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Floodplain Mapping - Model Study of the River Frome (Gloucestershire)

Final Report
Volume 1

Report EX 3191
August 1995



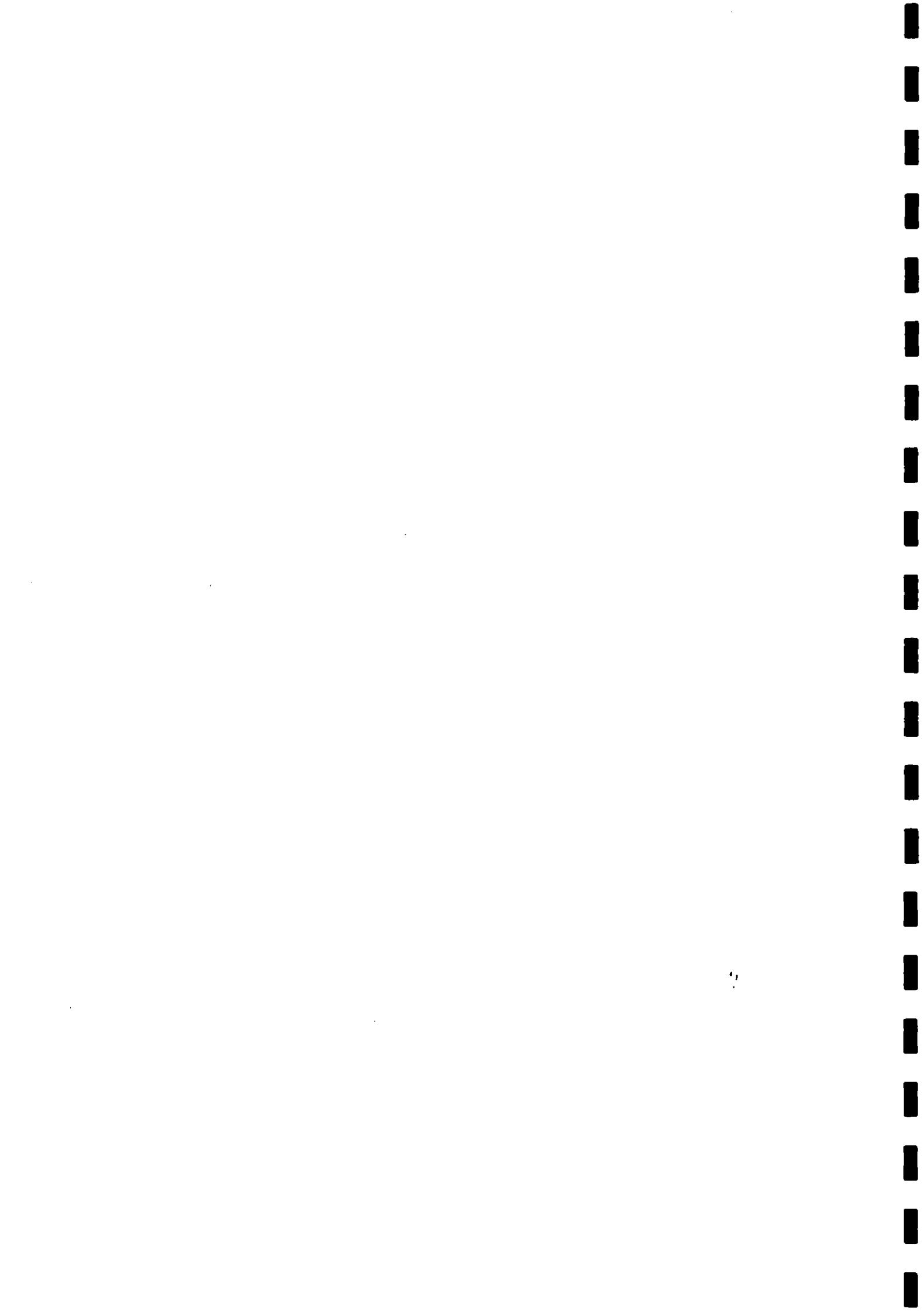




Floodplain Mapping - Model Study of the River Frome (Gloucestershire)

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Contract

This report describes the "Floodplain Mapping - Model Study of the River Frome" carried out by Wallingford Water and commissioned by the National Rivers Authority - Severn Trent Region. The NRA representative was Mr D Pettifer, and Wallingford Water was represented by Mr TE Parkinson and Mr RJ Millington. The HR Wallingford job number was RQR 1568. The work was carried out by Mr PG Hollinrake (HR), Mr RJ Millington (HR) and Miss HA Houghton-Carr (IH).

Prepared by R.J.MILLINGTON
(name) JENNER MARELLER
(Job title)

Approved by D.M.BAMFORTH GRAPHIC MANAGER

Date 7-9-95

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Summary

**Floodplain Mapping - Model Study of the River Frome (Gloucestershire)
Final Report**

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In September 1993 the National Rivers Authority - Severn Trent Region commissioned Wallingford Water, the joint venture between the Institute of Hydrology and HR Wallingford, to carry out the "Floodplain Mapping, Model Study of the River Frome (Gloucestershire)" study.

This report gives a detailed description of the hydraulic modelling components of the study, and provides a summary of the hydrological components which are presented in detail in Report EX3171. The objective of the study was to develop a computational hydraulic model for the purposes of identifying flooded outlines for events of various return periods. The hydraulic model was constructed using the SALMON-F modelling software, modified to cope with supercritical flows, and was calibrated using observed data from three events, as well as data available from the physical modelling study of the Ebley Mill gauging station, presented in Report EX3170.

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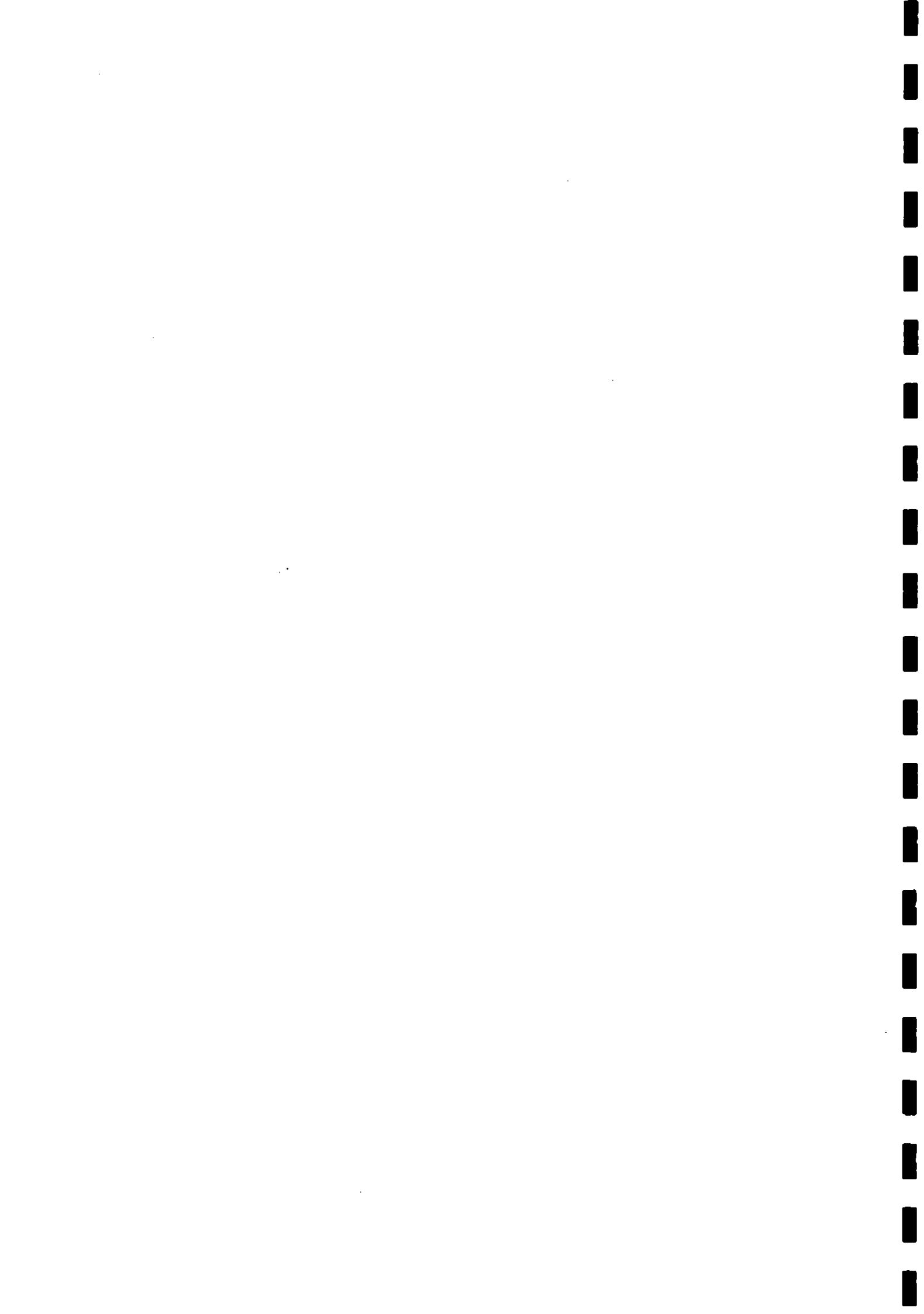
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1 Introduction

1.1 Background

In September 1993 the National Rivers Authority - Severn Trent Region (NRA-ST) commissioned Wallingford Water (WW), the joint venture between the Institute of Hydrology and HR Wallingford Ltd, to carry out the "Floodplain Mapping, Model Study of the River Frome (Gloucestershire)" study. The overall objective of the study was to construct and prove a hydraulic model of the River Frome and a part of its tributary, the Nailsworth Stream, in order to determine the flood plain limits for six design events of specified return periods of between 5 and 150 years.

This report presents the results of the hydraulic modelling, including a summary of the hydrological aspects of the overall study.

1.2 Terms of reference

The terms of reference for the overall study are defined in the NRA-ST document "Brief for Report and Advisory Works. Floodplain Mapping - Model Study of the River Frome (Gloucestershire)" of July 1993, the WW proposal to undertake the study of August 1993 and the NRA-ST letter of appointment dated 24 September 1993. The terms of reference for the study can be summarised as follows:

- (a) To identify current data availability for the Frome catchment, including hydrological, hydrometric, topographical and structure data. Also to determine the requirement for further survey data required to complete the model study.
- (b) To undertake a hydrological study to identify suitable calibration events for the modelling, and thereby to derive calibration and design inflows for the hydraulic modelling.
- (c) To set up and calibrate a hydrodynamic model of the River Frome between the Main River Limit at Whitehall Bridge and the flapped outfall into the River Severn, and of the Nailsworth Stream between Egypt Mill and its confluence with the River Frome.
- (d) To determine the flood levels for the 1 in 5, 1 in 10, 1 in 25, 1 in 50, 1 in 100 and 1 in 150 return period flood events and plot these on 1:2500 scale plans of the River Frome.
- (e) To identify where existing residential and commercial property is at risk from flooding in a 1 in 100 year flood event.
- (f) To produce a reduced hydrodynamic model of the Lower Frome to investigate the effects of flows from the Gloucester and Sharpness canal in relation to flows in the River Frome and levels in the River Severn.

1.3 The River Frome

The Frome catchment extends from the Cotswold escarpment in the east, on the boundary of the Thames and Severn-Trent regions of the NRA, through to the River Severn in the west. A plan of the catchment and river system is shown in Figure 1.

The River Frome rises in the north-east of the catchment, high up on the Cotswold escarpment, and flows southwards. After about 10km the river turns westwards for another 10km or so, during which it is joined by two tributaries from the north, the Holly Brook and the Toadsmoor Brook. The Holly Brook confluence is immediately downstream of the Main River Limit at Whitehall Bridge. Along much of this stretch the river runs parallel to the now disused Thames and Severn Canal. The river then turns northwards for about 5km towards Stroud, the largest town in the catchment, and then westwards again to Ebley Mill gauging station. Ebley Mill is the only gauging station in the catchment, and has a catchment area of 198km². Just upstream of Ebley Mill the river is joined by the Nailsworth Stream from the south and the Dudbridge Bypass channel from the north. The flood relief channel is part of the old Stroudwater Canal and carries the flows from three northern tributaries, the Randwick Stream, the Painswick Stream and the Slad Brook.

Downstream of Ebley Mill the river continues in a north-westerly direction for a further 10km towards its confluence with the River Severn. Along much of this stretch the river runs parallel to the now disused Stroudwater Canal. About 1km before the confluence, there is a flow diversion into the Gloucester and Sharpness Canal for water supply to the Bristol area. The total catchment area upstream of the River Severn outfall is approximately 226km².

The Frome catchment is characterised by steep valley sides sloping down to the river below and small, fast-flowing streams, particularly in the upper reaches. The catchment lies on heavily fissured, oolitic limestone and liassic sandstone bedrock which dips from the Thames basin into the Frome basin. The limestone is thought to act like a sponge, absorbing water until the aquifers are filled; heavy rain may take several days to have an effect, and water lost in the upper reaches may well reappear further downstream. The soils tend to be well-drained and calcareous, with clayey, loamy and stony components. In the downstream part of the catchment some non-calcareous soils are also present.

The catchment is predominantly agricultural in nature, though urban areas account for around 10% of all land use. Bailey, Reference 1, assigned 50% of the catchment to permanent grassland and 15% to temporary grassland, with another 10% to woodland. The remainder is made up of crop-growing areas and open water such as canals and lakes. The Stroud conurbation extends for some distance along the nearby valley bottoms, as does the smaller town of Nailsworth in the south of the catchment. There are also numerous small villages.

The river system itself can be visualised in terms of four reaches of differing characteristics.

Frampton to Chalford Reach

This is the uppermost reach of the River Frome and is distinguished by the general absence of floodplain development and a limited number of control structures. The floodplain is relatively narrow and is shared with the relict Thames and Severn Canal, which is thought to carry a proportion of the flow in a flood event. The reservoir at Bakers Mill originally built to feed the canal is one

of the major features of the reach and the operation of the sluices at this location may impact on downstream flooding. The downstream end of the reach is characterised by housing development adjacent to the floodplain, and a history of flooding of the gardens of these properties. The end of the reach can be considered as the bridge at the main Stroud - Cirencester Road.

Chalford to Ebley Reach

From Chalford to Bowbridge the Frome is characterised by a generally narrow floodplain and the large number of control structures and mill buildings. These are at their most dense in the vicinity of Thrupp and the channel frequently splits into two channels to provide separate flow paths around and through these. The majority of the mills are disused and many of the controlling structures have been rationalised in order to reduce the need for maintenance and operation. A number of the structures are derelict and inoperable. The Thames and Severn canal is intermittent in this reach, though there appear to be a number of locations where interaction between the canal and river could take place given sufficiently high flows. Much of the floodplain is developed, and this includes both areas of housing and industrial development of varying age. The end of the reach is marked by the culvert carrying the river under the new Dudbridge road, and its confluence with the Nailsworth Stream.

