<br>1446 | 99293<br>99686 | 134/1<br>118/4 | 2480                         | 2362                         | 14/12/51                       |
| 641                | 1447         | 99722          | 118/4          | 2380                         | 2341<br>2144                 | 12/12/51                       |
| 652                | 2134         | 99722          | 133/4          | 2220<br>1900                 | C144'                        | 29/11/51<br>14/01/52           |
| 662                | 2081         | 98118          | 160/2          | 860                          |                              | 14/01/52                       |
| 666                | 1820         | 99664          | 119/3          | 1880                         | 1817                         | 23/01/52                       |
| 713                | 2432         | 98255          | 161/1          | 1840                         | 1785                         | 04/03/52                       |
| 726                | 2234         | 99004          | 134/3          | 2080                         | 1821                         | 31/03/52                       |
| 749                | 1577         |                | 118/4          | 2280                         | 2195                         | 10/04/52                       |
| 794                | 2294         | 99072          | 134/3          | 2740                         | 2560                         | 21/06/52                       |
| 795                | 2296         | 99254          | 134/1          | 2510                         | 2378                         | 14/07/52                       |
| 795                | 2296         | 99254          | 134/1          | 2510                         | 2378                         | 14/7/52                        |
| 798                | 1812         | 99405          | 133/1          | 1900                         | 1768                         | 08/07/52                       |
| 330                | 2282         | 99262          | 134/1          | 2500                         | 2372                         | 17/08/52                       |
| 843                | 2105         | 98983          | 133/4          | 2070                         | <1814                        |                                |
| 850                | 2329         | .99226         | 134/1          | 2550                         | 2410                         | 09/09/52                       |
| 851                | 2237         | 99119          | 134/3          | 2340                         | 2083                         | 23/01/52                       |
| 877                | 1869         | 99371          | 133/1          | 1940                         | 1782                         | 22/11/52                       |
| 892                | 2214         | 99107          | 133/4          | 2200                         | 1966                         | 26/12/52                       |
| 898                | 2164         | 99252          | 133/2          | 2020                         | 1959                         | 20/01/53                       |
| 911                | 1667         | 99295          | 133/1          | 2900                         | <2728                        | 29/01/53                       |
| 912                | 1668         | 99293          | 133/1          | 2860                         | <2709                        | 16/02/53                       |
| 913                | 1663         | 99292          | 133/1          | 2900                         | 2861                         | 16/02/53                       |
| 914                | 1656         | 99280          | 132/2          | 2890                         | 2867                         | 28/02/53                       |
| 924                | 2095         | 99577          | 119/4          | 2260                         | 2137                         | 21/03/53                       |

| BOREHOLE<br>NUMBER | EASTING      | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--------------------|--------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| C1926              | 2094         | 99054          | 133/4          | 1980                         | 1890                         | 20/02/53                       |
| C1927              | 2069         | 99078          | 133/4          | 1895                         | 1877                         | 26/03/53                       |
| C1929              | 2337         | 99139          | 134/3          | 2600                         | 2500                         | 09/03/53                       |
| C1935              | 1596         | 99627          | 118/4          | 2160                         | 2045                         | 15/01/53                       |
| C1941              | 1802         | 99402          | 133/1          | 1920                         | 1781                         | 28/03/53                       |
| C1947              | 2146         | 99194          | 133/2          | 1920                         | 1905                         | 17/04/53                       |
| C1951              | 2123         | 99566          | 119/4          | 2220                         | 2111                         | 02/04/53                       |
| C1952              | 2126         | 99572          | 119/4          | 2290                         | 2178<br>2451                 | 07/05/53<br>02/05/53           |
| C1970<br>C1990     | 1869<br>1889 | 98992<br>99428 | 133/3<br>133/1 | 2580<br>1840                 | 1778                         | 21/01/53                       |
| C1990              | 2277         | 99426          | 134/3          | 2560                         | 2360                         | 30/06/53                       |
| C2005              | 2293         | 99143          | 134/3          | 2600                         | 2372                         | 30/00/33                       |
| C2007              | 1851         | 99516          | 119/3          | 1884                         | 1785                         | 04/09/53                       |
| C2033              | 2025         | 99706          | 119/4          | 2600                         | 2525                         | 24/09/53                       |
| C2039              | 2035         | 99720          | 119/4          | 2640                         | <2460                        | 06/10/53                       |
| C2042              | 1878         | 99092          | 133/3          | 2080                         | <1889                        | 25/07/53                       |
| C2058              | 2141         | 99157          | 133/4          | 1910                         | 1995                         | 04/11/53                       |
| C2059              | 1799         | 99447          | 119/3          | 1830                         | 1810                         | 25/04/53                       |
| C2061              | 2163         | 99658          | 119/4          | 2300                         | 2279                         | 01/11/53                       |
| C2062              | 2283         | 99185          | 134/3          | 2620                         | 2392                         | 27/10/53                       |
| C2063              | 2306         | 99099          | 134/3          | 2670                         | 2571                         | 24 /00 /52                     |
| C2069              | 1989         | 99087          | 133/4          | 1920<br>1900                 | 187.4<br>1888                | 24/09/53<br>05/10/53           |
| C2071<br>C2076     | 2028<br>2030 | 99092<br>99467 | 133/4<br>119/4 | 2020                         | 1901                         | 27/07/50                       |
| C2070              | 2044         | 99461          | 119/4          | 2000                         | 1906                         | 27/08/50                       |
| C2097              | 2041         | 99665          | 119/4          | 2500                         | 2381                         | 28/11/53                       |
| C2108              | 2281         | 99212          | 134/1          | 2530                         | 2364                         | 15/12/53                       |
| C2109              | 2024         | 99717          | 119/4          | 2600                         | 2558                         | 16/12/53                       |
| C2110              | 2210         | 99559          | 119/4          | 2440                         | 2341                         | 22/12/53                       |
| C2117              | 2139         | 99161          | 133/4          | 1900                         | 1888                         | 11/11/53                       |
| C2118              | 1949         | 99595          | 119/4          | 2220                         | 2071                         | 23/12/53                       |
| C2128              | 1830         | 99680          | 119/3          | 1902                         | 1870                         | 06/11/53                       |
| C2129              | 1844         | 99677          | 119/3          | 1919                         | 1870                         | 09/12/53                       |
| C2138              | 2318         | 98981          | 134/3          | 2200                         | 2165                         | 25/11/53                       |
| C2149              | 2316<br>2215 | 99244<br>99567 | 134/1<br>119/4 | 2540<br>2480                 | 2396<br>2349                 | 16/02/54<br>13/03/54           |
| C2160<br>C2170     | 2361         | 99247          | 134/1          | 2610                         | 2424                         | 18/03/54                       |
| C2170              | 1920         | 99003          | 133/3          | 2160                         | <1935                        | 19/07/57                       |
| C2172              | 2315         | 98979          | 134/3          | 2180                         | 2138                         | 22/02/54                       |
| C2176              | 2371         | 99150          | 134/3          | 2540                         | 2524                         | 14/01/54                       |
| C2197              | 2346         | 99191          | 134/1          | 2540                         | 2427                         | 19/05/54                       |
| C2234              | 1943         | 99552          | 119/4          | 1860                         | 1783                         | 12/06/54                       |
| C2241              | 1901         | 99199          | 133/1          | 1980                         | 1871                         | 17/07/54                       |
| C2246              | 2107         | 99246          | 133/2          | 1890                         | 1876                         | 24/07/54                       |
| C2263              | 2290         | 99050          | 134/3          | 2710                         | <2436                        | 20 /07 /54                     |
| C2264              | 2297         | 99058          | 134/3          | 2740                         | 2591                         | 28/07/54                       |
| C2269              | 1813<br>1596 | 99668<br>99556 | 119/3<br>118/4 | 1874<br>2315                 | 1814<br>2282                 | 14/10/54<br>09/09/54           |
| C2276<br>C2288     | 1807         | 99345          | 133/1          | 2060                         | <1787                        | 09/09/54                       |
| C2289              | 1764         | 99350          | 133/1          | 2020                         | 1933                         | 20/10/54                       |
| C2292              | 2078         | 99705          | 119/4          | 2360                         | 2298                         | 25/11/54                       |
| C2294              | 2394         | 98521          | 148/3          | 1880                         | 1864                         | 05/01/55                       |
| C2296              | 2141         | 99649          | 119/4          | 2320                         | 2290                         | 10/12/54                       |
| C2300              | 1901         | 99099          | 133/3          | 2000                         | 1899                         | 18/11/54                       |
| C2304              | 1973         | 99176          | 133/2          | 1900                         | 1894                         | 08/12/54                       |
| C2322              | 1978         | 99705          | 119/4          | 2540                         | 2428                         | 30/01/55                       |

| BOREHOLE EASTING NORTHING MAP NUMBER NO.         | HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--|---------------------|------------------------------|--------------------------------|
| C2332 1978 99678 119/4                           | 24.80               | 2425                         | 18/02/55                       |
| C2338 2430 98588 148/3                           | 2000                | 1805                         | 19/01/51                       |
| C2347 2183 99186 133/2                           | 2060                | 1941                         | 12/02/55                       |
| C2358 2324 98668 148/1                           | 2160                | 1895                         | 25/03/55                       |
| C2388 2024 99462 119/4                           | 2030                | 1788                         | 04/06/55                       |
| C2402 1805 99675 119/3                           | 1866                | 1799                         | 18/06/53                       |
| C2420 2339 99090 134/3                           | 2640                | 2572                         | 30/09/55                       |
| C2421 2347. 99084 134/3                          | 2620                | 2432                         | 05/10/55                       |
| C2430 2119 99184 133/2                           | 1900                | 1894                         | 01/10/55                       |
| C2432 1649 99608 118/4                           | 2060                | 1944                         | 21/09/55                       |
| C2447 2347 98678 148/1                           | 2080                | 1878                         | 28/11/55                       |
| C2448 1652 99510 118/4                           | 2180                | 2023                         | 22/11/55                       |
| C2466 2365 98865 148/1                           | 2360                | 2305                         | 22/12/55                       |
| C2468 2371 97801 161/3                           | 1460                | 1328<br>1770                 | 12/12/55<br>01/02/56           |
| C2480 1808 99479 119/3<br>C2482 1665 99310 133/1 | 1810<br>2820        | <2715                        | 24/02/56                       |
| C2482 1665 99310 133/1<br>C2493 1879 99658 119/3 | 1930                | 1836                         | 01/03/56                       |
| C2496 1621 99270 132/2                           | 2820                | 2676                         | 06/03/56                       |
| C2497 1553 99284 132/2                           | 2750                | 2645                         | 22/03/56                       |
| C2499 1929 99589 119/3                           | 1928                | 1822                         | 14/04/56                       |
| C2504 1861 99682 119/3                           | 1940                | 1870                         | 02/05/56                       |
| C2521 1918 99213 133/1                           | 1940                | 1866                         | 08/04/56                       |
| C2522 1940 99198 133/2                           | 1940                | 1894                         | 28/04/56                       |
| C2523 2002 99206 133/2                           | 1900                | 1870                         | 28/05/56                       |
| C2534 2096 99100 133/4                           | 1910                | 1893                         | 13/06/56                       |
| C2535 2035 99229 133/2                           | 1897                | 1890                         | 22/06/56                       |
| C2536 2025 99216 133/2                           | 1890                | 1886                         | 25/06/56                       |
| C2537 2046 99208 133/2                           | 1900                | 1897                         | 27/06/56                       |
| C2538 2008 99213 133/2                           | 1891                | 1881                         | 29/06/56<br>01/07/56           |
| C2539 2022 99207 133/2<br>C2541 1912 99363 133/1 | 1900<br>1960        | 1895<br><1911                | 06/01/56                       |
| C2541 1912 99363 133/1<br>C2542 1915 99338 133/1 | 2160                | <2100                        | 27/01/56                       |
| C2542 1915 99325 133/1                           | 2180                | 2030                         | 02/04/56                       |
| C2564 1483 99723 118/4                           | 2120                | 2011                         | 27/08/56                       |
| C2600 1915 99355 133/1                           | 2020                | 1834                         | 15/10/56                       |
| C2620 2465 98553 148/3                           | 1820                | 1753                         | 12/10/56                       |
| C2636 2101 99109 133/4                           | 1895                | 1890                         | 06/02/57                       |
| C2646 2468 97862 161/3                           | 1680                | 1629                         | 06/03/57                       |
| C2647 2387 97632 172/1                           | 1600                | 1582                         | 24/03/57                       |
| C2657 1948 99125 133/4                           | 1920                | 1897                         | 17/04/57                       |
| C2659 1974 99121 133/4                           | 1900                | 1893                         | 06/03/57                       |
| C2660 1969 99120 133/4                           | 1900                | 1880                         | 23/05/57                       |
| C2662 2280 99070 134/3                           | 2620                | 2419                         | 11/03/57                       |
| C2663 2309 99094 134/3                           | 2665                | 2345                         | 20/03/57                       |
| C2664 1877 98998 133/3                           | 2300                | <2105<br>2265                | 21/03/57<br>06/02/57           |
| C2667 2262 99153 134/3<br>C2670 1656 99668 118/4 | 2420<br>2000        | 1833                         | 15/04/57                       |
| C2670 1656 99668 118/4<br>C2680 1397 99705 118/4 | 2440                | 2392                         | 01/12/56                       |
| C2697 2164 99646 119/4                           | 2300                | 2270                         | 14/03/57                       |
| C2701 1967 99089 133/4                           | 1890                | 1883                         | 26/07/57                       |
| C2703 2050 99215 133/2                           | 1900                | 1897                         | 04/05/57                       |
| C2704 1798 99444 133/1                           | 1840                | 1780                         | 01/07/57                       |
| C2705 1987 99208 133/2                           | 1899                | 1882                         | 24/07/57                       |
| C2706 2006 99222 133/2                           | 1920                | 1881                         | 12/08/57                       |
| C2709 1872 99083 133/3                           | 2140                | 1944                         | 24/06/57                       |
| C2717 2311 98609 148/3                           | 1940                | 1701                         | 08/10/57                       |

| BOREHOLE<br>NUMBER | EASTING      | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--------------------|--------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| C2720              | 2288         | 99102          | 134/3          | 2660                         | 2384,                        | 04/10/57                       |
| C2745              | 1575         | 99606          | 118/4          | 2240                         | 2148                         | 18/12/57                       |
| C2753              | 2074         | 99497          | 119/4          | 2220                         | 2097                         | 06/03/58 <sup>-</sup>          |
| C2758              | 2315         | 98675          | 148/1          | 2054                         | 1952                         | 12/02/58                       |
| C2773              | 2071         | 99490          | 119/4          | 2170                         | 2098                         | 26/03/58                       |
| C2813              | 1974         | 99204          | 133/2          | 1887                         | 1846                         | 14/04/58                       |
| C2823              | 2199         | 99025          | 133/4          | 2130                         | 1870                         | 15/09/58                       |
| C2851              | 1793         | 99348          | 133/1          | 2040                         | 1809                         | 22/01/59                       |
| C2863              | 2068         | 99082          | 133/4          | 1900                         | 1401                         |                                |
| C2866              | 2271         | 98458          | 148/3          | 1570                         | 1481                         | 05/03/59                       |
| C2870              | 1950         | 99293          | 133/2          | 2637<br>2630                 | , 25.03                      | 05/02/59                       |
| C2871              | 1934<br>2130 | 99305          | 133/1          | 2620<br>1939                 | <sup>2583</sup> 1886         | 16/02/59<br>03/01/60           |
| C2883<br>C2885     | 1968         | 99294<br>99043 | 133/2<br>133/4 | 2020                         | 1000                         | 03/01/00                       |
| C2886              | 1985         | 99053          | 133/4          | 1980                         |                              |                                |
| C2887              | 1965         | 99295          | 133/4          | 2640                         |                              | 12/02/59                       |
| C2894              | 1606         | 99576          | 118/4          | 2230                         | 2218                         | 21/03/59                       |
| C2899              | 1966         | 99335          | 133/2          | 2133                         |                              | 25/04/59                       |
| C2900              | 1960         | 99316          | 133/2          | 2124                         |                              | 30/04/59                       |
| C2901              | 1959         | 99314          | 133/2          | 2124                         |                              | 06/05/59                       |
| C2902              | 2364         | 98641          | 148/1          | 2020                         | 1961                         | 27/05/59                       |
| C2910              | 2322         | 98778          | 148/1          | 2185                         | 2008                         | 11/07/59                       |
| C2966              | 2101         | 99606          | 119/4          | 2260                         | 2206                         |                                |
| C2970              | 1832         | 99680          | 119/3          | 1910                         | 1884                         | 19/02/59                       |
| C2997              | 2099         | 98999          | 133/4          | 2160                         | 1880                         | 22/01/60                       |
| C3003              | 2272         | 98596          | 148/3          | 1770                         | 1530                         | 09/03/60                       |
| C3005              | 1446         | 99605          | 118/4          | 2403                         | 2365                         | 18/03/60                       |
| C3024              | 1805         | 99238          | 133/1          | 2400                         | 2308                         | 04/05/60                       |
| C3032<br>C3047     | 1801<br>1796 | 99248<br>99664 | 133/1<br>119/3 | 2400<br>1822                 | 2358<br>1763                 | 16/04/60<br>08/06/60           |
| C3047              | 1998         | 99203          | 133/2          | 1900                         | 1885                         | 09/08/60                       |
| C3066              | 2061         | 99721          | 119/4          | 2460                         | 2390                         | 00/02/60                       |
| C3067              | 2098         | 99631          | 119/4          | 2300                         | 2240                         | 00,02,00                       |
| C3087              | 2363         | 98624          | 148/1          | 1990                         | 1949                         | 13/07/60                       |
| C3136              | 1945         | 99643          | 119/4          | 2320                         | 2275                         | 19/08/61                       |
| C3164              | 1825         | 99248          | 133/1          | 2400                         | 2381                         | 07/03/62                       |
| C316D              | 1810         | 99690          | 119/3          |                              | 1798                         | 17/04/50                       |
| C3216              | 2115         | 99210          | 133/2          | 1900                         | 1895                         |                                |
| C3217              | 2114         | 99204          | 133/2          | 1900                         | 1895                         |                                |
| C3243              | 1578         | 99593          | 118/4          | 2260                         | 2192                         | 08/06/63                       |
| C3266              | 2355         | 98775          | 148/1          | 2280                         | 2187                         | 30/10/63                       |
| C3280              | 2365         | 98585          | 148/3          | 2000                         | 1918                         | 24/01/63                       |
| C3292              | 2134         | 99215          | 133/2          | 1893                         | 1885                         | 16/05/64                       |
| C3298              | 2104         | 99244          | 133/2          | 1900                         | 1895                         | 22/05/64                       |
| C3299              | 2103         | 99230          | 133/2          | 1887                         | 1885                         | 14/06/64                       |
| C3324              | 1691         | 99612          | 119/3          | 1940<br>2660                 | 1750<br>2593                 | 05/02/65 <sup>-</sup>          |
| C3327<br>C3351     | 1665<br>1600 | 99339<br>99288 | 133/1<br>133/1 | 2880                         | 2727                         | 03/02/03                       |
| C3351              | 1665         | 99291          | 133/1 $133/1$  | 2900                         | 2687                         |                                |
| C3353              | 1649         | 99273          | 132/2          | 2880                         | 2843                         | 03/07/65                       |
| C3358              | 2381         | 97822          | 161/3          | 1500                         | <1318                        | 05/08/65                       |
| C3363              | 2390         | 97889          | 161/3          | 1500                         | 1421                         | 30/10/65                       |
| C3365              | 2114         | 99235          | 133/2          | 1900                         | 1889                         | 08/11/65                       |
| C3366              | 2120         | 99233          | 133/2          | 1899                         | 1889                         | 27/10/65                       |
| C3371              | 1634         | 99586          | 118/4          | 2145                         | 2044                         | 02/11/65                       |
| C3377              | 2363         | 98812          | 148/1          | 2340                         | 2247                         | 23/11/65                       |

| BOREHOLE<br>NUMBER | EASTING                   | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--------------------|---------------------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| C3397              | 1671                      | 99315          | 133/1          | 2730                         | 2622                         | 23/08/66                       |
| C3417              | 2091                      | 99261          | 133/2          | 1900                         | 1892.                        | 04/12/66                       |
| C3418              | 2365                      | 98653          | 148/1          | 2080                         | 1938                         | 03/02/67                       |
| C3422              | 2367                      | 98882          | 148/1          | 2400                         | 2343                         | 17/10/64                       |
| C3431              | 1783                      | 99301          | 133/1          | 2200                         | 2084                         | 20/02/67                       |
| C3436              | 2445                      | 97865          | 161/3          | 1620                         | 1577                         | 06/05/67                       |
| C3451              | 2480                      | 97692          | 172/1          | 1620                         | 1605                         | 30/06/67                       |
| C3467              | 1625                      | 99622          | 118/4          | -2135<br>2280                | <1906<br>2173                | 25/11/67                       |
| C3490<br>C3523     | 1608<br>2427              | 99627<br>98626 | 118/4<br>148/1 | 1900                         | 1875                         | 02/05/68<br>20/10/68           |
| C3523              | 2427                      | 98630          | 148/1          | 1920                         | 1907                         | 20/10/68                       |
| C3525              | 1811                      | 98475          | 147/3          | 1380                         | 1293                         | 19/10/68                       |
| C3551              | 2112                      | 99228          | 133/2          | 1900                         | 1895                         | 22/02/69                       |
| C3562              | 1762                      | 98973          | 133/3          |                              | <2669                        |                                |
| C3576              | 2408                      | 98377          | 148/3          | 1880                         | 1876                         | 21/05/69                       |
| C3615              | 2396                      | 98657          | 148/1          | 2060                         | 1988                         | 10/03/69                       |
| C3616              | 2022                      | 99091          | 133/4          | 1920                         | 1898                         | 21/09/67                       |
| C3627              | 1624                      | 99627          | 118/4          | 2132                         | 2932                         | 05/11/68                       |
| C3650              | 1646                      | 99283          | 132/2          | 2830                         | 2822                         | 10/01/70                       |
| C3674              | 2034                      | 99252          | 133/2          | 1885                         | 1879                         | 20/04/70                       |
| C3675              | 2122                      | 99223          | 133/2          | 1890                         | 1885                         | 04/03/70                       |
| C3677<br>C3678     | 2120<br>2114              | 99244<br>99249 | 133/2<br>133/2 | 1900<br>1901                 | 1885<br>1884                 | 25/02/68<br>17/04/70           |
| C3693              | 2450                      | 98633          | 148/1          | 1880                         | 1869                         | 05/07/70                       |
| C3694              | 2410                      | 98670          | 148/1          | 2140                         | 2107                         | 03/07/70                       |
| C3710              | 2395                      | 98651          | 148/1          | 2080                         | 2022                         | 21/09/70                       |
| C3713              | 2346                      | 98803          | 148/1          |                              | <2308                        | 12/11/70                       |
| C3721              | 2433                      | 98635          | 148/1          | 1940                         | 1901                         | 22/12/70                       |
| C3739              | 2449                      | 98617          | 148/1          | 1900                         | 1852                         | 01/10/69                       |
| C3740 .            | 2131                      | 99142          | 133/4          | 1905                         | 1888                         | 15/01/71                       |
| C3763              | 2441                      | 98638          | 148/1          | 1920                         | 1894                         | 21/03/71                       |
| C3764              | 2414                      | 98648          | 148/1          | 1900                         | 1866                         | 23/05/71                       |
| C3765              | 2416                      | 98626          | 148/1          | 1980                         | 1944                         | 05/02/71<br>26/05/71           |
| C3767<br>C3771     | 1946 <sup>.</sup><br>2492 | 99093<br>98693 | 133/4<br>148/1 | 1900<br>1880                 | 1874<br>1841                 | 14/07/71                       |
| C3779              | 2087                      | 99710          | 119/4          | 2340                         | 2330                         | 30/08/71                       |
| C3784              | 2087                      | 99706          | 119/4          | 2340                         | 2334                         | 07/10/71                       |
| C3799              | 2383                      | 98626          | 148/1          | 2240                         | 2199                         | 03/12/71                       |
| C3870              | 2458                      | 97868          | 161/3          |                              | <1552                        | 26/05/72                       |
| C3874              | 1795                      | 99661          | 119/3          | 1800                         | 1746                         | 30/11/72                       |
| C3875              | 1797                      | 99666          | 119/3          | 1800                         | 1747                         | 11/11/72                       |
| C3897              | 2458                      | 98822          | 148/1          | 2170                         | 2135                         | 03/03/73                       |
| C3910              | 2466                      | 98633          | 148/1          | 1847.                        | 1829                         | 10/05/73                       |
| C3919              | 2495                      | 98814          | 148/1          | 1980                         | 1952                         | 10/03/73                       |
| C3924              | 2051                      | 99081          | 133/4          | 1900                         | 1893                         | 14/06/73                       |
| C3925<br>C3929     | 1434<br>2062              | 99696<br>99313 | 118/4<br>133/2 | 2400<br>1900                 | 2306<br>1884                 | 02/07/73<br>02/07/73           |
| C3923              | 1819                      | 99215          | 133/2          | 2200                         | 2077                         | 16/05/75                       |
| C3937              | 2397                      | 98509          | 148/3          | 1900                         | 1897                         | 08/08/73                       |
| C3939              | 2368                      | 97628          | 172/1          | 1540                         | 1459                         | 07/09/77                       |
| C3942              | 2371                      | 97908          | 161/3          | 1500                         | 1400                         | 06/10/73                       |
| C3951              | 2459                      | 97876          | 161/3          | 1640                         | 1611                         | 23/11/73                       |
| C3955              | 1453                      | 99658          | 118/4          | 2440                         | 2437                         | 05/10/73                       |
| .C3965             | 1881                      | 99706          | 119/3          | 2060                         | 1998                         | 07/11/73                       |
| C3970              | 2410                      | 97886          | 161/3          | 1600                         | 1573                         | 31/01/74                       |
| C3976              | 2402                      | 98715          | 148/1          | 2140                         | 2084                         | 19/03/74                       |

| BOREHOLE<br>NUMBER | EASTING      | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--------------------|--------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| C3995              | 2470         | 98733          | 148/1          | 1940                         | 1927                         | 11/04/74                       |
| C3999              | 2397         | 98606          | 148/3          | 2000                         | 1952                         | 25/04/74                       |
| C4003              | 2494         | 98724          | 148/1          | 2000                         | 1997                         | 19/06/74                       |
| C4037              | 2400         | 98710          | 148/1          | 1920                         | 1874                         | 15/07/74                       |
| C4057              | 2104         | 99114          | 133/4          | 1900                         | 1897.                        | 10/09/74                       |
| C4061              | 1976         | 98991          | 133/4          | 2068                         |                              | 04/03/74                       |
| C4062              | 1990         | 99012          | 133/4          | 1941                         | 1377                         | 07/08/74                       |
| C4077              | 1644         | 99565          | 118/4          | 2120                         | 2036                         | 31/10/74                       |
| C4092              | 2413         | 98467          | 148/3          | 1900                         | 1892                         | 14/03/80                       |
| C4116<br>C4121     | 1704<br>1992 | 99468<br>99680 | 119/3<br>119/4 | 2010<br>2480                 | 1866<br>2387                 | 05/03/75<br>08/03/75           |
| C4121              | 1587         | 98675          | 146/2          | 1880                         | <1698                        | 00/03/73                       |
| C4131              | 1587         | 98674          | 146/2          | 1880                         | 1708.                        |                                |
| C4143              | 2326         | 98956          | 134/3          | 2180                         | 2169                         | 23/09/77                       |
| C4155              | 2145         | 99266          | 133/2          | 1940                         | 1913                         | 15/08/78                       |
| C4157              | 2135         | 99216          | 133/2          | 1894                         | 1883                         | 30/06/75                       |
| C4161              | 2133         | 99236          | 133/2          | 1900                         | 1884                         | 11/08/75                       |
| C4168              | 2120         | 99237          | 133/2          | 1900                         | 1883                         | 04/09/75                       |
| C4174              | 2304         | 98709          | 148/1          | 2080                         | 2023                         | 18/12/75                       |
| C4177              | 2140·        | 99235          | 133/2          | 1910                         | 1894                         | 24/11/75                       |
| C4178              | 2131         | 99234          | 133/2          | 1902                         | 1886                         | 12/11/75                       |
| C4179              | 2425         | 98428          | 148/3          | 1840                         | 1738                         | 16/10/75                       |
| C4185              | 2488         | 97659          | 172/1          | 1680                         | <1560                        | 30/01/76                       |
| C4186              | 2422         | 98416          | 148/3          | 1870                         | 1865                         | 21/11/75                       |
| C4200              | 2427         | 98466          | 148/3          | 1820                         | 1746                         | 24/06/76                       |
| C4201              | 2422         | 98486          | 148/3          | 1900                         | 1884                         | 18/03/76                       |
| C4206<br>C4208     | 1594         | 99631<br>99205 | 118/4<br>133/2 | 2160<br>1890                 | 2052<br>1884                 | 17/05/76<br>14/07/76           |
| C4208              | 2135<br>2130 | 99205          | 133/2          | 1889                         | 1885                         | 20/02/76                       |
| C4214              | 1605         | 99629          | 118/4          | 2150                         | 2047                         | 27/03/76                       |
| C4252              | 1985         | 99707          | 119/4          | 2570                         | 2450                         | 01/07/76                       |
| C4279              | 2431         | 98831          | 148/1          | 2771                         | 2194                         | 24/11/76                       |
| C4292              | 2459         | 98696          | 148/1          | 1940                         | 1914                         | 26/08/77                       |
| C4301              | 2110         | 99263          | 133/2          | 1916                         | 1883                         | 04/03/77                       |
| C4302              | 2136         | 99215          | 133/2          | 1900                         | 1890                         | 09/06/77                       |
| C4306              | 2475         | 98596          | 148/3          | 1820                         | 1767                         | 17/03/77                       |
| C4331              | 1835         | 98845          | 147/1          | 2180                         | <1980                        | 03/06/77                       |
| C4332              | 1709         | 98781          | 147/1          | 1850                         | 1788                         | 04/11/77                       |
| C4350              | 1573         | 99264          | 132/2          | 2790                         | 2777                         | 30/04/77                       |
| C4360              | 2443         | 98743          | 148/1          | 1960                         | 1938                         | 22/06/77                       |
| C4369              | 1816         | 99714          | 119/3          | 1910                         | 1879 <sup>-</sup>            | 26/08/77                       |
| C4370              | 1804         | 99690          | 119/3          | 1880                         | 1838                         | 12/10/77                       |
| C4397              | 2045         | 99085          | 133/4          | 1900                         | 1893                         | 16/08/77                       |
| C4403<br>C4413     | 2380         | 99130          | 134/3<br>118/4 | 2540<br>2340                 | 2497<br>2272                 | 14/10/77                       |
| C4415 .            | 1571<br>2371 | 99558<br>98554 | 148/3          | 2000                         | <1817                        | 13/01/78                       |
| C4410              | 2039         | 99086          | 133/4          | 1900                         | 1893                         | 09/09/77                       |
| C4431              | 2371         | 98643          | 148/1          | 2032                         | 1971                         | 28/02/78                       |
|                    | 2398         | 98678          | 148/1          | 2040                         | 2027                         | 27/03/78                       |
| C4484              | 2299         | 97899          | 161/3.         | 1380                         | 1298                         | 03/07/78                       |
| C4491              | 1888         | 99685          | 119/3          | 2030                         | 2022                         | 00/03/78                       |
| C4492              | 1886         | 99689          | 119/3          | 2020                         | 1962                         | 28/09/77                       |
| C4493              | 1875         | 99686          | 119/3          | 1960                         | 1948                         | 20/01/78                       |
| C4498              | 2471         | 98013          | 161/3          | 1720                         | 1695                         | 19/06/78                       |
| C4499              | 1949         | 99158          | 133/4          | 1940                         | <1727                        | 28/04/77                       |
| C4500              | 1964         | 99144          | 133/4          | 1900                         | 1885                         | 28/08/77                       |