Ebley to the River Severn

This reach sees a marked change in the size of the river, predominantly due to the inflows of the Nailsworth Stream and Dudbridge Bypass channel in close proximity to each other. Upstream of the Nailsworth Stream confluence the floodplain remains relatively narrow and a number of mill structures occur but downstream of this point the floodplain begins to expand and the mills become less frequent. Downstream of Ebley Corn Mill the river bifurcates into distinct north and south channels, and these do not have a confluence until Churchend, close to the M5 motorway. These channels in turn have a number of subsidiary bifurcations, in particular the Banty Ditch which flows in-between the two channels downstream of Ryeford. The enclosed floodplain is in the main undeveloped, and is generally lower lying than the water level in the bounding channels.

Downstream of Churchend the river reverts to a single channel within a relatively wide floodplain and the river is embanked to varying degrees. The embanking is particularly pronounced downstream of Fromebridge Mill where low lying land on the Severn floodplain is protected. At Whitminster part of the river flow is split by a control structure into the old Stroudwater canal and from there into the Gloucester and Sharpness canal which provides the water supply for Bristol. The remaining flow passes into twin channels which cross under the Gloucester and Sharpness canal by siphon and then discharge into the River Severn via a tide flap. The area downstream of the canal and enclosed by the two channels is a flood storage area designed to alleviate the possibility of overtopping of the main embankments onto the Severn floodplain.

The Nailsworth Stream

The Nailsworth stream is the largest of the Frome tributaries and is similar in characteristics to it. The stream flows through a small valley which it shares throughout most of its length with the main Stroud - Nailsworth road. In its upper reaches between Egypt Mill and Dunkirk Mill the channel is split and flows on either side of disused mill ponds which are now heavily vegetated. The confluence of the channels occurs within a culvert at the Critchley's site upstream of Merrett's Mills and downstream of here the river is predominantly within a

single channel. There are a number of mill structures though the control structures on these are predominantly redundant. The floodplain is restricted both by the proximity of the road and by the presence of new housing development. At the Erinoid works the channel enters a long culvert before re-emerging and then passing through a second culvert upstream of its confluence with the River Frome. The stream drops over a weir into the old channel of the River Frome at Dudbridge then passes under the new Dudbridge road by culvert to join the River Frome.

2 Hydrological investigation

2.1 Introduction and approach to hydrological study

This section summarises the hydrological review of the Frome catchment which is described in full in the "Hydrological Study", Report EX 3171. The review made use of all available data to develop the best possible estimates of the design flood inflows required by the hydraulic model, and also incorporated a routing model of the Frome catchment and a physical model of the Ebley Mill gauging station. The methods of flood estimation adopted were those of the FSR and associated documents. The FSR rainfall-runoff method, whereby rainfall is converted to flow using a deterministic model of catchment response (the unit hydrograph and losses model), was used for the hydrological modelling because it synthesises the entire flow hydrograph, which is required in cases such as this where flood routing is involved.

The three parameters of the unit hydrograph and losses model are:

- T_p - time-to-peak of the unit hydrograph which determines how quickly the catchment responds to effective rainfall input
- PR - the percentage runoff which is the ratio of total to effective rainfall i.e. the proportion of the total rainfall input which becomes response runoff in the river. PR is divided into two parts: a standard part SPR and a dynamic part DPR
- ANSF - the average non-separated flow or baseflow which represents the flow in the river before the event started.

The model parameters are related via multiple regression equations to physical and climatic characteristics of the catchment, enabling flood estimates to be made at ungauged sites. However, the FSR recommends that where possible such no-data estimates are refined using observed data from or near to the site of interest. There are three main ways in which these local data may be used, all of which were used in the hydrological study:

- direct estimation of the model parameters at the subject site through analysis of observed flood events
- indirect estimation of the model parameters at the subject site through estimation of hydrological characteristics which are related to the model parameters i.e. catchment lag time is closely related to T_p , whilst baseflow index is similarly related to SPR
- transfer of information from neighbouring catchments.

2.2 Physical modelling of Ebley Mill gauging station

The initial phase of the hydrological study involved a review of the out-of-bank rating in use for the Ebley Mill gauging station. This was required for the purpose of accurately assessing the magnitude of flows which were greater than bankfull, and therefore beyond the range of the current rating curves. Under flood conditions the weir, and the cableway site 90m upstream which is used to calibrate the weir for in-bank flows, is bypassed by flow over the left bank floodplain. The work was carried out using a physical model and the main conclusions of the study were as follows:

- the existing rating for the station was suitable for flows up to 20m³/s (ie all recorded flows to date)
- the rating derived from the physical model should be used for all flows in excess of this (ie over bankfull).

The results of the physical modelling are presented in full in the "Ebley Mill Gauging Station Physical Model Study", Report EX 3170.

2.3 Data collection and processing

Both flood peak and flood event data were available for, and used in, the hydrological study. The flood peak data were available in the form of annual maxima data and peaks-over-threshold series. The flood event data typically required for analysis include flow data for the event, recording raingauge data for the event, daily raingauge data for both the event and the five days preceding it, and estimated soil moisture deficit data at 09:00 on the first day of the event. Full details of the events selected and the flood event analysis are given in the Hydrology Report. The locations of gauges and stations from which data were collected are shown in Figure 2.

Flow data were derived from stage data at Ebley Mill gauging station using the appropriate rating equations. The flow record was continuous from January 1969 up to the present day, and data up to January 1994 were collected, thus providing 24 complete water years of data. Major floods are known to have occurred during the 1950's and 1960's, prior to installation of the gauging station, but unfortunately very little information concerning these events was available. Some stage data from six continuous level recorders within the catchment were also available.

The raingauge coverage of the Frome catchment is adequate and generally better for daily gauges than for recording gauges. For a number of mid-1980's events only one recording gauge, usually some distance from the catchment, was operational whereas the daily gauges were spread fairly evenly across the catchment. The only long-term recording raingauge within the Frome catchment is at Miserden in the north-east of the catchment. There are, however, four long-term recording raingauges nearby at Dowdeswell, Longford and Netheridge, all to the north, and at Kingswood to the south-west. In addition, three new recording raingauges were installed within the catchment during May and June 1993 at Painswick Lodge in the north, at Eastington Park in the east, and at Avening Court in the south. Daily rainfall data from raingauges within or close to the Frome catchment were also obtained.

Estimates of soil moisture deficit at the beginning of each selected flood event were obtained from three sites: Cheltenham to the north, Cirencester to the south-east, and Monmouth to the west on the Welsh side of the River Severn.

Physical and climatic characteristics of the catchments were derived from maps to enable no-data estimates of the model parameters to be made using FSR regression equations. These catchment characteristics are tabulated in the full hydrological report.

2.4 Derivation of model parameters

The model parameters for the catchment to Ebley Mill were estimated directly by analysis of observed flood events, and are presented in Table 1. The derived model parameters showed considerable variation, indicating the dominating influence of the downstream urban areas. Many of the flood peaks are clearly the products of rapid urban runoff from the Stroud conurbation, which reach the gauging station and pass before the rural runoff component has travelled downstream. This made it necessary to divide the flood events into a group where the flow peak was caused by urban runoff, and a group where the entire catchment was believed to be responding. This separation was done on the basis of mean catchment lag time, as indicated in Table 1, and reduced the variability in the derived model parameters. Table 2 shows that the unit hydrograph time-to-peak was some 44% lower than the value estimated from catchment characteristics, whilst the standard percentage runoff was some 75% lower than the value derived from catchment characteristics. Similarly the catchment characteristics method overestimated the baseflow by around 30%.

In another approach, hydrological characteristics which are related to the model parameters were estimated. The catchment lag analysis at Ebley Mill gave time-to-peak values which agreed closely with those derived by flood event analysis, as shown in Table 2. Lag analysis from the continuous level recorders in the catchment gave inconclusive results. Standard percentage runoff derived from BFI was similar to the value derived from catchment characteristics, whilst the value derived from the new HOST classification was some 60% higher, again as shown in Table 2.

The model parameter values derived from the rainfall-runoff analysis were taken as the best estimate of the true values for the Frome catchment to Ebley Mill. The limits of the hydrodynamic model divided the Frome catchment naturally into six subcatchments: Upper Frome, Toadsmoor Valley, Slad Brook, Painswick Stream, Randwick Stream and Nailsworth Stream, as shown in Figure 3. The model parameter information was transferred to each of these six subcatchments by simply applying the ratio of the observed value to the no-data estimate of the value at Ebley Mill to the no-data estimate for the particular subcatchment. The model parameter values for each of the subcatchments are given in Table 3.

The transfer was straightforward for four of the subcatchments, where the observed value used was that from the events showing a combined rural and urban response, but more complicated for the Slad Brook and Nailsworth Stream which both have a fairly large rural area with an urban area concentrated at the catchment outfall. For these two subcatchments it was necessary to model the rural and urban responses separately, with the rural parts modelled in the same way as for the other four subcatchments, and the urban parts modelled in the corresponding way, but where the observed value used was that from the events resulting solely from urban runoff. The two hydrographs produced for each of these subcatchments were added together to give the total subcatchment hydrograph. Four remaining areas were modelled as diffuse lateral inflows, with their hydrographs modelled on those for the Nailsworth Stream subcatchment, as described in the Hydrology Report.

2.5 Derivation of calibration inflows and design inflows

Inflow hydrographs were derived for calibration of the hydraulic model, and for the six return period design flood events. Three calibration events were chosen occurring in December 1965, May 1979 and January 1994, and inflow hydrographs were generated for each of the subcatchments using the observed rainfall and soil moisture deficit data. Inflow hydrographs for return periods of 5, 10, 25, 50, 100 and 150 years were generated for each of the subcatchments using FSR design rainfall statistics.

The predicted calibration event inflow hydrographs for the May 1979 and January 1994 events were verified using a RIBAMAN routing model of the River Frome, and checking the shapes and peak flows of the routed hydrographs at Ebley Mill. Results are presented in the Hydrology Report. The main feature apparent from the routing was the inability of the FSR model to simulate the raised baseflow component of the hydrograph which occurs after the event has passed. This baseflow is interpreted as water entering into storage unrepresented in the model for example groundwater. However, the routed inflows produced reasonable estimates of peak discharge at Ebley Mill, which were conservative in terms of the peak flow.

The full hydrodynamic model, which provides a full representation of flood plain storage and performance of structures, produced a further reduction in peak flow at Ebley Mill, possibly also associated with an increase in the length of time the hydrograph took to peak. The design events were run only with the full hydrodynamic model, due to the greater accuracy attributable to the results from this model.

2.6 Flood frequency analysis

Flood frequency analysis was carried out at Ebley Mill using both the 24 years of observed annual maxima data and a 26-year series including estimates of the July 1968 and May 1969 flood peaks. The fitted curves are presented in Figure 4.

The 24 years of observed flow data at Ebley Mill, fitted by an EV1 line, appear to be not wholly representative of the catchment. This record does not contain any of the major floods reported in the 1950s and 1960's before the gauging station was installed. The flood frequency curve fitted to the annual maxima steepens significantly, from EV1 to EV2, when the estimated 1968 flood peak is included. If the 1968 flood is typical of large floods on the catchment, then this EV2 curve may be a better representation of the true flood frequency curve of the catchment. This EV2 curve corresponds fairly closely with the curve derived from the observed mean annual flood and the region 4 growth curve.

The flood frequency curve derived from the routed design events has a higher mean annual flood, but otherwise is of similar gradient to the EV2 curve. This would be expected if large floods are missing from the observed record from which the mean annual flood was derived. The curve from routed flows corresponds fairly closely with the curve derived from the observed mean annual flood and the region 6/7 growth curve. This suggests that the behaviour of the Frome catchment may be more like that of catchments in the neighbouring Thames basin, than that of catchments in the Severn region.

A fairly narrow band can be defined which indicates the most likely position of the true flood frequency curve for the Frome at Ebley Mill. This band has a width of about $3 \text{ m}^3\text{s}^{-1}$ at the low (5-year) return period end, and widens to about $8 \text{ m}^3\text{s}^{-1}$

at 150-years return period. The flood frequency curve derived from the routed flows forms the upper limit of this band, and it may be possible to narrow the band by further data collection and analysis.

3 The hydraulic model

3.1 General description

The hydraulic model was constructed using the HR package SALMON-F, which is a general purpose river simulation model suitable for branched and looped river systems. It can include floodplains where the water level is the same on the floodplain as in the adjacent channel, or floodplains which are separated from, and have different water levels to, the river. The version of SALMON-F used for the River Frome modelling includes the ability to spill directly between adjacent channels as well as a modification to the calculation of channel flow which allows the model to cope with the occurrence of supercritical flows.

A SALMON-F model is constructed by dividing the area to be modelled into cells which can be of varying types including river, structure, junction and floodplain. The cell boundaries can be made up of river sections, embankment sections, floodplain or causeway sections or no-flow boundaries which act as a hard boundary to the flow domain. Structures can be incorporated either within structure cells, which allow multiple structure elements at a particular location, or within embankments and causeways.

It is assumed within the software that the water level is constant across any section, and that the direction of flow is perpendicular to that section. The selection of section location is therefore critical. Storage in floodplain cells is calculated from a tabulation of storage area against water depth used in conjunction with the flow into and out of the cell.

Inflows to the model are given at the upstream model boundaries, and tributary inflows can be specified between adjacent river sections. Lateral inflows can also be specified to allow a hydrograph to be input over a reach of the model. Downstream boundaries within the model require either a stage hydrograph or a rating curve.

3.2 Availability of survey data

At the outset of the study all available floodplain and channel survey data were collected from the NRA-ST offices at Tewkesbury. These data were then collated in order to identify possible shortfalls in the data availability. The data initially supplied included the following:

- contoured floodplain plans for the River Frome between the A38 and the River Severn (from the River Severn floodplain survey - Cartographical Services)
- contoured floodplain plans for the River Frome between the A38 and Chalford (Cartographical Services)
- contoured & spot height plans for the River Frome from Chalford to Whitehall Bridge
- channel and structure survey for the River Frome between Millend Mills and Stanley Mills (1984)
- channel and structure survey for the River Frome between the River Severn and Meadow Bridge, between Stanley Mills and Whitehall Bridge, and of the Dudbridge Bypass channel (Simmons Survey Partnership - 1987)

- channel survey for the River Frome between Whitminster Weir and the M5 motorway (Land Development Services - 1990)
- channel survey for the River Frome between Whitminster Weir and the A38 (NRA - 1991).

Additionally, a survey was carried out by Merrett Survey Partnership in 1992 of the following reaches of the Frome:

- River Frome right channel downstream of Whitminster House (reach 1)
- Fromebridge Mill bypass and mill channels downstream of the A38 (reaches 2 and 3)
- A38 to Millend Mill (reach 5)
- Churchend Mill bypass channel (reach 4)
- Meadow Bridge to railway upstream of Bond's Mill (reach 6)
- Bond's Mill culvert channel (reach 7)
- Railway upstream of Bond's Mill to the bifurcation downstream of Ebley Corn Mill (reach 8)
- Stanley Mills to the bifurcation downstream of Ebley Corn Mill (reach 9)
- Fromehall Mill to the Thames and Severn Canal siphon (reach 10)
- Bowbridge to Griffin Mill estate (reach 11)
- Griffin Mill estate right hand channel (reach 12)
- Phoenix Mill to Brimscombe Pond (reach 14)
- Brimscombe Port to St Marys Mills (reach 17).