| BOREHOLE<br>NUMBER. | EASTING      | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|---------------------|--------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| C4501               | 1961         | 99138          | 133/4          | 1910                         | 1889                         | 03/11/77                       |
| C4502               | 1669         | 99515          | 119/3          |                              | 2045                         | 01/10/76                       |
| C4504               | 2036         | 99258          | 133/2          | 1890                         | 1878                         | 18/05/77                       |
| C4510               | 1816         | 99713          | 119/3          | 1893                         | 1865                         | 20/07/78                       |
| C4511               | 1816         | 99715          | 119/3          | 1910                         | 1883                         | 11/11/78                       |
| C4512               | 1815         | 99716          | 119/3          | 1910                         | 1882                         | 31/01/79                       |
| C4517<br>C4531      | 1572<br>2080 | 99602<br>98112 | 118/4<br>160/2 | 2280 -<br>860                | 2183<br>790                  | 30/05/78<br>16/09/78           |
| C4551               | 2414         | 98802          | 148/1          | 2280                         | 2234                         | 19/09/78                       |
| C4555               | 2102         | 99317          | 133/2          | 1830                         | 1802                         | 15/08/78                       |
| C4564               | 1765         | 99448          | 133/1          | 1840                         | 1787                         | 24/11/70                       |
| C4565               | 2185         | 98051          | 160/4          | 1020                         | <820                         | 21/01/79                       |
| C4575               | 2356         | 98524          | 148/3          | 1950                         | 1828                         | 08/01/79                       |
| C4591               | 1957         | 99152          | 133/4          | 1900                         | 1879                         | 04/01/79                       |
| C4594               | 1918         | 99193          | 133/1          | 1940                         | 1834                         | 19/12/82                       |
| C4597               | 2374         | 98720          | 148/1          | 2220                         | 2105                         | 14/07/79                       |
| C4610<br>C4615      | 2132<br>2385 | 99233<br>98663 | 133/2<br>148/1 | 1890<br>2100                 | . 1874<br>2038               | 28/03/79<br>10/05/79           |
| C4624               | 2454         | 98490          | 148/1          | 1800                         | 1767                         | 05/06/79                       |
| C4634               | 2325         | 98961          | 134/3          | 2220                         | 2201                         | 06/01/78                       |
| C4665               | 2460         | 98738          | 148/1          | 1940                         | 1903                         | 18/10/79                       |
| C4669               | 1586         | 99592          | 118/4          | 2240                         | 2219                         | 20/09/79                       |
| C4685               | 2395         | 98666          | 148/1          | 2080                         | 1999                         | 27/11/81                       |
| C4687               | 2452         | 98428          | 148/3          | 1820                         | 1805                         | 13/12/80                       |
| C4713               | 2493         | 98457          | 148/3          | 1750                         | 1707                         | 21/01/80                       |
| C4743               |              | 98462          | 148/3          | 2000                         | 1994                         | 05/05/80                       |
| C4792               | 2366         | 98644<br>98562 | 148/1          | 2060                         | 1968                         | 28/07/80<br>16/01/81           |
| C4804<br>C4807      | 2412<br>2363 | 98562          | 148/3<br>148/1 | 1880<br>2060                 | 1816<br>1890                 | 02/03/81                       |
| C4812               | 2362         | 98647          | 148/1          | 2060                         | 1981                         | 18/11/80                       |
| C4829               | 2277         | 97682          | 172/1          |                              | <1195                        | 05/11/80                       |
| C4850               | 2405         | 98675          | 148/1          | 2140                         | 2135                         | 11/02/81                       |
| C4855               | 2395         | 98703          | 148/1          | 2120                         | 2112                         | 18/11/80                       |
| C4863               | 2426         | 98425          | 148/3          | 1820                         | 1805                         | 10/01/81                       |
| C4881               | 2448         | 98498          | 148/3          | 1920                         | 1866                         | 17/02/80                       |
| C4893               |              | 98764          | 148/1          |                              | <1924                        | 11/04/81                       |
| C4897               | 1863         | 99123          | 133/3<br>148/3 | 2220                         | 2007<br>1873                 | 08/01/82<br>30/11/81           |
| C4907<br>C4909      | 2422<br>2329 | 98484<br>98636 | 148/1          | 1880<br>2060                 | 1931                         | 17/04/81                       |
| C4909               | 1815         | 99665          | 119/3          | 1870                         | 1724                         | 04/07/81                       |
| C4927               | 2442         | 98536          | 148/3          | 1880                         | 1763                         | 20/06/81                       |
| C4966               | 2429         | 98465          | 148/3          | 1840                         | 1767                         | 31/12/81                       |
| C4968               | 2428         | 98502          | 148/3          | 1860                         | 1801                         | 15/09/81                       |
| C4971               | 2246         | 98723          | 148/1          |                              | <1250                        | 08/11/81                       |
| C4974               | 2306         | 98710          | 148/1          | 2080                         | 1861                         | 09/09/81                       |
| C4981               | 2430         | 98440          | 148/3          | 1840                         | 1805                         | 12/10/81                       |
| C4986               | 2085         | 99092          | 133/4          | 1900                         | 1895                         | 16/06/81                       |
| C4989<br>C4997      | 2086<br>2430 | 99093<br>98438 | 133/4<br>148/3 | 1900<br>1820                 | 1899<br>1749                 | 04/07/81<br>04/01/82           |
| C5002               | 2430         | 98438          | 133/2          | 2280                         | 2174                         | 04/01/82                       |
| C5002               | 1595         | 99596          | 118/4          | 2210                         | 2122                         | 01/01/82                       |
| C5111               | 1883         | 99650          | 119/3          | 1900                         | 1800                         | 23/12/81                       |
| C5117               | 2397         | 98502          | 148/3          | 1920                         | 1911                         | 23/02/83                       |
| C5143               | 1789         | 99694          | 119/3          | 1890                         | 1855                         | 28/09/82                       |
| C5161               | 2451         | 98436          | 148/3          | 1800                         | 1775                         | 17/06/82                       |
| C5175               | 2408         | 98752          | 148/1          | 2160                         | 2122                         | 19/08/82                       |

| BOREHOLE<br>NUMBER | EASTING      | NORTHING       | MAP<br>NO.     | BORE-<br>HOLE<br>ALT.<br>(m) | REST<br>WATER<br>ALT.<br>(m) | BOREHOLE<br>COMPLETION<br>DATE |
|--------------------|--------------|----------------|----------------|------------------------------|------------------------------|--------------------------------|
| C5206              | 1596         | 99588          | 118/4          | 2215                         | 2180                         | 08/11/82                       |
| C5257              | 1548         | 99236          | 132/2          | 2720                         | 2609                         | 17/12/82                       |
| C5343              | 2377         | 98687          | 148/1          | 2120                         | 2023                         | 25/05/83                       |
| C5348              | 2384         | 98672          | 148/1          | 2100                         | 1976                         | 26/06/83                       |
| C5375              | 2397         | 98630          | 148/1          | 2060                         | 1984                         | 24/10/83                       |
| C5411              | 2400         | 98645          | 148/1          | 2140                         | 2057                         | 19/10/83                       |
| C5520              | 2273         | 99406          | 134/1          | 2438                         | 2374                         | 17/03/84                       |
| C5564              | 2407         | 98418          | 148/3          | 1920                         | 1904                         | 29/08/84                       |
| C5754              | 1919         | 99673          | 119/3          | 2240                         | 2232                         | 00/00/00                       |
| C5798              | 2399         | 98442          | 148/3          | 2000                         | 1962                         | 06/09/84                       |
| C6056              | 1606         | 99252          | 132/2          | 2770                         | 2756                         | 29/01/85                       |
| C6095<br>C6186     | 1922         | 99682          | 119/3          | 2260                         | 2250                         | 25/03/85                       |
| C6211              | 2441<br>2403 | 98601          | 148/3          | 1880                         | 1872                         | 16/08/85                       |
| C6211              | 2382         | 98471          | 148/3          | 1900                         | 1858                         | 27/07/84                       |
| C6271              | 2302<br>1571 | 98697<br>99589 | 148/1          | 2134                         | 2004                         | 25/09/84                       |
| C6290              | 2008         | 99403          | 118/4          | 2260                         | 2225                         | 00 /07 /05                     |
| C6300              | 2264         | 99149          | 133/2<br>134/3 | 2030<br>2490                 | 1833<br>2357                 | 00/07/85                       |
| C630D              | 1983         | 99067          | 134/3          | 1970                         | 1870                         | 17/06/85<br>29/10/53           |
| C6377              | 2397         | 98483          | 148/3          | 1966                         | 1918                         | 16/12/85                       |
| C6378              | 2369         | 98606          | 148/3          | 2000                         | 1910                         | 09/11/85                       |
| C6494              | 2391         | 98478          | 148/3          | 1990                         | 1984                         | 06/03/86                       |
| C6495              | 1692         | 99141          | 133/3          |                              | <2755                        | 00/03/80                       |
| C6524              | 2409         | 98525          | 148/3          | 1880                         | 1817                         | 13/11/85                       |
| C6613              | 2376         | 98684          | 148/1          | 2109                         | 2019                         | 19/01/86                       |
| KJ1                | 2260         | 99081          | 134/3          |                              | <2268                        | 00/00/84                       |
| M0001              | 2036         | 99394          | 133/2          | 1960                         | 1805                         |                                |
| P0002              | 2385         | 98514          | 148/3          | 1940                         | 1924                         | 10/11/27                       |
| P0012              | 2387         | 98503          | 148/3          | 1900                         | 1876                         | 20/03/28                       |
| P0016              | 2268         | 98487          | 148/4          | 1580                         | 1486                         | 09/08/28                       |
| P0023              | 2258         | 98512          | 148/3          | 1500                         | 1430                         | 06/10/28                       |
| P0027              |              | 98563          | 147/4          | 1230                         |                              |                                |
| P0036              | 2189         | 98565          | 147/4          |                              |                              |                                |
| P0037              | 2189         | 98562          | 147/4          |                              |                              |                                |
| P0053              | 2264         | 98939          | 134/3          | 1860                         | 1647                         | 28/08/29                       |
| P0065              | 2342         |                | 134/3          | 2620                         | 2559                         | 10/10/29                       |
| P0071              | 2306         | 98606          | 148/3          | 1940                         | <1750                        |                                |
| P0089              | 2297         | 99181          | 134/1          | 2570                         | <2528                        | 24/3/30                        |
| SA58               | 1791         | 99687          | 119/3          | 1856                         | 1808                         | 16/08/41                       |

# APPENDIX 2 - BOREHOLE COMPLETION DATA

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER<br>(m) | PLAIM<br>CASING<br>DEPTH<br>(m) | ì                  |  |
|--------------------|--------------------------|-----------------------------|---------------------------------|--------------------|--|
| 0001C              | 206.9                    | 0.20                        |                                 | ·<br>·             |  |
| C0054              | 46.0                     | 0.15                        |                                 | •                  |  |
| C0057              | 93.9                     | 0.00                        | 100.0                           |                    |  |
| C0059              | 140.2                    | 0.20                        | 129.8                           | SAND               |  |
| C0079<br>C0092     | 116.4<br>158.5           | 0.15                        | 102.6                           |                    |  |
| C0092<br>C0107     | 74.9                     | 0.20                        |                                 |                    |  |
| C0107              | 39.6                     | 0.15                        | 24.9                            |                    |  |
| C0115              | 249.9                    | 0.15                        | 16.0                            |                    |  |
| C0131              | 45.7                     | 0.15                        | 26.7                            |                    |  |
| C0132              | 45.7                     | 0.15                        | 25.3                            |                    |  |
| C0152              | 66.9                     | 0.15                        |                                 | ALLUVIAL SEDIMENTS |  |
| C0164              | 66.5                     | 0.15                        | 20.1                            | LAVA + PUMICE      |  |
| C0165              | 155.0                    | 0.15                        |                                 |                    |  |
| C0202              | 137.2                    | 0.15                        |                                 | LAVA + CLAY + SAND |  |
| C0204              | 76.0                     | 0.20                        | 22.2                            | 4001 0450 475      |  |
| C0205              | 140.0                    | 0.15                        | 56.1                            | AGGLOMERATE        |  |
| C0208<br>C0210     | 199.6<br>67.1            | 0.20                        |                                 |                    |  |
| C0210<br>C0211     | 135.3                    | 0.20                        | 57 O                            | TRACHYTE           |  |
| C0214              | 121.9                    | 0.15                        | 57.0                            | TRACITIE           |  |
| C0220              | 152.4                    | 0.15                        | 35.7                            | ASH + PHONOLITE    |  |
| C0223              | 186.8                    | 0.15                        | 36.3                            |                    |  |
| C0227              | 167.6                    | 0.15                        | 65.8                            | ASH                |  |
| C0231              | 45.7                     | 0.15                        | 34.0                            |                    |  |
| C0258              | 106.1                    | 0.15                        | 40.5                            |                    |  |
| C0261              | 150.0                    | 0.20                        | 56.4                            |                    |  |
| C0264              | 182.9                    | 0.15                        |                                 | LAVA               |  |
| C0266              | 150.0                    | 0.20                        | 14.4                            |                    |  |
| C0288<br>C0295     | 182.9<br>86.0            | 0.15<br>0.15                | 23.7                            | ·                  |  |
| C0293              | 73.2                     | 0.13                        | 71 N                            | LAKE SEDIMENTS     |  |
| C0307              | 70.1                     | 0.20                        |                                 | LAKE SEDIMENTS     |  |
| C0321              | 98.1                     | 0.20                        | 43.3                            | ,                  |  |
| C0325              | 132.6                    | 0.15                        |                                 | CLAY + SAND        |  |
| C0376              | 91.4                     | 0.15                        | 38.2                            |                    |  |
| C0379              | 75.0                     | 0.15                        | 26.5                            |                    |  |
| C0381              | 128.3                    | 0.15                        | 19.1                            | ,                  |  |
| C0407              | 200.0                    | 0.15                        | 100 5                           |                    |  |
| C0408              | 138.0                    | 0.20                        | 109.5                           |                    |  |
| C0416<br>C0417     | 146.0<br>182.1           | 0.20<br>0.20                | 71.0                            | TUFF + CLAY        |  |
| C0417<br>C0419     | 182.1                    | 0.20                        |                                 | LAKE SEDIMENTS     |  |
| C0413              | 213.4                    | 0.15                        | 57.3                            | EARL SEDIFICATS    |  |
| C0429              | 100.8                    | 0.20                        |                                 | LAKE SEDIMENTS     |  |
| C0431              | 216.0                    | 0.20                        |                                 | LAVA               |  |
| C0440              | 167.6                    | 0.15                        | 54.3                            | LAVA + CLAY        |  |
| C0451              | 137.2                    | 0.15                        |                                 |                    |  |
| C0456              | 190.0                    | 0.15                        |                                 | LAKE SEDIMENT      |  |
| C0457              | 76.2                     | 0.20                        |                                 | LAKE SEDIMENTS     |  |
| C0458              | 102.4                    | 0.15                        |                                 | LAKE SEDIMENTS     |  |
| C0463<br>C0465     | 106.7                    | 0.15                        | 94.0                            | TUFF + PHONOLITE   |  |
| C0403              | 99.0                     | 0.13                        |                                 |                    |  |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER<br>(m) | PLAIM<br>CASING<br>DEPTH<br>(m) | ·                       |
|--------------------|--------------------------|-----------------------------|---------------------------------|-------------------------|
| C0466              | 77.4                     | 0.20                        | 75.9                            | PUMICE + LAVA           |
| C0467              | 95.4                     | 0.15                        |                                 | ·                       |
| C0468              | 46.3                     | 0.20                        | 40.0                            | FINE GRAVEL             |
| C0485<br>C0510     | 120.1<br>183.0           | 0.15                        | 40.8                            |                         |
| C0510<br>C0511     | 171.0                    | 0.15                        |                                 | •                       |
| C0531              | 61.0                     | 0.20                        | 18.0                            | PYROCLASTICS            |
| C0533              | 220.1                    | 0.15                        | 162.5                           |                         |
| C0553              | 106.7                    | 0.15                        |                                 | BASALT + LAKE SEDIMENTS |
| C0562              | 56.4                     | 0.15                        |                                 |                         |
| C0563              | 31.0                     | 0.15                        |                                 | LAKE SEDIMENTS & LAVAS  |
| C0567              | 102.1                    | 0.15                        |                                 | LAVA PEBBLES            |
| C0570              | 142.5                    | 0.15                        | 82.5                            | LAVA                    |
| C0572<br>C0579     | 229.0<br>42.7            | 0.15<br>0.15                | 14.9                            | ACH .                   |
| C0579              | 67.1                     | 0.15                        |                                 | TUFF                    |
| C0581              | 30.5                     | 0.15                        |                                 | LAKE SEDIMENTS          |
| C0582              | 56.1                     | 0.15                        |                                 | LAKE SEDIMENTS          |
| C0605              | 149.0                    | 0.17                        | 77.0                            | GNEISS                  |
| C0624              | 91.4                     | 0.15                        |                                 | TUFF + LAKE SEDIMENTS   |
| C0628              | . 45.7                   | 0.15                        |                                 | LAVA & ASH              |
| C0631              | 46.0                     | 0.15                        | 23.0                            | THEE                    |
| C0633<br>C0634     | 183.0<br>104.0           | 0.15<br>0.15                | 42.7                            | TUFF                    |
| C0634<br>C0648     | 229.0                    | 0.15                        |                                 | IUFF                    |
| C0651              | 161.5                    | 0.13                        |                                 |                         |
| C0655              | 149.4                    | 0.20                        | 38.1                            |                         |
| C0665              | 204.0                    |                             |                                 |                         |
| C0667              | 36.6                     | 0.20                        |                                 | ASH & SEDIMENT          |
| C0670              | 112.7                    | 0.15                        | 25.1                            | SEDIMENTS + LAVAS       |
| C0677              | 182.9                    | 0.15                        | 1.0                             |                         |
| C0678<br>C0691     | 61.0<br>109.7            | 0.15<br>0.15                | 1.8                             |                         |
| C0692              | 192.0                    | 0.15                        | 9.5                             | LAKE SEDIMENTS + TUFF   |
| C0699              | 91.4                     | 0.20                        |                                 | SAND + TUFF             |
| C0703              | 310.0                    | 0.15                        |                                 | TUFF                    |
| C0704              | 152.0                    | 0.15                        | 12.0                            | •                       |
| C0705              | 46.0                     | 0.15                        |                                 |                         |
| C0706              | 40.0                     | 0.15                        |                                 |                         |
| C0707              | 103.0                    | 0.15                        | 22.6                            |                         |
| C0719<br>C0729     | 153.0<br>182.9           | 0.15<br>0.15                | 30.3                            | FRACTURED LAVA          |
| C0723              | 152.4                    | 0.15                        |                                 | PYROCLASTICS            |
| C0733              | 240.8                    | 0.15                        | 40.2                            |                         |
| C0741              | 133.5                    | 0.15                        |                                 | TUFF + LAKE SEDIMENTS   |
| ·C0745             | 182.8                    | 0.15                        | 50.7                            |                         |
| C0780              | 210.3                    |                             |                                 | TUFF + PALEOSOIL        |
| C0783              | 120.0                    | 0.20                        | 20.3                            | LAKE SEDIMENTS          |
| C0804              | 100.8                    | 0.15                        | 20 C                            | PYROCLASTICS            |
| C0805              | 166.4                    | 0.15<br>0.10                | 29.6<br>12.4                    | FRACTURED LAVA          |
| C0811<br>C0813     | 152.7                    | 0.10                        |                                 | SEDIMENTS               |
| C0813              |                          | 0.15                        | 7.3                             | LAKE SEDIMENTS + ASH    |
| C0822              | 138.0                    |                             |                                 | The SEPTHENTS - NOIL    |
| C0824              | 183.0                    | 0.15                        | •                               | GNEISS                  |
| C0836              | 172.8                    | 0.20                        | 104.7                           | LAKE SEDIMENTS          |
|                    |                          |                             |                                 |                         |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER:<br>·(m) | PLAIN<br>CASING<br>DEPTI<br>(m) | G e e<br>H e e e e e e e e e e e e e e e e e            |
|--------------------|--------------------------|-------------------------------|---------------------------------|---|
| C0839              | 45.7                     | 0.20                          |                                 | ASH + LAVA  |
| C0845              | 217.0                    | 0.20                          |                                 | LAKE SEDIMENTS + LAVA                                   |
| C0855              | 189.9                    | 0.15                          |                                 | PYROCLASTICS  |
| C0858              | 150.5                    | 0.15                          |                                 | PALEOSOIL   |
| C0869              | 137.0<br>102.9           | 0.20<br>0.10                  | 43.4                            | LAKE SEDIMENTS<br>TUFF + CLAY                           |
| C0870<br>C0872     | 102.9                    | 0.10                          | -                               | TUFF + CLAT   |
| C0875              | 152.0                    | 0.15                          |                                 | GNEISS  |
| C0882              | 182.0                    | 0.15                          | 13.2                            |   |
| C0910              | 32.9                     | 0.15                          | 7.3                             | LAKE SEDIMENTS & PUMICE                                 |
| C0916              | 213.4                    | 0.15                          |                                 | TUFF  |
| C0921              | 228.6                    | 0.15                          |                                 | BASALT + TUFF + TRACHYTE                                |
| C0939              | 150.0                    | 0.15                          | 76.2                            |   |
| C0946              | 245.4                    | 0.15                          |                                 | LAVA + SAND + GRAVEL                                    |
| C0947<br>C0953     | 49.4<br>143.2            | 0.15<br>0.15                  |                                 | SEDIMENT TUFF + LAVA + SEDIMENTS                        |
| C0955              | 183.5                    | 0.15                          | . 101.7                         | TOTE T CAVA T SEDIFICATS                                |
| C0984              | 106.9                    | 0.15                          | 19.8                            |   |
| C0994              | 98.0                     | 0.15                          |                                 | CLAYEY TUFF   |
| C1000              | 148.0                    | 0.15                          |                                 | LAVA  |
| C1001              | 243.8                    | 0.15                          |                                 |   |
| C1007              | 61.0                     | 0.20                          | 100.0                           | DECOMPOSED LAVA   |
| C1013              | 201.8                    | 0.15                          |                                 | TUFF + GRAVEL + SAND + CLAY TUFF + GRAVEL + SAND + CLAY |
| C1013<br>C1019     | 201.8<br>217.2           | 0.15<br>0.20                  |                                 | CLAYS + TRACHYTE  |
| C1013              | 118.9                    | 0.20                          |                                 | WEATHERED TRACHYTE                                      |
| C1027              | 106.7                    | 0.15                          | 65.8                            |   |
| C1029              | 137.2                    |                               |                                 |   |
| C1033              | 183.0                    | 0.20                          | 90.0                            | ÷   |
| C1043              | 210.0                    | 0.15                          | 0.0                             | T   |
| C1051              | 194.2                    | 0.15                          |                                 | TUFF + CLAY + GRAVEL                                    |
| C1062<br>C1063     | 32.0<br>40.8             | 0.15<br>0.15                  | 21.6<br>23.5                    |   |
| C1003              | 160.0                    | 0.15                          |                                 | FRACTURED LAVA + SEDIMENTS                              |
| C1082              | 110.5                    | 0.15                          |                                 | FRACTURED LAVAS   |
| C1082              | 108.9                    | 0.15                          |                                 | TUFF + TRACHYTE   |
| C1089              | 244.0                    | 0.15                          |                                 |   |
| C1112              | 152.4                    |                               |                                 | •   |
| C1125              | 125.0                    | 0.15                          | 19.2                            |   |
| C1126              | 215.5                    | 0.15                          |                                 | OLD LAND SURFACE  |
| C1148<br>C1161     | 72.5<br>216.0            | 0.15<br>0.15                  | 23.2                            |   |
| C1250              | 168.0                    | 0.15                          | 80 O                            | FRACTURED LAVA  |
| C1259              | 142.0                    | 0.25                          | 20.0                            | ·   |
| C1265              | 245.0                    | 0.15                          |                                 |   |
| C1277              | 114.3                    | 0.20                          | 13.3                            | SAND + TRACHYTE   |
| C1279              | 182.9                    | 0.20                          | 6.4                             |   |
| C1281              | 31.0                     | 0.15                          |                                 | PUMICE & ASH  |
| C1287              | 102.7                    | 0.20<br>0.25                  | 100.3                           | PEBBLES + ASH   |
| C1294<br>C1325     | 182.9<br>192.0           | 0.25                          | 102 0                           | SANDS   |
| C1325              | 30.8                     | 0.20                          |                                 | LAVA PEBBLES  |
| C1358              | 204.0                    | 0.20                          |                                 | RHYOLITE  |
| C1361              | 249.9                    | 0.15                          |                                 | TUFF +TRACHYTE  |
| C1362              | 199.4                    | 0.15                          |                                 | WEATHERED TRACHYTE                                      |
| C1374              | 105.0                    | 0.15                          | 4.8                             | FRACTURED LAVAS   |
|                    |                          |                               |                                 |   |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER<br>(m) | PLAIN<br>CASING<br>DEPTI<br>(m) | i ,                                     |      |
|--------------------|--------------------------|-----------------------------|---------------------------------|---|------|
| C1379              | 126.0                    | 0.15                        | 36.0                            | TUFF                                    |      |
| C1383              | 97.5                     | 0.15                        | 9.1                             | TRACHYTE                                |      |
| C1390              | 171.0                    | 0.20                        |                                 |   |      |
| C1391              | 152.0                    | 0.20                        |                                 |   | ·    |
| C1394              | 181.8                    | 0.25                        |                                 | PUMICE + LAVA                           |      |
| C1402              | 232.0                    | 0.25                        | 22.7                            |   |      |
| C1404              | 103.5                    | 0.20                        | 75.3                            | SAND                                    |      |
| C1425              | 283.0                    | 0.15                        |                                 |   |      |
| C1434              | 137.2                    | 0.15                        | 85.8                            |   | •    |
| C1436              | 142.0                    | 0.15                        | 11 0                            | eri |      |
| C1464<br>C1475     | 31.1                     | 0.15                        | 11.0                            |   |      |
| C1475<br>C1482     | 107.0<br>36.3            | 0.15                        | 91.0                            | LAVE CEDIMENTS                          |      |
| C1482              | 30.3<br>45.7             | 0.15<br>0.15                | 6.1                             | LAKE SEDIMENTS                          |      |
| C1486              | 152.4                    | 0.15                        |                                 | TRACHYTE                                |      |
| C1487              | 155.4                    | 0.25                        | 83.6                            |   |      |
| C1487              | 91.4                     | 0.23                        |                                 | TUFF + LAKE SEDIMENTS                   |      |
| C1491              | 162.1                    | 0.15                        | 20.7                            | TOTT FEARCE SEDIFICATS                  |      |
| C1499              | 129.5                    | 0.15                        | 20.7                            |   |      |
| C1503              | 296.4                    | 0.15                        |                                 | DECOMPOSED TRACHYTE                     |      |
| C1504              | 152.4                    | 0.15                        | 128.7                           |   |      |
| C1523              | 132.0                    | 0.15                        |                                 | •                                       |      |
| C1524              | 244.0                    | 0.20                        |                                 |   |      |
| C1525              | 217.0                    |                             | • •                             |   |      |
| C1535              | 188.9                    | 0.15                        | 18.0                            | PALEOSOILS + LAVAS                      |      |
| C1545              | 46.0                     | 0.15                        | 29.6                            |   |      |
| C1558              | 135.0                    | 0.15                        |                                 | SEDIMENTS                               |      |
| C1559              | 119.2                    | 0.20                        | 13.4                            | LAVA                                    |      |
| C1584              | 86.3                     | 0.15                        | 43.6                            | :                                       | •    |
| C1585              | 155.0                    | 0.15                        | 6.6                             | WEATHERED LAVA                          |      |
| C1602              | 172.0                    | 0.15                        |                                 |   |      |
| C1614              | 189.0                    | 0.15                        |                                 | TUFF + WEATHERED TRACHYTE               |      |
| C1625              | 91.4                     | 0.15                        | 31.5                            | TUFF                                    |      |
| C1641              | 182.9                    | 0.15                        | 5.5                             |   |      |
| C1652<br>C1662     | 61.0                     | 0.15                        | 18.3                            |   |      |
| C1666              | 182.9<br>187.4           | 0.15<br>0.15                | 142.0                           | LAKE SEDIMENTS+FRACTURED LA             | ۸۱/۸ |
| C1713              | 259.7                    | 0.15                        | 109.5                           | LAVA                                    | HVA  |
| C1713<br>C1726     | 283.6                    | 0.20                        | 30 E                            | BASALT + BASALT SAND                    |      |
| C1749              | 175.3                    | 0.15                        |                                 | WEATHERED LAVA                          |      |
| C1794              | 236.3                    | 0.15                        | 0.0                             | LAVA                                    |      |
| C1795              | 162.8                    | 0.15                        | 6.1                             | LAVA + PUMICE                           |      |
| C1795              | 162.8                    | 0.15                        |                                 | LAVA + PUMICE                           |      |
| C1798              | 186.6                    | 0.20                        |                                 | FRACTURED LAVA                          |      |
| C1830              | 170.4                    | 0.15                        |                                 | TUFF + SAND                             |      |
| C1843              | 256.0                    | 0.15                        | 13.3                            |   |      |
| C1850              | 192.0                    | 0.15                        | 5.8                             | LAVA                                    |      |
| C1851              | 306.3                    | 0.15                        | •                               | • •                                     |      |
| C1877              | 191.1                    | 0.25                        |                                 | LAVA + TUFF                             |      |
| C1892              | 256.3                    | 0.15                        | 30.8                            | **                                      |      |
| C1898              | 102.4                    | 0.20                        | 3.3                             |   |      |
| C1911              | 172.2                    | 0.15                        |                                 |   |      |
| C1912              | 151.2                    | 0.20                        |                                 | 01.41                                   |      |
| C1913              | 147.0                    | 0.15                        |                                 | CLAY + SAND                             |      |
| C1914              | 76.2                     | 0.15                        | 51.8                            |   |      |
| C1924              | 157.5                    | 0.15                        | ٥.٥                             | TUFF SAND + GRIT                        |      |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER<br>(m) | PLAII<br>CASING<br>DEPTI<br>(m) | 3                              |
|--------------------|--------------------------|-----------------------------|---------------------------------|--------------------------------|
| C1926              | 125.0                    | 0.20                        |                                 | SEDIMENT                       |
| C1927              | 41.8                     | 0.20                        | 5.8                             | ASH                            |
| C1929              | 136.0                    | 0.20                        | <b>CO O</b>                     | GRAVEL                         |
| C1935<br>C1941     | 197.0<br>170.1           | 0.15                        | 60.0                            | TRACHYTE                       |
| C1947              | 67.0                     | 0.25                        | 16.8                            | TRACITIE                       |
| C1951              | 147.6                    | 0.15                        |                                 | TUFF                           |
| C1952              | 138.0                    | 0.15                        |                                 | TUFF + TRACHYTE                |
| C1970              | 225.0                    | 0.20                        |                                 | SAND + CLAY + BASALT           |
| C1990              | 102.0                    | 0.25                        | 45.3                            | LAKE SEDIMENTS                 |
| C1997              | 223.5                    | 0.15                        | •                               | HETEROGENEOUS SAND IN BUFF MTX |
| C2005<br>C2007     | 255.0                    | 0.15<br>0.20                | 100.3                           | DACALT                         |
| C2007              | 107.6<br>126.6           | 0.20                        |                                 | BASALT<br>ASH + TUFF           |
| C2033              | 180.0                    | 0.15                        | 0.9                             | ASR T TOFF                     |
| C2042              | 191.4                    | 0.20                        |                                 |                                |
| C2058              | 46.6                     | 0.20                        | 0.0                             | ,                              |
| C2059              | 118.3                    | 0.15                        |                                 |                                |
| C2061              | 123.9                    | 0.15                        | 6.2                             | PUMICE + SAND                  |
| C2062              | 260.8                    | 0.15                        |                                 | CLAYEY SANDY SEDIMENTS         |
| C2063              | 129.0                    | 0.15                        |                                 | SCORIA                         |
| C2069<br>C2071     | 79.0<br>18.9             | 0.15                        | 76.2<br>11.6                    |                                |
| C2071              | 221.4                    | . 0.20                      | 11.0                            |                                |
| C2077              | 204.0                    |                             |                                 | LAVA                           |
| C2097              | 180.9                    | 0.15                        | 21.0                            | TUFF                           |
| C2108              | 187.8                    | 0.15                        |                                 | LAVA + LAKE SEDIMENTS          |
| C2109              | 90.0                     | 0.15                        |                                 | TUFF + PUMICE                  |
| C2110              | 129.3                    | 0.15                        | 10.5                            | A C ! !                        |
| C2117<br>C2118     | 26.2<br>208.8            | 0.20<br>0.15                | 6.4                             | SAND + GRAVEL                  |
| C2118              | 135.0                    | 0.15                        |                                 | WELDED PYROCLASTICS            |
| C2129              | 183.0                    | 0.20                        |                                 | PYROCLSTICS + LAVAS            |
| C2138              | 124.1                    | 0.20                        |                                 | PEBBLES + GRAVEL               |
| C2149              | 198.1                    | 0.15                        | 16.2                            | TUFF + GRAVEL                  |
| C2160              | 185.1                    | 0.15                        |                                 | BASALT                         |
| C2170              | 228.6                    | 0.15                        | 12.3                            | TUFF + PUMICE + CLAY           |
| C2170<br>C2172     | 225.0<br>142.0           | 0.20<br>0.20                |                                 | SAND                           |
| C2172              | 76.0                     |                             | 23 9                            | COARSE GRAVEL                  |
| C2197              | 182.9                    |                             | 1/1 2                           | CAMD                           |
| C2234~             | 162.9                    | 0.20                        | 111.0                           | CLAY + TUFF                    |
| C2241              |                          | 0.20                        | 75.3                            | LAVA + ASH                     |
| C2246              | 38.1                     | 0.20                        | 32.0                            | SEDIMENTS                      |
| C2263              | 274.0                    | 0.45                        |                                 |                                |
| C2264              | 273.0                    | 0.15                        |                                 |                                |
| C2269<br>C2276     | 150.0<br>137.2           | 0.15<br>0.20                | 58.2                            | TUFFS                          |
| C2288              |                          | 0.15                        | 120.4                           | TUFFS                          |
| C2289              | 139.2                    |                             | 24.6                            | PHONOLITE                      |
| C2292              |                          | 0.15                        |                                 | LAKE SEDIMENT + CLAY           |
| C2294              |                          | 0.20                        | 51.2                            | BASALT                         |
| C2296              |                          | 0.15                        | •                               | TUFF + PUMICE                  |
| C2300              |                          | 0.15                        | 98.4                            | ASH                            |
| C2304<br>C2322     | 42.0<br>138.0            | 0.25<br>0.15                | 12.3                            | IGNIMBRITE + GRAVEL            |
| CLJLL              | 130.0                    | 0.13                        | 23.4                            | IGNIPIDATIC T GRAVEL           |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>·· (m) | BOREHOLE<br>DIAMETER<br>(m) | PLAII<br>CASING<br>DEPTI<br>(m) | G<br>H                             | Y   |
|--------------------|-----------------------------|-----------------------------|---------------------------------|------------------------------------|-----|
| C2332              | 119.1                       | 0.15                        |                                 | TUFF + PHONOLITE                   |     |
| C2338              | 238.0                       | 0.15                        |                                 | TUFFS + SANDS                      |     |
| C2347              | 41.0                        | 0.20                        | 40.8                            |                                    |     |
| C2358              | 311.0                       | 0.15                        |                                 | SANDS                              |     |
| C2388<br>C2402     | 264.0<br>99.1               | 0.23<br>0.20                |                                 | SAND + SILT<br>FRACTURED LAVA      |     |
| C2402<br>C2420     | 124.0                       | 0.20                        | 19.5                            |                                    | •   |
| C2421              | 193.0                       | 0.15                        |                                 | TUFF                               | •   |
| C2430              | 31.0                        | 0.25                        | 17.4                            |                                    | •   |
| C2432              | 173.0                       | 0.20                        | 59.1                            | •                                  |     |
| C2447              | 213.0                       | 0.20                        |                                 | TUFF                               |     |
| C2448              | 288.0                       | 0.20                        | 17.7                            |                                    | •   |
| C2466              | 98.0                        | 0.20                        | 88.4                            | LAVA SAND                          | •   |
| C2468              | 179.0                       | 0.15                        | 10.1                            | GNEISS                             | . * |
| C2480<br>C2482     | 71.6<br>105.0               | 0.15<br>0.20                | 18.3                            | FELDSPATHIC SAND                   | •   |
| C2493              | 146.9                       | 0.20                        | 8 4                             | LAVA SAND                          |     |
| C2496 -            | 167.6                       | 0.15                        |                                 | TUFF                               |     |
| C2497              | 158.5                       | 0.15                        | 21.6                            | ,                                  | ,   |
| C2499              | 213.4                       | 0.15                        | 122.8                           | TUFF                               |     |
| C2504              | 167.6                       | 0.15                        |                                 | PYROCLASTICS                       | • • |
| C2521              | 102.6                       | 0.20                        |                                 | FRACTURED LAVA                     |     |
| C2522              | 51.5                        | 0.20                        | 39.3                            |                                    | •   |
| C2523              | 56.7                        | 0.13                        |                                 | FRACTURED LAVA                     |     |
| C2534<br>C2535     | 22.3<br>12.8                | 0.15<br>0.20                |                                 | TUFF & PUMICE<br>LAVA              |     |
| C2535              | 9.7                         | 0.20                        |                                 | VESICULAR LAVA                     |     |
| C2537              | 15.8                        | 0.20                        |                                 | VESICULAR LAVA                     |     |
| C2538              | 13.7                        | 0.31                        |                                 | PUMICE                             |     |
| C2539              | 12.5                        | 0.20                        | 1.5                             | TUFF                               |     |
| C2541              | 49.5                        | 0.31                        |                                 | •                                  |     |
| C2542              | 60.0                        | 0.15                        |                                 |                                    |     |
| C2543              | 150.0                       | 0.15                        | 12.0                            | EDACTUBED LAVA                     | •   |
| C2564<br>C2600     | 218.0<br>213.0              | 0.23<br>0.20                |                                 | FRACTURED LAVA<br>TUFF + LAVA SAND |     |
| C2620              | 152.4                       | 0.15                        |                                 | TRACHYTE + PHONOLITE               |     |
| C2636              | 30.5                        | 0.10                        |                                 | SEDIMENTS                          |     |
| C2646              | 91.4                        | 0.15                        |                                 | GNEISS                             |     |
| C2647              | 104.0                       | 0.15                        |                                 |                                    |     |
| C2657              | 32.6                        | 0.15                        | 33.1                            |                                    |     |
| C2659              | 24.4                        | 0.25                        |                                 | SEDIMENTS & PUMICE                 |     |
| C2660              | 28.3                        | 0.20                        | 25.2                            |                                    |     |
| C2662<br>C2663     | 256.2<br>137.0              | 0.15<br>0.15                | 20 7                            | SAND                               |     |
| C2664              | 195.0                       | 0.13                        | 30.7                            | SAND                               |     |
| C2667              | 205.9                       | 0.15                        |                                 | •                                  |     |
| C2670              | 192.7                       | 0.15                        | 6.3                             |                                    |     |
| C2680              | 85.3                        | 0.15                        |                                 |                                    |     |
| C2697              | 165.0                       | 0.15                        | 34.5                            | ALLUVIUM + ASH MATRIX              |     |
| C2701              | 25.9                        | 0.25                        |                                 | VOLCANIC SAND                      |     |
| C2703              | 30.8                        | 0.20                        | 14.7                            |                                    |     |
| C2704              | 76.2                        | 0.20                        | 76.5                            |                                    |     |
| C2705<br>C2706     | 31.0<br>62.5                | 0.20<br>0.20                | 30.2                            | LAVA<br>ASH                        |     |
| C2706<br>C2709     | 225.0                       | 0.20                        | 202 5                           | FRACTURED LAVA                     | •   |
| C2703              | 324.0                       | 0.25                        |                                 | OLD LAND SURFACE                   |     |
| ·-·                | 320                         | 3.23                        | ,                               |                                    |     |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER,<br>(m) | PLAI<br>CASIN<br>DEPT<br>(m) | G  |
|--------------------|--------------------------|------------------------------|------------------------------|--|
| C2720              | 301.0                    | 0.15                         |                              |  |
| C2745              | 178.3                    | 0.20                         |                              | LAKE SEDIMENTS   |
| C2753              | 210.0                    | 0.15                         |                              | ALLUVIUM + ASH MATRIX  |
| C2758              | 177.1                    | 0.15                         | 63.2                         | FRACTURED TRACHYTE + TUFF  |
| C2773<br>C2813     | 159.0                    | 0.20                         | 1/1 /                        | TUFF<br>LAVA   |
| C2813              | 63.1<br>305.5            | 0.36<br>0.15                 | 83.0                         |  |
| C2851              | 259.0                    | 0.15                         |                              | LAVA + LAKE SEDIMENTS  |
| C2863              | 152.0                    | 0.13                         | 0.0                          | ENVA - EARE SEDITIENTS   |
| C2866              | 147.5                    | 0.25                         | 98.4                         | LAVA   |
| C2870              | 105.5                    | 0.15                         | 3.0                          | LAVA   |
| C2871              | 36.6                     | 0.15                         | 3.0                          |  |
| C2883              | 106.7                    | 0.20                         | 85.9                         | TUFFS  |
| C2885              | 377.0                    |                              |                              | •  |
| C2886<br>C2887     | 933.3<br>97.5            |                              | 3.0                          | •  |
| C2894              | 180.4                    | 0.20                         |                              | TUFF + GRAVEL  |
| C2899              | 39.6                     | 0.15                         |                              | LAVA   |
| C2900              | 77.1                     | 0.15                         | 3.0                          | LAVA   |
| C2901              | 77.1                     | 0.15                         | 3.0                          | •  |
| C2902              | 110.0                    | 0.25                         | 33.0                         | VOLCANIC SAND  |
| C2910              | 305.0                    | 0.15                         | •                            | TRACHYTE SAND  |
| C2966<br>C2970     | 123.0<br>53.0            | 0.25                         | · 60 E                       | PALEOSOILS + PYROCLASTICS  |
| C2970<br>C2997     | 320.0                    | 0.25<br>0.15                 |                              | ASH & PUMICE   |
| C3003              | 295.6                    | 0.15                         | 32.1                         | TRACHYTE   |
| C3005              | 124.0                    | 0.25                         | 63.0                         |  |
| C3024              | 105.0                    | 0.15                         | 3.6                          | TUFF + SAND  |
| C3032              | 225.0                    | 0.15                         |                              | TUFF   |
| C3047              | 73.2                     | 0.30                         | 52.1                         |  |
| C3064              | 118.0                    | 0.20                         | 12.0                         |  |
| C3066<br>C3067     | 93.0<br>96.0             | 0.15<br>0.12                 | 12.0                         | ·  |
| C3087              | 76.0                     | 0.15                         | 6.0                          | TUFF   |
| C3136              | 180.0                    | 0.15                         | 30.0                         |  |
| C3164              | 73.5                     | 0.20                         |                              | SANDY CLAY   |
| C316D              | 134.4                    | 0.15                         | 9.9                          |  |
| C3216              | 42.7                     | 0.30                         |                              | LAKE SEDIMENTS   |
| C3217              | 42.7                     | 0.30                         |                              | LAKE SEDIMENTS   |
| C3243<br>C3266     | 188.9<br>111.0           | 0.15<br>0.15                 |                              | WEATHERED PHONOLITE, SAND  |
| C3280              | 137.2                    | 0.10                         |                              | LAVA + CLAY  |
| C3292              | 76.0                     | 0.20                         | 50.2                         | CATALOG CATALO |
| C3298              | 39.6                     | 0.30                         |                              | SAND + GRAVEL  |
| C3299              | 39.4                     | 0.30                         | 52.0                         | PYROCLASTICS   |
| C3324              | 201.2                    | 0.20                         | 182.9                        |  |
| C3327              | 141.0                    | 0.20                         | 126.0                        | LAKE SEDIMENTS   |
| C3351              | 186.0                    | 0.20                         |                              |  |
| C3352<br>C3353     | 264.0<br>142.7           | 0.15                         | 115 2                        | TUFFS + LAKE SEDIMENTS   |
| C3358              | 182.0                    | 0.13                         | 113.6                        | 10110 - CHINE DEDIFICIALD  |
| C3363              | 165.0                    | 0.15                         |                              | WEATHERED GNEISS   |
| C3365              | 82.0                     | 0.20                         |                              | LAKE SEDIMENTS   |
| C3366              | 76.8                     | 0.20                         |                              | LAKE SEDIMENTS   |
| C3371              | 185.9                    | 0.15                         |                              | LAVA + SEDIMENTS   |
| C3377              | 165.0                    | 0.15                         | 44.0                         | ·  |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER<br>(m) | PLAIN<br>CASING<br>DEPTH<br>(m) |                                 |
|--------------------|--------------------------|-----------------------------|---------------------------------|---------------------------------|
| C3397              | 117.3                    | 0.20                        | 6.6                             |                                 |
| C3417              | 91.7                     | 0.20                        |                                 | SEDIMENTS + LAVA                |
| C3418              | 240.0                    | 0.20                        | 61.2                            | SAND + GRAVEL                   |
| C3422<br>C3431     | 117.0<br>174.6           | 0.15<br>0.25                | 18.0                            | SANU + GRAVEL                   |
| C3436              | 76.0                     | 0.15                        | 10.0                            |                                 |
| C3451              | 122.0                    | 0.15                        |                                 |                                 |
| C3467              | 228.7                    | 0.15                        |                                 |                                 |
| C3490              | 193.9                    | 0.15                        | 34.4                            | TUFF + SAND                     |
| C3523              | 61.6                     | 0.15                        | 12.0                            | GRAVEL                          |
| C3524              | 106.7                    | 0.15                        |                                 | GRAVEL                          |
| C3525              | 143.3                    | 0.15                        | 110.6                           | •                               |
| C3551              | 76.8                     | 0.20                        | 4.5                             | SAND + GRAVEL                   |
| C3562              | 91.4                     | 0.20                        |                                 | 1.01(0                          |
| C3576              | 137.2                    | 0.15                        | 12.0                            | LAVA<br>TUFF                    |
| C3615<br>C3616     | 85.0<br>57.0             | 0.15<br>0.20                |                                 | LAVA                            |
| C3627              | 138.1                    | 0.15                        | 50.7                            | LAVA                            |
| C3650              | 121.9                    | 0.15                        |                                 | TUFFS                           |
| C3674              | 30.4                     | 0.15                        |                                 | TRACHYTE                        |
| C3675              | 61.0                     | 0.20                        |                                 | SAND + GRAVEL                   |
| C3677              | 91.4                     | 0.20                        | 3.0                             | SEDIMENTS                       |
| C3678              | 72.5                     | 0.20                        |                                 | SAND + GRAVEL                   |
| C3693 `            | 122.0                    | 0.15                        | 24.0                            | TUFF                            |
| C3694              | 122.0                    | 0.15                        | 37.0                            |                                 |
| C3710              | 87.0                     | 0.20                        | 31.0                            |                                 |
| C3713<br>C3721     | 80.8<br>140.0            | 0.15<br>0.15                | 18.0                            | TRACHYTE                        |
| C3721<br>C3739     | 73.0                     | 0.15                        |                                 | OLD LAND SURFACE                |
| C3740              | 35.7                     | 0.20                        |                                 | VOLCANIC SAND                   |
| C3763              | 85.0                     | 0.15                        |                                 | OLD LAND SURFACE                |
| C3764              | 107.0                    |                             | 6.0                             | OLD LAND SURFACE                |
| C3765              | 67.0                     | 0.15                        | 6.0                             |                                 |
| C3767              | 72.2                     | 0.15                        |                                 |                                 |
| C3771              | 91.0                     |                             |                                 | TUFFS + GRAVEL                  |
| C3779              | 150.6                    | 0.15                        | 111.9                           |                                 |
| C3784<br>C3799     | 150.0<br>83.0            | 0.15                        |                                 | TUFF<br>GRAVEL + WEATHERED LAVA |
| C3870              | 107.9                    | 0.15                        |                                 | GRAVEE , WEATHERED LAVA         |
| C3874              | 71.0                     |                             | 54.0                            | FRACTURED LAVAS                 |
| C3875              | 73.0                     | 0.30                        | 53.8                            |                                 |
| C3897              | 105.5                    | 0.20                        | 42.7                            | OLD LAND SURFACE                |
| C3910              | 98.0                     | 0.20                        | 9.0                             |                                 |
| C3919              | 152.4                    | 0.30                        | 126.1                           |                                 |
| C3924              | 00                       | 0.30                        | 56.0                            | THEE                            |
| C3925<br>C3929     | 122.0<br>61.0            |                             |                                 | TUFF                            |
| C3929              | 165.0                    | 0.20                        | 60.0                            | TUFF                            |
| C3937              | 260.6                    | 0.15                        | 66.5                            | 1011                            |
| C3939              | 152.0                    | 0.10                        |                                 |                                 |
| C3942              | 152.4                    | 0.15                        | 87.8                            | GNEISS                          |
| C3951              | 122.0                    | 0.15                        |                                 | GNEISS                          |
| C3955              | 143.0                    | 0.15                        |                                 | TRACHYTE + SANDSTONE            |
| C3965              | 158.5                    |                             |                                 | PYROCLASTICS + FRACTURED LAVAS  |
| C3970              | 137.5                    | 0.15                        |                                 | GNEISS                          |
| C3976              | 126.5                    | 0.15                        | 37.6                            |                                 |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER<br>(m) | PLAIN<br>CASING<br>DEPTH<br>(m) |                                |
|--------------------|--------------------------|-----------------------------|---------------------------------|--------------------------------|
| C3995              | 122.0                    | 0.15                        | 13.8                            |                                |
| C3999              | 138.5                    | 0.20                        |                                 | TUFF + LAVA + SEDIMENTS        |
| C4003              | 183.0                    | 0.30                        | 33.0                            |                                |
| C4037              | 198.5                    | 0.20                        | 13.5                            | T.155                          |
| C4057              | 61.0                     | 0.15                        |                                 | TUFF                           |
| C4061              | 1002.0                   | 0.20                        |                                 | LAVA & TUFF                    |
| C4062<br>C4077     | 1350.0<br>226.0          | 0.20<br>0.15                | 13.0                            | LAVA & TUFF                    |
| C4077              | 143.0                    | 0.15                        |                                 |                                |
| C4032              | 251.0                    | 0.15                        | 36.5                            | TUFF + CLAY                    |
| C4121              | 178.0                    | 0.15                        | 12.0                            | TOTT CENT , STATE              |
| C4131              | 181.5                    | 0.10                        | 22.0                            |                                |
| C4143              | 197.0                    |                             |                                 |                                |
| C4152              | 144.6                    | 0.15                        | _                               | TUFF                           |
| C4155              | 128.0                    | 0.15                        | 12.0                            |                                |
| C4157              | 78.0                     | 0.25                        |                                 | TUFF                           |
| C4161              | 52.0                     | •                           |                                 | SAND + GRAVEL                  |
| C4168              | 52.0                     | 0.20                        |                                 | SAND + GRAVEL                  |
| C4174              | 68.0                     | 0.15                        |                                 | SAND + GRAVEL                  |
| C4177              | 52.0                     | 0:20                        |                                 | SAND + GRAVEL                  |
| C4178              | 52.0                     | 0.25                        |                                 | SAND + GRAVEL                  |
| C4179              | 116.0                    | 0.20                        | 107.0                           |                                |
| C4185              | 120.0<br>152.0           | 0.15                        | <u>.</u>                        | WEATHERED BASALT + TUFF        |
| C4186<br>C4200     | 226.0                    | 0.20<br>0.20                | /3 Q                            | GRAVEL                         |
| C4200              | 155.0                    | 0.20                        |                                 | GRAVEL                         |
| C4201              | 250.0                    | 0.20                        | 65.0                            | GRAVEC                         |
| C4208              | 61.0                     | 0.25                        |                                 | PUMICE + SAND                  |
| C4209              | 62.0                     | 0.25                        | 12.0                            | TORICE SAME                    |
| C4214              | 248.0                    | 0.15                        | 0.0                             |                                |
| C4252              | 181.0                    | 0.15                        | 43.0                            |                                |
| C4279              | 141.0                    | 0.15                        | 19.0                            |                                |
| C4292              | 200.0                    | 0.20                        | 21.4                            | GRAVEL                         |
| C4301              | 109.7                    | 0.30                        | 29.7                            |                                |
| C4302              | 76.0                     |                             |                                 | LAKE SEDIMENTS                 |
| C4306              | 232.0                    | 0.32                        | 30.3                            | LAVA + CLAY + SANDSTONE        |
| C4331              | 200.0                    | 0.25                        | 66.0                            |                                |
| C4332              | 112.0                    | 0.30                        | 66.0                            |                                |
| C4350<br>C4360     | 170.0                    | 0.15<br>0.20                | 12.0                            | •                              |
| C4369              | 135.0<br>166.0           | 0.20                        | 26.0<br>111.8                   | •                              |
| C4303              | 180.0                    | 0.20                        |                                 | PALEOSOILS + PYROCLASTICS      |
| C4397              | 33.5                     | 0.25                        | 16.8                            | TACEOSOTES TIMOCEASTICS        |
| C4403              | 00.5                     | 0.15                        | 11.0                            | •                              |
| C4413              | 137.0                    | 0.15                        |                                 | SANDSTONE                      |
| C4416              | 183.0                    | 0.25                        | 25.0                            |                                |
| C4420              | 25.0                     | 0.40                        | 16.8                            |                                |
| C4431              | 240.0                    | 0.30                        | 78.6                            | BASALT + TRACHYTES             |
| C4461              | 221.0                    | 0.20                        |                                 |                                |
| C4484              | 200.0                    | 0.15                        |                                 |                                |
| C4491              | 69.0                     | 0.25                        |                                 | PYROCLASTICS + FRACTURED LAVAS |
| C4492              | 150.0                    | 0.20                        |                                 | PYROCLASTICS + SCORIA          |
| C4493              | 75.0                     | 0.20                        |                                 | LAKE SEDIMENTS + PYROCLASTICS  |
| C4498              | 100.0                    | 0.15                        |                                 | MEDIUM/FINE SANDS              |
| C4499              | 213.0                    | 0.15                        | 40.0                            | 1 040                          |
| C4500              | 61.0                     | 0.30                        | 46.0                            | LAVA                           |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER<br>(m) | PLAIN<br>CASING<br>DEPTH<br>(m) |  |
|--------------------|--------------------------|-----------------------------|---------------------------------|--|
| C4501              | 58.0                     | 0.30                        |                                 | LAVA   |
| C4502              | 112.0                    | 0.15                        |                                 | SANDSTONE                                    |
| C4504              | 30.5                     | 0.30                        | 2.0                             | LAVA   |
| C4510              | 150.0                    | 0.25                        |                                 |  |
| C4511              | 148.0                    | 0.25                        | 90.0                            |  |
| C4512              | 150.0                    | 0.25<br>0.15                | 24 0                            | GRAVEL + CLAY                                |
| C4517<br>C4531     | 188.0<br>150.0           | 0.15                        | 24.0                            | GRAVEL + CLAT                                |
| C4551<br>C4554     | 86.0                     | 0.15                        |                                 | •  |
| C4555              | 128.0                    | 0.15                        | 12 0                            | LAKE SEDIMENTS                               |
| C4564              | 120.0                    | 0.15                        | 12.0                            | FRACTURED TRACHYTE                           |
| C4565              | 200.0                    | 0.30                        |                                 |  |
| C4575              | 196.0                    | 0.22                        | 23.0                            |  |
| C4591              | 45.7                     | 0.53                        | 12.0                            | TUFF   |
| C4594              | 213.6                    | •                           |                                 |  |
| C4597              | 260.0                    | 0.20                        |                                 | TRACHYTE                                     |
| C4610              | 53.0                     | 0.25                        | 13.3                            | GRAVEL + SAND                                |
| C4615              | 157.0                    | 0.20                        |                                 | ·  |
| C4624              | 230.2                    | 0.20                        | 12.0                            | TDACHVTE                                     |
| C4634              | 110.0                    | 0.20                        | 6.0                             | TRACHYTE                                     |
| C4665<br>C4669     | 153.0<br>214.0           | 0.20<br>0.20                | 6.0                             | WEATHERED TUFF                               |
| C4685              | 122.0                    | 0.25                        | 29.0                            | WEATHERED TOFF                               |
| C4687              | 102.0                    | 0.20                        |                                 | TUFFS  |
| C4713              | 150.0                    | 0.20                        |                                 | TRACHYTE                                     |
| C4743              | 104.0                    | 0.20                        | 21.0                            |  |
| C4792              | 204.0                    | 0.25                        |                                 | TUFF   |
| C4804              | 140.0                    | 0.20                        | 8.0                             | TRACHYTE + PHONOLITE                         |
| C4807              | 206.0                    | 0.20                        |                                 |  |
| C4812              | 193.0                    | 0.25                        | 15.4                            |  |
| C4829              | 185.0                    | 0.22                        |                                 |  |
| C4850              | 80.0                     |                             | 53.0                            | WEATHERED TRACHYTE                           |
| C4855              | 150.0                    |                             | 50.0                            | THEFE  |
| C4863              |                          | 0.20                        | 89.0                            | TUFFS  |
| C4881<br>C4893     |                          | 0.20<br>0.25                | 23.0                            |  |
| C4897              |                          | 0.25                        |                                 | SEDIMENTS                                    |
| C4907              |                          |                             |                                 | WEATHERED GNEISS                             |
| C4909              |                          | 0.30                        |                                 |  |
| C4924              |                          | 0.20                        |                                 | FRACTURED LAVA +LAKE SEDIMENT                |
| C4927              |                          | 0.20                        | 9.0                             |  |
| C4966              |                          |                             |                                 | AGGLOMERATE + LAVA                           |
| C4968              |                          | 0.30                        |                                 | ASH  |
| C4971              |                          | 0.15                        |                                 |  |
| C4974              |                          | 0.15                        |                                 | TRACHYTE                                     |
| C4981              |                          |                             |                                 | WEATHERED PHONOLITE                          |
| C4986<br>C4989     |                          | 0.30<br>0.30                | 6.0                             |  |
| C4989<br>C4997     |                          | 0.30                        |                                 | FRACTURED BASALT                             |
| C5002              |                          | 0.30                        |                                 | LAKE SEDIMENTS                               |
| C5029              | 210.0                    |                             |                                 | AGGLOMERATE                                  |
| C5111              | 188.8                    |                             |                                 | · · · · · = - · · <del>- · · · · · · ·</del> |
| C5117              | 117.0                    |                             |                                 | WEATHERED BASALT                             |
| C5143              | 165.0                    | 0.20                        | 12.0                            | LAVAS + PYROCLASTICS                         |
| C5161              | 150.0                    |                             |                                 | WEATHERED ASH                                |
| C5175              | 51.0                     | 0.20                        | 36.6                            | ASH.   |

| BOREHOLE<br>NUMBER | BOREHOLE<br>DEPTH<br>(m) | BOREHOLE<br>DIAMETER<br>(m) | PLAIR<br>CASING<br>DEPTH<br>(m) | G  |
|--------------------|--------------------------|-----------------------------|---------------------------------|--|
| C5206              | 220.2                    | 0.15                        |                                 | WEATHERED AGGLOMERATE                        |
| C5257<br>C5343     | 200.0<br>152.0           | 0.15<br>0.20                |                                 | PYROCLASTICS + SEDIMENTS WEATHERED TRACHYTE  |
| C5343              | 152.0                    | 0.20                        |                                 | WEATHERED TUFF                               |
| C5346<br>C5375     | 96.0                     | 0.20                        |                                 | WEATHERED TUFF                               |
| C5411              | 116.0                    | 0.20                        |                                 | WEATHERED TUFF                               |
| C5520              | 100.0                    | 0.15                        |                                 | PUMICE + GRAVEL                              |
| C5564              | 160.0                    | 0.20                        |                                 | BASALTS                                      |
| C5754              | 100.0                    | 0.18                        | ,,,                             | D. G. C. |
| C5798              | 134.0                    | 0.25                        | 112.0                           | TRACHYTE                                     |
| C6056              | 150.0                    | 0.15                        |                                 | WEATHERED TUFF                               |
| C6095              | 120.0                    | 0.18                        |                                 | •  |
| C6186              | 31.0                     | 0.12                        | 20.0                            | SILTSTONE                                    |
| C6211              | 100.0                    | 0.15                        | 6.0                             |  |
| C6213              | 185.0                    | 0.15                        | 35.0                            |  |
| C6271              | 74.8                     |                             |                                 |  |
| C6290              | 208.0                    | 0.20                        | 107.0                           |  |
| C6300              | 200.0                    | 0.20                        | 130.5                           | •  |
| C630D              | 126.0                    | 0.20                        | 101.8                           |  |
| C6377              | 200.0                    | 0.20                        | 62.0                            | T0 4 0 1 1 1 T                               |
| C6378              | 131.0                    | 0.20                        |                                 | TRACHYTE                                     |
| C6494<br>C6495     | 160.0<br>99.4            | 0.20                        | 30.0                            |  |
| C6524              | 134.0                    | 0.25                        | 89.0                            |  |
| C6613              | 204.0                    | 0.15                        | 41.5                            |  |
| KJ1                | 232.0                    | 0.20                        | 2.0                             |  |
| M0001              | 183.0                    | 0.20                        | 2.0                             |  |
| P0002              | 82.6                     |                             | 40.4                            | BRECCIA                                      |
| P0012              | 96.9                     |                             | 14.3                            | · .  |
| P0016              | 147.5                    |                             | 27.4                            | LAVA   |
| P0023              | 82.9                     |                             | 42.5                            |  |
| P0027              | 36.7                     |                             |                                 |  |
| P0036              | 34.1                     |                             | •                               |  |
| P0037              | 21.2                     |                             |                                 | •  |
| P0053              | 229.0                    |                             | 34.7                            | •  |
| P0065              | 100.6                    | 0.16                        | 5.4                             |  |
| P0071              | 189.8                    |                             |                                 | •  |
| P0089              | 42.1                     | 0.15                        | 20.0                            | FOACTURED LAVA                               |
| SA58               | 98.5                     | 0.15                        | 26.6                            | FRACTURED LAVA                               |