The above surveys totalled c.600 sections and provided the majority of data required for the construction of the Frome hydraulic model, with some exceptions. Initially, additional survey were identified as being required for the construction of the physical model and ten sections were surveyed along the Ebley reach of the river by Cartographical Services in December 1993 for this purpose. Further data were required for the whole of the Nailsworth Stream, and for the reach of the Frome upstream of Golden Valley Lock, and also for a large number of structures throughout the River Frome valley which had either not been surveyed previously or for which the available survey data was insufficient. In total an extra 420 sections were identified as being required, 168 on the Nailsworth Stream, 39 on the upper reach of the Frome and 213 as infill for the previous surveys. The survey data were collected by HR Wallingford's survey team under a separate contract and as such details of the survey work are not given here. A set of master plans indicating the locations of all the Frome survey data has been prepared for the purposes of this study and these have been supplied separately to NRA-ST along with the surveyed section data itself.

3.3 The River Frome Models

Due to the length of the reach and the complexity of the features to be modelled, the overall model was subdivided into three separate sub-models. The Upper Frome sub-model extended from Whitehall Bridge to upstream of the Bath Road Bridge in Stroud, the Lower Frome sub-model extended from the downstream end of this first model to the outfall into the River Severn at Framilode, and the Nailsworth Stream sub-model comprised the reach of the Nailsworth Stream between Egypt Mill to downstream of the weir at the Frome confluence at Dudbridge. The schematisation of each model is described in detail in Section 3.4.

3.4 Model schematisation

The model schematisation for each of the sub-models was undertaken with regard to the need to represent the following:

- structures within the modelled reach
- areas of floodplain storage and floodplain flow separated from the channel by natural or man-made embankments
- the potential for flow between adjacent channels
- adequate representation of flow splits
- adequate resolution of the channel, particularly in steep reaches.

Schematic drawings of the River Frome models have been produced detailing the location and extent of each of the model sections, plotted at 1:2500 scale for direct comparison with the contoured plans. These drawings are presented in Volume 2 of this report and a summary of the schematisation is provided in Table 4.

The Upper Frome sub-model

The Upper Frome sub-model included a total of 482 sections, of which 343 were river sections, 110 were embankments and the remainder floodplain sections. A total of 83 structure complexes were modelled, of which 28 were bridges. The majority of the river was modelled using river sections representing both the channel and adjacent floodplain. However, 40 floodplain cells were used in the following locations:

Griffin's Mill	- a flow path overland above the mill culvert (floodplain cell 107)
Thrupp works	- a flow path around the works separated from the channel (floodplain cell 108)
Brimscombe Football Ground	- floodplain storage (floodplain cell 109)
Brimscombe Pond	- a flow path from upstream of Brimscombe Mill Pond Culvert to the channel downstream of the control sluices (floodplain cells 110, 111)
Brimscombe Port	- floodplain storage and a separate flow path around the Brimscombe Port area (floodplain cells 112, 113, 114, 115)
Wimberley Mills	- floodplain storage and a separate overland flow path avoiding the culverts (floodplain cells 116, 117)
St Marys Mill	- floodplain storage between the river and the canal upstream of St Marys House Culvert (floodplain cell 118)
Chalford Industrial Estate	- floodplain storage and overland flow route avoiding the culverts (floodplain cells 119, 120)
Golden Valley	- floodplain storage and flow route on the right floodplain between Bakers Mill and Golden Valley Lock (floodplain cells 121 to 136)
Bakers Mill	- Bakers Mill reservoir is represented by a series of floodplain cells between the canal and the river (floodplain cells 137, 138, 139, 140)

Puck Mill to Whitehall Bridge - floodplain storage and flow paths adjacent to the river (floodplain cells 141 to 147).

The disused Thames and Severn Canal was included in the model as two separate river reaches. The first of these began at the siphon downstream of Arundell Mill and continued up to the caravan park at Brimscombe. The second reach began upstream of Brimscombe Port, and then ran continuously up to the upstream model limit at Whitehall Bridge. Where interaction was possible either between adjacent branches of the river or between the river and the canal, embankments were incorporated into the model allowing direct spilling between the two channels. Spills of this type were included in the following areas:

- | | |
|---------------------|---|
| Arundell Mill | - between the canal and the millpond, and around the siphons |
| Bowbridge | - between the canal and the river in the area of Bowbridge housing estate |
| Griffin's Mill | - between the twin branches of the river downstream of Griffin's Mill |
| Griffin Mill Estate | - between the canal and the river |
| Phoenix Mill | - between the twin branches of the river and also between the canal and the river |
| Bourne Mill | - between the canal and the river and between the upper and lower levels of the river |
| Wimberley Mills | - between the canal and the river |
| St Marys Mill | - between the canal and the river adjacent to St Marys Mill Weir |
| Iles Mill | - between the upper and lower branches of the river upstream of Iles Mill Bypass Sluices |
| Belvedere Mill | - between the canal and the mill pond adjacent to Belvedere Pond Bridge |
| Golden Valley | - throughout the reach between Golden Valley Lock and Whitehall Bridge between the river and the canal. |

The Lower Frome sub-model

The Lower Frome sub-model included a total of 765 sections, of which 354 were river sections, 267 embankments and the remainder floodplain sections. A total of 69 structure complexes were modelled, of which 23 were bridges. Unlike the Upper Frome sub-model this reach included significantly more floodplain cells (112) in the following areas:

- | | |
|-----------------------------------|---|
| Gloucester & Sharpness Canal | - floodplain storage between the twin arms of the River Frome and the Gloucester and Sharpness canal, and adjacent to Wheatenhurst Sluices (floodplain cells 1 to 10) |
| Walk Rhine to Fromebridge Mill | - embanked floodplain storage (floodplain cells 11 to 20) |
| Fromebridge Mill to Meadow Bridge | - left and right bank embanked floodplain storage (floodplain cells 21 to 40) |
| Meadow Bridge to Ebley Refuse Tip | - central floodplain between the northern and southern branches of |

- Beards Mill - the River Frome (floodplain cells 41 to 52, 58 to 63, 69 to 73, 79 to 92) left bank floodplain adjacent to the mill (floodplain cells 53 to 57)
- Bridgend Mill - right bank floodplain between Bridgend Kennels and the railway embankment (floodplain cells 64 to 68)
- Banty Ditch - floodplain between the northern arm of the River Frome and Banty Ditch (floodplain cells 74 to 78, 83, 84)
- Ryeford Stroudwater Canal - representation of the storage within the canal adjacent to Ryeford Saw Mills
- Redhill Bridge - left bank floodplain adjacent to the southern arm of the River Frome (floodplain cells 93A to 95A)
- Ebley Corn Mill - floodplain storage between the mill channel and the bypass channel and on both banks upstream of the mill (floodplain cells 93 to 95)
- Ebley Mill - left bank floodplain adjacent to the gauging station and storage on the rugby ground between the Dudbridge Bypass channel and the River Frome (floodplain cells 98 to 101)
- Fromehall Mill - upstream mill pond and adjacent floodplain (floodplain cells 102, 103)
- Lodgemore Mill - storage upstream of the mill between the River Frome and the Stroudwater canal.

As with the Upper Frome sub-model embankments were included to allow direct spilling between channels where there was no appreciable storage between them, or where the floodplain in each channel was being modelled as part of the river channel section. Spills of this type were incorporated in the following locations:

- Meadow Bridge - between the twin branches of the river, downstream of Meadow Bridge
- Churchend - between the Churchend weir and bypass channels
- Bonds Mill - between the culvert and bypass channels downstream of Bonds Mill.

The Stroudwater Canal was not modelled explicitly in its lower reaches, the storage associated with this being incorporated into the associated floodplain cells where appropriate. The canal adjacent to Ryeford Saw Mills was represented as a single floodplain cell which provided storage in the event of overtopping of the embankment between the canal and the northern arm of the river. The Dudbridge Bypass channel was modelled as a river reach, using weirs to represent the residual structures at each of the locks.

It should be noted that none of the River Severn Floodplain between the Gloucester and Sharpness canal and the River Severn was modelled. However

the model is capable of identifying if flow occurs over the embankments without modelling the exact floodplain levels that occur.

The Nailsworth Stream sub-model

The Nailsworth Stream sub-model was significantly smaller than the Upper and Lower Frome sub-models, including a total of 200 sections, of which 165 were river sections. However, 45 structures were still modelled, 22 of which were bridges, in what is a relatively short reach compared to the other models. As no contoured floodplain data were available for the Nailsworth Stream, the schematisation was based on the surveyed sections. In consequence, floodplain cells were only used in one location, upstream of Dunkirk Mills, in order to represent a sequence of mill ponds.

For the majority of its lower length the river only has a single channel. Downstream of Egypt Mill however, the channel splits initially into two, and then again into three at Dunkirk Mills. Flows into the left hand channel downstream of Egypt Mills occur through a water wheel which is operated regularly as a feature associated with the hotel which now occupies the site. For the purposes of the modelling, it has been assumed that the flow in this channel is negligible compared to the flow in the main river channel. The left hand channel therefore begins downstream of Egypt Mills, close to the link channel between the two streams where it has been assumed that flows into the left hand channel may be significant. The channels recombine in the area of Critchley's works. In order to represent satisfactorily the flows in the area of Critchley's, embankments were used between the adjacent channels to allow for exchanges of water between them.

3.5 Topographical data

River section data were taken from all of the previous surveys which covered the reach, including data from the 1984, 1987, 1992 and 1994 surveys. The data were imported into AutoCAD as three dimensional xyz string data, and this then allowed the use of the KeySALMON model builder developed by Key Systems for use with SALMON-F. KeySALMON allows the surveyed data and other data digitised into the AutoCAD drawing to be manipulated into a form for direct importation into SALMON-F. Thus each model section can be labelled on screen, model cells can be constructed and the appropriate data then associated with each cell.

River sections were directly imported by identifying the spatial location of the ends of each section on the 1:2500 scale contoured plans, and from this calculating the xyz coordinate of each point on the section. These strings of coordinates were then imported into AutoCAD to give a set of three dimensional polylines. Once the sections to be used in the model had been identified, these were then inspected and where necessary they were extended to cover the full width of the floodplain by digitising further data points from the contoured plans. Where embankments and floodplains were being used, these were also digitised as polylines directly from the contoured plans.

Once all the section data had been imported, KeySALMON was used to define the cell network for the model, and to label each of the model sections. For simplicity the model sections were re-numbered using a standard system since it was not possible to produce a satisfactory labelling system which referenced the section numberings used in the previous surveys. However, the origin of any particular model section can be determined by visual inspection of the section location and model layout plans supplied.

Floodplain cell data where required were extracted by digitising areas from the contoured plans, again within AutoCAD. The storage volume in any cell is specified by a stage-area table defining the area covered by water within a floodplain cell at a particular stage.

Roughness coefficients for the model were based on an assessment of the channels being modelled. However, initially the channel roughness was set to a ks length of 0.60m in the channel, and 2.0m on the floodplain throughout the model.

3.6 Bridge data

SALMON-F uses a separate module to calculate tables of afflux for bridges within the modelled reach using the United States Bureau of Public Roads method, Reference 2. The module calculates afflux tables based on a comparison of the hydraulic properties of the bridge site with and without the bridge present. These tables are then referenced by the simulation program and appropriate values of bridge afflux obtained. A limitation of the method is that it is unable to cope adequately with supercritical flows at a bridge structure, and these were encountered in a number of places in the River Frome sub-models, primarily due to the steepness of the modelled channels. In each case where this was a problem, attempts were initially made to model the structure using the USBPR method prior to adopting an alternative representation of the structure.

The USBPR method requires information about each bridge structure to be abstracted from the structure drawings and plans of the bridge site. This includes data on the shape of the bridge abutments and piers, on the skew angle of the bridge structure to the direction of flow on both the floodplain and in the channel, and a surveyed section of the channel and floodplain itself.

In the three River Frome sub-models a total of 73 bridge structures were modelled using the USBPR method. Tables 5, 6 and 7 detail list all the structures modelled and the representation used in each case. The USBPR method was unable to cope with a number of the structures initially modelled as bridges and these were subsequently changed to an alternative structure type. The bridges where this was necessary in the Upper Frome sub-model were as follows:

Griffin Mill Footbridge
Brimscombe Mill Pond Culvert
Bensons Culvert
Wimberley Mills Culvert 1
Wimberley Mills Culvert 2
Chalford Chairs Culvert
Thanet House Bridge
Red Lion Bridge.

In the Lower Frome sub-model:

Lodgemore Mills Culvert
GWR Embankment Bridge
Banty Ditch Culvert.

And in the Nailsworth Stream sub-model:

Erinoid Bridge
Cotswold House Bridge

Frogmarsh Lane Bridge.

In each case except for Erinoid Bridge a discrete headloss was used to replace the bridge. Erinoid Bridge was replaced with a sluice as the use of a head loss produced an instability in the model which could not be resolved.

3.7 Structure data

Of the 197 structure complexes included in all three models, 73 were bridges, and as such the incorporation of the data for these has been discussed in section 3.6. Where culverts were present in the modelled reach these were, in the main, beyond the limit of applicability of the USBPR method since a significant headloss is usually associated with them. The representation of a culvert was therefore dependent on its characteristics. Culverts with control structures, for instance a weir or a sluice, were modelled as sluices. In the case of a culvert with a weir control, the sluice opening was set to be a constant value and the sluice width then adjusted. This then allows the sluice to have the correct area of opening and to surcharge at approximately the correct level as the culvert being modelled. Where there was no pronounced control structure at the opening, the culvert was in the majority of cases represented as a discrete headloss.

Sluice gates, weirs and siphons on the river were represented using the appropriate structure type within SALMON-F. Where a weir had crests at varying levels, or where sluices and weirs occurred at a location in combination, multiple structure elements were included within a structure cell to represent this. The locks on the Thames and Severn and Stroudwater canals which use weirs to impound the correct upstream level of water were all represented as weirs. However, in a number of cases a low level sluice was also incorporated into the structure cell for the weir in order to lower the upstream water level to that which was observed as being "normal". This was necessary as in some reaches the weir at the upstream sill of the lock is at a high level, but the openings by which the lock would have been filled when in use are at a lower level and provide the normal drainage for the reach.

Initial discharge and drowning coefficients for each structure were derived by an assessment of each based on site visits, photographs and experience of coefficients used in previous modelling studies. In effect each structure was grouped into a set of similar structures, and each group was then ranked and default coefficients assigned to the group. For instance, all structures in group 1 would be expected to have standard discharge coefficients (a Cd of 1.0), all structures in group 2 a coefficient of 0.9 and so on. This system potentially allows any calibration data which is available for one structure to be extended to all similar structures being modelled.

Sluice openings were identified for each structure by inspection of the survey drawings and of the structures on the ground. For the purposes of the modelling, the maximum opening and the apparent normal opening were identified, together with whether or not it was feasible to operate the gate. Tables 8, 9 and 10 give the sluice gate openings used in each of the models. The "gates" which are fixed represent structures which it is either not feasible to operate, primarily due to the dereliction of many of them, or which represent culverts and other features for which an orifice type flow equation is suitable. The maximum and minimum openings for moveable gates are also identified.