### APPENDIX 3 - BOREHOLE WATER STRIKES AND LEVELS

| BOREHOLE<br>NUMBER  | MINOR WATER STRIKE<br>DEPTHS<br>(m) | MINOR REST WATER<br>LEVELS<br>(m) | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m)        | MAIN<br>REST<br>WATER<br>LEVEL<br>(m)               |
|---|-------------------------------------|-----------------------------------|--|---|
| 0001C<br>C0054  |                                     |                                   | 30.0   | 133.4<br>15.0                                       |
| C0057<br>C0059<br>C0079<br>C0092                            | ,                                   |                                   | 124.1<br>102.9                                 | 103.6<br>96.3                                       |
| C0107<br>C0108<br>C0115                                     |                                     |                                   | 22.8   | 19.8  |
| C0131<br>C0132<br>C0152<br>C0164                            | 24.3 36.0                           |                                   | 41.0<br>42.1<br>48.4<br>60.9                   | 13.1<br>.15.8<br>48.4<br>18.8                       |
| C0165<br>C0202<br>C0204<br>C0205<br>C0208                   | 61.0                                |                                   | 133.0<br>61.0<br>116.0                         | 38.0<br>26.0<br>104.0                               |
| C0210<br>C0211<br>C0214<br>C0220<br>C0223<br>C0227          | 15.8<br>106.7<br>118.9              | <b>15.2</b>                       | 36.6<br>93.0<br>64.0<br>62.5<br>173.7<br>143.3 | 15.2<br>89.9<br>54.9<br>33.5<br>53.3<br>63.1        |
| C0227<br>C0231<br>C0258<br>C0261<br>C0264<br>C0266<br>C0288 | 110.9                               |                                   | 8.8<br>91.4<br>81.0<br>149.3<br>139.5<br>106.7 | 8.8<br>55.5<br>70.8<br>143.3<br>104.0<br>82.0       |
| C0295<br>C0306<br>C0307<br>C0321<br>C0325<br>C0376<br>C0379 | 18.2<br>69<br>54.8                  |                                   | 72.5<br>13.7<br>95.0<br>115.8<br>70.0<br>40.0  | 37.5<br>18.9<br>10.1<br>67.0<br>23.2<br>37.0<br>0.0 |
| C0381<br>C0407<br>C0408<br>C0416                            |                                     |                                   | 31.1<br>146.3<br>72.3<br>80.8                  | 22.6<br>138.1<br>96.9<br>67.1                       |
| C0417<br>C0419<br>C0423<br>C0429                            | 171.0 179.0<br>159.4                | 159.9                             | 182.0<br>182.9<br>195.0<br>77.4                | 138.7<br>159.9<br>64.0<br>70.5                      |
| C0431<br>C0440<br>C0451                                     | 201.0                               | 159.0                             | 198.0<br>76.2<br>134.0                         | 159.0<br>45.7<br>44.0                               |
| C0456<br>C0457<br>C0458<br>C0463                            | 34<br>61<br>11                      | 27.0                              | 48.9<br>76.0<br>44.8<br>61.0                   | 47.4<br>27.0<br>36.6<br>13.0                        |
| 30.00   |                                     |                                   | 01.0   | 13.0  |

| BOREHOLE<br>NUMBER  | MINOR WATER STRIKE<br>DEPTHS<br>(m) | MINOR REST WATER<br>LEVELS<br>(m) | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m)                | MAIN<br>REST<br>WATER<br>LEVEL<br>(m)                  |
|---|-------------------------------------|-----------------------------------|--|--|
| C0465<br>C0466<br>C0467<br>C0468                            | 87                                  |                                   | 96.6<br>52.5<br>87.0<br>18.3                           | 41.4<br>49.2<br>82.9<br>17.0                           |
| C0485<br>C0510<br>C0511                                     | •                                   |                                   | 84.0   | 64.0   |
| C0531<br>C0533<br>C0553<br>C0562<br>C0563                   |                                     |                                   | 16.0<br>205.7<br>88.4<br>42.7<br>21.3                  | 16.0<br>205.7<br>88.4<br>22.9<br>7.3                   |
| C0567<br>C0570<br>C0572<br>C0579<br>C0580                   | •                                   |                                   | 81.4<br>115.8<br>227.0<br>27.4<br>51.8                 | 56.1<br>30.0<br>210.0<br>22.3<br>45.7                  |
| C0581<br>C0582<br>C0605<br>C0624<br>C0628<br>C0631<br>C0633 | 113.0 130.0                         |                                   | 27.4<br>21.3<br>136.0<br>61.0<br>33.5<br>33.2<br>180.0 | 23.2<br>13.7<br>122.0<br>61.0<br>33.5<br>27.4<br>164.0 |
| C0634<br>C0648<br>C0651<br>C0655<br>C0665<br>C0667          | 64                                  |                                   | 91.0<br>130.0<br>139.0<br>22.9<br>101.0                | 76.0<br>137.0<br>22.9<br>52.0                          |
| C0677<br>C0678<br>C0691                                     | 36.0 35.0                           |                                   | 50.6   | 32.9   |
| C0692<br>C0699<br>C0703<br>C0704<br>C0705                   | 80                                  |                                   | 167.6<br>76.2<br>85.3                                  | 158.5<br>76.2<br>85.3                                  |
| C0706<br>C0707<br>C0719<br>C0729<br>C0732                   | 67                                  |                                   | 69.0<br>164.0<br>137.0                                 | 66.0<br>160.0<br>61.0                                  |
| C0733<br>C0741<br>C0745<br>C0780<br>C0783                   | 115.5                               | 91.4                              | 223.0<br>124.9<br>133.5<br>183.2<br>98.1               | 193.2<br>42.0<br>94.8<br>181.7<br>91.4                 |
| C0804<br>C0805<br>C0811<br>C0813                            | 112.8 136.2                         |                                   | 78.0<br>160.6<br>23.8<br>146.3                         | 42.0<br>112.8<br>17.9<br>121.3                         |
| C0814<br>C0822  |                                     |                                   | 79.2   | 42.7   |

| BOREHOLE<br>NUMBER | MINOR WATER STRIKE<br>DEPTHS<br>(m) |            | REST WATER<br>LEVELS<br>(m) |   | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m) | MAIN<br>REST<br>WATER<br>LEVEL<br>(m) |
|--------------------|-------------------------------------|------------|-----------------------------|---|---|---------------------------------------|
| C0824              |                                     |            |                             |   | 138.0                                   | 137.0                                 |
| C0836              | ••                                  |            |                             |   | 162.5                                   | 69.0                                  |
| C0839              |                                     |            |                             |   | 42.1                                    | 25.3                                  |
| C0845              | ·                                   |            |                             | • | 133.5                                   | 126.0                                 |
| C0855              |                                     |            |                             | • | 184.1                                   | 183.0                                 |
| C0858<br>C0869     |                                     |            |                             |   | 143.0<br>133.0                          | 116.0<br>131.0                        |
| C0870              | ,                                   |            |                             | - | 90.0                                    | 78.0                                  |
| C0872              |                                     |            |                             |   | 78.0                                    | 48.0                                  |
| C0875              |                                     |            |                             |   | 103.0                                   | 73.0                                  |
| C0882              | .:                                  |            |                             |   | 162.0                                   | 160.0                                 |
| C0910              |                                     |            |                             |   | 18.3                                    | 12.8                                  |
| C0916              | 128.9                               |            |                             |   | 156.1                                   | 118.0                                 |
| C0921              |                                     |            |                             |   | 158.4                                   | .98.1                                 |
| C0939              |                                     |            |                             |   | 128.0                                   | 126.4                                 |
| C0946<br>C0947     | ·.                                  |            |                             |   | 242.6                                   | 237.7<br>24.4                         |
| C0947<br>C0953     |                                     |            |                             |   | 24.4<br>129.0                           | 24.4<br>94.5                          |
| C0955              | •                                   |            |                             |   | 129.0                                   | 3,4.3                                 |
| C0984              |                                     |            |                             |   | 57.3                                    | 39.6                                  |
| C0994              |                                     |            |                             |   | 45.7                                    | 42.7                                  |
| C1000              |                                     |            |                             |   | 125.9                                   | 125.0                                 |
| C1001              |                                     |            |                             |   |   |                                       |
| C1007              |                                     |            |                             |   | 45.0                                    | 23.0                                  |
| C1013<br>C1013     |                                     |            |                             |   | 179.8<br>179.8                          | 165.5                                 |
| C1013<br>C1019     | 165.9                               |            |                             |   | 215.1                                   | 165.5<br>163.5                        |
| C1013              | 103.9                               |            |                             |   | 60.0                                    | 21.0                                  |
| C1027              |                                     |            |                             |   | 82.3                                    | 79.2                                  |
| C1029              |                                     | • • *      |                             |   |   |                                       |
| C1033              | t                                   |            |                             |   | 61.3                                    | 34.3                                  |
| C1043              |                                     |            |                             |   | 135.0                                   | 135.0                                 |
| C1051              | •                                   |            |                             |   | 167.6                                   | 160.0                                 |
| C1062              | :                                   |            |                             |   | 12.2                                    | 11.3                                  |
| C1063<br>C1080     | 109.7                               | 107        |                             |   | 18.9<br>147.8                           | 10.5<br>107.0                         |
| C1080<br>C1082     | 65.5 85.3                           | 107        |                             |   | 147.8                                   | 60.0                                  |
| C1082              | 64.5 85.3                           | ٠          |                             |   | 105.0                                   | 60.0                                  |
| C1089              | 3.13                                |            |                             |   | 200.0                                   |                                       |
| C1112              |                                     |            |                             |   |   |                                       |
| C1125              |                                     |            |                             |   | 108.0                                   | 85.3                                  |
| C1126              |                                     |            |                             | , | 207.3                                   | 204.2                                 |
| C1148              |                                     |            |                             | - | 71.6                                    | 9.8                                   |
| C1161<br>C1250     |                                     |            |                             |   | 201.0<br>160.0                          | 195.0<br>149.0                        |
| C1250<br>C1259     |                                     |            |                             |   | 17.7                                    | 9.1                                   |
| C1265              | •                                   |            |                             |   | 41.1                                    | J. 1                                  |
| C1277              |                                     |            |                             |   | 112.5                                   | 68.6                                  |
| C1279              |                                     |            |                             |   | 139.3                                   | 121.9                                 |
| C1281              |                                     |            |                             |   | 29.6                                    | 23.8                                  |
| C1287              |                                     |            |                             |   | 54.9                                    | 50.6                                  |
| C1294              | 100 7                               |            |                             |   | 21.3                                    | 9.1                                   |
| C1325<br>C1356     | 109.7<br>18.3                       | 90<br>12.2 |                             |   | 187.4<br>29.9                           | 90.0<br>12.2                          |
| C1358              | 10.5                                | 16.6       |                             |   | 154.5                                   | 147.0                                 |
|                    |                                     | •          | •                           |   | 151.5                                   | 117.0                                 |

| BOREHOLE<br>NUMBER |            | WATER STRIKE<br>EPTHS<br>(m) |               | REST WATER<br>LEVELS<br>(m) | MAIN<br>WATER<br>STRIKE<br>- DEPTH<br>(m) | MAIN<br>REST<br>WATER<br>LEVEL<br>(m) |
|--------------------|------------|------------------------------|---------------|-----------------------------|---|---------------------------------------|
| C1361              | 4.5        |                              | ·             |                             | 216.9                                     | 186.0                                 |
| C1362<br>C1374     | 46<br>67.1 |                              | 61            |                             | 195.0<br>102.0                            | 175. <u>0</u><br>61.0                 |
| C1374              | 36.0       | 107.0                        | 01            |                             | 120.0                                     | 36.0                                  |
| C1383              | 55.0       | 82.0                         | 54.9          | 54.9                        | 97.5                                      | 54.9                                  |
| C1390              |            |                              |               |                             |   | 4                                     |
| C1391              |            |                              |               |                             | 137.0                                     | 111.0                                 |
| C1394              |            |                              |               |                             | 96.0                                      | 90.0                                  |
| C1402<br>C1404     |            |                              |               |                             | 228.0                                     | 57.6                                  |
| C1404<br>C1425     |            |                              |               |                             | 52.5<br>263.0                             | 57.6<br>261.0                         |
| C1434              |            |                              |               |                             | 37.0                                      | 36.6                                  |
| C1436              | •          |                              |               |                             | 45.1                                      | 45.1                                  |
| C1464              |            |                              | •             |                             | 11.3                                      | 7.6                                   |
| C1475              |            |                              |               |                             | 177.0                                     | 61.0                                  |
| C1482<br>C1483     |            |                              |               |                             | 35.1                                      | 11.3                                  |
| C1485              |            |                              |               |                             | 39.6<br>106.0                             | 31.0<br>10.7                          |
| C1487              |            |                              |               |                             | 97.0                                      | 91.4                                  |
| C1488              |            |                              |               |                             | 82.3                                      | 76.2                                  |
| C1491              |            |                              |               |                             | 107.0                                     | 85.0                                  |
| C1499              |            |                              |               |                             |   |                                       |
| C1503<br>C1504     |            |                              |               |                             | 265.0                                     | 261.0                                 |
| C1504<br>C1523     |            |                              |               |                             | 147.0                                     | 91.0                                  |
| C1524              |            |                              |               |                             |   |                                       |
| C1525              |            |                              |               |                             | -   | • .                                   |
| C1535              |            |                              |               |                             | 178.0                                     | 177.0                                 |
| C1545              |            |                              |               | •                           | 6.7                                       | 6.1                                   |
| C1558<br>C1559     |            |                              |               |                             | 129.5                                     | 125.0                                 |
| C1559              |            |                              |               |                             | 94.5<br>79.2                              | 83.8<br>17.7                          |
| C1585              |            |                              |               |                             | 93.0                                      | 8.7                                   |
| C1602              |            |                              |               |                             | 165.0                                     | 150.0                                 |
| C1614              |            |                              |               |                             | 134.1                                     | 118.3                                 |
| C1625              | 39.6       |                              | 39            |                             | 39.6                                      | 39.0                                  |
| C1641<br>C1652     | ų.         |                              |               |                             | 135.6                                     | 76.2                                  |
| C1662              |            |                              | ٠             |                             | 1.  |                                       |
| C1666              |            |                              |               | •                           | 175.3                                     | 62.7                                  |
| C1713              |            |                              |               |                             | 97.2                                      | 54.9                                  |
| C1726              |            |                              | •             |                             | 262.2                                     | 259.2                                 |
| C1749              | 68         |                              | 101           |                             | 134.0                                     | 85.3                                  |
| C1794<br>C1795     | 128        | •                            | 131           |                             | 173.4<br>135.6                            | 179.8                                 |
| C1795              |            |                              |               |                             | 135.6                                     | 131.7<br>131.7                        |
| C1798              |            |                              |               |                             | 174.0                                     | 132.0                                 |
| C1830              | 136.0      |                              | 128.3         |                             | 143.3                                     | 128.3                                 |
| C1843              |            |                              |               |                             |   |                                       |
| C1850              | 164.6      |                              | 150.0         |                             | 190.5                                     | 139.6                                 |
| C1851<br>C1877     | 161        | 186                          | 15 <i>6 A</i> | 164 6                       | 259.9                                     | 256.6                                 |
| C1877              | 101        | 100                          | 156.4         | 104.0                       | 194.2<br>236.2                            | 157.6<br>233.8                        |
| C1898              | •          |                              |               |                             | 62.6                                      | 60.7                                  |
| C1911              |            |                              |               |                             |   | , , , , , , , , , , , , , , , , , , , |

| BOREHOLE<br>NUMBER | MINOR WATER STRIKE<br>DEPTHS<br>(m) | MINOR REST WATER<br>LEVELS<br>(m) | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m) | MAIN<br>REST<br>WATER<br>LEVEL<br>(m) |
|--------------------|-------------------------------------|-----------------------------------|---|---------------------------------------|
| C1912              |                                     |                                   |   |                                       |
| C1913              |                                     |                                   | 75.0                                    | 39.0                                  |
| C1914              | 54.9                                | 22.9                              | 71.6                                    | 22.9                                  |
| C1924              |                                     |                                   | 141.0                                   | 123.0                                 |
| C1926<br>C1927     |                                     |                                   | 103.6<br>35.1                           | 90.5<br>18.3                          |
| C1927              | •                                   |                                   | 124.6                                   | 100.3                                 |
| C1925              | 122                                 |                                   | 195.0                                   | 115.2                                 |
| C1941              | 166                                 |                                   | 168.0                                   | 139.5                                 |
| C1947              | 22.0 41.0                           | 15.0 15.0                         | 51.0                                    | 15.0                                  |
| C1951              |                                     |                                   | 117.0                                   | 109.5                                 |
| C1952              | 119.4                               | 109.7                             | 137.7                                   | 111.9                                 |
| C1970              |                                     | ·                                 | 135.0                                   | 129.5                                 |
| C1990              |                                     |                                   | 81.0                                    | 61.8                                  |
| C1997              | 206                                 | 196                               | 208.0                                   | 199.8                                 |
| C2005<br>C2007     |                                     |                                   | 249.0<br>105.5                          | 241.5<br>98.5                         |
| C2007              | . 1                                 |                                   | 84.0                                    | 75.0                                  |
| C2033              |                                     |                                   | 04.0                                    | 73.0                                  |
| C2042              | • '                                 |                                   |   |                                       |
| C2058              | 39.6                                | 21.0                              | 44.2                                    | 15.2                                  |
| C2059              |                                     |                                   |   | 20.4                                  |
| C2061              | 25.9                                | 22.6                              | 115.8                                   | 21.3                                  |
| C2062              |                                     |                                   | 259.3                                   | 228.0                                 |
| C2063              | 107                                 | 99                                | 112.7                                   | 99.0                                  |
| C2069              | 47.0 55.0                           | 45.7 45.7                         | 76.2                                    | 45.7                                  |
| C2071<br>C2076     |                                     |                                   | 16.8                                    | 11.6<br>118.8                         |
| C2070              |                                     |                                   | i.                                      | 94.2                                  |
| C2097              | 135                                 | 118.8                             | 174.0                                   | 118.8                                 |
| C2108              |                                     | 11010                             | 168.8                                   | 166.4                                 |
| C2109              |                                     |                                   | 84.0                                    | 42.0                                  |
| C2110              | 105.9                               | 99.4                              | 125.4                                   | 99.3                                  |
| C2117              | •                                   |                                   | 22.0                                    | 12.2                                  |
| C2118              |                                     |                                   | 202.5                                   | 148.8                                 |
| C2128              | 01.4                                |                                   | 36.5                                    | 32.3                                  |
| C2129<br>C2138     | 91.4<br>50.2                        | 41.5                              | 191.4<br>42.6                           | 48.8<br>34.7                          |
| C2136<br>C2149     | 153.0                               | 140.2                             | 195.0                                   | 144.2                                 |
| C2149              | 132.6                               | 131.4                             | 148.5                                   | 131.4                                 |
| C2170              | 189.0                               | 131.1                             | 207.3                                   | 186.5                                 |
| C2170              |                                     |                                   |   |                                       |
| C2172              |                                     |                                   | 86.0                                    | 42.0                                  |
| C2176              | 28.0                                |                                   | 73.0                                    | 16.0                                  |
| C2197              | 14.0 180.0                          |                                   | 134.1                                   | 113.4                                 |
| C2234              | 87.3 140.8                          | 78.3 55.8                         | 148.7                                   | 77.4                                  |
| C2241              |                                     |                                   | 119.4                                   | 108.6                                 |
| C2246<br>C2263     |                                     |                                   | 17.1                                    | 13.7                                  |
| C2263              | 103 207                             | 149.4 149.4                       | 219.5                                   | 149.4                                 |
| C2269              | 67.0 107.0                          | 61.0 60.0                         | 132.6                                   | 60.0                                  |
| C2276              | 69 108                              | 61 42                             | 132.0                                   | 33.0                                  |
| C2288              |                                     |                                   |   | ,                                     |
| C2289              | 115 134                             |                                   | 96.0                                    | 87.0                                  |
| C2292              | 64                                  |                                   | 116.0                                   | 62.4                                  |

| BOREHOLE<br>NUMBER  | MINOR WATER STRIKE DEPTHS (m)                   | MINOR REST WATER<br>LEVELS<br>(m)      | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m)                      | MAIN<br>REST<br>WATER<br>LEVEL<br>(m)                        |
|---|---|--|--|--|
| C2294<br>C2296<br>C2300<br>C2304<br>C2322                                     | 44.5 91.4                                       | 16.2 16.2                              | 149.4<br>81.0<br>111.3<br>6.0<br>124.0                       | 16.2<br>30.0<br>100.6<br>6.0<br>112.2                        |
| C2332<br>C2338<br>C2347<br>C2358  | 191.0   | 191.0                                  | 115.5<br>228.6<br>171.6<br>289.6                             | 55.5<br>195.1<br>119.5<br>265.0                              |
| C2388<br>C2402<br>C2420<br>C2421<br>C2430<br>C2432                            | 145.1<br>79.2<br>55 101<br>39 85<br>10.6<br>141 | 140.2<br>74.7<br>27 29<br>24 21<br>6.0 | 242.6<br>91.4<br>117.7<br>193.0<br>31.0<br>164.0             | 241.7<br>67.1<br>68.3<br>188.0<br>6.0<br>116.0               |
| C2447<br>C2448<br>C2466<br>C2468<br>C2480<br>C2482                            | 56.4 75.0<br>192 243<br>40.0                    | 52.7 72.8<br>156.9 156.9<br>37.0       | 75.3<br>280.0<br>90.0<br>15.0<br>35.1                        | 202.0<br>156.9<br>55.0<br>132.0<br>39.6                      |
| C2493<br>C2496<br>C2497   | 105.0   | 95.1                                   | 138.7<br>155.0<br>112.8                                      | 93.9<br>144.5<br>104.9                                       |
| C2499<br>C2504<br>C2521<br>C2522  | 120.0<br>85                                     | 113.4<br>70.4                          | 173.7<br>158.0<br>98.1<br>50.9                               | 106.0<br>70.4<br>74.1<br>46.0                                |
| C2523<br>C2534<br>C2535<br>C2536<br>C2537<br>C2538<br>C2539<br>C2541<br>C2542 | 32.3  | 30.8                                   | 52.7<br>15.2<br>7.3<br>5.2<br>7.9<br>15.6                    | 30.5<br>17.1<br>6.7<br>4.3<br>3.0<br>9.8<br>4.6              |
| C2543<br>C2564<br>C2600<br>C2620  | 103 158   | 106 110                                | 192.0<br>183.0<br>67.1                                       | 109.0<br>186.0<br>67.1                                       |
| C2636<br>C2646<br>C2647<br>C2657<br>C2659<br>C2660<br>C2662<br>C2663<br>C2664 | 60.9<br>82.3                                    | 59.4                                   | 6.1<br>80.8<br>91.4<br>32.6<br>9.0<br>19.8<br>219.5<br>360.0 | 4.6<br>51.2<br>18.0<br>23.5<br>7.6<br>19.8<br>201.3<br>320.0 |
| C2667<br>C2670<br>C2680<br>C2697<br>C2701                                     | 75.0<br>8.5                                     | 30.0                                   | 189.1<br>181.4<br>79.2<br>156.0<br>25.4                      | 154.8<br>166.7<br>48.2<br>30.0<br>7.0                        |

| BOREHOLE<br>NUMBER | MINOR WATER STRIKE<br>DEPTHS<br>(m)   | MINOR REST WATER<br>LEVELS<br>(m) | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m) | MAIN<br>REST<br>WATER<br>LEVEL<br>(m) |
|--------------------|---------------------------------------|-----------------------------------|---|---------------------------------------|
|                    | · · · · · · · · · · · · · · · · · · · |                                   | ······································  |                                       |
| C2703              | •                                     |                                   | 3.4                                     | 3.4                                   |
| C2704              |                                       |                                   | 64.3                                    | 60.3                                  |
| C2705              |                                       |                                   | 18.9                                    | 16.8                                  |
| C2706              | •                                     |                                   | 39.0                                    | 38.7                                  |
| C2709              | · 198                                 | 196                               | 213.0                                   | <b>195.7</b>                          |
| C2717              | 159.7 245.0 256.0                     | 152.4 187.0 205.4                 | 323.0                                   | 239.3                                 |
| C2720              |                                       |                                   |   | 276.0                                 |
| C2745              | 109.7                                 | 92.4                              | 170.7                                   | 92.4                                  |
| C2753              |                                       |                                   | 123.0                                   | 123.0                                 |
| C2758              | 114.3                                 | 108.2                             | 128.0                                   | 102.1                                 |
| C2773              |                                       |                                   | 72.0                                    | 72.0                                  |
| C2813              | 45.7                                  | 41.5                              | 63.1                                    | 41.5                                  |
| C2823              |                                       |                                   | 275.3                                   | 260.4                                 |
| C2851              |                                       |                                   | 237.0                                   | 231.0                                 |
| C2863              |                                       | •                                 |   | -,                                    |
| C2866              | 92.9                                  | 89.0                              | 147.5                                   | 89.0                                  |
| C2870              |                                       |                                   | 15.2                                    |                                       |
| C2871              | •                                     |                                   |   | •                                     |
| C2883              | 57.9                                  | 48.8                              | 91.4                                    | 52:7                                  |
| C2885              |                                       |                                   |   |                                       |
| C2886              |                                       |                                   |   |                                       |
| C2887              | 9.1                                   |                                   |   |                                       |
| C2894              | 19.5 35.5 89.3                        | 10.1 9.8 10.7                     | 188.5                                   | 11.6                                  |
| C2899              |                                       |                                   | 20000                                   |                                       |
| C2900              | ,*                                    |                                   |   |                                       |
| C2901              |                                       |                                   |   |                                       |
| C2902              | 67.0                                  | 59.0                              | 98.0                                    | 59.4                                  |
| C2910              | 137.0                                 | 125.0                             | 223.0                                   | 176.8                                 |
| C2966              | 78                                    |                                   | 78.0                                    | 54.0                                  |
| C2970              | 33                                    | 25.6                              | 42.6                                    | 25.6                                  |
| C2997              |                                       |                                   | 287.7                                   | 280.4                                 |
| C3003              |                                       |                                   | 249.9                                   | 240.0                                 |
| C3005              | •                                     |                                   |   | 38.1                                  |
| C3024              |                                       |                                   | 93.0                                    | 91.8                                  |
| C3032              |                                       |                                   | 39.0                                    | 42.0                                  |
| C3047              | 56.0 58.0                             | 56.0 53.0                         | 67.0                                    | 59.4                                  |
| C3064              |                                       |                                   | 14.9                                    | 14.9                                  |
| C3066              | 10.6                                  | 2.1                               | 82.3                                    | 70.0                                  |
| C3067              |                                       |                                   | 75.0                                    | 60.0                                  |
| C3087              |                                       |                                   | 43.0                                    | 41.0                                  |
| C3136              | 45.0 137.0                            | 45.0 45.0                         | 165.0                                   | 45.0                                  |
| C3164              | 21.3                                  | 19.2                              | 42.7                                    | 18.9                                  |
| C316D              | 85                                    | 1311                              | 131.0                                   | 77.0                                  |
| C3216              |                                       | •                                 | 6.1                                     | 4.9                                   |
| C3217              |                                       |                                   | 6.1                                     | 4.8                                   |
| C3243              | 7-                                    |                                   | 176.0                                   | 67.6                                  |
| C3266              |                                       |                                   | 93.0                                    | 93.0                                  |
| C3280              |                                       |                                   | 93.3                                    | 82.3                                  |
| C3292              | 10.7                                  | 7.3                               | 30.5                                    | 7.6                                   |
| C3298              |                                       |                                   | 4.8                                     | 4.8                                   |
| C3299              |                                       |                                   | 3.0                                     | 2.1                                   |
| C3324              |                                       |                                   | 192.0                                   | 190.2                                 |
| C3327              |                                       |                                   | 81.0                                    | 67.5                                  |
| C3351              |                                       |                                   | 157.5                                   | 153.0                                 |
| C3352              | 57.6                                  | 51.8                              | 243.8                                   | 213.4                                 |
|                    | J                                     | 51.0                              | 273.0                                   | CIJ.7                                 |

| BOREHOLE<br>NUMBER |            | WATER S<br>DEPTHS<br>(m) | TRIKE |               | REST WATER<br>LEVELS<br>(m) | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m) | MAIN<br>REST<br>WATER<br>LEVEL<br>(m) |
|--------------------|------------|--------------------------|-------|---------------|-----------------------------|---|---------------------------------------|
| C3353              | 45.7       |                          |       | 36.6          |                             | 133.5                                   | 36.6                                  |
| C3358              | 124.0      | )                        |       |               |                             |   |                                       |
| C3363              |            |                          |       |               |                             | 87.0                                    | 79.0                                  |
| C3365              |            |                          |       |               |                             | 15.0                                    | 10.9                                  |
| C3366              |            |                          |       |               | *.                          | 13.7                                    | 9.9                                   |
| C3371<br>C3377     | . 07 0     |                          |       | 07.0          |                             | 152.0                                   | 100.6                                 |
| C3377              | 87.0       |                          |       | 97.0          | -                           | 131.0                                   | 93.0                                  |
| C3397              | 10 4       | 27 /                     |       | 0.0           |                             | 108.0                                   | 108.0                                 |
|                    | 10.4       | 27.4                     |       | 8.2           | 8.2                         | 46.0                                    | 8.2                                   |
| C3418              | 85.3       | 146.3                    |       | 85.3          | 138.1                       | 240.0                                   | 141.7                                 |
| C3422              | 27.0       | 120 0                    | 124 0 | 22.0          |                             | 113.0                                   | 57.0                                  |
| C3431<br>C3436     | 75.0       | 128.0                    | 134.0 |               |                             | 170.7                                   | 115.8                                 |
|                    | 10 0       |                          |       | .12 0         |                             | 42.7                                    | 42.7                                  |
| C3451<br>C3467     | 19.0       |                          |       | 13.0          |                             | 73.0                                    | 14.9                                  |
| C3467<br>C3490     | 93         | 134 -                    |       | 115 0         |                             | 100.0                                   | 107.0                                 |
| C3523              | 93<br>42.7 | 134                      |       | 115.8<br>25.3 | **                          | 189.0                                   | 107.0                                 |
| C3523              | 18.0       |                          |       | 13.0          |                             | 61.0                                    | 25.3                                  |
| C3524<br>C3525     | 10.0       |                          | •     |               |                             | 100.0                                   | 13.1                                  |
| C3551              |            |                          |       | į.            | •                           | 88.1                                    | 86.9                                  |
| C3562              |            |                          |       |               |                             | 6.0                                     | 4.6                                   |
| C3576              | 12.2       |                          |       |               |                             | 17 1                                    | 1 5                                   |
| C3615              | 12.2       |                          |       |               |                             | 17.1                                    | 4.5                                   |
| C3616              |            |                          |       |               | • • •                       | 79.0                                    | 72.0                                  |
| C3627              | 54.9       | 105.8                    | -     |               |                             | 24.4                                    | 21.6                                  |
| C3650              | 12.2       | 105.6                    |       | 6.7           |                             | 54.9                                    | 99.6                                  |
| C3674              | 12.2       |                          |       | 0.7           |                             | 118.9                                   | 8.2                                   |
| C3675              |            |                          |       |               | •                           | 6.0                                     | 5.8                                   |
| · C3677            | *¢         |                          |       | •             |                             | 9.1<br>18.3                             | 4.8<br>15.2                           |
| C3678              |            |                          |       |               |                             |   | 15.2                                  |
| C3693              | 80.0       | 111.0                    |       | 13.0          | 11.0                        | 21.3<br>116.0                           | 11.0                                  |
| C3694              | 43.0       | 76.0                     |       | 32.0          | 34.0                        | 116.0                                   | 33.0                                  |
| C3710              | 77.7       | 70.0                     |       | 58.0          | 34.0                        | 83.2                                    | 58.0                                  |
| C3713              | 40.0       |                          |       | 32.0          |                             | 03.2                                    | 0.00                                  |
| C3721              | 27.0       |                          |       | 23.0          |                             | 88.0                                    | 39.0                                  |
| C3739              | 52.0       |                          |       | 48.0          |                             | 67.0                                    | 48.0                                  |
| C3740              | 32.0       |                          |       | 40.0          |                             | 21.3                                    | 17.1                                  |
| C3763              | 49.0       |                          |       | 49.0          |                             | 61.0                                    | 26.0                                  |
| C3764              | 40.0       |                          |       | 27.7          | •                           | 85.0                                    | 23.5                                  |
| C3765              | 40.0       |                          |       | 35.7          |                             | 45.7                                    | 35.7                                  |
| C3767              | 27.4       | 36.6                     |       | 27.4          | 26.5                        | 67.0                                    | 26.5                                  |
| C3771              | 60.9       | 30.0                     |       | 36.5          | 20.5                        | 70.1                                    | . 39.0                                |
| C3779              | 18.0       | 90.0                     |       | 12.2          | 10.7                        | 128.0                                   | 10.7                                  |
| C3784              | 7.5        | 39.6                     |       | 3.6           | 6.1                         | 128.0                                   | 6.1                                   |
| C3799              | 41.0       | 33.0                     |       | 41.0          | 0.1                         | 64.0                                    | 41.0                                  |
| C3870              | 11.0       |                          |       | 71.0          |                             | 04.0                                    | 71.0                                  |
| C3874              | 58.5       |                          |       | 54.3          |                             | 66.5                                    | 54.2                                  |
| C3875              | 55.5       |                          |       | 51.5          |                             | 58.0                                    | 53.3                                  |
| C3897              | 30.0       |                          |       | 25.2          |                             | 90.0                                    | 35.0                                  |
| C3910              | 10.0       | 66.0                     |       | 17.0          | 18.0                        | 93.0                                    | 18.0                                  |
| C3919              | _0.0       | -3.3                     |       | _,,,          | -0.0                        | 39.2                                    | 27.1                                  |
| C3924              | •          |                          |       |               |                             | 10.7                                    | 7.5                                   |
| C3925              |            |                          |       |               |                             | 120.0                                   | 94.0                                  |
| C3929              |            |                          |       |               |                             | 16.8                                    | 15.9                                  |
| C3932              | 129        |                          |       |               |                             | 152.0                                   | 122.7                                 |
| _                  |            |                          |       |               |                             |   |                                       |