Embankment structures were incorporated in locations where they were observed or known to exist. These included culverts through embankments at road and rail crossings of the valley, as well as links between the river and canal

system where these could be clearly identified and were thought to be significant. Table 11 gives a list of the culverts and other embankment structures included in the models.

3.8 Hydrometric data

The Upper Frome sub-model

Inflows for the sub-models were required at all upstream reach ends, where tributaries entered the main channels and as lateral inflows along particular reaches. Figure 3 shows the ten Frome sub-catchments for which hydrological estimates were produced for the calibration and design events. The Upper Frome catchment provides the upstream input to the River Frome at section RFA_389. A tributary point inflow is included for the Toadsmoor Stream at Wimberley Mills, between sections RFA_278 and RFA_279. The upstream boundaries of the Thames and Severn Canal reaches have nominal inflows at SCC_070 and at SCB_024 in order to ensure that there is always some flow along these reaches. The lateral inflow of the Upper Middle Frome catchment is proportioned along the various reaches between RFA_175 and RFA_278 using scaling factors based on the lengths of each reach. These scaling factors are necessary as a lateral inflow can only be incorporated along a single reach, and cannot bridge across junctions between reaches. The scaling factors applied are given in Table 12.

The downstream condition for each of the model downstream boundaries is provided by a rating curve. For the River Frome at section RFA_175 this is based on the conveyance table used by the model for this section. For the two downstream ends of the canal reaches, the rating allows a flow at all levels equivalent to the constant inflow included at the upstream end. As a result the canal reaches will cause ponding at their downstream ends of any additional flow and this will then overflow as appropriate once all available storage is filled.

The Lower Frome sub-model

The Lower Frome sub-model takes as its upstream boundary at RFA_175 the predicted flow from the Upper Frome sub-model at the same section. Similarly the flow upstream of the Nailsworth Stream outfall weir at section NSA_002 is provided by the flow hydrograph taken from the Nailsworth Stream model at the same point. The upstream inflow for the Dudbridge Bypass channel at SCA_016 is provided by the Slad Brook hydrograph, and the Painswick Stream is then specified into the same reach of channel as a tributary inflow between SCA_011 and SCA_012. Similarly the Randwick Stream forms a tributary inflow between SCC_005 and SCC_006. These are the main inflows to the Lower Frome sub-model.

The downstream boundary for the Lower Frome sub-model is provided by the River Severn downstream of the tide flap in the River Severn embankments and close to the Epney level gauge. This is a tidal reach of the River Severn and as such the stage boundary is specified directly to the model as a hydrograph.

Lateral inflows to the model are provided from both the Lower Middle Frome and Lower Frome catchments and, as for the Upper Frome sub-model, these were proportioned throughout the appropriate reaches of the model using scaling factors based on the relative reach lengths, Table 12. Nominal boundary inflows were also provided at RFM_003 and RFX_007. RFM_003 is the upstream end of the channel which flows out from under Stanley Mills but which now appears to carry no flow through the mill. The inflow is provided as a means of including

this reach of channel in the model. This is also the case for RFX_007, which is the upstream end of the old River Frome adjacent to the Nailsworth Stream where the Dudbridge Culverts now carry the diverted River Frome.

The Nailsworth Stream sub-model

The Nailsworth Stream sub-model takes as its upstream inflow the hydrograph for the Nailsworth Stream catchment upstream of Egypt Mill at NSA_124. The Lower Nailsworth catchment is specified as a series of lateral inflows to the various model reaches, with scaling factors as shown in Table 12. A nominal inflow is given for the upstream end of the reach leading from the Egypt Mill water wheel, NSD_024, as this does not necessarily carry flow at all times, and as such would cause a failure of the model otherwise. The downstream boundary is given as a stage hydrograph downstream of the Nailsworth Stream outfall weir, but with a constant level. This is necessary as the Nailsworth Stream sub-model has to be run prior to the Lower Frome model, so no information on stage downstream of the weir is available. However, due to the height of the outfall weir it is reasonable to assume that the weir is in free-flow conditions for most of the time and therefore the inflow from the Nailsworth Stream is independent of conditions in the River Frome.

3.9 Initial conditions

Due to their complexity and size, attempts to initialise the sub-models using water levels calculated using normal depth proved unsuccessful. The initialisation was therefore undertaken by preventing flow over the model embankments (by setting their discharge coefficients to be zero), and then specifying a single water surface throughout the model which was above the level of the highest channel section (RFA_389). A simulation was then run which gradually increased the discharge into model boundaries, tributaries and lateral inflows to that required at the start of the events to be modelled, whilst at the same time gradually lowering the downstream tailwater level. This allowed the model to achieve a stable state for the required discharge, thereby giving an in-channel "cold" initial condition.

As floodplain cells had been used to represent Baker's Mill reservoir in the Upper Frome sub-model and Dunkirk Mills ponds in the Nailsworth Stream sub-model it was then necessary to allow flow onto the floodplains and generate a second initial condition which included water in these floodplain cells. This was achieved by setting the embankments to have a low coefficient of discharge, allowing a small amount of flow over them, and then running this simulation for sufficiently long to allow the water levels to equalise between the channels and the floodplain. This then gave a "warm" initial condition for the purpose of starting the simulations. As a result, the Upper Frome and Nailsworth Stream sub-models require an initial simulation in order to produce a suitable initial condition, whilst the Lower Frome sub-model can be initialised directly.

4 *Hydraulic model calibration*

4.1 Calibration events

Three calibration events were specified for the model study, these being flood events occurring on:

- (i) 5 January 1994
- (ii) 30 May 1979
- (iii) 18 December 1965.

The January 1994 event is the smallest of the three events, being not much more than bankfull at most locations in the model. The recorded peak flow at Ebley Mill was 11.8 m³/s on 5 January 1994. However, the event was the largest since the installation of the continuous level recorders and the availability of this data was significant. The overall availability of data for this event is shown in the top part of Table 13. Continuous level data were obtained from five of the six recorders, the sixth being outside of the modelled area on the Painswick Stream. Peak level data had also been obtained by NRA-ST from eight recorders which had been read on either the 5 January or 23 February 1994. Flows and levels at Ebley Mill were also available for the event.

The 30 May 1979 event is the largest event for which flow data are available at Ebley Mill, a peak flow of 19.2 m³/s having been recorded, equivalent to a bankfull event in this part of the river. As such, it was thought important to use this event as part of the calibration procedure, despite the absence of any other level data elsewhere on the River Frome or Nailsworth Stream.

The December 1965 event is the largest on record for the River Frome for which there are any observed level data available, and there were a large number of observations made on the river system during the flood. However, the event predated the installation of the level recorder at Ebley Mill and no peak level was collected at this point. As a result, the peak flow for the event is unknown. A list of locations where level data were collected is given in Table 13.

4.2 Tidal water levels at Framilode

Level data for the January 1994 event at the Epney gauge on the River Severn were supplied by NRA-ST for use in modelling the 1994 flood event. These data were supplied in digital format and directly imported into the hydrometric data files. At the time of the 1965 and 1979 events the Epney level recorder had not been installed and as such no level data for the River Severn were available. Whilst it would have been possible to obtain level data for the downstream Lower Frome sub-model boundary by running the River Severn model with the observed flows in the river and observed tide curve at Avonmouth, this was discounted as being outside of the scope of the current study. As such, the 1979 and 1965 events were both simulated with a constant water level in the River Severn, allowing a free outfall through the tidal flap on the River Frome at Framilode.

4.3 Fluvial inflows

The fluvial inflows for each model for each calibration event were taken directly from the flow hydrographs derived in the hydrological component of the study. During the actual calibration there was some modification to the timings and to the baseflows of these hydrographs, but these alterations are discussed in full in the appropriate sections. The lateral inflow hydrographs were proportioned as discussed in section 3.8.

4.4 Calibration of Ebley Mill gauging station

In order to ensure that the model accurately modelled the relationship between stage and discharge at Ebley Mill weir, calibration was undertaken of a sub-model of the Ebley area. This extended from downstream of the confluence of the River Frome and Nailsworth Stream to downstream of Ebley Mill bridge. This sub-model was calibrated against two sets of flows and levels:

- the May 1979 flood event

- the flows and levels recorded from the Ebley physical model previously in the study.

The work was undertaken by producing a small sub-model of the Ebley area, extending between sections RFA_133 and RFA_143 and neglecting the Dudbridge Bypass canal, but otherwise identical to the same area in the Lower Frome sub-model. Ebley Mill weir was split up into three separate weir elements, and these were given standard discharge coefficients. The recorded flow for the May 1979 event or steady flows equivalent to those modelled in the physical model study were then used as the upstream inflow for the model. The level at RFA_139 was then matched to that recorded for the event by adjusting the discharge coefficients for each of the three weir elements.

Calibration for the 1979 event was carried out by using the recorded flows at Ebley (predicted by the NRA rating from observed levels) as the model input, whilst the downstream tailwater level was fixed at a constant 29.80m. This gave free flow conditions over the weir throughout the event and this simplification can be accepted as the physical model showed no signs of drowning of the weir until flows in excess of 50 cumecs begin to surcharge the bridge downstream of the weir. The embankment coefficients for the left bank around Ebley weir were given a discharge coefficient and drowning ratio of 0.40, values shown in a number of previous studies to provide an acceptable representation of flow over embankments. The weir flow coefficients for the three elements of the weir were then adjusted until the predicted level hydrograph for the 1979 event matched that observed at the station. A calibration to within 20mm was achieved throughout the event, with the peak level being matched exactly. The stage hydrograph from this calibration is shown in Figure 5.

Calibration for the steady flows modelled with the physical model was carried out using a stepped flow hydrograph at the upstream boundary, which gave a series of steady flows each of eight hours duration, whilst the matching physical model tailwater levels were applied to the downstream boundary. No further adjustment of the weir or embankment coefficients was carried out during this calibration, and the results are shown in Table 14. These show that, except at a flow of 20m³/s where the predictions differ by 70mm, the physical model and SALMON-F model agree to within 50mm for flows up to 50m³/s. This is sufficient to cover all the flows to be modelled within this study (ie up to the 150 year return period event). The larger difference at the flow of 20m³/s occurs at approximately bankfull, where the approximations within SALMON-F relating to the modelling of embankments (a single mean level is calculated from the input data) have greatest significance.

4.5 January 1994 event

For the January 1994 event, observed level data were available at the following locations:

Upper Frome sub-model

- Thrupp (C3 continuous level gauge)
- Golden Valley (C4 continuous level gauge)
- Brimscombe (M6 peak level gauge)
- Chalford (M7 peak level gauge)

Nailsworth Stream Model

- Persimon Homes (C1 continuous level gauge)
- Egypt Mill (C5 continuous level gauge)
- Woodchester (M10 peak level gauge)

Lower Frome Model

- Dudbridge Weir (C2 continuous level recorder)
- Ebley Mill weir (gauging station)
- Ryeford (M4 peak level gauge)
- Eastington (M1 peak level gauge)
- Wallbridge (M5 peak level gauge)
- Upper Framilode (M8 peak level gauge)
- Saul (M9 peak level gauge).

These levels are detailed in Table 15. There is some doubt attached to the peak levels recorded in the upper catchment, since a slightly higher event was recorded in some locations subsequent to that modelled for the calibration. The levels were read on the day of the peak of the calibration event, 5 January 1994, at an unknown time, and also on 23 February. At a number of the peak level recorders, the peak reading on 23 February exceeded that of 5 February, implying a second, greater event between the two dates. However, an alternative possibility is that the peak levels were collected prior to the peak of the event, and therefore that the second level may refer to the peak of the actual calibration event. Additionally, the level record at the Thrupp and Golden Valley gauges shown in Figures 8 and 9 does not show a hydrograph with a distinct peak as such, but more a continuously increasing flow in this part of the river throughout the event. There is some doubt with regard to the M9 and M8 gauges at Saul and Framilode which, though both read on the same day, have a level difference of 1.250m along a reach of c.700m in length, and which is controlled by a structure.

The initial calibration for this event showed that the high underlying baseflows were not being predicted by the hydrological model. In discussion with NRA-ST, it was decided to raise the baseflow component of the hydrograph, though without altering the peak of the event. This was achieved by identifying the shortfall in baseflow at Ebley Mill weir, around 7m³/s, then proportioning this additional flow required throughout the catchment based on the size of the baseflow predicted by the hydrological study.

Additionally, from the timing of the peak at Dudbridge and at Egypt Mill it was clear that the hydrological inputs for the Nailsworth Stream, Painswick Stream, Slad Brook and Ruscombe Brook all needed to be retarded slightly in order for the time of the peak levels at Egypt Mill and Dudbridge Weir to match with those observed. As such, the inflows for the Slad Brook, Painswick Stream and Ruscombe Brook have been delayed by 2.5 hours, and those for the Nailsworth Stream and its lateral inflow by 1.5 hours. This modification was then carried into the timings for the May 1979 and December 1965 calibration events and the design events.

The calibration results at the continuous level recorders and at Ebley Mill for the 1994 event are shown in Figures 6 to 12, and a comparison of peak levels at all sites is given in Table 15. Accepting the nearest value for locations M6 and M5, then all of the sites except for M7 and M9 are calibrated to within 80mm, with the

majority calibrated to 50mm or better. These results are discussed in more detail in section 4.9.

4.6 May 1979 flood event

For the event occurring on 30 May 1979, observed data is only available in the form of flows and levels at Ebley Mill, and these are plotted against the model predictions in Figures 13 and 14. However, levels at the calibration points used for the 1994 event are also given for comparative purposes in Table 16.

The calibration plots show a peak stage at Ebley of 32.008m compared with a recorded peak of 31.923m, a difference of 85mm. This difference must be attributable to the overprediction of the peak discharge at the site as the previous calibration of Ebley Mill weir gives an exact stage match for the recorded discharge. The peak flow prediction by the model is $21.3 \text{ m}^3/\text{s}$ compared with the rated flow of $19.2 \text{ m}^3/\text{s}$, an overprediction of c.10%. The shape of the hydrographs is, however, reasonably good although the high baseflow component which persists after the peak of the event is not represented. Because of the limited amount of data for this event, no adjustments of model parameters were made and this event can therefore be considered as purely verifying some of the model characteristics for flows up to bankfull at Ebley.

4.7 December 1965 flood event

The December 1965 event differs from the other two calibration events in that there are a large number of level observations on the River Frome for the event, but no record of the flood hydrograph exists. The model inflows are therefore purely based on the FSR modelling of the rainfall for the event as discussed in Chapter 2, without any flow validation data. The predicted stage and discharge hydrographs at Ebley Mill are shown in Figures 15 and 16, and these indicate a distinct triple peaked event. The level observations have been extracted by NRA-ST from their level books, though the quality of a number of these is unknown. The observed and predicted levels for this event are given in Table 17. It should be noted that only one adjustment was made to the model to account for possible changes in the condition and operation of structures since 1965. This was at Meadow Mill where a significantly higher headloss coefficient was used to represent the presence in 1965 of the mill sluices which have now been removed.