| BOREHOLE<br>NUMBER      | · D           | WATER<br>EPTHS<br>(m) | STRIKE | MINOR<br>I   | REST<br>LEVELS<br>(m) |      | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m) | MAIN<br>REST<br>WATER<br>LEVEL<br>(m) |
|-------------------------|---------------|-----------------------|--------|--------------|-----------------------|------|---|---------------------------------------|
| C3937<br>C3939<br>C3942 | 45.0          | 80.0                  | 128.0  | 4.0          | 2.4                   | 4.3  | 255.0<br>82.0<br>106.7                  | 3.0<br>81.5<br>100.0                  |
| C3951<br>C3955<br>C3965 | 2.6           |                       |        | 2.6          |                       |      | 36.6<br>118.0<br>64.0                   | 28.7<br>2.6<br>62.5                   |
| C3970<br>C3976          | ,<br>70.0     | <i>\</i>              |        | 60.7         |                       |      | 25.6<br>118.0                           | 17.1<br>56.4                          |
| C3975                   | 25.0          | 50.0                  |        | 78.0         | 13.4                  |      | 110.0                                   | 13.4                                  |
| C3999                   | 77.0          | 85.0                  |        | 49.0         | 47.0                  |      | 115.0                                   | 48.5                                  |
|                         | 3.0           | 45.0                  | 120.0  | 21.0         | 21.0                  | 26.0 | 91.0                                    | 3.0                                   |
| C4037<br>C4057          | 62.0          | 89.0                  | 128.0  | 31.0         | 31.0                  | 36.0 | 182.0<br>.6.0                           | 45.7                                  |
| C4061                   |               |                       |        |              |                       |      | 618.0                                   | 120.0                                 |
| C4062                   |               |                       |        |              |                       | •    | 786.0                                   | 564.0                                 |
| C4077                   | 84            | 91                    |        |              |                       |      | 152.0                                   | 84.0                                  |
| C4092<br>C4116          | 167           | 210                   |        | 166          | 160                   |      | 234.0                                   | 7.7<br>144.0                          |
| C4121                   | 151           |                       |        | 100          | 100                   |      | 170.0                                   | 93.0                                  |
| C4131                   |               |                       |        |              |                       |      |   |                                       |
| C4143<br>C4152          | 24            | 61                    |        | 11           | 11                    |      | 131.0                                   | 172.0<br>11.0                         |
| C4155                   | 65.0          | 117.0                 | 143.0  | 40.5         | 36.0                  | 34.0 | 174.0                                   | 27.0                                  |
| C4157                   | - •           |                       |        |              |                       |      | 18.0                                    | 10.7                                  |
| C4161                   | 21.0          | 31.0                  |        | 16.0         | 16.0                  |      | 45.0                                    | 16.0                                  |
| C4168<br>C4174          | 58.0          |                       |        | 47.0         |                       |      | 48.0<br>68.0                            | 16.9<br>57.0                          |
| C4177                   | 18.0          | 25.0                  |        | 16.0         | 16.0                  |      | 42.0                                    | - 16.1                                |
| C4178                   |               |                       |        |              |                       |      | 20.0                                    | 16.4                                  |
| C4179<br>C4185          |               |                       |        | •            |                       |      | 104.0                                   | 102.0                                 |
| C4185                   | 70.0          | 123.0                 |        |              |                       |      | 141.0                                   | 4.9                                   |
| C4200                   | 19.0          | 82.0                  | 108.0  | 14.0         | 14.0                  | 19.0 | 224.0                                   | 74.0                                  |
| C4201                   | 26.0          | 38.0                  | 64.0   | 12.0         | 12.0                  | 16.0 | 104.0                                   | 16.0                                  |
| C4206<br>C4208          | 130           | 157                   |        | 102          | 98                    |      | 240.0<br>6.0                            | 108.5<br>5.6                          |
| C4209                   |               |                       |        |              |                       |      | 5.0                                     | 4.3                                   |
| C4214                   | 12            | 110                   |        | 51           | 104                   |      | 146.0                                   | 103.0                                 |
| C4252                   | 108           |                       |        | 24.0         |                       |      | 153.0                                   | 122.0                                 |
| C4279<br>C4292          | 23.0<br>144.8 |                       |        | 24.0<br>24.0 |                       |      | - 140.0<br>176.7                        | 77.0<br>26.2                          |
| C4301                   |               |                       |        | 24.0         |                       |      | 54.8                                    | 32.7                                  |
| C4302                   |               |                       |        |              |                       |      | 17.6                                    | 10.0                                  |
| C4306                   | 180.0         |                       |        | 68.0         |                       |      | 200.0                                   | 53.4                                  |
| C4331<br>C4332          |               | •                     |        |              |                       |      | 107.0                                   | 62.0                                  |
| C4350                   | 18.0          |                       |        | 13.0         |                       |      | 128.0                                   | 13.0                                  |
| C4360                   | 22.0          |                       |        |              |                       |      | 100.0                                   | 21.8                                  |
| -C4369<br>C4370         | 48            |                       |        | 45           |                       |      | 93.0<br>98.0                            | 31.2<br>33.9                          |
| C4370<br>C4397          | 10.0          |                       |        | 45<br>7.0    |                       |      | 17.0                                    | 33.9<br>7.0                           |
| C4403                   | 26            |                       |        | 26           |                       |      | 106.0                                   | 43.0                                  |
| C4413                   | 43            |                       |        |              |                       |      | 131.0                                   | 68.5                                  |
| C4416<br>C4420          | 8             |                       |        | 7            |                       |      | 17.0                                    | 7.0                                   |
| CTTLU                   | J .           |                       |        | ,            |                       |      | 17.0                                    | 7.0                                   |

| BOREHOLE<br>NUMBER | MINOR WATER STRIKE DEPTHS (m) | MINOR REST WATER LEVELS (m) | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m) | MAIN<br>REST<br>WATER<br>LEVEL<br>(m) |
|--------------------|-------------------------------|-----------------------------|---|---------------------------------------|
| C4431              | 95.0                          | 61.0                        | 170.0                                   | 61.0                                  |
| C4461              |                               |                             | 124.0                                   | 12.8<br>82.3                          |
| C4484<br>C4491     | 90.0<br>44.8                  | 9                           | 54.0                                    | 8.0                                   |
| C4492              | 44.0                          | 3                           | 44.8                                    | 58.5                                  |
| C4493              |                               |                             | 67.0                                    | 12.2                                  |
| C4498              |                               |                             | 45.0                                    | 25.0                                  |
| C4499              |                               |                             | •                                       |                                       |
| C4500              | 26                            | 26 .                        | 42.0                                    | 15.2                                  |
| C4501              | 27                            | 27                          | 49.0                                    | 21.3                                  |
| C4502<br>C4504     | . 30                          | ,                           | 80.0<br>11.9                            | 50.7<br>11.9                          |
| C4504<br>C4510     | 52                            | •                           | 102.0                                   | 27.7                                  |
| C4511              | 42                            | 42.2                        | 94.0                                    | 27.0                                  |
| C4512              |                               |                             | 98.0                                    | 27.6                                  |
| C4517              | ·                             |                             | 180.0                                   | 97.0                                  |
| C4531              | 76.0                          | 70.0                        | 102.0                                   | 70.0                                  |
| C4554              | •                             |                             | 75.0                                    | 46.0                                  |
| C4555              | 36                            | 36                          | 80.0                                    | 28.4                                  |
| C4564<br>C4565     | 63                            | 53                          | 102.0                                   | 53.0                                  |
| C4505<br>C4575     | •                             |                             |   | 122.0                                 |
| C4591              | 23                            | 21.4                        | 35.4                                    | 21.4                                  |
| C4594              |                               |                             | 178.0                                   | 105.7                                 |
| C4597              | 142.0                         | 260.0                       | 230.0                                   | 114.6                                 |
| C4610              | _:                            |                             | 26.0                                    | 16.0                                  |
| C4615              | 71.0 81.0 92.0                | 22.0                        | 104.0                                   | .62.2                                 |
| C4624<br>C4634     | 40.0                          | 33.0                        | 210.0<br>85.0                           | 33.0<br>18.6                          |
| C4665              | 22.0                          | 17.8                        | 100.0                                   | 36.8                                  |
| C4669              | 14                            | 9.5                         | 118.0                                   | 20.6                                  |
| C4685              | <del>-</del> ·                |                             | 95.0                                    | 81.0                                  |
| C4687              | 18.0                          | 12.0                        | 76.0                                    | 15.0                                  |
| C4713              | 50.0                          | 44.0                        | 138.0                                   | 43.0                                  |
| C4743              | 12.0                          | 5.2                         | 25.0                                    | 6.2                                   |
| C4792              | 96.0                          | 89.0                        | 114.0                                   | 91.8                                  |
| C4804<br>C4807     | •                             |                             | 122.0<br>90.3                           | 63.8<br>170.0                         |
| C4807              |                               | •                           | 98.0                                    | 79.5                                  |
| C4829              |                               |                             | 30.0                                    | , , , ,                               |
| C4850              |                               | . •                         | 50.0                                    | . 5.0                                 |
| C4855              |                               |                             | 100.0                                   | 8.0                                   |
| C4863              | 12.0                          | 5.0                         | 65.0                                    | 15.0                                  |
| C4881              | 57.0                          | 48.6                        | 80.0                                    | 54.0                                  |
| C4893<br>C4897     |                               | •                           | 267.0                                   | 213.0                                 |
| C4897<br>C4907     | .9.0                          | 7.2                         | 14.0                                    | 7.4                                   |
| C4909              | 270.0                         | r • ba                      | 285.0                                   | 135.5                                 |
| C4924              | 132.0                         | 146.0                       | 152.0                                   | 146.0                                 |
| C4927              | 45.0                          |                             | 162.0                                   | 116.8                                 |
| C4966              | 24.0                          | 18.0                        | 216.0                                   | 73.0                                  |
| C4968              | 58.0                          | 32.0                        | 186.0                                   | 59.0                                  |
| C4971<br>C4974     |                               |                             |   | 219.0                                 |
| C4974<br>C4981     | 42.0                          | 34.6                        | 56.0                                    | 35.0                                  |
|                    | - <del></del>                 | - · · ·                     | 33.0                                    | 55.0                                  |

| BOREHOLE<br>NUMBER | DI       | WATER STRIKE<br>EPTHS<br>(m) | MINOR REST W<br>LEVELS<br>(m) | ATER | MAIN<br>WATER<br>STRIKE<br>DEPTH<br>(m) | MAIN<br>REST<br>WATER<br>LEVEL<br>(m) |
|--------------------|----------|------------------------------|-------------------------------|------|---|---------------------------------------|
| C4986              | <u> </u> |                              |                               |      | ·<br>5.5                                | 5.4                                   |
| C4989              |          |                              |                               |      | 2.0                                     | 1.4                                   |
| C4997              | 20       |                              | 15                            |      | 190.0                                   | 70.7                                  |
| C5002              | 20       |                              | 21 5                          |      | 111.0                                   | 106.0                                 |
| C5029              | 30       |                              | 21.5                          | .•   | 138.0                                   | 88.0                                  |
| C5111              |          |                              |                               |      | 18.9<br>21.0                            | 100.3<br>9.0                          |
| C5117<br>C5143     | 34.0     |                              | 27.0                          |      | 60.0                                    | 35.0                                  |
| C5143<br>C5161     | 34.0     |                              | 21.0                          |      | 43.0                                    | 24.8                                  |
| C5175              | 42       |                              | 30                            |      | 107.0                                   | 38.3                                  |
| C5206              | 34       |                              | 34.4                          |      | 158.0                                   | 34.7                                  |
| C5257              | 120.0    |                              |                               |      | 140.0                                   | 111.5                                 |
| C5343              | 102      |                              |                               |      | 126.0                                   | 97.4                                  |
| C5348              | 138.8    |                              | 125.6                         |      | 147.8                                   | 124.0                                 |
| C5375              |          |                              |                               |      | 88.0                                    | 76.0                                  |
| C5411              | 98.0     |                              | 78.0                          | •    | 110.0                                   | 83.0                                  |
| C5520              |          |                              |                               |      | 72.0                                    | 64.0                                  |
| C5564              |          |                              |                               |      | 148.0                                   | 16.0                                  |
| C5754              |          |                              |                               |      |   | 7.7                                   |
| C5798              |          |                              |                               |      | 68.0                                    | 38.0                                  |
| C6056              |          |                              |                               |      | 15.0                                    | 13.8                                  |
| C6095              |          |                              | •                             |      | 20.0                                    | 9.7<br>7.5                            |
| C6186<br>C6211     | 43.0     |                              | 42.0                          |      | 46.3                                    | 42.0                                  |
| C6211              | 130.0    |                              | 134.0                         |      | 145.0                                   | 130.0                                 |
| C6271              | 130.0    |                              | 137.0                         |      | 143.0                                   | 34.6                                  |
| C6290              |          |                              |                               |      | 194.0                                   | 197.0                                 |
| C6300              |          | •                            |                               |      | 166.0                                   | 132.9                                 |
| C630D              |          |                              |                               |      | 119.0                                   | 99.7                                  |
| C6377              |          |                              |                               |      | 52.0                                    | 48.3                                  |
| C6378              | 104.0    |                              | 99.0                          |      | 118.0                                   | 100.3                                 |
| C6494              |          |                              |                               |      | 77.0                                    | 6.0                                   |
| C6495              |          |                              |                               |      |   |                                       |
| C6524              |          |                              |                               | •    | 88.0                                    | 62.7                                  |
| C6613              | 130.0    |                              |                               |      | 150.0                                   | 90.0                                  |
| KJ1                |          |                              |                               |      |   | 155.0                                 |
| M0001              |          |                              |                               |      | 34.0                                    | 155.0<br>16.5                         |
| P0002<br>P0012     | 29.3     |                              | ·                             |      | 69.5                                    | 24.4                                  |
| P0012<br>P0016     | 96.9     |                              |                               |      | 147.5                                   | 94.5                                  |
| P0010              | 30.3     |                              |                               |      | 74.6                                    | 70.0                                  |
| P0023              |          |                              |                               |      | 71.0                                    | , , , ,                               |
| P0036              |          |                              |                               |      |   |                                       |
| P0037              |          |                              |                               | ,    |   |                                       |
| P0053              |          |                              |                               |      | 221.6                                   | 213.4                                 |
| P0065              | 22       | 30                           |                               |      | 90.0                                    | 61.0                                  |
| P0071              |          |                              |                               |      |   |                                       |
| P0089              |          |                              |                               |      |   |                                       |
| SA58               |          |                              |                               |      | 47.9                                    | 47.2                                  |
|                    |          |                              |                               |      |   |                                       |

#### APPENDIX 4 - BOREHOLE PRODUCTIVITY

|                    |                | F                     | RODUCTION                       | N TEST                          |       | • |
|--------------------|----------------|-----------------------|---------------------------------|---------------------------------|-------|---|
| BOREHOLE<br>NUMBER | YIELD<br>(1/s) | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES |   |
| 0001C              |                |                       |                                 |                                 |       |   |
| C0054              | 3.4            |                       |                                 |                                 |       |   |
| C0057              | 0.0            | 0.0                   |                                 | 0.00                            | DRY   |   |
| C0059              | 0.4            |                       |                                 |                                 | *     |   |
| C0079              | 1.9            |                       |                                 |                                 |       |   |
| C0092              | 0.0            | 0.0                   |                                 | 0.00                            | DRY   |   |
| C0107              | 0.0            | 0.0                   |                                 | 0.00                            | DRY   |   |
| C0108              | 0.6            |                       |                                 |                                 |       |   |
| C0115              | 0.0            | 0.0                   |                                 | 0.00                            | DRY [ |   |
| C0131              | 0.2            |                       |                                 |                                 |       |   |
| C0132              | 2.5            |                       |                                 |                                 |       | • |
| C0152              | 5.2            |                       |                                 |                                 |       |   |
| C0164              | 1.2            |                       |                                 |                                 |       |   |
| C0165              | 0.0            | 0.0                   |                                 | 0.00                            | DRY   |   |
| C0202              | 0.2            |                       |                                 |                                 |       |   |
| C0204              | 4.6            |                       |                                 |                                 |       |   |
| C0205              | 0.2            |                       |                                 |                                 |       |   |
| C0208              | 0.0            | 0.0                   |                                 | 0.00                            | DRY   |   |
| C0210              | 4.5            |                       |                                 |                                 |       |   |
| C0211              | 0.5            |                       |                                 |                                 |       |   |
| C0214              | 0.8            |                       |                                 |                                 |       |   |
| C0220              | 0.1            |                       |                                 |                                 |       | • |
| C0223              | 0.1            |                       |                                 | ÷                               |       |   |
| C0227              | 0.6            |                       |                                 |                                 |       | • |
| C0231              | 58.3           |                       |                                 |                                 |       |   |
| C0258              | 2.9            |                       |                                 |                                 |       |   |
| C0261              | 1.8            |                       |                                 |                                 |       |   |
| C0264              | 0.1            |                       |                                 |                                 |       |   |
| C0266              | 1.7            |                       |                                 |                                 |       |   |
| C0288              | 2.1            |                       |                                 |                                 |       |   |
| C0295              | 0.4            |                       |                                 |                                 |       |   |
| C0306              | 3.8            |                       |                                 |                                 |       |   |
| C0307              | 2.9            |                       |                                 |                                 |       |   |
| C0321              | 3.8            |                       |                                 |                                 |       |   |
| C0325              | 1.6            |                       |                                 |                                 |       | • |
| 00070              |                |                       |                                 |                                 |       |   |

WELL OVERFLOWED

C0376

C0379

C0381

C0407

C0408

C0416

C0417

C0419

C0423

C0429

C0431

C0440

C0451

C0456

C0457

C0458

3.3

3.4

0.6

0.3

1.6

4.3

1.5

1.3

2.1

2.1

1.3

2.7

2.1

0.5

2.1

0.5

| BOREHOLE<br>NUMBER   | YIELD<br>(1/s)                                       | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC CAPACITY (1/s/m) | NOTES                                      | · |
|--|--|-----------------------|---------------------------------|---------------------------|--|---|
| C0463<br>C0465<br>C0466<br>C0467<br>C0468<br>C0485                   | 5.1<br>1.5<br>2.2<br>2.5<br>2.4<br>3.8               |                       |                                 |                           |  |   |
| C0510<br>C0511<br>C0531<br>C0533<br>C0553                            | 0.0<br>0.0<br>5.1<br>1.3<br>0.8                      | 0.0                   |                                 | 0.00                      | DRY<br>DRY                                 |   |
| C0562<br>C0563<br>C0567<br>C0570                                     | 2.5<br>1.8<br>1.7<br>1.8                             |                       |                                 |                           |  |   |
| C0572<br>C0579<br>C0580<br>C0581<br>C0582                            | 0.9<br>1.9<br>1.9<br>1.9<br>2.3                      |                       |                                 |                           |  |   |
| C0605<br>C0624<br>C0628<br>C0631                                     | 2.5<br>2.3<br>2.3<br>2.3                             |                       |                                 |                           |  |   |
| C0633<br>C0634<br>C0648<br>C0651<br>C0655<br>C0665                   | 1.9<br>0.0<br>0.0<br>1.5<br>0.1<br>2.3               | 0.0                   | . • •                           | 0.00<br>0.00              | DRY<br>DRY                                 | • |
| C0670<br>C0677   | 4.0<br>0.0   | 0.0                   |                                 | 0.00                      | DRY  |   |
| C0678<br>C0691<br>C0692<br>C0699<br>C0703                            | 1.3<br>0.0<br>0.8<br>0.6<br>3.8                      | 0.0                   |                                 | 0.00                      | DRY  |   |
| C0703<br>C0704<br>C0705<br>C0706<br>C0707                            | 0.1<br>0.0<br>0.0                                    | 0.0                   |                                 | 0.00<br>0.00              | STEAM STRUCK<br>DRY<br>DRY<br>STEAM STRUCK | · |
| C0719<br>C0729<br>C0732<br>C0733<br>C0741<br>C0745<br>C0780<br>C0783 | 1.8<br>1.1<br>2.6<br>1.0<br>3.8<br>0.5<br>1.1<br>2.5 |                       |                                 |                           |  |   |
| C0804<br>C0805<br>C0811<br>C0813                                     | 2.1<br>2.3<br>1.2<br>2.6                             |                       |                                 |                           | HOT WATER                                  |   |

| BOREHOLE<br>NUMBER | YIELD<br>(1/s) | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES           |
|--------------------|----------------|-----------------------|---------------------------------|---------------------------------|-----------------|
| C0814              | 2.1            | 0.0                   | •                               | 0.00                            |                 |
| C0822<br>C0824     | 0.0<br>0.1     | 0.0                   |                                 | 0.00                            | DRY             |
| C0836              | 1.6            |                       |                                 |                                 | •               |
| C0839              | 2.5            |                       |                                 | •                               | •               |
| C0845<br>C0855     | 1.5<br>1.3     |                       |                                 |                                 | WATER TEMP 59C  |
| C0858              | 3.2            |                       |                                 |                                 | WATER TENE 350  |
| C0869              | 1.1            |                       |                                 |                                 |                 |
| C0870              | 0.5            | 0.5                   | 109.00                          | 0.02                            | •               |
| C0872<br>C0875     | 1.0<br>0.1     |                       |                                 |                                 |                 |
| C0875              | 1.5            |                       |                                 |                                 |                 |
| C0910              | 1.6            |                       |                                 |                                 | · ·             |
| C0916              | 1.0            |                       |                                 |                                 |                 |
| C0921<br>C0939     | 0.4<br>1.5     |                       |                                 |                                 | •               |
| C0939              | 0.3            |                       |                                 |                                 |                 |
| C0947              | 1.3            |                       |                                 |                                 | Y               |
| C0953              | 2.0            | 0.0                   |                                 | 0.00                            | nnv             |
| C0965<br>C0984     | 0.0<br>2.3     | 0.0                   | •.                              | 0.00                            | DRY             |
| C0994              | 1.8            |                       |                                 |                                 |                 |
| C1000              | 1.1            |                       | •                               |                                 |                 |
| C1001              | 0.0            | 0.0                   |                                 | 0.00                            | DRY             |
| C1007<br>C1013     | 6.3<br>0.7     |                       |                                 |                                 |                 |
| C1013              | 0.7            |                       |                                 | •                               | ·               |
| C1019              | 1.0            | • •                   |                                 |                                 | WARM WATER.50C. |
| C1021              | 3.9<br>2.3     |                       |                                 |                                 | •               |
| C1027<br>C1029     | 0.0            | 0.0                   |                                 | 0.00                            | DRY             |
| C1033              | 3,4            | 0.0                   |                                 | 0.00                            |                 |
| C1043              | 0.2            |                       |                                 |                                 | •               |
| C1051              | 0.8<br>3.4     |                       |                                 |                                 |                 |
| C1062<br>C1063     | 3.4            |                       |                                 |                                 | •               |
| C1080              | 2.3            |                       |                                 |                                 |                 |
| C1082              | 4.2            |                       |                                 |                                 |                 |
| C1082              | 4.2<br>0.0     | 0.0                   |                                 | 0.00                            | DRY             |
| C1089<br>C1112     | 0.0            | 0.0                   |                                 | 0.00                            | DRY             |
| C1125              | 3.5            |                       |                                 |                                 |                 |
| C1126              | 0.3            |                       |                                 |                                 | •               |
| C1148<br>C1161     | 1.5<br>0.8     |                       |                                 |                                 |                 |
| C1250              | 1.8            |                       |                                 |                                 |                 |
| C1259              | 5.1            |                       |                                 |                                 | •               |
| C1265              | 0.0            | 0.0                   | •                               | 0.00                            | DRY             |
| C1277<br>C1279     | 2.9<br>1.9     |                       |                                 |                                 |                 |
| C1281              | 2.1            |                       |                                 |                                 |                 |
| C1287              | 2.9            |                       |                                 |                                 |                 |
| C1294              | 0.4            |                       |                                 |                                 |                 |

| BOREHOLE<br>NUMBER | YIELD<br>(1/s) | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES                                 |       |
|--------------------|----------------|-----------------------|---------------------------------|---------------------------------|---------------------------------------|-------|
| C1325<br>C1356     | 1.3            |                       | -                               |                                 |                                       |       |
| C1358              |                |                       |                                 |                                 |                                       |       |
| C1361              | 0.8            | 8.0                   | 235.00                          | 0.02                            |                                       | • •   |
| C1362<br>C1374     | 1.3            |                       |                                 |                                 |                                       | •     |
| C1379              |                |                       |                                 |                                 |                                       | ÷     |
| C1383              | 1.5            | 0 0                   |                                 | 0.0                             | DDV                                   |       |
| C1390<br>C1391     | 0.0<br>2.9     | 0.0                   |                                 | 0.0                             | DRY                                   | . •   |
| C1394              | 1.9            |                       |                                 |                                 |                                       | •     |
| C1402              | 2.0            | 2.6                   | 00.00                           | 0.00                            | STEAM STRUCK                          | •     |
| C1404<br>C1425     | 3.8<br>0.3     | 3.6                   | 96.00                           | 0.09                            |                                       |       |
| C1434              | 1.7            |                       |                                 |                                 | •                                     |       |
| C1436              | 3.8            |                       |                                 |                                 |                                       | •     |
| C1464<br>C1475     | 3.5<br>0.6     | •                     |                                 |                                 |                                       |       |
| C1482              | 0.6            |                       |                                 |                                 | ÷ .                                   |       |
| C1483              | 0.5            |                       |                                 |                                 |                                       |       |
| C1486<br>C1487 ·   | 0.5<br>8.2     | 0.5                   | 91.40                           | 0.01                            |                                       | •     |
| C1488              | 15.1           |                       |                                 |                                 |                                       |       |
| C1491              | 2.9            |                       |                                 |                                 |                                       |       |
| C1499<br>C1503     | 0.0<br>0.6     | 0.0                   | :                               | 0.00                            | DRY<br>WATER HOT                      |       |
| C1503              | 0.0            |                       | •                               |                                 | WATEK HOT                             |       |
| C1523              | 0.0            | 0.0                   |                                 | 0.00                            | DRY                                   |       |
| C1524<br>C1525     | 0.0            | 0.0                   | •                               | 0.00                            | STEAM STRUCK                          | 158M  |
| C1525              | 1.4            | 0.0                   |                                 | 0.00                            | DRY                                   |       |
| C1545              | 1.6            |                       |                                 | <b>'</b> .                      |                                       |       |
| C1558<br>C1559     | 2.6<br>3.6     |                       |                                 |                                 | * * * * * * * * * * * * * * * * * * * |       |
| C1559<br>C1584     | 3.6            |                       |                                 |                                 |                                       |       |
| C1585              | 2.9            |                       |                                 |                                 |                                       | •     |
| C1602              | 0.4            |                       |                                 |                                 |                                       |       |
| C1614<br>C1625     | 0.2<br>0.2     |                       |                                 |                                 |                                       |       |
| C1641              | 1.7            |                       |                                 |                                 |                                       |       |
| C1652              | 2.5            |                       |                                 |                                 | NO 144750 4 545                       |       |
| C1662<br>C1666     | 0.1<br>4.4     |                       |                                 |                                 | NO WATER LEVE                         | LUATA |
| C1713              | 0.2            |                       |                                 |                                 | ·                                     |       |
| C1726              | 1.1            |                       |                                 |                                 | RWL IS SUSPEC                         | T.    |
| C1749<br>C1794     | 1.5<br>0.3     | 0.1                   | 208.70                          | 0.01                            |                                       |       |
| C1795              | 2.2            | 2.2                   | 146.30                          | 0.15                            |                                       |       |
| C1795              | 2.2            | 2.2                   | 146.30                          | 0.15                            |                                       |       |
| C1798<br>C1830     | 2.5<br>0.8     | 2.2<br>0.8            | 138.10<br>132.60                | 0.36<br>0.19                    |                                       |       |
| C1843              | 0.0            | 0.0                   | 132.00                          | 0.00                            | DRY                                   |       |
| C1850              | 1.5            | 1.5                   | 182.90                          | 0.04                            |                                       |       |
| C1851              | 0.1            |                       |                                 |                                 |                                       | ·     |

| BOREHOLE<br>NUMBER | YIELD<br>(1/s) | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES                 |          |
|--------------------|----------------|-----------------------|---------------------------------|---------------------------------|-----------------------|----------|
| C1877              | 1.9            | 1.9                   | 157.60                          | >9.50                           |                       |          |
| C1892              | 1.1            | 0.9                   | 237.70                          | 0.23                            |                       | •*       |
| C1898              | 1.0            | 0 0                   |                                 |                                 | :DDV                  |          |
| C1911<br>C1912     | 0.0<br>0.0     | 0.0<br>0.0            |                                 | 0.00<br>0.00                    | DRY<br>DRY            | •        |
| C1913              | 0.2            | 0.2                   | 100.00                          | <0.01                           | UKT                   | •        |
| C1914              | 2.0            | 0.2                   | 100.00                          | (0.01                           | •                     |          |
| C1924              | 0.6            | 0.6                   | 143.00                          | 0.03                            |                       |          |
| C1926              | 1.9            | 1.4                   | 111.20                          | 0.07                            |                       | •        |
| C1927              | 1.3            |                       |                                 |                                 | ٠                     | •        |
| C1929              | 0.8            | 0.8                   | 118.60                          | 0.04                            | •                     | •        |
| C1935<br>C1941     | 1.9<br>1.5     | 1.7<br>1.5            | 126.50<br>160.00                | 0.15<br>0.07                    |                       | •        |
| C1947              | 12.6           | 12.6                  | 22.30                           | 1.73                            | *                     | •        |
| C1951              | 0.5            | 0.5                   | 138.00                          | 0.02                            | •                     |          |
| C1952              | 1.9            | 1.9                   | 131.00                          | 0.10                            | •                     | · ·      |
| C1970              | 0.3            | 0.3                   | 150.30                          | 0.01                            |                       | -        |
| C1990              | 2.1            |                       |                                 |                                 |                       |          |
| C1997              | 0.9            | 0.9                   | 216.60                          | 0.05                            | *                     |          |
| C2005<br>C2007     | 0.2<br>2.3     | 0.2                   | 250.60                          | 0.02                            |                       | -        |
| C2033              | 1.9            | 1.9                   | 82.00                           | 0.27                            |                       | •        |
| C2039              | 0.0            | 0.0                   | 02.00                           | 0.00                            | DRY                   | ~ ;      |
| C2042              | 0.0            | 0.0                   |                                 | 0.00                            | DRY                   |          |
| C2058              | 1.8            | 1.5                   | 30.80                           | 0.10                            |                       |          |
| C2059              | 0.9            | 0.0                   | 07.70                           |                                 | ,                     | ·<br>·   |
| C2061<br>C2062     | 3.3<br>0.6     | 2.3                   | 27.70<br>245.70                 | 0.36                            |                       |          |
| C2062              | 1.5            | 0.6<br>1.5            | 150.00                          | 0.03<br>0.03                    |                       | •        |
| C2069              | 1.1            | 0.4                   | 63.40                           | 0.02                            |                       | ·        |
| C2071              | 1.1            | 1.1                   | 11.60                           | >5.50                           |                       |          |
| C2076              | 1.9            | 1.9                   | 147.00                          | 0.07                            | <sup>~</sup> 150F @ 1 | 82.9M    |
| C2077              | 1.8            |                       | 150.00                          |                                 |                       | •        |
| C2097<br>C2108     | 0.5            | 0.5                   | 152.00                          | 0.02                            |                       |          |
| C2108<br>C2109     | 1.6<br>3.3     | 1.6<br>3.3            | 179.80<br>44.00                 | 0.12<br>1.65                    |                       |          |
| C2110              | 3.8            | 3.3                   | 44.00                           | 1.05                            |                       |          |
| C2117              | 2.3            |                       |                                 | -                               | *                     | · -      |
| C2118              | 8.0            | 0.8                   | 176.00                          | 0.03                            |                       |          |
| C2128              | 4.6            |                       |                                 |                                 |                       |          |
| C2129              | 1.6            | 0.1                   | 40.60                           | 40.04                           |                       |          |
| C2138<br>C2149     | 0.1<br>0.3     | 0.1                   | 42.60                           | <0.01                           | WATER TEM             | P. 47.26 |
| C2149<br>C2160     | 1.2            | 1.2                   | 147.00                          | ,0.08                           |                       | •        |
| C2170              | 0.9            | 0.9                   | 210.30                          | 0.04                            |                       | •        |
| C2170              | 0.0            | 0.0                   |                                 | 0.00                            | DRY                   | •        |
| C2172              | 1.7            | 1.7                   | 45.70                           | 0.46                            | WATER TEM             | P. 43C   |
| C2176              | 2.7            | 2.7                   | 54.40                           | 0.07                            | -                     |          |
| C2197              | 1.5            | 1.5                   | 174.90                          | 0.02                            |                       |          |
| C2234<br>C2241     | 2.4<br>2.5     | 2.4                   | 111.00                          | 0.07                            |                       |          |
| C2241<br>C2246     | 1.4            | 1.4                   | 28.00                           | 0.10                            |                       |          |
| C2263              | 0.0            | 0.0                   | 20.00                           | 0.00                            | DRY                   |          |
| C2264              | 1.4            | 1.1                   | 176.80                          | 0.04                            |                       |          |
|                    |                |                       |                                 |                                 |                       |          |