At the majority of locations for which observations are available, water levels are matched to within 0.16m which in view of the uncertainties in the input hydrographs, quality of level records and the date of the event is reasonable.

4.8 Calibration parameters

The final values of the roughness and structure coefficients are listed in Tables 18, 19, 20 and 21.

Channel roughnesses were increased from the initial values of a k_s of 0.6m in the channel and 2.0m on the floodplain where necessary in order to reproduce observed water levels. However, as discussed in section 4.9, in much of the model water levels were found to be insensitive to roughness and were more dependent on local structure coefficients. Floodplain roughnesses were set to a k_s of 2.0m throughout the model.

As with roughness values, structure discharge and drowning coefficients were adjusted where appropriate to reproduce observed water levels. In general structure coefficients were not altered unless the changes were justified.

Changes in discharge coefficients from the default values were made where approach conditions were thought to be particularly poor, for instance at very narrow side sluices.

Embankment coefficients were set throughout the model to have a discharge coefficient and drowning coefficient of 0.40. This is a value found in a number of studies to represent flow satisfactorily across an embankment modelled as a broad crested weir which is the representation used within SALMON-F.

4.9 Discussion of calibration results

For the 1994 calibration event peak water levels are within 70mm throughout most points in the model. The unsatisfactory calibration at M7 may be due to the representation of the supercritical or near-supercritical flow which occurs at this site, combined with the complex channel geometry where the river turns through 90 degrees downstream of the gauge. The level at M9 appears to be inconsistent with that at M8, indicating that the peak level recorded is either inaccurate, or that it relates to a previous high level in this tidally influenced reach of the Lower Frome. It seems improbable that a water surface slope of 1 in 460 could be obtained in a reach of the river where levels are in the backwater of the tidal outfall.

For this event the model also shows a general tendency for the model to produce a limited attenuation of the flood as it passes down the model and as such the predicted peak occurs too early by about 1 hour and is over the observed peak level by 58mm, Figure 12. The discharge peak exceeds that calculated from the Ebley rating by about 1 m³/s which represents an overestimate of 10%. The 1979 peak is overpredicted by a similar amount, but the timing of the peak is considerably better, Figure 14. In the case of both events the raised baseflow occurring after the peak of the event is not found in the model. This is however a function of the limitations of the hydrological study with regard to modelling baseflows and as such is discussed in detail elsewhere.

The 1965 event in theory provides the most valuable set of data against which to calibrate due to this being a major flood event. This has to be qualified by reservations over the quality of the level readings which were collected either during or after the flood event; over changes in the river system which have taken place over the 30 years since the event occurred; and over the lack of calibration data against which to compare the flows being modelled. Of these, changes in the river system, and in particular in the condition of structures along the river system, many of which are now abandoned, are of the greatest concern. As such, where predicted water levels have differed significantly from the observed, then possible causes for this have been sought prior to carrying out any adjustment of the model parameters. The predicted level is outside of the recorded level by more than 150mm in a number of locations, and the locations of these and possible causes are considered below.

RFA_331 - d/s Red Lion Pub

Supercritical flow occurs at this point, and the model has been simplified in terms of the representation of the bridge in order to cope with this. The predicted level is, however, conservative (+0.542m).

RFA_271 - u/s Boume Mill

This is a complex area where the exact location of the level is unknown, but is downstream of a structure which is now disused, and is represented as such in the model. It is possible that operation of this structure would have produced a significant increase in water levels immediately downstream of it.

RFA_232 - u/s Phoenix Mills

The level here is underpredicted, possibly due to operation of a now disused sluice adjoining the weir structure.

RFA_184 - u/s canal siphon**RFA_183 - d/s canal siphon**

The levels both upstream and downstream of the siphon are underpredicted for unknown reasons. The upstream may possibly be due to blockage of the siphon. Downstream the level could not be matched using roughness coefficients and the reason for the discrepancy is unknown.

RFA_182 - u/s Railway Mill

The location of the recorded level at this site is unknown and the structure is now dilapidated. The lower level may be a function of the blockage of the sluice parts of the structure which has now occurred.

RFA_175 - Wallbridge**RFA_172 - Wallbridge**

Both levels in the vicinity of Wallbridge are below the observed levels. The level at RFA_172 may be unreliable, whilst the exact location of the level assumed to be at RFA_175 is unknown. The steepness of this reach of the river means that supercritical flow is also present and this may also be a factor in the predicted and observed level discrepancy.

RFA_104 - u/s Stanley Mills

The level at this site was taken immediately upstream of the sluices and weirs, and as such may be in structure drawdown and as such is lower than that predicted by the model where the drawdown is assumed to occur within the structure cell. The level is hard to reconcile with that at RFA_106 upstream of Stanley Mills bridge which the model matches satisfactorily and which would imply an improbable water surface gradient.

RFA_087 - d/s Stanley Downton

The level at this point is underpredicted by 0.592m for reasons unknown. This reach of the model is insensitive to roughness coefficients and is also outside of any structure backwater. The level may be a function of a lack of discharge within the southern channel, possibly due to the assumption that Stanley Mills sluices are now inoperable.

RFA_054 - u/s Millend Mills
RFA_053 - d/s Millend Mills

Both the levels at Millend appear excessively high. The level downstream of the mill may be a function of the blockage of the footbridge in the reach downstream. However, the upstream level would imply overtopping of a 500m stretch of bank which has a level 0.4m below that of the observed level. This seems unlikely as the floodplain onto which the water is spilling would require a depth of water of over 2m in order to drown the flow over the embankment.

RFD_061 - Upper Mills Bridge

The exact location of this level is unknown, and it is in the vicinity of a bridge which has been replaced recently in connection with the new Ryeford Bypass.

RFD_033 - d/s Lower Mills

This observation is downstream of the now disused side sluices at the mill complex. Operation of these sluices may have produced a different distribution of flow around Lower Mills which may account for the higher level in this channel than predicted.

CELL 52 - d/s railway bank

This level was taken in the abandoned central channel of the Frome almost immediately downstream of the railway. The level predicted by the model represents an average for the cell in which the observation was taken. A significant water surface slope along the abandoned channel may therefore result in the observed level being significantly higher than the model prediction.

CELL 81 - d/s Ryeford Road

This level was taken close to the Ryeford Road in the vicinity of the railway, and is associated with flow through the Ryeford Road bridge. The flow is predicted by the SALMON-F model, but as in the case of the railway embankment above the model gives a single level for the whole cell downstream of this point. Additionally there have been significant improvements in the bridge and culvert arrangements for water on the north side of the railway in association with the new road bypass which follows the line of the railway and these may have a significant effect on water levels in the upper part of the Banty Ditch.

CELL 89 - Ryeford Saw Mills
CELL 90 - Ryeford Saw Mills

Both water levels on the floodplain upstream of Ryeford Road occur at the extreme edges of floodplain cells, for example close to the river bank. This implies that they are likely to be higher than the model predictions as in the cases discussed above due to the single water level predicted by SALMON-F for each cell.

CELL 85 - Ryeford Canal

The storage cell representing the canal in this reach is purely present in order to provide an approximate representation of the storage available if the bank between the river and canal upstream of Ryeford Saw Mills is overtopped.

Changes in water level which may be a function of flow into the reach of the canal from elsewhere or due to other links between the canal and river which are not included in the model are therefore not represented.

A general tendency observed in all three sub-models was an insensitivity to roughness coefficients used for the channel reaches and also for the floodplain sections. This is primarily thought to be a function of the steepness of the majority of reaches, though also in many locations roughness effects are masked by the backwater effect from structures. As such, roughness values have in the main remained at the default values to which they were set in the initial phases of the modelling. However, it has been observed in some reaches, in particular the smaller channels, that small increases in discharge can produce a significant increase in modelled levels. This suggests that where flow splits occur in the model, in particular in the Ryeford area, that level predictions are particularly sensitive to the volume of water flowing along each channel.

5 Design event tests and floodplain mapping

5.1 Introduction

The primary aim of the Frome study was to produce maps defining the extent of the Frome floodplain for a series of six design flood events. These represent estimates of the 5, 10, 25, 50, 100 and 150 year flood events on the river system. The inflows for the events were produced in the hydrological study as described in Chapter 2, with the slight modifications in timing described in Section 4.5. The tidal hydrograph for the events was based on results taken from the River Severn model where the standard 6.7m repeating spring tide used throughout the River Severn study was simulated with the mean flow in the fluvial part of the river. This gave a tidal hydrograph at Framilode which repeats between 5.00m and 7.49m and which was used as a downstream condition for all of the design event tests. This hydrograph is shown in Figure 29.

There was no change to the model parameters between the final calibration of the model and the design events. However, it was assumed that all sluice gates which were physically capable of being operated would be fully open during the design events, or in the case of the lower return period events would be open as far as necessary to prevent upstream flooding.

5.2 Test results

From the simulation of the six design events, peak levels at every model section and floodplain cell were extracted giving a total of over 1000 points with predicted peak water levels. Additionally, peak flows at every river, floodplain, embankment and causeway section were also extracted from the model. From this information it was then possible to draw up the following presentations of the modelled data.

- An annotated table of peak flow and level at every river section. This is presented in Appendix 1, together with the peak water levels for each floodplain cell. Selected peak levels for the design events are presented in Table 22, along with the peak total flow predicted at Ebley Mill.
- Long profiles for each model reach of maximum water level, bank levels and minimum bed level. These were produced using AutoCAD and plotted at a scale of 1:5000 horizontally and 1:50 vertically. These plots are presented in Volume 3 of the report.

- 1:2500 scale contoured floodplain maps of the River Frome. The 100 year return period flood event is presented on one set of maps as Volume 4 of this report, and the 5, 10, 25, 50 and 150 year events are presented as a further set of maps in Volume 5. For the 100 year event, properties at risk of flooding have been identified from their threshold levels and are identified on the maps. A list of all the threshold levels identifying the properties at risk of flooding is presented in Appendix 2.

5.3 Method of floodplain mapping

The floodplain maps were produced by combining a number of separate sources of information. Firstly, contoured plans of the River Frome at 1:2500 scale were provided by NRA-ST. These had been produced from three separate aerial surveys of the river and from a ground survey of the reach above Chalford. The peak water levels at every river section were then plotted onto these maps to produce an envelope of channel and adjacent floodplain peak flood levels. The peak water levels in each floodplain cell were then identified and plotted onto the same set of maps. As each floodplain cell is assumed by SALMON-F to have a single constant water level, it was then necessary to interpolate a continuous water level surface from the level information. This then gave an envelope of flooding on the floodplain. The final refinement was to identify every location where flow onto the floodplain was occurring and to extend the flooded outlines to include these areas as part of the floodplain.

One set of maps was produced for the 100 year event by this method whilst a second set was used to depict the flooded outlines for the other events. For the 100 year flood event, maps indicating property threshold levels were supplied by NRA-ST together with a listing of the addresses of each mapped property. From this information, properties at risk of flooding in the 100 year event were identified as accurately as possible. The process was complicated by discrepancies between the information on the list of threshold levels and information on the threshold maps. As such, some properties at risk of flooding may not appear on the address list. Additionally, where properties are protected by features such as walls then they may be indicated as at risk of flooding as without full surveys of the protection it is not possible to identify whether they may be protected from channel or floodplain water levels.

For the Nailsworth Stream no information was available on general floodplain levels and threshold levels so it has not been possible to prepare maps of flood extent or lists of flooded properties. The results are therefore presented purely in tabular form and do not form part of the following discussion.

5.4 Discussion of results

The following discussion of the results of the design event testing has been structured on a reach by reach basis for clarity. The reaches are presented in a downstream to upstream order to match the order of the floodplain maps.

Wheatenhurst Sluices to A38

This reach is characterised by embankments on both sides of the river. The results of the design tests indicate that neither embankment is overtopped by any of the design events tested. The right bank floodplain is dry for the 5 year event but for the larger magnitude events flow occurs through the culverts on the right bank of the A38 and the floodplain then acts purely as floodplain storage. For the 100 year event and over the levels on the floodplain are sufficient for water to reach the Stroudwater Canal though this ends in high ground at both ends. It has

been assumed for the design tests that the sluice carrying Walk Rhine under the Frome will be closed to prevent flooding of the left bank floodplain from the Walk Rhine. A feature of this reach is the area of dry ground between the A38 culverts and the river upstream of Fromebridge, which results from the line of higher ground running from the A38 along the floodplain.

A38 to Meadow Bridge

Meadow Mill is the cause of a significant headloss for all the events modelled. This has the effect of forcing flow over the embankments upstream and onto the floodplain for events exceeding 5 years in return period. Localised flooding occurs for the 10 year event, whilst for the 25 year event the whole of the left floodplain between the A38 and Meadow Bridge is flooded. Flow onto the right floodplain upstream of Meadow Mill is prevented from passing down the floodplain by the higher ground that the mill buildings stand on and as such right bank flooding is restricted to upstream of Meadow Mill and downstream of the M5 embankment. The mill buildings themselves are at risk of flooding in the 100 year event. The caravan park immediately downstream of Meadow Bridge is just at a sufficiently high level not to be flooded by the 100 year flood event but is threatened by the 150 year event.

Meadow Bridge to Railway Embankment

This reach is characterised by the splitting of the river into two main southern and northern channels. However, in the vicinity of Churchend a number of smaller channels are also present. The splitting of the channels in this way produces a wide central floodplain which is significantly lower than normal water levels in the two channels. As a result, this central area is flooded for all the design events tested. Flow onto the floodplain comes from upstream of Bonds Mill, from upstream of the Market Garden Weir, and from locations on the south channel where the banks are lower. Once on the central floodplain, flow passes under Millend Lane via culverts and returns to the northern channel downstream of this point. For events of 50 years and over Millend Lane itself is overtopped. The buildings at Bonds Mill are at risk of flooding for the 100 year event as are those at Beards Mill.

Railway Embankment to Downton Road

Upstream of the railway the river maintains two separate channels, but the width of the central floodplain decreases considerably. Bridgend Mill is the major feature on the north branch of the Frome and for all the design events flooding occurs upstream of the mill on the right floodplain. This progressively increases and for the 100 year event properties at the mill are at risk of flooding. The northern road into the mill forms an obstruction to flow around the north of the mill buildings.

For all the events, flow occurs onto the central floodplain from both channels upstream of the railway embankment. Additionally, for the 100 and 150 year events flow will cross Downton Road itself and will flood the upper part of the floodplain.

Downton Road to Ebley Refuse Tip

This reach sees an expansion in width of the central floodplain, together with the presence of a third channel, the Banty Ditch, which runs between the north and

south channels. The Banty Ditch is significantly lower than the other two channels and this forms the line of flooding along the floodplain. Downstream of Ryeford Road there is no flooding from the south channel onto the floodplain for any of the events modelled, though immediately downstream the flood envelope links with the relict channel leading from Stanley Mills. Flow from the north channel onto the floodplain occurs from upstream of Upper Mills and from the area between Upper Mills and Bridgend Kennels. Flow also occurs from between Ryeford Saw Mills culvert and the disused railway (now a new road) which then links through a small culvert to the Banty Ditch. This is reflected in the pattern of flooded properties along the lower half of the reach, all of which lie along the north channel. The exceptions to this are two properties at Stanley Mills which are potentially at risk of flooding.