| BOREHOLE<br>NUMBER                        | YIELD<br>(1/s)           | PUMP<br>RATE<br>(1/s)    | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES     |   |
|---|--------------------------|--------------------------|---------------------------------|---------------------------------|-----------|---|
| C2269<br>C2276<br>C2288<br>C2289<br>C2292 | 2.8<br>2.5<br>0.0<br>2.0 | 2.8<br>2.0<br>0.0<br>2.0 | 110.60<br>73.20<br>99.20        | 0.06<br>0.05<br>0.00<br>0.16    | DRY       | :<br>                                   |
| C2294<br>C2296<br>C2300                   | 3.9<br>3.1<br>2.7        | 3.9                      | 102.10<br>92.00                 | 0.05<br>0.05                    | •         |   |
| C2304<br>C2322                            | 13.9<br>2.0              | 13.9                     | 6.60                            | 23.20                           |           | •                                       |
| C2332                                     | 2.0                      | 2.0                      | 91.00                           | 0.06                            |           |   |
| C2338                                     | 1.9                      | 1.9                      | 201.20                          | 0.31                            | •         |   |
| C2347                                     | 1.1                      | 1.1                      | 129.50                          | 0.11                            |           | 2 -                                     |
| C2358                                     | 0.4                      | , ,                      | 040 00                          | 1 15                            | ,         |   |
| C2388                                     | 1.5                      | 1.5<br>3.8               | 243.00<br>67.10                 | 1.15                            |           |   |
| C2402<br>C2420                            | 3.8<br>5.4               | 3.8                      | 67.10                           | >19.00                          |           |   |
| C2421                                     | 5.4                      |                          |                                 |                                 | WATER LOS | S 193M. CO <sub>2</sub>                 |
| C2430                                     | 6.3                      | 6.3                      | 6.00                            | >31.50                          | MATER 200 | 3 130(1. 002                            |
| C2432                                     | 1.5                      |                          |                                 |                                 |           | ٠                                       |
| C2447                                     | 1.9                      |                          |                                 |                                 |           |   |
| C2448                                     | 2.0                      | 2.0                      | 185.00                          | 0.07                            |           |   |
| C2466                                     | 3.2                      | 3.2                      | 64.10                           | 0.35                            | -         |   |
| C2468                                     | 0.1                      |                          |                                 |                                 | -         | • |
| C2480<br>C2482                            | 1.9<br>0.0               | 0.0                      | •                               | 0.00                            | DRY       |   |
| C2493                                     | 0.3                      | 2.5                      | 100.00                          | 0.41                            | DICT      | 4                                       |
| C2496                                     | 1.3                      | 1.3                      | 152.40                          | 0.17                            |           | ž vieto                                 |
| C2497                                     | 1.9                      | 1.9                      | 104.90                          | 9.50                            | •         |   |
| C2499                                     | 1.4                      |                          |                                 | •                               |           |   |
| C2504                                     | 1.2                      | 1.2                      | 128.00                          | 0.02                            |           |   |
| C2521                                     | 2 6                      | 2 5                      | 46.00                           | N16 E0                          |           |   |
| C2522<br>C2523                            | 3.5<br>2.5               | 3.5                      | 46.00                           | >16.50                          |           |   |
| C2534                                     | 3.7                      | 3.7                      | 17.10                           | >18.50                          |           |   |
| C2535                                     | 3.8                      |                          |                                 | • •                             |           |   |
| C2536                                     | 3.2                      | 3.2                      | 4.30                            | >16.00                          |           |   |
| C2537                                     | 3.8                      | 3.8                      | 3.00                            | >19.00                          |           |   |
| C2538                                     | 3.8                      | 3.8                      | 9.80                            | >19.00                          |           |   |
| C2539<br>C2541                            | 2.5<br>0.0               | 2.5<br>0.0               | 7.50                            | 0.86<br>0.00                    | DRY       |   |
| C2542                                     | 0.0                      | 0.0                      |                                 | 0.00                            | DRY       |   |
| C2543                                     | 0.0                      | 0.0                      |                                 | 0.00                            | DRÝ       |   |
| C2564                                     | 2.3                      | 2.0                      | 137.00                          | 0.07                            |           |   |
| C2600                                     | 1.8                      | 1.8                      | 186.00                          | >9.00                           |           | ,                                       |
| C2620                                     | 3.3                      | 3.3                      | 146.30                          | 0.04                            |           | •                                       |
| C2636                                     | 8.1                      | 6.7                      | 6.10                            | 4.50                            |           |   |
| C2646                                     | 0.4                      | 0.4                      | 86.60                           | 0.01                            |           |   |
| C2647<br>C2657                            | 1.2<br>3.8               | 3.8                      | 25.30                           | 2.10                            |           |   |
| C2659                                     | 7.8                      | 7.8                      | 10.70                           | 2.52                            | •         |   |
| C2660                                     | 8.1                      | 8.1                      | 19.80                           | 40.50                           |           |   |
| C2662                                     | 1.5                      | 0.4                      | 210.40                          | 0.04                            |           |   |
| C2663                                     | 3.2                      | 3.2                      | 341.30                          | 0.15                            |           |   |

| BOREHOLE<br>NUMBER | YIELD<br>(1/s)    | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES                               |
|--------------------|-------------------|-----------------------|---------------------------------|---------------------------------|-------------------------------------|
| C2664<br>C2667     | 0.0<br>1.5<br>0.8 | 0.0                   |                                 | 0.00                            | DRY                                 |
| C2670<br>C2680     | <0.8              |                       |                                 |                                 | •                                   |
| C2697              | 3.1               |                       |                                 |                                 |                                     |
| C2701<br>C2703     | 3.8<br>7.5        | 8.8<br>7.5            | 11.60<br>3.40                   | 1.91<br>>37.50                  |                                     |
| C2704              | 2.5               | 7.5                   | 3.40                            | /37.30                          |                                     |
| C2705              | 2.8               | 2.8                   | 16.80                           | >14.00                          |                                     |
| C2706<br>C2709     | 7.6<br>1.6        | 7.6<br>1.4            | 39.00<br>202.70                 | 25.30<br>0.20                   |                                     |
| C2717              | 1.0               | 1.0                   | 281.00                          | 0.02                            |                                     |
| C2720              | 0.6               |                       |                                 |                                 |                                     |
| C2745<br>C2753     | 2.7<br>0.1        | 2.7                   | 121.90                          | 0.09                            | •                                   |
| C2758              | 3.8               |                       |                                 |                                 |                                     |
| C2773              | 0.1               | 0.06                  |                                 | <0.01                           | •                                   |
| C2813<br>C2823     | 3.8               | 3.8                   | 41.50                           | >19.00                          |                                     |
| C2851              | 0.9               | 0.9                   | 243.20                          | 0.07                            |                                     |
| C2863              |                   |                       |                                 |                                 | •                                   |
| C2866<br>C2870     | 1.3               | 1.3                   | 108.20                          | 0.07                            | STEAM STRUCK                        |
| C2871              | 0.0               | 0.0                   |                                 | 0.00                            | DRY                                 |
| C2883              | 2.0               | 2.0                   | 100.50                          | 0.04                            | ,                                   |
| C2885<br>C2886     |                   |                       |                                 |                                 | X1 STEAM BOREHOLE X2 STEAM BOREHOLE |
| C2887              |                   |                       |                                 |                                 | AZ SILAM BUKENUEL                   |
| C2894              | 1.2               |                       |                                 |                                 |                                     |
| C2899<br>C2900     |                   |                       | •                               |                                 | STEAM STRUCK<br>STEAM STRUCK        |
| C2901              |                   |                       |                                 | •                               | STEAM STRUCK                        |
| C2902              | 1.5               | 1.5                   | 97.50                           | 0.04                            |                                     |
| C2910<br>C2966     | 1.2<br>0.6        | 1.3                   | 219.50                          | 0.03                            |                                     |
| C2970              | 1.1               | 1.1                   | 46.30                           | 0.05                            |                                     |
| C2997              | 2.2               | 2.2                   | 282.90                          | 0.88                            | •                                   |
| C3003<br>C3005     | 0.2<br>5.0        | 5.0                   | 47.50                           | 0.53                            |                                     |
| C3024              | 0.8               | 0.8                   | 99.10                           | 0.11                            |                                     |
| C3032<br>C3047     | 0.3               | 10.0                  | EO 40                           | <b>&gt;05</b> 00                |                                     |
| C3047<br>C3064     | 19.0              | 19.0                  | 59.40                           | >95.00                          | •                                   |
| C3066              | 1.3               |                       |                                 |                                 |                                     |
| C3067<br>C3087     | 1.3<br>1.3        |                       |                                 |                                 |                                     |
| C3087              | 3.1               | 1.3                   | 127.00                          | 0.02                            |                                     |
| C3164              | 1.5               | 1.5                   | 21.60                           | 0.56                            |                                     |
| C316D<br>C3216     | 3.2<br>1.2        |                       |                                 |                                 |                                     |
| C3210              | 3.0               |                       |                                 |                                 |                                     |
| C3243              | 3.0               | 3.0                   | 67.60                           | >15.00                          |                                     |
| C3266<br>C3280     | 3.2<br>0.1        | 0.1                   | 133.40                          | <0.01                           |                                     |
| 03200              | 0.1               | 0.1                   | 133.40                          | \ <b>0.</b> 01                  |                                     |

| BOREHOLE<br>NUMBER                                 | YIELD<br>(1/s)                         | PUMP<br>RATE<br>(1/s)           | PUMPED<br>WATER<br>LEVEL<br>(m)         | SPECIFIC<br>CAPACITY<br>(1/s/m)         | NOTES         |            |
|--|--|---------------------------------|---|---|---------------|------------|
| C3292<br>C3298<br>C3299<br>C3324<br>C3327<br>C3351 | 4.1<br>5.1<br>5.1<br>0.8<br>1.9<br>0.8 | 4.4<br>4.6<br>5.1<br>0.8<br>1.5 | 7.90<br>4.90<br>3.60<br>190.20<br>69.00 | 14.67<br>46.00<br>3.40<br>>4.00<br>1.00 | WARM WATER    | * :<br>• : |
| C3352<br>C3353<br>C3358<br>C3363<br>C3365          | 0.1<br>1.8<br><0.1<br>2.3              | 1.7                             | 47.20                                   | 1.32                                    | WATER LOSS A  | T 213.4M   |
| C3366<br>C3371<br>G3377<br>C3397<br>C3417<br>C3418 | 1.3<br>3.2<br>1.5<br>1.3               | 1.5                             | 108.00                                  | >7.50                                   | •             |            |
| C3422<br>C3431<br>C3436<br>C3451<br>C3467          | 1.2<br>1.2<br>2.0<br>0.9<br>0.0        | 0.3<br>2.0                      | 134.10<br>73.20                         | 0.02<br>0.07<br>0.0                     | DRY           |            |
| C3490<br>C3523<br>C3524<br>C3525<br>C3551<br>C3562 | 3.8<br>0.6<br>0.7<br>2.0<br>4.6<br>0.0 | 2.1<br>2.0<br>4.6<br>0.0        | 86.98<br>5.20                           | 10.50<br>25.00<br>7.70<br>0.00          | DRY           |            |
| C3576<br>C3615<br>C3616<br>C3627                   | 0.1<br>1.1<br>2.5                      | 1.2                             | 80.80<br>118.00                         | 0.14                                    | DKI           |            |
| C3650<br>C3674<br>C3675<br>C3677<br>C3678          | 1.8<br>6.3<br>2.1<br>2.1               | 1.9                             | 28.70                                   | 0.09                                    |               |            |
| C3693<br>C3694<br>C3710<br>C3713<br>C3721<br>C3739 | 1.1<br>2.2<br>3.8<br>0.0<br>1.0<br>0.8 | 2.1<br>4.5<br>0.0<br>1.0        | 115.00<br>58.00<br>115.00               | 0.03<br>22.50<br>0.0<br>0.01            | WATER LOST AT | Г 72М      |
| C3740<br>C3763<br>C3764<br>C3765<br>C3767          | 1.4<br>0.7<br>1.3<br>0.9<br>3.0        | 0.7<br>1.3<br>0.9               | 73.00<br>67.10<br>54.90                 | 0.01<br>0.04<br>0.05                    |               |            |
| C3771<br>C3779<br>C3784<br>C3799<br>C3870          | 1.9<br>3.8<br>3.8<br>1.5<br>0.0        | 1.9<br>3.8<br>3.6               | 82.30<br>36.00<br>63.00                 | 0.04<br>0.15<br>0.06                    | ORY           | •          |
| C3874  | 1.3                                    | -                               |   |   |               |            |

| BOREHOLE<br>NUMBER      | YIELD<br>(1/s)    | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES     | • •        |
|-------------------------|-------------------|-----------------------|---------------------------------|---------------------------------|-----------|------------|
| C3875                   | 1.3               |                       |                                 |                                 |           |            |
| C3897<br>C3910<br>C3919 | 3.5<br>0.2<br>1.6 | 2.3<br>0.2            | 65.50<br>105.00                 | 0.08<br><0.01                   |           |            |
| C3919                   | 22.2              | 22.2                  | 9.65                            | 10.14                           | .•        | ,          |
| C3925                   | 1.4               | 0.8                   | 110.00                          | 0.05                            |           | •          |
| C3929<br>C3932          | 8.8<br>2.5        | 8.8<br>2.3            | 19.00<br>131.80                 | 2.84<br>0.25                    |           |            |
| C3937                   | 0.8               |                       |                                 |                                 |           |            |
| C3939<br>C3942          | 0.2<br>1.8        | 0.2<br>1.8            | 135.00                          | <0.01<br>0.12                   | <b>b</b>  |            |
| C3951                   | 0.5               | 0.5                   | 114.60<br>41.00                 | 0.12                            | •         |            |
| C3955                   | 4.6               | 4.6                   | 18.00                           | 0.30                            |           | . •        |
| C3965                   | 2.8               | 2.8                   | 82.00                           | 0.14                            | ,         |            |
| C3970<br>C3976          | 0.6<br>1.9        | 0.6<br>1.9            | 124.00<br>61.10                 | <0.01<br>0.40                   |           | •          |
| C3995                   | 0.8               | 0.8                   | 91.00                           | 0.01                            |           | •          |
| C3999                   | 3.7               | 2.5                   | 99.00                           | 0.05                            |           | ,          |
| C4003<br>C4037          | 3.7<br>1.3        | 3.7<br>1.3            | 53.60<br>122.00                 | 0.07<br>0.02                    |           |            |
| C4057                   | 4.7               | 4.7                   | 30.00                           | 0.17                            | :         |            |
| C4061                   |                   |                       |                                 |                                 |           |            |
| C4062<br>C4077          |                   |                       |                                 |                                 |           |            |
| C4092                   | 1.3               | 1.3                   | 14.80                           | 0.18                            |           |            |
| C4116                   | 2.2               | 2.2                   | 178.00                          | 0.07                            | •         | • •        |
| C4121<br>C4131          | 23.6<br>0.0       | 23.6<br>0.0           | 168.00                          | 0.32<br>0.00                    | DRY       |            |
| C4143                   | 0.0               | 0.0                   |                                 | 0.00                            |           |            |
| C4152                   | 0.5               | 0.5                   | 84.00                           | <0.01                           | TED 0.00  | AT 1744    |
| C4155<br>C4157          | 9.1<br>3.1        | 9.1                   | 36.00                           | 1.01                            | WATER 360 | A1 1/4M    |
| C4161                   | 10.0              | 10.0                  | 20.00                           | 2.50                            |           | •          |
| C4168                   | 10.0              | 10.0                  | 19.00                           | 4.76                            |           | •          |
| C4174<br>C4177          | 1.9<br>15.6       | 1.9<br>15.6           | 58.50<br>35.00                  | 1.27<br>0.83                    | •         | · ·        |
| C4178                   | 10.0              | 10.0                  | 36.88                           | 0.49                            |           | •          |
| C4179                   | 1.0               | 1.0                   | 108.00                          | 0.17                            | 201       |            |
| C4185<br>C4186          | 0.0               | 0.0                   | •                               | 0.00                            | DRY!      |            |
| C4200                   | 7.0               | 7.0                   | 106.00                          | 0.22                            |           |            |
| C4201                   | 9.9               | 9.1                   | 18.80                           | 3.25                            |           | <b>:</b> . |
| C4206<br>C4208          | 5.7<br>10.8       | 5.7<br>10.8           | 131.10<br>5.90                  | 0.25<br>36.00                   |           |            |
| C4208                   | 10.8              | 10.8                  | 4.60                            | 36.00                           |           |            |
| C4214                   | 0.6               | 2.5                   | 154.00                          | 0.05                            |           |            |
| C4252<br>C4279          | 1.8<br>4.7        | 1.8<br>4.7            | 150.00                          | 0.06                            |           |            |
| C4279                   | 0.2               | 4.7                   | 81.70                           | 1.00                            |           |            |
| C4301                   | 8.7               | 8.7                   | 33.60                           | 9.67                            |           | -          |
| C4302                   | 50.0              | 10.3                  | 11.00                           | 10.30                           |           | •          |
| C4306<br>C4331          | 1.8<br>0.0        | 1.8<br>0.0            | 88.60                           | 0.05<br>0.00                    | DRY       |            |
| C4332                   | 0.7               | 0.2                   | 91.30                           | <0.01                           | J.,,      | ٠.         |
|                         |                   |                       |                                 |                                 |           |            |

| BOREHOLE<br>NUMBER | YIELD<br>(1/s) | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES |     |
|--------------------|----------------|-----------------------|---------------------------------|---------------------------------|-------|-----|
| C4350              | 0.7            | 0.8                   | 148.00                          | <0.01                           |       |     |
| C4360              | 1.4            | 1.0                   | 43.00                           | 0.05                            |       |     |
| C4369              | 8.9            | 8.9                   | 32.00                           | 8.90                            |       |     |
| C4370              | 3.5            | 3.5                   | 76.20                           | 0.08                            | -     |     |
| C4397              | 31.6           | 1 5                   | 00 00                           | 0.00                            |       |     |
| C4403<br>C4413     | 0.6<br>1.1     | 1.5<br>1.9            | 90.00<br>115.00                 | 0.03<br>0.04                    |       | •   |
| C4416              | 0.0            | 0.0                   |                                 | 0.04                            | DRY.  |     |
| C4420              | 0.0            | 0.0                   |                                 | 0.00                            | DICT, |     |
| C4431              | 3.6            |                       |                                 |                                 |       |     |
| C4461              | 1.9            |                       |                                 |                                 |       |     |
| C4484              | 2.1            |                       | <b></b>                         |                                 |       |     |
| C4491              | 4.9            | 4.9                   | 52.00                           | 0.11                            |       |     |
| C4492<br>C4493     | 1.3<br>3.8     |                       |                                 |                                 | •     |     |
| C4498              | 1.2            | 1.3                   | 55.70                           | 0.04                            |       |     |
| C4499              | 0.0            | 0.0                   | , 00110                         | 0.00                            | DRY   |     |
| C4500              | 5.4            | 5.4                   | 15.80                           | 9.00                            | ·     | . , |
| C4501              | 5.4            | 5.4                   | 22.00                           | 7.71                            |       |     |
| C4502              | 0.7            | 0.7                   | 131.00                          | 0.01                            | •     | •   |
| C4504<br>C4510     | 22.8<br>32.6   | 22.8<br>32.6          | 11.90<br>31.70                  | >114.00<br>8.15                 |       |     |
| C4510<br>C4511     | 3.3            | 3.3                   | 27.30                           | 11.00                           |       |     |
| C4512              | 3.5            | 0.0                   | 27.00                           | 11.00                           |       |     |
| C4517              | 3.8            | 3.8                   | 108.60                          | 0.33                            |       |     |
| C4531              | 1.2            | 1.2                   | 72.00                           | 0.60                            | -     | •   |
| C4554<br>C4555     | 1.5<br>4.5     | 4.5                   | 32.00                           | 1 25                            |       |     |
| C4555<br>C4564     | 3.8            | 3.8                   | 76.00                           | 1.25<br>0.17                    |       |     |
| C4565              | 0.0            | 0.0                   | ,                               | 0.00                            | DRY   |     |
| C4575              | 0.1            | 0.1                   | 122.70                          | 0.14                            |       |     |
| C4591              | 37.9           | 37.9                  | 21.50                           | 379.00                          |       |     |
| C4594              |                |                       | 107.00                          | á 00                            |       |     |
| C4597<br>C4610     | 1.6<br>32.6    | 1.6<br>32.6           | 187.30<br>33.50                 | 0.02<br>1.86                    |       |     |
| C4615              | 6.3            | 6.3                   | 62.40                           | 31.50                           |       |     |
| C4624              | 0.9            | 1.3                   | 73.20                           | 0.03                            |       |     |
| C4634              | 1.7            |                       |                                 |                                 | •     |     |
| C4665              | 6.8            | 6.8                   | 55.30                           | 0.37                            |       |     |
| C4669              | 3.2            | 4.4                   | 33.70                           | 0.34                            |       |     |
| C4685<br>C4687     | 3.6<br>1.8     | 3.6<br>3.0            | 85.10<br>40.00                  | 0.88<br>0.12                    |       |     |
| C4007<br>C4713     | 3.8            | 3.8                   | 60.00                           | 0.12                            |       |     |
| C4743              | 1.6            | 1.6                   | 19.20                           | 0.12                            |       |     |
| C4792              | 0.7            | 0.6                   | 121.30                          | 0.02                            |       |     |
| C4804              | 3.3            | 3.3                   | 120.10                          | 0.06                            |       |     |
| C4807              | 5.0            |                       | 07.45                           |                                 |       |     |
| C4812              | 1.3            | 1.4                   | 97.10                           | 0.08                            | DOV   | •   |
| C4829<br>C4850     | 0.0<br>6.3     | 0.0<br>6.3            | 40.10                           | 0.00<br>0.18                    | DRY   |     |
| C4855              | 1.5            | 0.3                   | 40.10                           | J.10                            |       |     |
| C4863              | 1.3            | 1.1                   | 24.00                           | 0.12                            | -     |     |
| C4881              | 2.1            | 2.1                   | 103.00                          | 0.04                            |       |     |
| C4893              | 0.0            | 0.0                   |                                 | 0.00                            | DRY   |     |
|                    |                |                       |                                 |                                 |       |     |

| BOREHOLE<br>NUMBER | YIELD<br>(1/s) | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC CAPACITY (1/s/m) | NOTES            |
|--------------------|----------------|-----------------------|---------------------------------|---------------------------|------------------|
| C4897              | 0.6            | 0.6                   | 252.00                          | 0.02                      |                  |
| C4907              | 1.8            |                       |                                 |                           |                  |
| C4909              | 2.0            | 2.0                   | 150.50                          | 0.44                      | HOT WATER        |
| C4924<br>C4927     | 2.0<br>2.0     | 2.0<br>3.1            | 148.90                          | 0.10                      | HOI WATER        |
| C4966              | 6.1            | 6.1                   | 93.00                           | 0.31                      | ·                |
| C4968              | 6.1            | 6.1                   | 75.00                           | 0.38                      |                  |
| C4971              | 0.0            | 0.0                   |                                 | 0.00                      | DRY              |
| C4974              |                |                       |                                 |                           |                  |
| C4981              | 1.9            | 1.9                   | 45.00                           | 0.19                      |                  |
| C4986              | 11.3           | 11.3                  | 5.53                            | 141.25                    |                  |
| C4989              | 11.3           | 11.3                  | 1.75                            | 29.74                     |                  |
| C4997              | 4.1<br>3.9     | 2.1                   | 89.40<br>114.00                 | 0.11<br>0.31              | •                |
| C5002<br>C5029     | 0.8            | 2.5<br>0.8            | 140.00                          | 0.02                      |                  |
| C5023              | 6.8            | 2.7                   | 101.50                          | 2.25                      |                  |
| C5117              | 2.8            | 2.8                   | 40.00                           | 0.09                      |                  |
| C5143              | 5.0            | 5.0                   | 38.00                           | 1.67                      |                  |
| C5161              | 2.5            | 2.5                   | 71.80                           | 0.05                      |                  |
| C5175              | 3.3            | 3.3                   | 74.80                           | 0.09                      |                  |
| C5206              | 2.8            | 1.3                   | 36.70                           | 0.65                      |                  |
| C5257              | 1.4            | 2.4                   | 130.10                          | 0.13                      |                  |
| C5343<br>C5348     | 1.7<br>1.1     | 1.7<br>1.1            | 100.10<br>126.30                | 0.63<br>0.48              |                  |
| C5346              | 1.2            | 1.9                   | 85.70                           | 0.20                      |                  |
| C5411              | 1.1            | 1.8                   | 110.00                          | 0.07                      |                  |
| C5520              | 1.3            | 2.1                   | 81.50                           | 0.12                      | •                |
| C5564              | 1.3            | 1.3                   | 73.00                           | 0.02                      |                  |
| C5754              |                |                       |                                 |                           |                  |
| C5798              | 2.1            | 2.1                   | 47.00                           | 0.23                      |                  |
| C6056<br>C6095     | 2.1            | 2.1                   | 49.00                           | 0.06                      |                  |
| C6186              |                |                       |                                 |                           |                  |
| C6211              | 0.8            | 0.8                   | 46.00                           | 0.20                      |                  |
| C6213              | 1.7            | 1.7                   | 145.00                          | 0.11                      |                  |
| C6271              |                |                       |                                 |                           |                  |
| C6290              |                |                       |                                 |                           |                  |
| C6300              | 1.3            | 1.3                   | 174.40                          | 0.03                      |                  |
| C630D              | 1.5            | 0.0                   | 74 00                           | 0.02                      |                  |
| C6377<br>. C6378   | 0.8<br>1.7     | 0.8<br>1.7            | 74.00<br>103.80                 | 0.03<br>0.49              |                  |
| . C6376<br>C6494   | 5.6            | 7.3                   | 103.80                          | 1.78                      |                  |
| C6495              | 0.0            | 0.0                   | 10.10                           | 0.00                      | DRY              |
| C6524              | 3.7            | 3.7                   | 64.30                           | 2.31                      |                  |
| C6613              | 1.3            | 1.1                   | 113.00                          | 0.05                      |                  |
| KJ1                | 0.0            | 0.0                   |                                 | 0.00                      | DRY              |
| M0001              |                |                       |                                 |                           |                  |
| P0002              | 0.3            |                       |                                 |                           |                  |
| P0012<br>P0016     | 0.4<br>0.5     |                       |                                 |                           | ,                |
| P0016<br>P0023     | 0.5            |                       |                                 |                           |                  |
| P0023              | U. T           |                       | •                               |                           | STEAM STRUCK 13M |
| P0036              | 0.0            | 0.0                   |                                 | 0.00                      | ABANDONED. DRY   |
| P0037              | 0.0            | 0.0                   |                                 | 0.00                      | ABANDONED. DRY   |
|                    |                |                       |                                 |                           |                  |

| BOREHOLE<br>NUMBER | YIELD<br>(1/s) | PUMP<br>RATE<br>(1/s) | PUMPED<br>WATER<br>LEVEL<br>(m) | SPECIFIC<br>CAPACITY<br>(1/s/m) | NOTES |  |
|--------------------|----------------|-----------------------|---------------------------------|---------------------------------|-------|--|
| P0053              | 0.4            |                       |                                 |                                 | •     |  |
| P0065              | 0.6            |                       |                                 |                                 |       |  |
| P0071              | 0.0            | 0.0                   |                                 | 0.00                            | DRY   |  |
| P0089              | 0.0            | 0.0                   |                                 | 0.00                            | DRY   |  |
| SA58               | 2.3            |                       |                                 |                                 | •     |  |

#### APPENDIX 5

#### BOREHOLE LOCATION LIST

## EASTING NORTHING BOREHOLE NUMBER

| 1391          | 99697 | C0131  |
|---------------|-------|--------|
| 1391          | 99694 | C0131  |
| 1394          | 99693 | C0108  |
| 1394          | 99705 | C2680  |
| 1404          | 99703 | C1504  |
| 1434          |       |        |
|               | 99696 | C3925  |
| 1440          | 99684 | C0288  |
| 1443          | 99714 | C0379  |
| 1444          | 99668 | C1033  |
| 1446          | 99605 | C3005  |
| 1446          | 99686 | C1625  |
| 1447          | 99722 | C1641  |
| 1453          | 99658 | C3955  |
| 1453          | 99663 | ·C1021 |
| 1456          | 99673 | C0376  |
| 1456          | 99704 | C0665  |
| 1464          | 99557 | C0463  |
| 1472          | 99687 | C0423  |
| 1478          | 99696 | C0984  |
| 1481          | 99691 | C1325  |
| 1483          | 99723 | C2564  |
| 1508          | 99595 | C0921  |
| 1516          | 99674 | C0655  |
| 1536          | 99662 | C0258  |
| 1538          | 99654 | C0624  |
| 1548          | 99236 | C5257  |
| 1548          | 99651 | C0208  |
| 1549          | 99671 | C0648  |
| 1553          | 99284 | C2497  |
| 1555          | 99598 | C0164  |
| 1560          | 99705 | C1089  |
| 1563          | 99607 | C0107  |
| 1567 · .      | 99567 | C0227  |
| <b>1567</b> . | 99595 | C0202  |
| 1571          | 99558 | C4413  |
| 1571          | 99589 | C6271  |
| 1572          | 99602 | C4517  |
| 1573          | 99264 | C4350  |
| 1574          | 99554 | C0223  |
| 1574          | 99606 | C0745  |
| 1575          | 99606 | C2745  |
| 1577          | 99587 | C1749  |
| 1578          | 99593 | C3243  |
| 1580          | 98674 | C4143  |
| 1581          | 99582 | C1585  |
| 1582          | 99625 | C0205  |
| 1586          | 99592 | C4669  |
| 1587          | 98675 | C4131  |
| 1587·         | 99615 | C0211  |
| 1589          | 99563 | C0220  |
| 1594          | 99631 | C4206  |
| 1595          | 99596 | C5029  |
| 1596          | 99556 | C2276  |
|               |       |        |

| 1506   | 22522 | 05005 |
|--------|-------|-------|
| 1596   | 99588 | C5206 |
| 1596   | 99627 | C1935 |
| 1598   | 99595 | C0916 |
| 1600   | 99288 | C3351 |
|        |       |       |
| 1605   | 99629 | C4214 |
| 1606   | 99252 | C6056 |
| 1606   | 99576 | C2894 |
| 1608   | 99627 | C3490 |
|        |       |       |
| 1621   | 99270 | C2496 |
| 1621   | 99411 | C1545 |
| 1624   | 99627 | C3627 |
| 1625   | 99425 | C1148 |
|        |       |       |
| 1625   | 99622 | C3467 |
| 1626   | 99634 | C1491 |
| 1626   | 99636 | C1125 |
| 1629   | 99518 | C0953 |
|        |       |       |
| 1634   | 99586 | C3371 |
| 1636   | 99646 | C0485 |
| 1643   | 99470 | C0741 |
| 1644   | 99565 | C4077 |
|        |       |       |
| 1644   | 99666 | C1362 |
| 1646   | 99283 | C3650 |
| 1649   | 99273 | C3353 |
| 1649   | 99608 | C2432 |
|        |       |       |
| 1652   | 99510 | C2448 |
| 1656   | 99280 | C1914 |
| 1656   | 99668 | C2670 |
| 1657   | 99674 | C0214 |
|        |       |       |
| 1663   | 99292 | C1913 |
| 1665   | 99291 | C3352 |
| 1665   | 99310 | C2482 |
| 1665   | 99339 | C3327 |
|        |       |       |
| 1665   | 99703 | C0855 |
| 1667   | 99295 | C1911 |
| 1668   | 99293 | C1912 |
| 1669   | 99515 | C4502 |
|        |       |       |
| 1671   | 99315 | C3397 |
| 1680   | 99619 | C0419 |
| 1691   | 99612 | C3324 |
| 1692   | 99141 | C6495 |
|        |       |       |
| 1696   | 99702 | C0882 |
| 1698   | 99688 | C0805 |
| 1701   | 99708 | C1535 |
| 1704   | 99468 | C4116 |
| 1705   |       |       |
|        | 99589 | C1001 |
| 1709   | 98781 | C4332 |
| 1721   | 99406 | C0783 |
| 1723   | 99637 | C0307 |
| 1724   | 99625 | C0306 |
|        |       |       |
| 1754   | 99468 | C1027 |
| 1759   | 99415 | C0845 |
| 1762   | 98973 | C3562 |
| 1764   | 99350 | C2289 |
|        |       |       |
| 1765   | 99448 | C4564 |
| 1767 · | 99337 | C0261 |
| 1783   | 99301 | C3431 |
| 1789   | 99694 | C5143 |
| 1790   |       |       |
| 1130   | 99685 | C0408 |
|        |       |       |

# EASTING NORTHING BOREHOLE NUMBER

| 1791<br>1793<br>1793<br>1795<br>1795<br>1795<br>1796<br>1797<br>1798<br>1799<br>1801<br>1802<br>1802<br>1802<br>1803<br>1804<br>1805<br>1805<br>1805<br>1805<br>1805<br>1805<br>1805<br>1811<br>1812<br>1812<br>1813<br>1814<br>1815<br>1816<br>1816<br>1816<br>1816<br>1816<br>1818<br>1819<br>1820<br>1823<br>1823<br>1823<br>1823<br>1823<br>1823<br>1823<br>1824<br>1825<br>1826<br>1827<br>1828<br>1829<br>1820<br>1821<br>1821<br>1821<br>1822<br>1823<br>1824<br>1825<br>1826<br>1827<br>1828<br>1828<br>1828<br>1828<br>1828<br>1828<br>1828 | 99687<br>99348<br>99685<br>99661<br>99684<br>99664<br>99416<br>99666<br>99413<br>99444<br>99411<br>99447<br>99513<br>99676<br>99676<br>99676<br>99675<br>99675<br>99675<br>99675<br>99675<br>99675<br>99675<br>99675<br>99675<br>99676<br>99676<br>99676<br>99676<br>99676<br>99676<br>99675<br>99675<br>99675<br>99676<br>99676<br>99676<br>99676<br>99680<br>99680<br>99598<br>99680<br>99680<br>99845 | SA58<br>C2851<br>C0152<br>C3874<br>C0204<br>C3047<br>C1394<br>C3875<br>C0079<br>C2704<br>C0059<br>C3032<br>C1584<br>C1941<br>C0321<br>C1558<br>C0719<br>C0670<br>C4370<br>C3024<br>C1080<br>C2402<br>C2288<br>C2402<br>C2288<br>C2402<br>C2288<br>C2402<br>C316D<br>C3525<br>C1798<br>C1082<br>C4512<br>C4512<br>C4512<br>C4512<br>C4513<br>C4511<br>C0165<br>C3932<br>C1666<br>C3932<br>C1666<br>C3164<br>C0431<br>C1383<br>C2128<br>C0858<br>C3164<br>C0431<br>C1383<br>C2128<br>C0858<br>C3164<br>C3183<br>C3164<br>C3183<br>C3184<br>C3183<br>C3184<br>C4311<br>C3183<br>C3184<br>C4311<br>C3183<br>C3184<br>C4311<br>C4312<br>C4312<br>C4312<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C4313<br>C |
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| 1816<br>1816<br>1818<br>1819<br>1820<br>1823<br>1825<br>1828   | 99714<br>99715<br>98719<br>99215<br>99664<br>99650<br>99248<br>99389<br>99489  | C4369<br>C4511<br>C0165<br>C3932<br>C1666<br>C0836<br>C3164<br>C0431<br>C1383   |
| 1831<br>1832<br>1835<br>1836<br>1841<br>1844<br>1844<br>1846<br>1847   | 99598<br>99680<br>98845<br>99418<br>99615<br>99621<br>99677<br>99364<br>98732<br>98788   | C0858<br>C2970<br>C4331<br>C0266<br>C0869<br>C0822<br>C2129<br>C0533<br>C0511<br>C0510  |
| 1851<br>1851<br>1853   | 99516<br>99621<br>99629  | C2007<br>C0813<br>C1250   |

| 1855   | 99704 | C1434   |
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| 1860   | 99713 | C1436   |
|        |       |         |
| 1861 - | 99682 | C2504   |
| 1863   | 99123 | C4897   |
| 1869   | 98992 | C1970   |
|        |       |         |
| 1869   | 99371 | C1877   |
| 1872   | 99083 | C2709   |
| 1875   | 99686 | C4493   |
|        |       |         |
| 1877   | 98998 | C2664   |
| 1878   | 99092 | C2042   |
| 1879   | 99658 | C2493   |
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| 1881   | 99706 | C3965   |
| 1883   | 99488 | C1287   |
| 1883   | 99650 | C5111   |
|        |       |         |
| 1886   | 99689 | C4492   |
| 1888   | 99685 | · C4491 |
| 1889   | 99428 | C1990   |
|        |       |         |
| 1889 - | 99431 | C0429   |
| 1901   | 99099 | C2300   |
| 1901   | 99199 | C2241   |
|        |       |         |
| 1902   | 99153 | C1404   |
| 1911   | 99165 | C0466   |
| 1912   | 99363 | C2541   |
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| 1915   | 99325 | C2543   |
| 1915   | 99338 | C2542   |
| 1915   | 99355 | C2600   |
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| 1918   | 99193 | C4594   |
| 1918   | 99213 | C2521   |
| 1919   | 99673 | C5754   |
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| 1920   | 99003 | C2170   |
| 1922   | 99682 | C6095   |
| 1929   | 99589 | C2499   |
| 1934   | 99305 | C2871   |
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| 1940   | 99198 | C2522   |
| 1943   | 99552 | C2234   |
| 1944   | 99552 | C0456   |
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| 1945   | 99643 | C3136   |
| 1946   | 99093 | C3767   |
| 1947   | 99295 | C2887   |
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| 1948   | 99125 | C2657   |
| 1949   | 99158 | C4499   |
| 1949   | 99595 | C2118   |
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| 1950   | 99293 | C2870   |
| 1957   | 99152 | C4591   |
| 1959   | 99106 | C0563   |
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| 1959   | 99314 | C2901   |
| 1960   | 99316 | C2900   |
| 1961   | 99138 | C4501   |
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| 1964   | 99144 | C4500   |
| 1964   | 99285 | C0704   |
| 1965   | 99296 | C0705   |
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| 1966   |       | C0707   |
| 1966   | 99294 | C0706   |
| 1966   | 99335 | C2899   |
| 1967   | 99089 | C2701   |
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| 1968   | 99043 | C2885   |
| 1969   | 99120 | C2660   |
| 1971   | 99679 | C0417   |
| 20.1   | 23013 | 55117   |
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| 2022     99207     C2539       2022     99552     C0570       2024     99462     C2388       2024     99717     C2109       2025     99216     C2536       2025     99706     C2033       2028     99092     C2071       2030     99467     C2076       2034     99252     C3674       2035     99229     C2535 | 2022     99552     C0570       2024     99462     C2388       2024     99717     C2109       2025     99216     C2536       2025     99706     C2033       2028     99092     C2071       2030     99467     C2076  | 1972<br>1973<br>1974<br>1974<br>1975<br>1975<br>1975<br>1976<br>1978<br>1983<br>1984<br>1985<br>1985<br>1986<br>1987<br>1989<br>1990<br>1992<br>1996<br>1998<br>2000<br>2002<br>2006<br>2008<br>2008<br>2008<br>2009<br>2013<br>2014<br>2015<br>2017<br>2019<br>2022 | 99180<br>99176<br>99121<br>99204<br>99194<br>99208<br>98991<br>99678<br>99677<br>99203<br>99053<br>99053<br>99053<br>99087<br>99208<br>99680<br>99680<br>99681<br>99203<br>99680<br>99631<br>99203<br>99222<br>99213<br>99403<br>99403<br>99403<br>9953<br>99403<br>99630<br>99627<br>99630<br>99627<br>99405<br>99091 | C1464<br>C2304<br>C2659<br>C2813<br>C1062<br>C0631<br>C4061<br>C2332<br>C630D<br>C1063<br>C2886<br>C4252<br>C0965<br>C2705<br>C2069<br>C4062<br>C4121<br>C1358<br>C3064<br>C1525<br>C0581<br>C2523<br>C2706<br>C2523<br>C2706<br>C2523<br>C2706<br>C1524<br>C0579<br>C0870<br>C1019<br>C1082<br>C0733<br>C3616 |
|---|---|--|--|--|
|   | 2035       99720       C2039         2036       99258       C4504         2036       99394       M0001         2038       98844       C0115         2039       99086       C4420         2041       99665       C2097         2043       98563       P0027         2044       99461       C2077 | 2024<br>2024<br>2025<br>2025<br>2028<br>2030<br>2034   | 99462<br>99717<br>99216<br>99706<br>99092<br>99467<br>99252  | C2388<br>C2109<br>C2536<br>C2033<br>C2071<br>C2076<br>C3674  |

| 2062 | 00010    | 62626 |
|------|----------|-------|
| 2062 | 99313    | C3929 |
| 2064 | 99646    | C1379 |
| 2068 | 99082    | C2863 |
|      |          |       |
| 2069 | 99078    | C1927 |
| 2071 | 99490    | C2773 |
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| 2072 | 98910    | C1402 |
| 2074 | .99497 . | C2753 |
| 2076 | 99718    | C0872 |
|      |          |       |
| 2078 | 99705    | C2292 |
| 2079 | 99702    | C0804 |
| 2080 | 98112    | C4531 |
|      |          |       |
| 2081 | 98118    | C1662 |
| 2084 | 99724    | C0325 |
| 2085 | 99092    | C4986 |
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| 2086 | 99093    | C4989 |
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| 2087 | 99706    | C3784 |
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| 2087 | 99710    | C3779 |
| 2090 | 99257    | C0468 |
| 2091 | 99261    | C3417 |
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| 2092 | 99094    | C0210 |
| 2094 | 99054    | C1926 |
| 2094 | 99104    | C1281 |
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| 2094 | 99264    | C0054 |
| 2095 | 99577    | C1924 |
| 2096 | 99100    | C2534 |
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| 2097 | 99081    | C0910 |
| 2098 | 99631    | C3067 |
| 2099 | 98999    | C2997 |
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| 2101 | 99109    | C2636 |
| 2101 | 99606    | C2966 |
| 2102 | 99317    | C4555 |
| 2103 | 99230    | C3299 |
|      |          |       |
| 2104 | 99114    | C4057 |
| 2104 | 99244    | C3298 |
| 2105 | 98983    | C1843 |
|      |          | 00000 |
| 2107 | 99148    | C0628 |
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| 2109 | 99116    | C0562 |
| 2110 | 99263    | C4301 |
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| 2110 | 99354    | C0457 |
| 2111 | 99145    | C0667 |
| 2112 | 99121    | C1356 |
|      |          | C1330 |
| 2112 | 99228    | C3551 |
| 2114 | 99204    | C3217 |
| 2114 | 99235    | C3365 |
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| 2114 | 99249    | C3678 |
| 2115 | 99210    | C3216 |
| 2119 | 99125    | C0582 |
| 2119 |          | C2430 |
| 5113 | 99184    |       |
| 2120 | 99233    | C3366 |
| 2120 | 99237    | C4168 |
| 2120 | 99244    | C3677 |
|      |          |       |
| 2122 | 99223    | C3675 |
| 2123 | 99566    | C1951 |
| 2124 | 99121    | C0947 |
| 2124 | 99331    | C0458 |
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| 2125 | 99039    | C0729 |
|      |          |       |

| 2126                 | 99572                   | C1952                            |
|----------------------|-------------------------|----------------------------------|
| 2130                 | 99202                   | C4209                            |
| 2130                 | 99294                   | C2883                            |
| 2131                 | 99142                   | C3740                            |
| 2131                 | 99234                   | C4178                            |
| 2132                 | 99233                   | C4610                            |
| 2133                 | 99236                   | C4161                            |
| 2134                 | 99154                   | C1652                            |
| 2134                 | 99215                   | C3292                            |
| 2135                 | 99205                   | C4208                            |
| 2135                 | 99216                   | C4157                            |
| 2136                 | 99215                   | C4302                            |
| 2139                 | 99098                   | C0567                            |
| 2139                 | 99161                   | C2117                            |
| 2139                 | 99166                   | C1482                            |
| 2140                 | 99235                   | C4177                            |
| 2141                 | 99157                   | C2058                            |
| 2141                 | 99649                   | C2296                            |
| 2142                 | 99072                   | C1279                            |
| 2142                 | 99146                   | C0580                            |
| 2143                 | 99198                   | C0231                            |
| 2145                 | 99266                   | C4155                            |
| 2146                 | 99194                   | C1947                            |
| 2146                 | 99196                   | C0531                            |
| 2156                 | 99126                   | C1487                            |
| 2156                 | 99142                   | C0467                            |
| 2157                 | 99257                   | C1483                            |
| 2157                 | 99260                   | C0295                            |
| 2159                 | 99129                   | C1486                            |
| 2163                 | .99658                  | C2061                            |
| 2164                 | 99252                   | C1898                            |
| 2164                 | 99646                   | C2697                            |
| 2180                 | 99223                   | C1488                            |
| 2181                 | 98278                   | C1559                            |
| 2183                 | 99186                   | C2347                            |
| 2185                 | 98051                   | C4565                            |
| 2187                 | 99111                   | C0057                            |
| 2189                 | 98562                   | P0037                            |
| 2189                 | 98565                   | P0036                            |
| 2191                 | 99108                   | C0092                            |
| 2197                 | 99293                   | C5002                            |
| 2199<br>2200<br>2204 | 99025<br>99243<br>99171 | C2823<br>C0814                   |
| 2210<br>2214<br>2215 | 99559<br>99107          | C0939<br>C2110<br>C1892<br>C2160 |
| 2225<br>2226         | 99567<br>99293<br>99108 | C1614<br>C1265                   |
| 2228                 | 99138                   | C0572                            |
| 2234                 | 99004                   | C1726                            |
| 2235                 | 99019                   | C1425                            |
| 2236                 | 99216                   | C0946                            |
| 2237                 | 99119                   | C1851                            |
| 2239                 | 99019                   | C1503                            |
| 2242                 | 99024                   | C1161                            |
| 2246                 | 98723                   | C4971                            |
| 2253                 | 97658                   | C1523                            |

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| 2258   | 98512  | P0023   |
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| 2258   | 99201  | C1013   |
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| 2258   | .99201 | C1013   |
| 2260   | 99081  | KJ1     |
| 2262   | 99153  | C2667   |
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| 2263   | 99149  | 0001C   |
| 2264   | 98939  | P0053   |
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| 2268   | 98487  | P0016   |
| 2268   | 99185  | C0780   |
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| 2268   | 99193  | C0691   |
| . 2269 | 99189  | C0692   |
| 2271   | 98458  | C2866   |
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| 2272   | 98596  | C3003   |
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| 2273   | 99406  | C5520   |
| 2277   | 97682  | C4829   |
| 2277   | 99166  | C1997   |
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| 2278   | 99078  | C1475   |
| 2278   | 99263  | C1029   |
| 2280   | 99070  | C2662   |
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| 2281   | 99212  | C2108   |
| 2282   | 99262  | C1830   |
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| 2283   | 99185  | C2062   |
| 2288   | 99102  | · C2720 |
| 2290   | 99050  | C2263   |
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| 2293   | 99143  | C2005   |
| 2294   | 99072  | C1794   |
| 2294   | 99190  | C1051   |
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| 2296   | 99254  | C1795   |
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| 2297   | 99058  | C2264   |
| 2297   | 99181  | P0089   |
| 2299   | 97899  | C4484   |
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| 2302   | 99053  | C1602   |
| 2304   | 98709  | C4174   |
| 2306   | 98606  | P0071   |
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| 2306   | 99099  | C2063   |
| 2309   | 99094  | C2663   |
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| 2311   | 98609  | C2717   |
| 2315   | 98675  | C2758   |
| 2315   | 98764  | C4893   |
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| 2315   | 98979  | C2172   |
| 2316   | 99244  | C2149   |
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| 2317   | 99074  | C0633   |
| 2318   | 98981  | C2138   |
| 2322   | 98778  | C2910   |
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| 2324   | 3000   | C2358   |
| 2325   | 98961  | C4634   |
| 2326   | 98956  | C4152   |
|        |        |         |
| 2327   | 98695  | C0407   |
| 2328   | 99092  | C0703   |
| 2329   | 97909  | C1390   |
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| 2329   | 98636  | C4909   |
| 2329   | 99226  | C1850   |
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| 2331   | 99147  | C1000   |
| 2337   | 99139  | C1929   |
|        |        |         |

| 2339   | 99090 | C2420   |
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| 2342   | 99122 | P0065   |
| 2345   | 99316 | C0651   |
| 2346   | 98803 | C3713   |
| 2346   | 99191 | C2197   |
| 2347   | 98678 | C2447   |
| 2347   | 99084 | C2421   |
| 2349   | 97803 | C1499   |
|        |       |         |
| 2349   | 99126 | C0634   |
| 2353   | 98613 | C0440   |
| 2355   | 98723 | C0416   |
| 2355   | 98775 | C3266   |
| 2355   | 99136 | C0994   |
| 2356   | 98524 | C4575   |
| 2361   | 99247 | C2170   |
| 2362   | 98647 | C4812   |
| 2363   | 98624 | C3087   |
|        |       |         |
| 2363   | 98645 | C4807   |
| 2363   | 98812 | C3377   |
| 2364   | 98641 | C2902   |
| 2364   | 99139 | C1007   |
| 2365   | 98545 | C1126   |
| 2365   | 98585 | C3280   |
| 2365   | 98653 | C3418   |
| 2365   | 98865 | C2466   |
| 2365   | 99283 | C1112   |
| 2366   | 98644 | C4792   |
|        |       |         |
| 2367   | 98882 | C3422   |
| 2368   | 97628 | C3939   |
| 2369   | 97893 | C1391   |
| 2369   | 98606 | C6378   |
| 2371   | 97801 | C2468   |
| 2371   | 97908 | C3942   |
| 2371   | 98554 | C4416   |
| 2371   | 98643 | C4431   |
| 2371   | 99150 | C2176   |
| 2371   | 99198 | C0699   |
| 2374   | 98720 | C4597   |
|        |       | C0553   |
| 2375   | 99219 |         |
| 2376   | 98684 | C6613   |
| 2377   | 98687 | C5343   |
| 2380   | 99130 | C4403   |
| 2381   | 97822 | C3358   |
| 2381   | 97887 | C0605   |
| 2382   | 98697 | C6213   |
| 2383   | 98626 | C3799   |
| 2384   | 98672 | C5348   |
| 2385   | 98514 | .P0002  |
| 2385   | 98663 | C4615   |
|        | 97632 |         |
| 2387   |       | C2647   |
| 2387   | 98503 | P0012   |
| - 2388 | 99188 | C1277   |
| 2389   | 99233 | C0677   |
| 2390   | 97883 | C0451   |
| 2390   | 97889 | · C3363 |
| 2390   | 99228 | C0678   |
| 2391   | 98478 | C6494   |
| 2394   | 98521 | C2294   |
|        |       |         |

| 2395 | 98651 | C3710   |
|------|-------|---------|
| 2395 | 98666 | C4685   |
| 2395 | 98703 | C4855   |
|      |       |         |
| 2396 | 98657 | C3615   |
| 2397 | 98483 | C6377   |
| 2397 | 98502 | C5117   |
| 2397 | 98509 | C3937   |
|      |       | 03937   |
| 2397 | 98606 | C3999   |
| 2397 | 98630 | C5375   |
| 2398 | 98678 | C4461   |
| 2399 | 98442 | C5798   |
|      |       |         |
| 2400 | 98645 | C5411   |
| 2400 | 98710 | C4037   |
| 2402 | 98715 | C3976   |
| 2403 | 98471 | C6211   |
|      | 98462 |         |
| 2404 |       | C4743   |
| 2405 | 98675 | C4850   |
| 2407 | 98418 | C5564   |
| 2408 | 97759 | C0875   |
| 2408 | 98377 | C3576   |
|      |       |         |
| 2408 | 98752 | C5175   |
| 2409 | 98525 | C6524   |
| 2410 | 97886 | C3970   |
| 2410 | 98670 | C3694   |
|      |       |         |
| 2412 | 98562 | C4804   |
| 2413 | 98410 | C1294   |
| 2413 | 98467 | C4092   |
| 2414 | 98648 | C3764   |
| 2414 | 98802 | C4554   |
|      |       |         |
| 2416 | 97788 | C0824   |
| 2416 | 98626 | C3765   |
| 2420 | 98413 | C1259   |
| 2422 | 98416 | C4186   |
| 2422 | 98484 | C4907   |
| 2422 | 98486 | C4201   |
|      |       |         |
| 2425 | 98428 | C4179   |
| 2426 | 98425 | C4863   |
| 2427 | 98466 | C4200   |
| 2427 | 98626 | C3523   |
| 2427 |       |         |
|      | 98630 | C3524   |
| 2428 | 98502 | C4968   |
| 2429 | 98465 | C4966   |
| 2430 | 98438 | C4997   |
| 2430 | 98440 | C4981   |
|      |       |         |
| 2430 | 98588 | C2338   |
| 2431 | 98831 | C4279   |
| 2432 | 98255 | C1713   |
| 2433 | 98635 | C3721   |
| 2434 | 97868 | . C0381 |
|      |       |         |
| 2435 | 98563 | C0839   |
| 2441 | 98601 | C6186   |
| 2441 | 98638 | C3763   |
| 2442 | 98536 | C4927   |
| 2443 |       | C4360   |
|      | 98743 |         |
| 2445 | 97865 | C3436   |
| 2448 | 98498 | C4881   |
| 2449 | 98617 | C3739   |
| 2450 | 98633 | C3693   |
|      | 2300  | 5555    |
|      |       |         |

## EASTING NORTHING BOREHOLE NUMBER

| 2451   | 98436 | C5161 |
|--------|-------|-------|
| 2452   | 98428 | C4687 |
| 2454   | 98490 | C4624 |
| 2458   | 97868 | C3870 |
| 2458   | 98822 | C3897 |
| 2459   | 97876 | C3951 |
| 2459   | 98696 | C4292 |
| 2460   | 98738 | C4665 |
| 2465   | 98553 | C2620 |
| 2466   | 98633 | C3910 |
| 2468   | 97862 | C2646 |
| 2470   | 98733 | C3995 |
| 2471   | 98013 | C4498 |
| 2474   | 98029 | C0811 |
| 2475   | 98596 | C4306 |
| 2480   | 97692 | C3451 |
| 2488   | 97659 | C4185 |
| 2492   | 98693 | C3771 |
| 2493   | 98457 | C4713 |
| 2494.  | 98724 | C4003 |
| 2495 - | 98814 | C3919 |

APPENDIX 6

## ESTIMATED HYDRAULIC PROPERTIES OF BOREHOLES

(From Thiem and Logan approximations - Section 3.4.1)

| BOREHOLE<br>NUMBER | GRID<br>REFERENCE      | TRANSMISSIVITY<br>(m <sup>2</sup> /d) | PERMEABILITY (m/d) |
|--------------------|------------------------|---------------------------------------|--------------------|
| C0407              | 232798695              | 1139                                  | 21.21              |
| C0692              | 226999189              | 1139                                  | 46.68              |
| C0870              | 201499720              | 2                                     | 0.19               |
| C1361              | 205999553              | 2                                     | 0.07               |
| C1404              | 190299153              | 10                                    | 0.19               |
| C1486              | 215999129              | 1                                     | 0.02               |
| C1794              | 229499072              | 1                                     | 0.02               |
| C1795              | 229699254              | 17                                    | 0.63               |
| C1795              | 229699254              | 17                                    | 0.63               |
| C1798              | 181299405              | 40                                    | 3.14               |
| C1830              | 228299262              | 22                                    | 0.80               |
| C1850              | 232999226              | 5                                     | 3.04               |
| C1877              | 186999371              | >1015                                 |                    |
| C1892              | 221499107              | 26                                    | 1.30               |
| C1913              | 166399292              | <1                                    | <0.01              |
| C1924              | 209599577              | 3                                     | 0.21               |
| C1926              | 209499054              | 8                                     | 0.36               |
| C1929              | 233799139              | 4                                     | 0.39               |
| C1935              | 159699627              | 17                                    | 8.54               |
| C1941              | 180299402              | 7                                     | 3.51               |
| C1947              | 214699194              | 185                                   | 11.56              |
| C1951              | 212399566              | 2                                     | 0.07               |
| C1952              | 212699572              | 11                                    | 37.97              |
| C1970<br>C1997     | 186998992<br>227799166 | 1<br>6                                | 0.01<br>0.37       |
| C2005              | 229399143              | 2                                     | 0.37               |
| C2003              | 202599706              | 31                                    | 0.38               |
| C2058              | 214199157              | 11                                    | 4.58               |
| C2058              | 216399658              | 41                                    | 5.06               |
| C2062              | 228399185              | 3                                     | 2.28               |
| C2063              | 230699099              | 3                                     | 0.21               |
| C2069              | 198999087              | 2                                     | 0.81               |
| C2071              | 202899092              | >605                                  | >287.98            |
| C2076              | 203099467              | 7                                     | 0.03               |
| C2097              | 204199665              | 2                                     | 0.33               |
| C2108              | 228199212              | 14                                    | 0.72               |
| C2109              | 202499717              | 188                                   | 31.32              |
| C2118              | 194999595              | 3                                     | 0.54               |
| C2138              | 231898981              | <1                                    | <0.01              |
| C2160              | 221599567              | 9                                     | 0.25               |
| C2170 ·            | 236199247              | 5                                     | 0.21               |
| C2172              | 231598979              | 51                                    | 0.90               |
| C2176              | 237199150              | 8                                     | 2.66               |
| C2197              | 234699191              | 2                                     | 0.05               |
| C2234              | 194399552              | 7                                     | 0.52               |
| C2246              | 210799246              | 11                                    | 0.52               |
|                    |                        |                                       |                    |

| BOREHOLE<br>NUMBER | GRID<br>REFERENCE      | TRANSMISSIVITY<br>(m <sup>2</sup> /d) | PERMEABILITY<br>(m/d) |
|--------------------|------------------------|---------------------------------------|-----------------------|
| C2264              | 229799058              | 5                                     | 0.09                  |
| C2269              | 181399668              | 7                                     | 0.39                  |
| C2276              | 159699556              | 6                                     | 1.06                  |
| C2289              | 176499350              | 18                                    | 0.42                  |
| C2294              | 239498521              | 6                                     | 0.90                  |
| C2296              | 214199649              | 6                                     | 0.38                  |
| C2304              | 197399176              | 2480                                  | 68.88                 |
| C2332              | 197899678              | 7                                     | 1.90                  |
| C2338              | 243098588              | 35                                    | 3.76                  |
| C2347              | 218399186              | 12                                    |                       |
| C2388              | 202499462              | 124                                   | 5.81                  |
| C2402              | 180599675              | >2089                                 | >271.32               |
| C2430              | 211999184              | >3367                                 |                       |
| C2448              | 165299510              | 8                                     | 0.96                  |
| C2466              | 236598865              | 38                                    | 4.81                  |
| C2493              | 187999658              | 45                                    | 5.50                  |
| C2496              | 162199270              | 19                                    | 1.54                  |
| C2497              | 155399284              | 1082                                  | 23.68                 |
| C2504              | 186199682              | 2                                     | 0.24                  |
| C2522              | 194099198              | >1814                                 | >3023.77              |
| C2534<br>C2536     | 209699100<br>202599216 | >2107<br>>1759                        | >296.80<br>>390.95    |
| C2536              | 204699208              | >2089                                 | >264.45               |
| C2537              | 200899213              | >1975                                 | /204.43               |
| C2538              | 202299207              | 95                                    | 7.00                  |
| C2564              | 148399723              | 8                                     | 0.29                  |
| C2600              | 191599355              | >990                                  | >32.99                |
| C2620              | 246598553              | 5                                     | 0.05                  |
| C2636              | 210199109              | 538                                   | 22.03                 |
| C2646              | 246897862              | 1                                     | 0.11                  |
| C2657              | 194899125              | 239                                   | •                     |
| C2659              | 197499121              | 269                                   | 17.49                 |
| C2660              | 196999120              | 4453                                  | 523.90                |
| C2662              | 228099070              | 5                                     | 0.12                  |
| C2663              | 230999094              | 17                                    |                       |
| C2701              | 196799089              | 204                                   | 408.32                |
| C2703              | 205099215              | >4123                                 | >150.49               |
| C2705              | 198799208              | >1539                                 | >127.22               |
| C2706              | 200699222              | 2782                                  | 118.38                |
| C2709              | 187299083              | 22                                    | 1.83                  |
| C2717              | 231198609              | 2                                     | 2.14                  |
| C2745              | 157599606              | 10                                    | 1.30                  |
| C2813              | 197499204              | >1936                                 | o' àc                 |
| C2851              | 179399348              | 8                                     | 0.36                  |
| C2866              | 227198458              | 7                                     | 0.20                  |
| C2883              | 213099294              | 4                                     | 0.29                  |
| C2902<br>C2910     | 236498641<br>232298778 | <b>4</b><br><b>3</b>                  | 0.36<br>0.04          |
| C2910<br>C2970     | 183299680              | 5<br>5                                | 0.51                  |
| C2970<br>C2997     | 209998999              | 100                                   | 3.10                  |
| C299/7<br>C3005    | 144699605              | · 57                                  | 0.45                  |
| C3024              | 180599238              | 13                                    | 1.04                  |
|                    |                        |                                       |                       |

| BOREHOLE<br>NUMBER | GRID<br>REFERENCE      | TRANSMISSIVITY (m <sup>2</sup> /d) | PERMEABILITY<br>(m/d) |
|--------------------|------------------------|------------------------------------|-----------------------|
| C2264              | 229799058              | 5                                  | 0.09                  |
| C2269              | 181399668              | 7                                  | 0.39                  |
| C2276              | 159699556              | 6                                  | 1.06                  |
| C2289              | 176499350              | 18                                 | 0.42                  |
| C2294              | 239498521              | 6                                  | 0.90                  |
| C2296              | 214199649              | 6                                  | 0.38                  |
| C2304              | 197399176              | 2480                               | 68.88                 |
| C2332              | 197899678              | 7                                  | 1.90                  |
| C2338              | 243098588              | 35                                 | 3.76                  |
| C2347              | 218399186              | 12                                 | r 01                  |
| C2388<br>C2402     | 202499462              | 124                                | 5.81                  |
| C2402              | 180599675<br>211999184 | >2089<br>>3367                     | >271.32               |
| C2430              | 165299510              | /3307<br>8                         | 0.96                  |
| C2446              | 236598865              | 38                                 | 4.81                  |
| C2493              | 187999658              | 45                                 | 5.50                  |
| C2496              | 162199270              | 19                                 | 1.54                  |
| C2497              | 155399284              | 1082                               | 23.68                 |
| C2504              | 186199682              | 2                                  | 0.24                  |
| C2522              | 194099198              | >1814                              | >3023.77              |
| C2534              | 209699100              | >2107                              | >296.80               |
| C2536              | 202599216              | >1759 -                            | >390.95               |
| C2537              | 204699208              | >2089                              | >264.45               |
| C2538              | 200899213              | >1975                              |                       |
| C2539              | 202299207              | 95                                 | 7.00                  |
| C2564              | 148399723              | 8                                  | 0.29                  |
| C2600              | 191599355              | >990                               | >32.99                |
| C2620<br>C2636     | 246598553              | 5                                  | 0.05                  |
| C2646              | 210199109<br>246897862 | 538<br>1                           | 22.03<br>0.11         |
| C2657              | 194899125              | 239                                | 0.11                  |
| C2659              | 197499121              | 269                                | 17.49                 |
| C2660              | 196999120              | 4453                               | 523.90                |
| C2662              | 228099070              | 5                                  | 0.12                  |
| C2663              | 230999094              | 17                                 | ***                   |
| C2701              | 196799089              | 204                                | 408.32                |
| C2703              | 205099215              | >4123                              | >150.49               |
| C2705              | 198799208              | >1539                              | >127.22               |
| C2706              | 200699222              | 2782                               | 118.38                |
| C2709              | 187299083              | 22                                 | 1.83                  |
| C2717              | 231198609              | 2                                  | 2.14                  |
| C2745              | 157599606              | 10                                 | 1.30                  |
| C2813              | 197499204              | >1936                              |                       |
| C2851              | 179399348              | 8                                  | 0.36                  |
| C2866              | 227198458              | 7                                  | 0.00                  |
| C2883              | 213099294              | 4                                  | 0.29                  |
| C2902              | 236498641              | <b>4</b><br>3                      | 0.36                  |
| C2910<br>C2970     | 232298778<br>183299680 | ა<br>5                             | 0.04<br>0.51          |
| C2970<br>C2997     | 209998999              | 100                                | 3.10                  |
| C3005              | 144699605              | 57                                 | 0.45                  |
| C3024              | 180599238              | 13                                 | 1.04                  |
| ·                  |                        | <b>20</b> .                        | 1.01                  |