Upstream of Ryeford Road, flooding of the central area is more extensive and flow occurs from both of the river channels. The overtopping becomes more extensive for each of the design events resulting in a greater depth of flooding on the central floodplain. For the 25 year design event and over flow occurs along the line of the old railway through Ryeford Road and onto the central floodplain downstream. The representation of this in the model has been based on existing data on the railway and floodplain layout as it was understood that the new road was to maintain the existing ground levels. If this has not been the case then the construction of the new road may be significant in altering the flow patterns and depths of flooding.

Ebley Refuse Tip to Dudbridge Culvert

The refuse tip at Ebley restricts all the flow in the Frome to a narrow channel with no floodplain prior to splitting into the north and south channels downstream of this point. Upstream of the tip, the channel briefly splits in two for the mill and bypass channels at the Com Mill itself before returning to a single channel throughout the reach to Dudbridge. The structures at Ebley Com Mill result in flow being forced onto the left floodplain upstream of the mill for all the design events, though for the 5 year event this acts purely as storage. For the other events flow is able to bypass the structures via this route. Flow onto the right floodplain occurs for the 10 year event and over, though this is unable to bypass the mill due to high ground to the north. For the 100 year event the buildings around the Com Mill are at risk of flooding.

At Ebley Mill the channel is again restricted by the mill buildings and the railway though bypassing of the gauging weir at Ebley occurs for flows of 25 year return period and over. Flow occurs over the river bank over the left bank adjacent to the confluence of the river with the Dudbridge Relief Channel. Flooding of the playing fields between the canal and the river occurs for the 50 year flood event and over.

Dudbridge Culvert to Bath Road Bridge

Between Dudbridge and Bath Road the Frome is generally tightly constrained to a single channel with no floodplain. Flooding of Redler's works is possible for the 50 year event and over though the mechanics of the flooding are difficult to represent within the model. Dependent on how water may flow through the Redler's site then other properties adjacent to the Dudbridge Road may also be at risk. The flooding occurs from a low point on the right bank at the upstream end of the works. The river is then constrained again until Fromehall Mill is reached where the river flows through a complicated series of culverts and

structures. Flooding of the area to the north of the mills occurs for the 25 year event and over from the upstream mill pond. A hydraulic link between the canal and the river has not been included in the model at this point though it is possible that water levels in the canal may be high enough to overtop the canal bank into this area.

At Lodgemore Mills, water levels in the mill pond appear not to exceed the level required for flooding of the mill buildings. However, potential flooding of one of the buildings in the 100 year flood has been indicated as the threshold level is below the level of the upstream water level although it is unclear where the threshold for the building is. Upstream of Lodgemore Mills flooding occurs of the depot to the north of the river for the 100 year event and over. This is primarily due to the poor culvert opening at the entrance to Lodgemore Mill Pond.

Bath Road Bridge to Thames and Severn Canal Syphon

This is one of the steepest reaches of the model and flow is near supercritical along much of the reach for all the events. Some inaccuracy in the water level predictions is therefore likely. Flooding of the properties on the left bank upstream of Bath Road Bridge is predicted for the 100 year flood event but the rest of this reach is deeply incised and there is no risk of other flooding for any of the events.

Thames and Severn Canal Syphon to Brimscombe Pond

Upstream of the syphon, some interaction occurs between the canal and the river for the larger events. However, the river is again within a deep channel until upstream of the housing estate at Bowbridge. The river channel then becomes noticeably smaller and begins a series of frequent bifurcations around the many mill buildings and structures which are present. In general, the channel splits produce a central area of undeveloped floodplain into which the larger floods can spill. However, the model identifies that localised properties are at risk of flooding. For the 100 year event these include works at Stafford Mills, Griffin Mill and Phoenix Mill. One of the industrial units upstream of the caravan park at Thrupp is also at risk of flooding for the 100 year event.

Brimscombe Pond to Wimberley Mills

At Brimscombe Pond flow occurs onto the left bank floodplain from upstream of the culvert leading into the pond for events of 25 year return period and over. This results in the potential flooding of a number of properties in this area. The river is then constrained through a number of culverts and bridges until Brimscombe Port is reached. Here there is flooding for the 100 year event of the Benson's site, though there is no flooding from any event of the Brimscombe Port Industrial Estate. This is protected by a line of slightly higher land and walls along the right bank of the river.

At Bourne Mills flooding occurs for the 100 year event and there is a significant area of flooding upstream of this point where flow from above the mill control structures spills across the downstream floodplain.

Wimberley Mills to Chalford Industrial Estate

Immediately upstream of Wimberley Mills, flooding occurs of the site car park for the 100 year event and over, though levels are not sufficiently high to cause flow

overland and through the mill buildings. Between Wimberley and Chalford two areas of localised flooding then occur. At St Marys Mill, flow occurs from upstream of the culvert at Ivy Cottage into the low lying area between the river and the canal but this does not threaten any properties. Similarly, flooding occurs upstream of St Iles Mill where the channels split but no properties are at risk. For the 100 year event, Clayfields Mill adjacent to the canal may be at risk of flooding due to a low threshold level.

At Chalford Industrial Estate the river passes under the site through various culverts and control structures, the main one of which is at the upstream end of the site. Water overtops the sluice headwall for the 100 year event and over and a number of industrial units are then at risk of flooding.

Chalford Industrial Estate to Whitehall Bridge

The model identifies a number of properties at risk of flooding in the 100 year event around Chalford Bottom and Rack Hill, in particular along the High Street. Upstream of this point the river takes on a rural characteristic and there are a limited number of properties affected by potential flooding. The right bank floodplain upstream of Golden Valley Lock is flooded for all events, though upstream of Ashmeade House the bank levels are sufficiently high to prevent flooding. Two properties along this reach are at risk in the 100 year event, including Ashmeade House.

Upstream of Bakers Mill the river interacts with Bakers reservoir and in the 100 year flood event Bakers Mill itself is threatened with flooding. The culvert at Puck Mill is then the last significant structure on the river and this acts as a major constriction due to its small size. As a result, flooding occurs of the whole of the floodplain upstream of this point and this results for the 25 year event and over in the canal carrying some of the flood flow.

6 Sensitivity tests

6.1 Introduction

In order to identify the sensitivity of the model to changes in flow and structure coefficients a set of 4 sensitivity tests were carried out. The four tests were as follows:

- 1) Increase in flow hydrographs by 10%
- 2) Increase in flow hydrographs by 20%.
- 3) Reduction of structure coefficients by 10%
- 4) Reduction of structure coefficients by 20%

These modifications were modelled with the 100 year flood event and the results tabulated in a similar way to the design event maximum levels. This table is presented in Appendix 3. Water level increases are discussed in section 6.2 for the flow sensitivity tests whilst Table 28 gives a list of model structures where significant increases in upstream water level occur for the structure coefficient sensitivity tests. These are then discussed in section 6.3.

6.2 Sensitivity to flows

For the purposes of the flow sensitivity tests every inflow was increased by 10% or 20% throughout each hydrograph for the 100 year design event. This gave an increase in peak flow at Ebley Mill of $2.3\text{m}^3/\text{s}$ for the 10% increase and $4.9\text{m}^3/\text{s}$ for the 20% increase over the original peak flow for the 100 year event of $37.4\text{m}^3/\text{s}$. The table presented in Appendix 3 was then produced comparing levels at each model section and cell for the existing 100 year design event and the 100 year event with either a 10% or 20% increase in flow. From this table, locations where the water level increase exceeded 0.10m were identified, this being considered a significant increase for these purposes. The following discusses locations where water level increases exceed this limit on a reach by reach basis.

Wheatenhurst Sluices to Fromebridge Mill

This reach of the model shows an almost constant level increase between the two structures. For the 10% test, the increase in water level only exceeds 0.10m at section RFA_020. However, for the 20% test the level increase is between 0.09m and 0.29m throughout the reach.

Fromebridge Mill to Ebley Refuse Tip

This whole reach of the model is characterised by the generally small increases in water level in the river for both sensitivity tests. At the same time water levels on the floodplain increase indicating that the lack of water level increase in the channel is the result of more water entering storage. The area of greatest change in floodplain levels is around the A38 where water levels rise by up to 0.5m for the 20% test, but large increases in water level also occur upstream of Ryeford Road. Localised channel water level increases occur in the channels upstream of Meadow Bridge (0.13m for the 10% test, 0.19m for the 20% test) and upstream of Beards Mill Bridge (0.07m and 0.12m).

Ebley Refuse Tip to the Thames and Severn Canal Syphon

At the bifurcation weirs at Ebley Refuse Tip the two tests produce water level increases of 0.05m and 0.11m respectively, and there are similar increases upstream of Ebley Corn Mill bridge (0.04m and 0.11m) and Ebley Mill weir (0.06m and 0.11m). However, for the reach of the river upstream of this point to Lodgemoore Mills there are no water level increases exceeding 0.10m. The exception to this is the Dudbridge Relief Channel which is sensitive to increases in flow. Levels in the channel rise by around 0.10m for the 10% test and up to 0.20m for the 20% test. Water levels upstream of the exit from Lodgemoore Mill pond rise by around 0.10m and 0.15m for the two tests until upstream of the Bath Road Bridge where the channel steepens considerably.

Thames and Severn Canal Syphon to Stafford Mills

The syphon carrying the river under the canal appears to be very sensitive to increases in discharge. The 10% increase in flow gives a 0.22m rise in water level, whilst a 20% increase results in a 0.43m rise in water levels. An effect of this is to cause a dramatic rise in levels within the disused canal due to flow passing over the river banks downstream of Butterow Bridge. Level increases upstream of this point as far as Thrupp Works are then of the order of 0.10m to 0.25m for the 10% test, and 0.16m to 0.45m for the 20% test.

Stafford Mills to Brimscombe Pond

Upstream of Stafford Mills water level increases are generally restricted to short reaches where the 0.10m increase is exceeded. Between Griffin's Mill Footbridge and Griffin's Mill bypass weir levels for the 20% test rise by 0.14m. Levels in the bypass channel around Phoenix Mill also rise significantly, the largest increases being 0.15m and 0.34m for the two tests upstream of the Swimming Pool bridge at section RFA_229. Levels upstream of the Thrupp caravan site bridge are also sensitive to discharge with the tests producing increases of 0.23m and 0.50m respectively. An increase of this magnitude would be sufficient to cause flooding of the caravan site on the left bank upstream of the bridge. The level increase at the bridge gradually reduces upstream until Brimscombe Pond is reached.

Brimscombe Pond to Belvedere Mill

The reach between Benson's culvert and Bourne Mill is relatively sensitive to increased discharge with a level increase of 0.18m throughout most of the reach for the 20% sensitivity test. However, this increase is still insufficient to cause flooding of Brimscombe Port. A second localised increase occurs around Wimberley Mills where levels between RFA_284 and RFA_288 rise by up to 0.18m for the 20% test. Water levels between St Marys Mill and St Iles Mill rise by up to 0.39m for the 20% test at section RFA_310.

Belvedere Mill to Whitehall Bridge

Water level increases throughout almost all of this reach exceed 0.10m for both the sensitivity tests. A particularly significant increase is at Chalford Industrial Estate sluices where water levels rise by 0.24m and 0.37m for the two events ensuring significantly more overtopping into the estate of the head wall for the sluices. Between Red Lion bridge and Ridley Mill water levels rise by 0.15m and 0.30m at almost every section. Upstream of Ridley Mill until Harley Lane is reached level increases are only over 0.10m (0.13m to 0.15m) for the 20% test. The reach between Harley Lane and Ashmead Sluices shows a dramatic rise in water level in both the channel and on the floodplain. For the 10% test levels increase by between 0.22m and 0.25m, whilst for the 20% test the increase is between 0.46m and 0.50m. Upstream of Ashmead sluices the increases only exceed 0.10m for the 20% test where the level rise immediately upstream of the structure is 0.31m. Bakers bridge is sensitive to discharge with upstream level increases of 0.17m and 0.47m for the two tests. Above Bakers Mill sluices the reservoir effectively limits level increases to below 0.10m until upstream of Puck Mill. Here level increases of 0.16m and 0.32 m for the tests occur throughout the reach. One effect of these increases is to cause more flow into the canal in its upper reaches.

The Nailsworth Stream

Due to the confined channel of the Nailsworth Stream, level increases occur almost everywhere for the two flow sensitivity tests. Between Selsley culvert and the downstream end of Erinoid culvert level increases are between 0.21m and 0.30m for the 10% test, and between 0.47m and 0.63m for the 20% test. Similar level increases are apparent upstream of the culvert, between Erinoid bridge and The Priory bridge. Above The priory increases do not exceed 0.10m for the 10% test, but are between 0.18m and 0.24m for the 20% test.

The most sensitive structures to increases in flow are the various culverts carrying the stream under Rooksmoor Mill. Immediately upstream of Rooksmoor Mill, levels increase by 0.50m for the 10% test, and 1.03m for the 20% test. A level increase of this magnitude would be likely to cause extensive flooding along the road down the Nailsworth valley though limitations on the available data mean that this is not fully represented in the Nailsworth Stream model. The backwater from Rooksmoor affects the reach upstream as far as Birds Crossing so it is not possible to determine the level increase in this reach due to the increase in discharge alone.

Once upstream of Birds Crossing there is then a long reach as far as Merretts Mills where water level increases are reasonably consistent, varying between 0.13m and 0.29m for the 10% test, and between 0.25m and 0.44m for the 20% test. There are then a series of localised increases in the area of Critchley's works where water level increases are around 0.40m for the 10% test and 0.80m for the 20% test.

From Dunkirk Mills up to the culvert downstream of Egypt Mill, water levels in the reach show a constant pattern of increase in both channels running beside the old mill ponds. Levels in the right hand channel rise by between 0.07m and 0.13m for the 10% test, and between 0.15m and 0.23m for the 20% test. In the left hand channel the increases are around 0.15m and 0.27m for the two tests throughout the reach.

For the remaining length of the model from the garage culvert to upstream of Egypt Mill larger level increases are again seen. These reach a peak of 0.27m and 0.67m in the short reach downstream of Egypt Mill before the culvert is reached.

6.3 Sensitivity to structure coefficients

Changes to the structure coefficients were made by reducing every coefficient in the model by either 10% or 20% as appropriate. The exception to this was at bridges where the bridge afflux coefficients were increased by the appropriate amount to achieve an increase in upstream head. No changes were made to coefficients relating to embankments or embankment structures.

From the results in Appendix 3 it is apparent that the effect of changing all the coefficients globally in the model produces a pattern of water level changes which is not straightforward to interpret. For example, levels upstream of some structures actually fall due to changes in the flow in the channel resulting from other structure coefficient changes. Structures where upstream water levels rise by more than 0.10m have been identified in Table 28. In the majority of these cases level rises are localised and restricted to immediately upstream of the structure. However, in some locations the level increases are sufficient to cause a significant increase in level throughout the reach upstream of the structure. These latter cases are discussed below.