| C3047         179699664         >9917         >1599.47           C3136         194599643         2         0.15           C3164         182599248         62         2.00           C3280         236598585         1         0.03           C3292         213499215         1613         35.45           C3298         210499244         4802         137.98           C3299         210399230         355         9.75           C3324         169199612         >440         >47.81           C3327         166599339         110         1.83           C3353         164999273         150         16.34           C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3627         16249627         15         0.18           C3650         164699283         10         3.42   | BOREHOLE<br>NUMBER   | GRID<br>REFERENCE | TRANSMISSIVITY<br>(m <sup>2</sup> /d) | PERMEABILITY<br>(m/d) |
|---|--|-------------------|---------------------------------------|-----------------------|
| C3136         194599643         2         0.15           C3164         182599248         62         2.00           C3280         236598855         1         0.03           C3292         213499215         1613         35.45           C3298         210499244         4802         137.98           C3299         210399230         355         9.75           C3324         169199612         >440         >47.81           C3327         166599339         110         1.83           C3357         167199315         >825         >88.67           C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3515         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3                                     | C3047  | 179699664         | >9917                                 | >1599.47              |
| C3164         182599248         62         2.00           C3280         236598585         1         0.03           C3292         213499215         1613         35.45           C3298         210499244         4802         137.98           C3299         210399230         355         9.75           C3324         169199612         >440         >47.81           C3327         166599339         110         1.83           C3353         164999273         150         16.34           C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         231299228         847         11.96           C3652         16499627         15         0.18           C3655         16499283         10         3.42           C3650         16499283         10         3.42           C3650         16499283         10         3.42           C364                                     |  |                   | 2                                     | 0.15                  |
| C3280         236598585         1         0.03           C3292         213499215         1613         35.45           C3298         210499244         4802         137.98           C3299         210399230         355         9.75           C3324         169199612         >440         >47.81           C3327         166599339         110         1.83           C3353         164999273         150         16.34           C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3440         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3652         162499627         15         0.18           C3655         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3650         164699283         10         3.42           C3761         24198638         1         0.05           C                                     |  | 182599248         | 62                                    | 2.00                  |
| C3298         210499244         4802         137.98           C3299         210399230         355         9.75           C3324         169199612         >440         >47.81           C3327         166599339         110         1.83           C3353         164999273         150         16.34           C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398638         1         0.02           C3763         24198638         1         0.05           C3771         249298693         4         0.19           C3765<                                     |  | 236598585         | 1                                     | 0.03                  |
| C3299         210399230         355         9.75           C3324         169199612         >440         >47.81           C3327         166599339         110         1.83           C3353         164999273         150         16.34           C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3763         244198638         1         0.02           C3764         241998638         1         0.05           C3771         249298693         4         0.21           C3779<                                     | C3292  | 213499215         | 1613                                  |                       |
| C3324         169199612         >440         >47.81           C3327         166599339         110         1.83           C3353         164999273         150         16.34           C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.05           C3763         24198638         1         0.05           C3764         24198638         1         0.05           C3771         249298693         4         0.21           C3772  | C3298  | 210499244         |                                       |                       |
| C3327         166599339         110         1.83           C3353         164999273         150         16.34           C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3651         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3763         24198638         1         0.02           C3763         24198638         1         0.05           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799766         6         0.29           C3874  | C3299  | 210399230         | _                                     |                       |
| C3353         164999273         150         16.34           C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3430         160899627         1196         244.08           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         24198638         1         0.05           C3764         241498648         4         0.19           C37755         241698626         6         0.27           C3771         249298693         4         0.21           C3772         245989822         9         0.57           C394   | C3324  | 169199612         |                                       |                       |
| C3397         167199315         >825         >88.67           C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3764         24198648         4         0.19           C3765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3874         179599661         104         23.20           C3875         17979666         104         6.96           C3925  |  |                   |                                       |                       |
| C3431         178399301         2         0.55           C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198638         1         0.05           C3764         241498648         4         0.19           C37765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3875         179799661         104         6.96           C3897   |  |                   |                                       |                       |
| C3436         244597865         8         0.24           C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198638         1         0.05           C3764         241498648         4         0.19           C3765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3374         179599661         104         6.96           C3897         245898822         9         0.57           C3924         <  |  |                   |                                       |                       |
| C3490         160899627         1196         244.08           C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198648         4         0.19           C3765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3874         179599661         104         6.96           C3897         245898822         9         0.57           C3924         205199081         1058         39.06           C3925         143499696         5         2.64           C3929  |  |                   |                                       |                       |
| C3525         181198475         2848         51.59           C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198638         1         0.05           C3764         241498648         4         0.19           C3765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3874         179599661         104         6.96           C3897         245898822         9         0.57           C3924         205199081         1058         39.06           C3925         143499696         5         2.64           C3929 <t< td=""><td></td><td></td><td></td><td></td></t<> |  |                   |                                       |                       |
| C3551         211299228         847         11.96           C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198638         1         0.05           C3764         241498648         4         0.19           C3765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3874         179599661         104         6.96           C3897         245898822         9         0.57           C3924         205199081         1058         39.06           C3925         143499696         5         2.64           C3929         206299313         299         6.77           C3932   |  |                   |                                       |                       |
| C3615         239698657         16         2.66           C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198638         1         0.05           C3764         241498648         4         0.19           C3765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3874         179599661         104         23.20           C3875         179799666         104         6.96           C3897         245898822         9         0.57           C3924         205199081         1058         39.06           C3925         143499696         5         2.64           C3929         206299313         299         6.77           C3932   |  |                   |                                       |                       |
| C3627         162499627         15         0.18           C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198638         1         0.05           C3764         241498648         4         0.19           C3765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3874         179599661         104         23.20           C3875         179799666         104         6.96           C3897         245898822         9         0.57           C3924         205199081         1058         39.06           C3929         206299313         299         6.77           C3932         181999215         27         2.11           C3939         236897628         <1   |  |                   |                                       |                       |
| C3650         164699283         10         3.42           C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198638         1         0.05           C3764         241498648         4         0.19           C3765         241698626         6         0.27           C3771         249298693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3874         179599661         104         6.96           C3897         245898822         9         0.57           C3924         205199081         1058         39.06           C3925         143499696         5         2.64           C3929         206299313         299         6.77           C3932         181999215         27         2.11           C3939         236897628         <1  |  |                   |                                       |                       |
| C3694         241098670         3         0.57           C3710         239598651         2474         651.05           C3721         243398635         1         0.02           C3763         244198648         4         0.19           C3765         241698626         6         0.27           C3771         24928693         4         0.21           C3779         208799710         17         0.76           C3784         208799706         6         0.29           C3874         179599661         104         23.20           C3875         179799666         104         6.96           C3897         245898822         9         0.57           C3924         205199081         1058         39.06           C3925         143499696         5         2.64           C3929         206299313         299         6.77           C3932         181999215         27         2.11           C3939         236897628         <1  |  |                   |                                       |                       |
| C3710       239598651       2474       651.05         C3721       243398635       1       0.02         C3763       244198638       1       0.05         C3764       241498648       4       0.19         C3765       241698626       6       0.27         C3771       249298693       4       0.21         C3779       208799710       17       0.76         C3784       208799706       6       0.29         C3874       179599661       104       23.20         C3875       179799666       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1   |  |                   |                                       |                       |
| C3721       243398635       1       0.02         C3763       244198638       1       0.05         C3764       241498648       4       0.19         C3765       241698626       6       0.27         C3771       249298693       4       0.21         C3779       208799710       17       0.76         C3784       208799706       6       0.29         C3874       179599661       104       23.20         C3875       179799666       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1   |  |                   |                                       |                       |
| C3763       244198638       1       0.05         C3764       241498648       4       0.19         C3765       241698626       6       0.27         C3771       249298693       4       0.21         C3779       208799710       17       0.76         C3784       208799706       6       0.29         C3874       179599661       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1  |  |                   |                                       |                       |
| C3764       241498648       4       0.19         C3765       241698626       6       0.27         C3771       249298693       4       0.21         C3779       208799710       17       0.76         C3784       208799706       6       0.29         C3874       179599661       104       23.20         C3875       179799666       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1   |  |                   |                                       |                       |
| C3765       241698626       6       0.27         C3771       249298693       4       0.21         C3779       208799710       17       0.76         C3784       208799706       6       0.29         C3874       179599661       104       23.20         C3875       179799666       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1  |  |                   |                                       |                       |
| C3771       249298693       4       0.21         C3779       208799710       17       0.76         C3784       208799706       6       0.29         C3874       179599661       104       23.20         C3875       179799666       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1   |  |                   | 6                                     |                       |
| C3779       208799710       17       0.76         C3784       208799706       6       0.29         C3874       179599661       104       23.20         C3875       179799666       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1  |  |                   |                                       |                       |
| C3874       179599661       104       6.96         C3875       179799666       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1  |  |                   | 17                                    |                       |
| C3875       179799666       104       6.96         C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1   |  |                   | 6                                     | 0.29                  |
| C3897       245898822       9       0.57         C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1  | C3874  | 179599661         | 104                                   | 23.20                 |
| C3924       205199081       1058       39.06         C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1   |  | 179799666         |                                       |                       |
| C3925       143499696       5       2.64         C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1  |  |                   |                                       |                       |
| C3929       206299313       299       6.77         C3932       181999215       27       2.11         C3939       236897628       <1   |  |                   |                                       |                       |
| C3932       181999215       27       2.11         C3939       236897628       <1  |  |                   |                                       |                       |
| C3939       236897628       <1  |  |                   |                                       |                       |
| C3942       237197908       14       0.30         C3951       245997876       5       0.05         C3955       145399658       34       1.37         C3965       188199706       15       0.16         C3970       241097886       <1   |  |                   |                                       |                       |
| C3951       245997876       5       0.05         C3955       145399658       34       1.37         C3965       188199706       15       0.16         C3970       241097886       <1   |  |                   |                                       |                       |
| C3955       145399658       34       1.37         C3965       188199706       15       0.16         C3970       241097886       <1  |  |                   |                                       |                       |
| C3965       188199706       15       0.16         C3970       241097886       <1  | and the second s |                   |                                       |                       |
| C3970       241097886       <1  |  |                   |                                       |                       |
| C3976       240298715       46       5.36         C3995       247098733       1       0.09         C3999       239798606       6       0.23         C4003       249498724       7       0.08         C4037       240098710       2       0.13         C4057       210499114       19       0.35         C4092       241398467       19       0.13         C4116       170499468       8       0.47         C4121       199299680       36       4.56         C4152       232698956       <1   |  |                   |                                       |                       |
| C3995       247098733       1       0.09         C3999       239798606       6       0.23         C4003       249498724       7       0.08         C4037       240098710       2       0.13         C4057       210499114       19       0.35         C4092       241398467       19       0.13         C4116       170499468       8       0.47         C4121       199299680       36       4.56         C4152       232698956       <1   |  |                   |                                       |                       |
| C3999       239798606       6       0.23         C4003       249498724       7       0.08         C4037       240098710       2       0.13         C4057       210499114       19       0.35         C4092       241398467       19       0.13         C4116       170499468       8       0.47         C4121       199299680       36       4.56         C4152       232698956       <1  |  |                   |                                       |                       |
| C4003       249498724       7       0.08         C4037       240098710       2       0.13         C4057       210499114       19       0.35         C4092       241398467       19       0.13         C4116       170499468       8       0.47         C4121       199299680       36       4.56         C4152       232698956       <1   |  |                   |                                       |                       |
| C4037       240098710       2       0.13         C4057       210499114       19       0.35         C4092       241398467       19       0.13         C4116       170499468       8       0.47         C4121       199299680       36       4.56         C4152       232698956       <1  |  |                   |                                       |                       |
| C4057       210499114       19       0.35         C4092       241398467       19       0.13         C4116       170499468       8       0.47         C4121       199299680       36       4.56         C4152       232698956       <1   |  |                   |                                       |                       |
| C4092       241398467       19       0.13         C4116       170499468       8       0.47         C4121       199299680       36       4.56         C4152       232698956       <1   |  |                   |                                       |                       |
| C4116       170499468       8       0.47         C4121       199299680       36       4.56         C4152       232698956       <1   |  |                   |                                       |                       |
| C4121 199299680 36 4.56<br>C4152 232698956 <1 <0.08   |  |                   | 8                                     |                       |
|   |  |                   |                                       |                       |
| C4155 214599266 115   |  |                   |                                       | <0.08                 |
|   | C4155  | 214599266         | 115                                   |                       |

| BOREHOLE<br>NUMBER | GRID<br>REFERENCE      | TRANSMISSIVITY<br>(m <sup>2</sup> /d) | PERMEABILITY<br>(m/d) |
|--------------------|------------------------|---------------------------------------|-----------------------|
| C4161              | 213399236              | 264                                   | 37.65                 |
| C4168              | 212099237              | 523                                   | 130.85                |
| C4174              | 230498709              | 145                                   | •                     |
| C4177<br>C4178     | 214099235<br>213199234 | 91<br>52                              | 9.13                  |
| C4178              | 242598428              | 52<br>19                              | 1.64<br>1.56          |
| C4179              | 242798466              | 24                                    | 12.10                 |
| C4200              | 242298486              | 357                                   | 7.01                  |
| C4206              | 159499631              | 28                                    | 2.85                  |
| C4208              | 213599205              | 3848                                  | 69.96                 |
| C4209              | 213099202              | 3848                                  | 67.51                 |
| C4214              | 160599629              | . 6                                   | 0.06                  |
| C4252              | 198599707              | 7                                     | 0.24                  |
| C4279              | 243198831              | 114                                   | 113.91                |
| C4301              | 211099263              | 1009                                  | 18.39                 |
| C4302              | 213699215              | 1086                                  | 18.59                 |
| C4306              | 247598596              | 5                                     | 0.16                  |
| C4332              | 170998781              | <1                                    | <0.21                 |
| C4350              | 157399264              | <1                                    | <0.03                 |
| C4360              | 244398743              | 6                                     | 0.16                  |
| °C4369             | 181699714              | 979                                   | 13.41                 |
| C4370              | 180499690              | 9 -                                   | 0.11                  |
| C4403              | 238099130              | 3                                     | 0.00                  |
| C4413<br>C4491     | 157199558<br>188899685 | 5<br>12                               | 0.76                  |
| C4491<br>C4498     | 247198013              | 5                                     | 0.78<br>0.08          |
| C4500              | 196499144              | 939                                   | 49.45                 |
| C4501              | 196199138              | 805                                   | 89.42                 |
| C4502 ·            | 166999515              | 1                                     | 0.04                  |
| C4504              | 203699258              | >11900                                | >639.79               |
| C4510              | 181699713              | 871                                   | 18.15                 |
| C4511              | 181699715              | 1176                                  | 21.77                 |
| C4517              | 157299602              | 38                                    | 4.70                  |
| C4531              | 208098112              | 68                                    | 1.42                  |
| C4555              | 210299317              | 142                                   | 2.97                  |
| C4564              | 176599448              | 18                                    |                       |
| C4575              | 235698524              | 15                                    | 0.08                  |
| C4591              | 195799152              | 36600                                 | 3553.43               |
| C4597              | 237498720              | 2                                     | 0.07                  |
| C4610              | 213299233              | 199                                   | 7.36                  |
| C4615              | 238598663              | 3464                                  | 65.35                 |
| C4624<br>C4665     | 245498490              | 3                                     | 0.16                  |
| C4669              | 246098738<br>158699592 | 41<br>37                              | 0.77                  |
| C4685              | 239598666              | 37<br>94                              | 0.39<br>3.48          |
| C4687              | 245298428              | 13                                    | 0.51                  |
| C4713              | 249398457              | 24                                    | 2.02                  |
| C4743              | 240498462              | 13                                    | 0.17                  |
| C4792              | 236698644              | 2                                     | 0.02                  |
| C4804              | 241298562              | 7                                     | 0.37                  |
| C4812              | 236298647              | 9                                     | 0.09                  |
| C4850              | 240598675              | 20                                    | 0.66                  |

| BOREHOLE<br>NUMBER | GRID<br>REFERENCE | TRANSMISSIVITY<br>(m <sup>2</sup> /d) | PERMEABILITY<br>(m/d) |
|--------------------|-------------------|---------------------------------------|-----------------------|
| C4863              | 242698425         | 13                                    | 0.45                  |
| C4881              | 244898498         | 4                                     | 0.08                  |
| C4897              | 186399123         | 2                                     | 0.07                  |
| C4924              | 181599665         | 48                                    | 1.94                  |
| C4927              | 244298536         | 11                                    | 0.61                  |
| C4966              | 242998465         | 33                                    | 2.37                  |
| C4968              | 242898502         | 40                                    | 0.73                  |
| C4981              | 243098440         | 20                                    | 0.46                  |
| C4986              | 208599092         | 14745                                 | 304.01                |
| C4989              | 208699093         | 3104                                  | 134.98                |
| C4997              | 243098438         | 11                                    | 1.04                  |
| C5002              | 219799293         | 34                                    | 0.45                  |
| C5029              | 159599596         | 2                                     | 0.03                  |
| C5111              | 188399650         | 256                                   | 1.51                  |
| C5117              | 239798502         | 10                                    | 0.10                  |
| C5143              | 178999694         | 184                                   | 1.75                  |
| C5161              | 245198436         | 6                                     | 0.05                  |
| C5175              | 240898752         | 10                                    |                       |
| C5206              | 159699588         | 74                                    | 1.19                  |
| C5257              | 154899236         | 15                                    | 0.25                  |
| C5343              | 237798687         | 69                                    | 2.66                  |
| C5348              | 238498672         | 53                                    | 8.51                  |
| C5375              | 239798630         | . 22                                  | 2.75                  |
| C5411              | 240098645         | 8                                     | 1.28                  |
| C5520              | 227399406         | 14                                    | 0.49                  |
| C5564              | 240798418         | 2                                     | 0.18                  |
| C5798              | 239998442         | 25                                    | 0.37                  |
| C6056              | 160699252         | 7                                     | 0.05                  |
| C6211              | 240398471         | 23                                    | 0.42                  |
| C6213              | 238298697         | · 13                                  | 0.31                  |
| C6300              | 226499149         | 3                                     | 0.10                  |
| C6377              | 239798483         | 3                                     | 0.02                  |
| C6378              | 236998606         | 54                                    | 4.14                  |
| C6494              | 239198478         | 196                                   | 2.36                  |
| C6524              | 240998525         | 247                                   | 5.37                  |
| C6613              | 237698684         | 6                                     | 0.11                  |

## Appendix 7 - List of Geochemical Sampling Sites (BGS and UNDP) including Grid Reference and Sample Source

| SITE NO. | BGS<br>Hydrochem<br>Ref | SITE NAME              | GRID REF   | SAMPLE SOURCE           |
|----------|-------------------------|------------------------|------------|-------------------------|
|          |                         |                        | <u> </u>   |                         |
| 1        | 85/967                  | Little Magadi l        | AJ973092   | Spring, 85 <sup>0</sup> |
| 2        | 85/968                  | Little Magadi 2        | AJ970094   | Spring, 81 <sup>0</sup> |
| 3        | 85/973                  | Little Magadi 3        | AJ967092   | Spring, 85 <sup>0</sup> |
| 4        | 85/974                  | Little Magadi 4        | AJ968090   | Spring, 81 <sup>0</sup> |
| 5        | 85/975                  | Little Magadi 5        | AJ965099   | Spring, 79 <sup>0</sup> |
| 6        | 85/976                  | Little Magadi 6        | AJ962098   | Stream, 83 <sup>0</sup> |
| 7        | 85/977                  | Little Magadi 7        | AJ961101   | Spring, 82 <sup>0</sup> |
| 8        | 85/978                  | Little Magadi 8        | AJ962105   | Spring, 830             |
| 9        | 85/971                  | NW Lagoon l, L. Magadi | AH903954   | Spring, 45 <sup>0</sup> |
| 10       | 85/972                  | NW Lagoon 2, L. Magadi | AH904933   | Spring, 44 <sup>0</sup> |
| 11       | 85/982                  | NE Lagoon l, L. Magadi | BJ001059   | Spring, 670             |
| 12       | 85/983                  | NE Lagoon 2, L. Magadi | AJ999054   | Spring, 60°             |
| 13       | 85/980                  | Magadi E2              | AH963834   | Spring, 40°             |
| 14       | 85/981                  | Magadi E2              | AH964835   | Spring, 390             |
| 15       | 85/984                  | Magadi E3              | AH999888   | Spring, 34 <sup>0</sup> |
| 16       | 85/965                  | Bird Rock l, L. Magadi | AH948794   | Spring, 41 <sup>0</sup> |
| 17       | 85/966                  | Bird Rock 2, L. Magadi | AH948794   | Spring, 41 <sup>0</sup> |
| 18       | 85/979                  | Magadi Sl              | AH919783   | Spring, 45 <sup>0</sup> |
| 19       | 85/986                  | Magadi Causeway        | AH970921   | Lake, surface brine     |
| 20       | 85/969                  | Ewasongiro             | AG714957   | River, ambient          |
| 21       | 85/970                  | Oloibortot             | AJ712001   | River, ambient          |
| 22       | 85/985                  | Oltepesi               | BJ181278   | Borehole, ambient       |
| 23       | 85/987                  | Olorgesailie           | BJ156256   | Rain                    |
| 24       | 85/998                  | Naivasha               | BK109150   | Lake                    |
| 25       | 85/993                  | C4635, Kijabe RVA      | BJ32 95    | Borehole, 350           |
| 26       | 85/991                  | Kijabe, Spring         | BJ318980   | Spring, 430             |
| 27       | Ŗ5/992                  | Kijabe, Stream         | BJ318980   | Stream, ambient         |
| 28       | 85/995                  | Mayer's Farm           | BJ31 82    | Spring, 28 <sup>0</sup> |
| 29       | 85/994                  | Mount Margaret         | BJ273887 · | Fumarole                |
| 30       | 85/997                  | Suswa, S. Slope        | BJ022693   | Shallow well            |
| 31       | 85/996                  | Akira Ranch            | BJ082903   | Fumarole                |
| 32       | 85/990                  | Ewasongiro             | AJ077730   | River, ambient          |
| 33       | 85/988                  | Majiyamoto l           | ZP013521   | Spring, 51 <sup>0</sup> |
| 34       | 85/989                  | Majiyamoto 2           | ZP013522   | Spring, 52 <sup>0</sup> |
| 35       | 86/596                  | Kariandusi             | AK988527   | Spring, 40°             |
| 36       | 86/597                  | Kariandusi             | AK977530   | Spring, 23 <sup>0</sup> |
| 37       | 86/598                  | Meroronyi              | AK894699   | Spring, 30°             |
| 38       | 86/599                  | Meroronyi              | AK893699 · | Spring, 24 <sup>0</sup> |
| 39       | 86/600                  | Chamuka                | AK93 69    | Spring, 29 <sup>0</sup> |
| ` 40     | 86/601                  | Ngosorr                | AK778660   | River                   |
| 41       | 86/602                  | Elmenteita             | AK938485   | Spring, 45 <sup>0</sup> |
| 42       | 86/603                  | Elmenteita             | AK938485   | Spring, 380             |
| 43       | 86/604                  | Eburru                 | AK966335   | Fumarole                |
| 44       | 86/605                  | Lorusio Sl             | AM788387   | Spring, 770             |
| 45       | 86/606                  | Lorusio S2             | AM788387   | Spring, 81°             |
| 46       | 86/607                  | Lorusio Nl             | AM788388   | Spring, 76°             |
| 47       | 86/608                  | Lorusio N2             | AM788388   | Spring, 750             |

| SITE NO.    | BGS<br>Hydrochem<br>Ref | SITE NAME      | GRID REF                | SAMPLE SOURCE  |
|-------------|-------------------------|----------------|-------------------------|--|
|             |                         |                |                         |  |
| 48          | 86/609                  | Kapedo Sl      | AM776298                | Spring, 500  |
| 49          | 86/610                  | Kapedo S2      | AM776298                | Spring, 500  |
| 50          | 86/611                  | Kapedo S3      | ^ AM778293 <sup>^</sup> | Spring, 27 <sup>0</sup>                                |
| 51          | 86/612                  | Kapedo N       | AM780306                | Spring, 50 <sup>0</sup>                                |
| 52          | 86/613                  | Kapedo         | AM767293                | River  |
| 53          | 86/614                  | Bala S2        | XQ696515                | Spring, 72 <sup>0</sup>                                |
| 54          | 86/615                  | Bala S2        | XQ696515                | Spring, 35 <sup>0</sup>                                |
| 55          | 86/616                  | Bala S3        | XQ697514                | Spring, 58 <sup>0</sup>                                |
| 56          | 86/617                  | Bala S3        | X0697514                | Spring, 75 <sup>0</sup>                                |
| 57          | 86/618                  | Bala S4        | XQ686513                | Spring, 36 <sup>0</sup>                                |
| 58          | 86/619                  | Homa Limeworks | XQ62 43                 | Lake Victoria  |
| 59          | 86/620                  | Simbi, Kisumu  | XQ82 59                 | Lake Simbi   |
| 60 ·        | 86/621                  | Homa Bay       | XQ62 43                 | Lake Victoria  |
| 61          | 86/622                  | Bogoria SE     | AL 79 23                | Spring, 970  |
| 62          | 86/623                  | Bogoria SE     | AL79 21                 | Stream   |
| 63          | 86/624                  | Bogoria S      | AL78 20                 | Stream   |
| 64          | 86/625                  | Bogoria SW     | AL77 23                 | Spring, 45 <sup>0</sup>                                |
| 65          | 86/626                  | Bogoria l      | AL77 25                 | Lake   |
| 66          | 86/627                  | Bogoria 2      | AL76 27                 | Lake   |
| 67 `        | 86/628                  | Bogoria 3      | AL75 37                 | Lake   |
| 68          | 86/629                  | Bogoria Wl     | AL75 27                 | Spring, 960  |
| 69          | 86/630                  | Bogoria W2     | AL75 29                 | Spring, 960  |
| 70          | 86/631                  | Baringo        | AL72 68                 | Lake   |
| 71          | 86/632                  | Olkokwe Island | AL76 69                 | Spring, 94 <sup>0</sup>                                |
| 72          | 86/633                  | Emerit         | BJ19 41                 | Borehole, 370  |
| 73          | 86/634                  | Magadi N       | AJ98 05                 | Spring, 630  |
| 74          | 86/635                  | Magadi NW      | AH90 95                 | Spring   |
| 75          | 86/636                  | Oltepesi       | BJ181278                | Borehole   |
| 76          | 86/637                  | Naivasha       | BK12 15                 | Lake   |
| 77          | 86/638                  | Nasagum        | ZR31 52                 | River  |
| 78          | 86/639                  | Tigeri         | ZR31 52                 | River  |
| 79          | 86/640                  | Malewa         | BK090264                | River  |
| 80          | 86/661                  | C4989          | BK086094                | Borehole, 210  |
| 81          | 86/663                  | C567           | BK139096                | Borehole, 220  |
| 82          | 86/664                  | C4178          | BK131233                | Borehole, 20°  |
| 83          | 86/665                  | C563           | AK959105                | Borehole, 260  |
| 84          | 86/666                  | C1487          | BK156126                | Borehole, 210  |
| 85          | 86/667                  | C5002          | BK198293                | Borehole, 20°  |
| 86          | 86/668                  | C1063          | AK983202                | Borehole, 260  |
| 87          | 86/669                  | C1488          | BK180223                | Borehole, 260  |
| 88          | 86/670                  | C467           | BK156142                | Borehole, 240  |
| 89          | 86/671                  | C580           | BK144146                | Borehole, 250  |
| 90          | 86/672                  | C814           | BK200243                | Borehole, 180  |
| 91          | 86/673                  | Kanyamwi Farm  | BK021552                | Spring, 24 <sup>0</sup>                                |
| 92          | 86/674                  | C570           | BK022552                |  |
| 93          | 86/675                  | C3784          | BK087706                | Borehole, 220  |
| 94          | 86/676                  | C307           | AK723638                | Borehole, 23 <sup>0</sup><br>Borehole, 19 <sup>0</sup> |
| 95          | 86/677                  | C1190          | AK723636<br>AK704612    |  |
| 96          | 86/678                  | P65            |                         | Borehole, 240  |
| 97          |                         | C3955          | BK342121                | Borehole, 230  |
| 98 .        | 86/679                  |                | ZQ132657                | Borehole, 230  |
| <i>70</i> . | 86/680                  | C2063          | BK306099                | Borehole   |

| SITE NO.     | BGS<br>Hydrochem<br>Ref | SITE NAME                     | GRID REF   | SAMPLE SOURCE             |
|--------------|-------------------------|-------------------------------|------------|---------------------------|
| 99           | 86/681                  | C4179                         | BJ425425   | Borehole, 260             |
| 100          | 87/218                  | Cl4O4, Ndabibi                | AK902155   | Borehole, 26 <sup>0</sup> |
| 101          | 87/219                  | Kokot, Maiella                | · AJ878992 | Gallery, ambient          |
| 102          | 87/220                  | Nakuru                        | AK787629   | Lakewater                 |
| 103          | 87/22].                 | Hell's Gate (Ol Njorowa)      | BJ012954   | Seepage                   |
| 104          | 87/222                  | Hell's Gate (Ol Njorowa)      | BJ017965   | Seepage, 200              |
| 105          | 87/223                  | Hell's Gate (Ol Njorowa)      | BJ016973   | Seepage                   |
| 106          | 87/224                  | Hell's Gate (Ol Njorowa)      | BJ015977   | Seepage, 520              |
| 107          | 87/225                  | Hell's Gate (Ol Njorowa)      | BJ011992   | Seepage, 320              |
| 108          | 87/226                  | Hell's Gate (Ol Njorowa)      | BK015010   | Seepage, 230              |
| 109          | 87/227                  | Hell's Gate (Ol Njorowa)      | BK014007   | Seepage, 72 <sup>0</sup>  |
| 110          | 87/368                  | Well 2, Olkaria               | BK00070015 | Geothermal well           |
| 111          | 87/369                  | Well 26, Olkaria              | BK01110244 | Geothermal well           |
| 112          | 87/370                  | Well 22, Olkaria              | BK01100114 | Geothermal well           |
| 113          | 87/371                  | Well 16, Olkaria              | BK00620107 | Geothermal well           |
| 114          | 87/372                  | Well 23, Olkaria              | BK01300167 | Geothermal well           |
| 115          | 87/373                  | Well <sup>-</sup> 21, Olkaria | BK00840086 | Geothermal well           |
| 116          | 87/374                  | Well 5, Olkaria               | BK00260120 | Geothermal well           |
| 117          | 87/375                  | Well 10, Olkaria              | BK00260161 | Geothermal well           |
| 118          | 87/382                  | Lanet, Nakuru No. 7 W.S.      | AK797664   | Borehole, 28 <sup>0</sup> |
| 119 .        | 87/376                  | EF-2, Eburru                  | AK946297   | Fumarole                  |
| 120          | 87/377                  | EF-13, Eburru                 | AK947315   | Fumarole                  |
| 121          | 87/378                  | C431, ADC Farm                | AK826389   | Borehole, 37 <sup>0</sup> |
| 122          | 87/379                  | Cl798, ADC Farm               | AK811405   | Borehole, 350             |
| 123          | 87/383                  | West Olkaria Fumarole         | AK968993   | Fumarole                  |
| 124          | 87/380                  | DEL, Soysambu                 | AK857430   | Borehole, 320             |
| 125          | 87/381                  | Cl990, Soysambu               | AK889428   | Borehole, 28 <sup>0</sup> |
| 126          | 87/384                  | F-3, Suswa                    | BJ056776   | Fumarole                  |
| 127          | 87/385                  | F-15, Domes                   | BJ063983   | Fumarole                  |
| 128          | 87/386                  | F-23, Longonot                | BJ164998   | Fumarole                  |
| 129          | 87/387                  | C3525, Mosiro                 | AJ811475   | Borehole, ambient         |
| F-1          |                         | Suswa, caldera floor          | BJ063760   | Fumarole                  |
| F-2          |                         | Suswa, caldera rim            | BJ072778   | Fumarole                  |
| F-3          | •                       | Suswa, caldera rim            | BJ056776   | Fumarole                  |
| F-4          |                         | Suswa, caldera rim            | BJ026764   | Fumarole                  |
| F-5          |                         | Suswa, caldera floor          | BJ046759   | Fumarole                  |
| F-6          |                         | Suswa, caldera floor          | BJ073751   | Fumarole                  |
| F-7          |                         | Suswa, caldera rim            | BJ062780   | Fumarole                  |
| F-8          |                         | Suswa, ring graben            | BJ027732   | Fumarole                  |
| F-9          |                         | Suswa, caldera rim            | BJ003751   | Fumarole                  |
| F-10         |                         | Suswa, caldera rim .          | BJ042775   | Fumarole                  |
| F-11         | •                       | Suswa, caldera rim            | BJ053775   | Fumarole                  |
| F-12         |                         | Suswa, ring graben            | BJ041744   | Fumarole                  |
| F-13         |                         | Suswa, ring graben            | BJ045708   | Fumarole                  |
| F-14         |                         | Suswa, ring graben            | BJ042713   | Fumarole                  |
| F-15<br>F-16 |                         | Domes                         | BJ063983   | Fumarole                  |
|              |                         | Domes                         | BJ061982   | Fumarole                  |
| F-17<br>F-18 |                         | Domes                         | BJ051972   | Fumarole                  |
| F-18<br>F-19 |                         | Hell's Gate (Ol Njorowa)      | BJ010959   | Fumarole                  |
| F-20         |                         | Hell's Gate (Ol Njorowa)      | BJ008953   | Fumarole                  |
| r –2U        |                         | Domes                         | BJ041989   | Fumarole                  |

| SITE NO. | BGS<br>Hydrochem<br>Ref | SITE NAME                | GRID REF             | SAMPLE SOURCE           |
|----------|-------------------------|--------------------------|----------------------|-------------------------|
| F-21     |                         | Domes                    | BJ045971             | Fumarole                |
| F-22     |                         | Domes                    | BJ016974             | Fumarole                |
| F-23     |                         | Longonot, crater         | BJ164998             | Fumarole                |
| F-24     | 1. 1. m                 | Longonot, crater         | BJ173986             | Fumarole                |
| F-25     |                         | Longonot, crater         | BJ171999             | Fumarole                |
| F-26     |                         | Longonot, S.E. slopes    | BJ187944             | Fumarole                |
| F-27     |                         | Mount Margaret           | BJ272884             | Fumarole                |
| F-28     |                         | Suswa, central island    | BJ072740             | Fumarole                |
| F-29     |                         | Suswa, S. slopes         | BJ056635             | Fumarole                |
| F-30     |                         | Suswa, central island    | BJ076736             | Fumarole                |
| H-1      |                         | Akira Ranch              | BJ082904             | Borehole, steam         |
| H-2      |                         | Hell's Gate (Ol Njorowa) | BJ010948             | Borehole, steam         |
| K-1      |                         | Meru, Kingua l           | E. side<br>Mt. Kenya | Spring, 21 <sup>0</sup> |
| K-2      |                         | Meru, Kingua 2           | E. side<br>Mt. Kenya | Spring, 19 <sup>0</sup> |

 $<sup>\</sup>mathsf{F}$ ,  $\mathsf{H}$  and  $\mathsf{K}$  prefixes - samples collected by  $\mathsf{Dr}$   $\mathsf{H}$  Armannsson of the UNDP