Thames and Severn Canal Syphon

The previous set of sensitivity tests indicated that this syphon is very sensitive to increases in flow. However, the effect of a 20% reduction in coefficients is to produce an even larger increase in upstream water level of 0.53m. This increase appears to affect sections until upstream of Eagle Mill, though clearly there may be some additional local increase in water level at these sites which is masked by the level increase at the syphon. The increased water level downstream of

Butterow Hill bridge may be the cause of the 0.22m increase in level upstream which affects sections until upstream of the second Bowbridge estate bridge.

Thrupp Caravan Site Bridge

This bridge is not as sensitive to increases in the afflux coefficient as it is to increases in discharge. However, water levels throughout the reach upstream to the football ground at Brimscombe pond are raised as a result. This rise in level may be sufficient to cause flooding in the area of the caravan park.

Puck Mill Culvert

Upstream of Puck Mill culvert the river has a relatively shallow gradient until the upstream model boundary is reached. As a result, increases in water level upstream of the culvert affect both the river reach, right bank floodplain and flow into the canal upstream. A 20% reduction in structure coefficients at this structure results in an increase in water levels of 0.26m throughout this reach.

Rooksmoor Mill Culverts

The culverts under Rooksmoor Mill are as sensitive to decreases in structure coefficients as they are to increases in discharge. A 10% reduction in coefficients produces an upstream increase in water level of 0.39m, whilst a 20% reduction gives an increase of 0.84m. The effect of this then probably extends as far upstream as Station Road Works though the effect of other structures along the reach may also be significant.

South Woodchester Works Bridge

A 20% reduction in coefficients at this bridge produces a 0.30m increase in water level which then effects upstream levels as far as Frogmarsh Lane Bridge.

6.4 Discussion of results

The sensitivity tests carried out indicate that water levels in the model, particularly in the upstream reaches and in the Nailsworth Stream, are sensitive to the estimates made of the structure coefficients and the inflow hydrographs. As such, a small error in either of these could lead to a much larger error in the peak water level predicted. However, what the tests do tend to indicate is locations where blockage of structures or the channel may be critical. Of major interest is the finding that for the River Frome downstream of Dudbridge the model is relatively insensitive to errors in the peak flow and assumed structure coefficients. The main reason for this is that flow is able to find other routes around structure complexes by spilling onto the floodplain. Assuming that the coefficients used for embankments in the model are reasonable, and the coefficients used are borne out both by previous work on other modelling studies and by the close match between the physical model and SALMON-F models of Ebley gauging station, then the model results can be treated with a reasonable degree of confidence.

Of more concern is the general sensitivity in the upper reaches of the Frome from the Thames and Severn Canal siphon to Whitehall Bridge to increases in peak discharge. This suggests that minor discrepancies in flow pattern resulting for example from unmodelled links between the canal and the river may have a significant effect on the model predictions. Whilst efforts have been made to identify and include in the model all the links between the channels, undoubtedly

a number of links exist which have not been modelled as no information is available as to their whereabouts or dimensions.

A number of structures have been identified where structure blockage is a major concern and these can in general terms be taken as those structures listed in Table 28. Obviously of these structures some are more critical than others in terms of the effects of raised water levels resulting from structure blockage. In particular Fromehall Mill, Lodgemore Mill, the Thames and Severn Canal siphon, Thrupp caravan site bridge and Chalford Industrial Estate sluices are critical on the River Frome. On the Nailsworth Stream the Rooksmoor culverts, Station Road works structures at Critchleys are of concern.

7 Modelling of additional flows downstream of the Gloucester to Sharpness Canal and the effects of tide lock

7.1 Introduction

The drainage system of the River Frome downstream of Wheatenhurst Sluices is complicated by the presence of the following factors:

- the River Severn
- the Gloucester and Sharpness Canal
- the River Frome offtake into the Stroudwater Canal.

The River Severn is tidal in this reach and has periodically overtopped the Severn flood defences. In order to preserve the continuity of the defences, the River Frome discharges into the Severn at Framilode through a pair of flap gates. The Gloucester and Sharpness Canal (GSC) acts as a feeder channel for water to the Purton Treatment Works which supply water to Bristol. Water is collected by the canal from the River Cam, from the River Severn (during periods of low flow) and from the River Frome. In the case of the Frome, water is diverted from upstream of Wheatenhurst sluices into the old Stroudwater Canal and from there into the GSC. As a result of this function of the GSC, it incorporates an overspill structure adjacent to the siphons which carry the River Frome underneath it. The overspill structure is designed to discharge excess capacity in the GSC into the Frome and from there into the River Severn through the tide flaps.

As a result of these interactions, the River Frome requires a significant storage capacity downstream of Wheatenhurst Sluices. Water passing through the sluices under flood conditions, as well as overspill from the GSC, may be unable to exit through the tide flaps due to tide locking from the Severn. To accommodate this, the embankments between the Frome channels and the Severn floodplain are of the order of 9.5m to 10.0m in height, whilst those between the twin Frome channels are lower to allow for the storage of water under extreme flows. Additionally, the carrying the Walk Rhine under the track which branches to the north from Walk Bridge incorporates a wooden flap to exclude water.

As part of the River Frome Study, NRA-ST requested that the effects of tide-locking by the Severn, overspill from the GSC and flooding in the Frome be considered together for this reach of the model.

7.2 Modelling of flows and tides

The model used for this aspect of the study was the same as that used previously, though the upstream model boundary was provided by the flows taken from the main model upstream of Wheatenhurst Sluices. The model takes no account of flow over the main Frome embankments or over the Stroudwater Canal, though models fully interaction between the twin channels and the intermediate storage. This representation gives a limitation to the model which is discussed in more detail below.

The 5, 10, 25, 50 and 100 year fluvial floods in the River Frome were combined with standard repeating tides with a peak level of 4.88m, 6.00m, 8.00m, 10.00m and 10.50m. The low tide level for each of these lay between 4.00m and 4.50m. The peak of the fluvial flood was timed to coincide with a peak tide level in the River Severn, in order to give a "worst case" scenario. Flows from the GSC were represented in each test by a continuous inflow of 10m³/s into the left hand channel downstream of the siphon.

7.3 Results of additional modelling

The results of the modelling are presented in tabular form in Tables 23 to 27. These indicate that the primary control on water levels downstream of Wheatenhurst Sluices is the period of tide-locking due to levels in the River Severn. Levels upstream of the tide flaps are shown in Figure 30. The 4.88m tide peaks at the level of the invert of the tide flaps. As such, no period of tide-locking occurs and these can be considered as the water levels which would result from each return period flood combined with the GSC overflow if the Frome was freely discharging. For the 5 year event, only the central floodplain upstream of the GSC is flooded. However, for events of 10 year return period and over the downstream area of storage is also filled. The floodplain between the Stroudwater Canal and the left branch of the Frome upstream of the GSC, is flooded only by the 100 year event. Water remains excluded from the floodplain upstream of Walk Bridge by the flap on Walk Rhine upstream of its confluence with the Frome for all events. Water levels in the channels for all the events are well below the levels of the surrounding embankments, so flooding is constrained to within the Frome itself.

The 6.00m tide gives identical peak level results to those from the 4.88m tide. Water levels are consistently at least 1m higher upstream of the tide flaps than downstream and as such the discharge through the flaps is only marginally affected by the increased peak tide level. The upstream water levels are therefore unchanged throughout the river channels and floodplain downstream of Wheatenhurst Sluices.

The 8.00m tide produces a significant increase in water levels immediately upstream of the flapped outfall compared to the 6.00m tide. However, the effect of the weir downstream of Framilode Bridge causes water levels upstream of this point to increase only by a small amount for all of the events modelled. The majority of water level increase are of the region of 30mm or less upstream of Framilode weir. The effect of these small increases is however significant in relation to the 100 year flood event where water levels in cells 3 to 10 are all of the order of 9.00m OD. There is also an increase in water level over the smaller tide events of 90mm in cells 1 and 2.

The 10.00m tide results in peak water levels upstream of the tide flap which exceed 9m OD for all the events. This level is sufficient to cause a significant increase in water levels throughout the whole system downstream of

Wheatenhurst sluices. The effect of tide-locking is particularly apparent in that water levels downstream of Wheatenhurst sluices are no more than 210mm above those at the outfall for any of the events, and also there is virtually no headloss across any of the channel structures except for the canal syphons. The 10.50m tide produces only a slight further increase in peak level over the 10.00m tide and shows a very similar pattern of water levels and flooding. For both events, the height of the embankments along the Frome is sufficient to restrict flooding to within the Frome floodplain itself so that no flow occurs onto the Severn floodplain.

One main feature of the two larger tide events is the water level reached in cell 10. The model simplifies the area adjacent to Wheatenhurst Sluices by assuming that flow is not possible back under the Stroudwater Canal into Walk Rhine thereby causing flooding of the land to the south of the canal and river. However, water levels of the magnitude of those resulting from the 10.00 and 10.50m tides for all the events would be likely to flood this land from Walk Rhine itself. As a result, it might be expected that flooding of this land would produce slightly lower levels than those predicted by the model as constructed through filling of this storage via the culverts under the Stroudwater Canal.

8 Conclusions

- 8.1 A combined hydraulic and hydrological modelling study has been carried out of the River Frome and its catchment at Stroud in Gloucestershire.
- 8.2 A physical model of the Ebley Mill gauging station was constructed to assess the rating curve for the site. A new rating curve for flows greater than bankfull was developed.
- 8.3 Flood Studies Report rainfall-runoff procedures backed by available local data for the catchment were used to develop models of the River Frome subcatchments. These models were used to predict flows per observed flood events in 1994, 1979, and 1965. The 1994 and 1979 events were verified against actual data at the Ebley Mill gauging station through the use of a RIBAMAN routing model.
- 8.4 The verified FSR models were used to provide flow predictions for the 1965 flood event, and for the 5, 10, 25, 50, 100 and 150 year return period flood events.
- 8.5 Three SALMON-F computational hydraulic models of the catchment were constructed, including the whole of the Main River Frome, and the Nailsworth stream downstream of Egypt Mill. The models were based on data surveyed between 1984 and 1994.
- 8.6 The SALMON-F models were calibrated for observed flood events in 1994, 1979 and 1965, the inflow hydrographs which had been produced in the hydrological study. The calibration for the 1994 event was satisfactory at most locations. For the 1965 event the calibration was unsatisfactory at some locations, though this may be a function of changes in structure condition and operation since 1965.
- 8.7 The SALMON-F models were used to simulate the 5, 10, 25, 50, 100 and 150 year return period flood events.

- 8.8 Floodplain maps for the 100 year flood event and for the 5, 10, 25, 50 and 150 year flood events have been produced at 1:2500 scale from contoured plans of the river.
- 8.9 Sensitivity tests indicate that the model is relatively insensitive to peak flood flows and choice of structure coefficients in the lower reaches of the model. The tests also indicate that water levels in the upper reaches of the model are generally sensitive to increases in peak discharge.
- 8.10 Modelling of the interaction of the River Frome, the Gloucester and Sharpness canal and the River Severn has been carried out for a range of flows and tide levels. The results indicate that the Frome defences are adequate for the events modelled.

9 *References*

- (1) Bailey R P, 1991. An investigation into the water resources of the River Frome near Stroud. MSc dissertation.
- (2) USBPR 1978. Hydraulics of bridge waterways. Hydraulics Design Series (HDS) No 1.



Tables

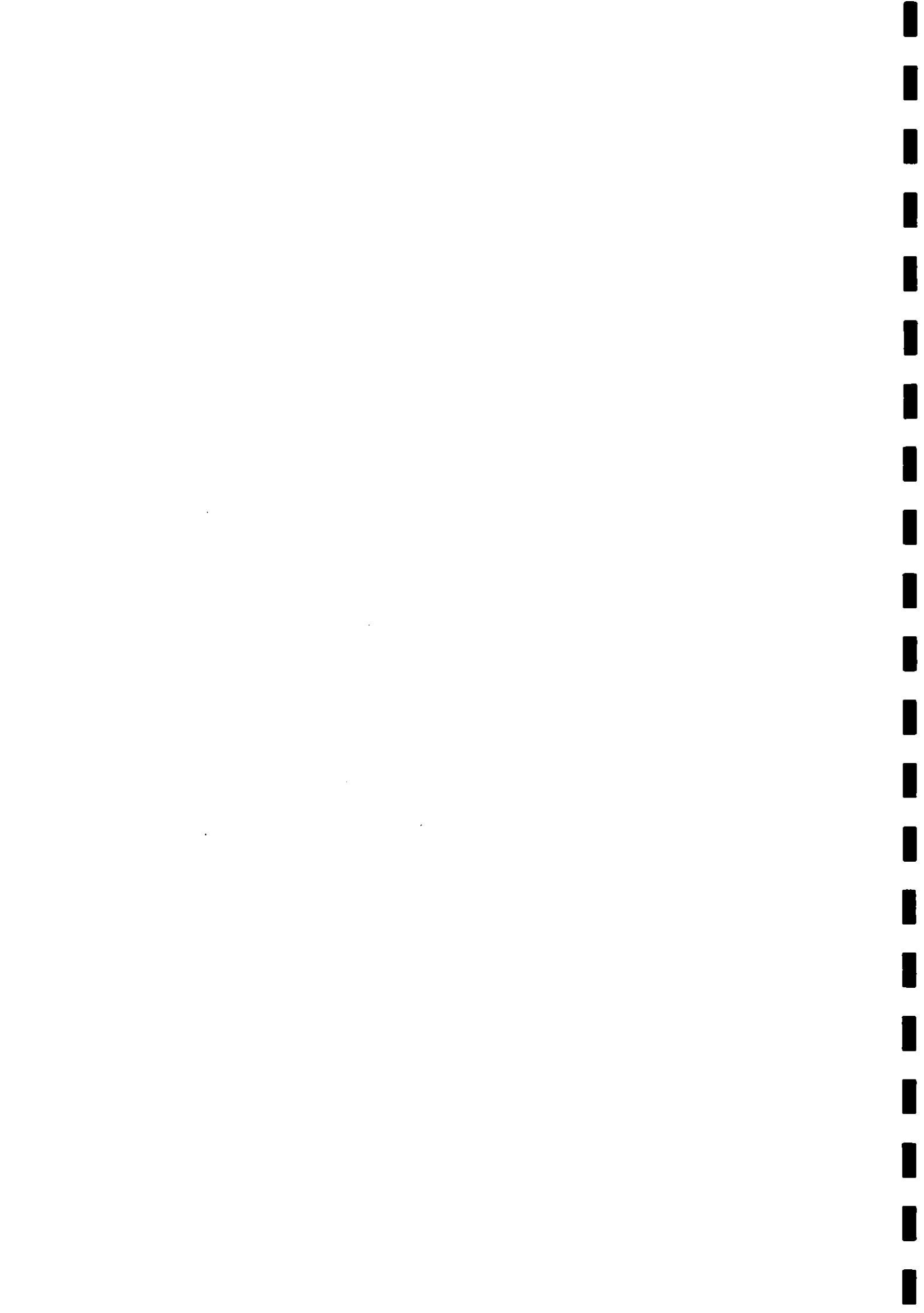


Table 1 Results of flood event analysis

Event date	Rainfall depth mm	Storm duration hr	Peak flow $m^3 \cdot s^{-1}$	LAG hr	ANSF $m^3 \cdot s^{-1}$	SMD mm	API5 mm	CWI mm	PR %	DPR RAIN %	DPR CWI %	SPR %	Tp (1) hr	Qp $m^3 \cdot s^{-1}$	Urban event	
May 79	39.4	12	19.18	5.8	4.34	2.9	5.7	127.8	7.6	5.83	0.00	0.55	5.13	4.5	32	N
Dec 79	59.2	23	16.99	8.4	2.16	0.0	2.2	127.2	6.3	4.49	3.56	0.28	0.36	3.5	29	N
Mar 86	15.3	8	4.52	4.0	3.02	6.0	2.5	121.5	2.3	0.38	0.00	-0.88	1.25	3.5	28	N
Jul 86	15.5	13	3.56	-	2.17	91.8	4.3	35.4	1.8	-0.14	0.00	-22.40	22.26	-	-	Y
Aug 86	42.5	12	7.25	-	1.50	73.2	2.9	54.7	2.4	0.48	0.86	-17.58	17.20	-	-	Y
Sep 86	17.9	11	2.35	1.3	1.40	59.2	0.3	66.1	0.7	-1.27	0.00	-14.73	13.46	2.0	68	Y
Oct 86	22.8	6	3.51	1.8	1.25	76.4	2.9	51.5	0.9	-1.06	0.00	-18.38	17.31	2.0	68	Y
Apr 87	26.0	15	9.31	6.5	4.49	0.0	3.1	128.1	4.7	2.85	0.00	0.78	2.07	5.5	27	N
Jun 87	23.9	8	4.82	-	2.29	60.7	6.9	71.2	1.7	-0.24	0.00	-13.45	13.21	-	-	Y
Jun 87	12.9	11	3.23	5.3	2.19	46.8	7.7	86.1	1.8	-0.14	0.00	-9.73	9.59	5.0	25	N
Nov 87	29.0	11	10.75	5.7	3.78	0.2	1.3	126.1	5.4	3.57	0.00	0.70	3.29	8.0	33	N
Dec 87	8.3	3	4.06	2.4	3.00	0.0	6.2	131.2	2.2	0.28	0.00	1.55	-1.27	3.0	42	Y
Aug 88	21.1	9	3.10	2.8	1.29	66.5	7.6	66.1	1.2	-0.75	0.00	-14.73	13.97	2.0	46	Y
Oct 88	21.3	7	5.04	-	1.83	35.7	2.7	82.0	1.8	-0.14	0.00	-8.25	8.11	-	-	Y
Nov 89	28.0	17	4.75	3.0	1.54	57.7	1.2	68.5	2.4	0.48	0.00	-14.13	14.81	3.0	30	Y
Jun 90	14.2	9	2.51	3.1	1.14	95.8	5.4	34.6	1.3	-0.65	0.00	-22.60	21.95	2.0	40	Y
Apr 91	30.4	26	3.52	6.8	2.10	19.0	0.9	106.9	1.4	-0.55	0.00	4.53	3.98	2.5	27	N
Jul 91	24.5	8	3.44	2.6	1.32	46.3	0.8	79.5	1.1	-0.86	0.00	-11.38	10.52	3.0	54	Y
Apr 93	12.6	8	2.76	2.9	1.95	13.9	3.8	114.9	0.9	-1.06	0.00	-2.53	1.48	3.0	40	Y
Apr 93	15.0	7	3.95	2.3	2.07	5.8	6.7	125.9	1.5	-0.44	0.00	0.23	-0.67	3.0	40	Y
May 93	10.7	5	3.33	1.7	2.01	21.0	2.8	100.8	1.0	-0.96	0.00	-6.05	5.09	2.5	60	Y
May 93	17.2	5	4.20	2.8	1.90	22.2	2.2	105.0	1.5	-0.44	0.00	-5.00	4.58	3.5	50	Y
Average values													2.4	0.44		
													8.52	3.5	41	
Averages from urban events only													1.5	0.35	9.49	1.6
Averages from events only rural/urban													6.1	3.15	4.2	2.35

Table 2 Estimation of unit hydrograph and losses model parameters by different methods

Method	Time-to-peak $T_p(0)$ (hr)	Standard percentage runoff SPR (%)	Baseflow ANSF ($m^3 s^{-1}$)
Catchment characteristics	7.3	14.3	4.80
Flood event analysis	3.0 4.1 rural/urban 1.1 urban	8.5 3.7 rural/urban 9.5 urban	2.22 3.15 rural/urban 1.57 urban
LAG from flood event analysis	2.8 4.7 rural/urban 1.0 urban	-	-
BFI from flow	-	14.8	-
BFI from HOST	-	23.4	-

Table 3 Refinement of unit hydrograph and losses model parameters for subcatchments

Catchment	Tp(0)ccs (hr)	Tp(0)obs (hr)	SPRccs (%)	SPRobs (%)	ANSF ccs (m ³ s ⁻¹)	ANSF obs (m ³ s ⁻¹)
Ebley Mill	7.30	4.10 rural/urban 1.10 urban	14.3	3.7 rural/urban 9.5 urban	4.80	3.15 rural/urban 1.57 urban
Upper Frome	6.62	3.72	12.7	3.3	1.25	0.82
Toadsmoor Valley	4.75	2.67	19.5	5.1	0.22	0.14
Painswick Stream	4.99	2.80	10.0	2.6	0.82	0.54
Randwick Stream	1.48	0.83	10.0	2.6	0.10	0.07
Slad Brook	4.81	2.70 rural/urban 1.00 urban	10.0	2.6 rural/urban 6.6 urban	0.30	0.20 rural/urban 0.03 urban
Nailsworth Stream	5.06	2.84 rural/urban 1.00 urban	19.5	5.1 rural/urban 13.0 urban	1.07	0.70 rural/urban 0.02 urban
Frome to Severn	7.84	4.40	14.1	3.6	5.47	3.60

Table 4 Breakdown of features of the River Frome models

Feature	Number of occurrences			
	Upper Frome	Lower Frome	Nailsworth Stream	Total
Total sections	482	765	200	1447
Total cells	376	531	173	1080
<hr/>				
River sections	343	354	165	862
Floodplain sections	27	82	0	109
Embankment sections	110	267	30	407
Causeway sections	0	19	3	22
<hr/>				
River cells	239	243	108	590
Structure cells	83	69	45	197
Floodplain cells	40	112	5	157
Junction cells	12	26	7	45
<hr/>				
Bridges	28	23	22	73
Headlosses	9	4	7	20
Sluice elements	35	47	15	97
Weir elements	65	47	15	127
Siphon elements	2	1	0	3
Tide flaps	0	1	0	1
<hr/>				
Permanent breaches	10	1	0	11
Culverts	1	12	0	13

Table 5 Upper Frome sub-model structure elements

Structure name	Structure cell	Element type	Element label
Railway Mill Weir	RFA_180	WR	GWRMLWR1
	RFA_181	WR	GWRMLWR2
		WR	GWRMLWR3
		WR	GWRMLWR4
		WR	GWRMLWR5
Canal Syphon	RFA_183 RFA_184	SY	THSEVSYP
Arundell Mill Sluces	RFA_186	WR	ARUMLWR1
	RFA_187	WR	ARUMLWR2
		SL	ARUMLSL1
		SL	ARUMLSL2
Eagle Mills	RFA_189 RFA_190	BR	CVNWKCUL
Butterow Hill Bridge	RFA_192	BR	BUTHILBR
	RFA_193		
Bowbridge Estate Bridge	RFA_194 RFA_195	BR	BOWESBR1
Housing Estate Link Bridge	RFA_198 RFA_199	BR	BOWESBR2
Stanton's Bridge	RFA_203 RFA_204	BR	BUTFTPBR
Stafford Mills	RFA_207	SL	THRUPSL1
	RFA_208	SL	THRUPSL2
		WR	THRUPWR1
		WR	THRUPWR2
Griffin's Mill Footbridge	RFA_214 RFA_215	HL	GRFMLBR1
Griffin's Mill Bypass Weir	RFA_217	SL	GRFBYSL1
	RFA_218	WR	GRFBYWR1
		WR	GRFBYWR2
		WR	GRFBYWR3
Griffin Mill Estate Bridge	RFA_219 RFA_220	BR	GRFACSBR
Griffin Mill Estate Bridge 2	RFA_221 RFA_222	BR	GRFMLBR2
Phoenix Mill Bypass Channel Bridge	RFA_224 RFA_225	BR	BROOKBR1

Table 5 Continued

Structure name	Structure cell	Element type	Element label
Phoenix Mill Lock Footbridge	RFA_226 RFA_227	BR	HAMLCKBR
Swimming Pool Footbridge	RFA_228 RFA_229	BR	SWMPOLBR
Phoenix Mill Bypass Wall	RFA_230 RFA_231	WR WR WR SL	PHXBYWR1 PHXBYWR2 PHXBYWR3 PHXBYSL1
Thrupp Works Bridge 1	RFA_233 RFA_234	BR	PHXACSBR
Thrupp Works Bridge 2	RFA_235 RFA_236	BR	PHXFTPBR
Thrupp Works Sluices	RFA_237 RFA_238	SL WR WR WR	PHXESSL1 PHXESWR1 PHXESWR2 PHXESWR3
Thrupp Works Bridge 3	RFA_239 RFA_240	BR	HAKSIDBR
Caravan Park Bridge	RFA_241 RFA_242	BR	THPCVNBR
Brimscombe Mill Pond Sluices	RFA_249 RFA_250	SL SL WR	BRIPOSL1 BRIPOSL2 BRIPOWR1
Brimscombe Mill Pond Culvert	RFA_252 RFA_253	HL	BRIPOCUL
Brimscombe Hill Bridge	RFA_254 RFA_255	BR	BRIMSCBR
Brimscombe Port Exit Bridge	RFA_256 RFA_257	BR	BURKETBR
Brimscombe Mill Culvert	RFA_258 RFA_259	HL	BENSNBR1
Brimscombe Mill Access Bridge	RFA_260	BR	BENSNBR2
Brimscombe Mill Sluices	RFA_262 RFA_263	SL WR WR	PTINDSL1 PTINDWR1 PTINDWR2

Table 5 Continued

Structure name	Structure cell	Element type	Element label
Iles Mill Culvert	RFS_002 RFS_003	SL SL WR	ILEMLSL1 ILEMLSL2 ILEMLWR1
Iles Mill Bypass Sluices	RFT_002 RFT_003	SL	ILEBYSL1
Butterow Hill Canal Bridge	SCB_006 SCB_007	HL	BUTCANBR
Bowbridge Lock Weir	SCB_008 SCB_009	WR	BOWLCKWR
Griffin's Mill Lock Weir	SCB_015 SCB_016	WR	GRIFMLWR
Phoenix Mill Lock Weir	SCB_019 SCB_020	WR	HAMLCKWR
Wimberley lock Weir	SCC_005 SCC_006	SL WR WR	WIMCNSL1 WIMCNWR1 WIMCNWR2
St Marys Mill Canal Culvert	SCC_013 SCC_014	WR	ILECNCUL
Iles Mill Lock Weir	SCC_015 SCC_016	WR	ILELCKWR
Springside Canal Culvert	SCC_017 SCC_018	WR	BELMLCUL
Greystones Canal Culvert	SCC_019 SCC_020	SL	CHCANCV1
Chalford Canal Culvert	SCC_021 SCC_022	SL	CHCANCV2
Cowcombe Hill Culvert	SCC_023 SCC_024	SL	CHCHCNCV
Clowes Lock Weir	SCC_026 SCC_027	WR	CLOWESWR
Golden Valley lock Weir	SCC_030 SCC_032	WR WR	GOLDVWR1 GOLDVWR2
Bakers Mill Lower Lock	SCC_046 SCC_047	WR WR SL	BAKCNWR1 BAKCNWR2 BAKCNSL1

Table 5 Continued

Structure name	Structure cell	Element type	Element label
Bakers Mill Upper Lock	SCC_050 SCC_051	WR WR WR	BAKCNWR3 BAKCNWR4 BAKCNWR5
Puck Mill Lower Lock	SCC_057 SCC_058	SL WR	PUCKMSL1 PUCKMWR1
Puck Mill Upper Lock	SCC_059 SCC_060	WR	PUCKMWR2
Whitehall Lower Lock	SCC_061 SCC_062	WR SL	WHITEHWR WHITESL1

Table 6 Lower Frome sub-model structure elements

Structure name	Structure cell	Element type	Element label
Dudbridge Weir	NSA_001 NSA_002	WR SL	NLSOUTWR NLSOUTSL
River Severn Outfall	RFA_001 RFA_001A	FL	RIVSEVFL
Upper Framilode Weir	RFA_002 RFA_003	SL SL SL SL	UFRAMSL1 UFRAMSL2 UFRAMSL3 UFRAMSL4
Gloucester & Sharpness Canal West Channel Siphon	RFA_008A RFA_009	SY	GSCLHCSY
Whitminster West Channel Weir	RFA_012 RFA_013	WR WR WR WR	WHILHWR1 WHILHWR2 WHILHWR3 WHILHWR4
Whitminster Bridge	RFA_015 RFA_016	BR	WHITMIBR
Wheatenhurst Sluices	RFA_018 RFA_019	SL WR WR	WHEATESL WHEATWR1 WHEATWR2
Walk Rhine Bridge	RFA_023 RFA_024	BR	WALKRHBR
Fromebridge Mill	RFA_032 RFA_033	WR WR WR SL	FROMEWR1 FROMEWR2 FROMEWR3 FROMESLS
A38 Road Bridge	RFA_034 RFA_035	BR	A38RODBR
M5 Road Bridge	RFA_039 RFA_040	BR	M5ROADBR
Meadow Mill	RFA_043 RFA_044	HL	MEADOWHL
Meadow Bridge	RFA_048 RFA_049	BR	MEADOWBR

Table 6 Continued

Structure name	Structure cell	Element type	Element label
Millend Mills	RFA_053 RFA_054	SL SL SL SL SL	MILLESL1 MILLESL2 MILLESL3 MILLESL4 MILLESL5
Beards Mill Bridge	RFA_074 RFA_075	BR	BEARMIBR
Beards Mill Side Weir	RFA_076 RFA_077	WR WR	BEARDWR1 BEARDWR2
Stanley Downton Bridge	RFA_087 RFA_088	BR	STDOWNBR
Stanley Mills Weir	RFA_103 RFA_104	SL SL SL SL SL	STANMSL1 STANMSL2 STANMSL3 STANMSL4 STANMSL5
Stanley Mills Bridge	RFA_105 RFA_106	BR	STANMIBR
Redhill Culvert	RFA_114 RFA_115	BR	REDHILBR
Refuse Tip Weir 1	RFA_118 RFA_119	WR WR	REFWR3-1 REFWR3-2
Ebley Corn Mill Sluices	RFA_125 RFA_126	SL	EBCORNSL
Ebley Corn Mill Bridge	RFA_128 RFA_129	BR	EBCORNBR
Ebley Mill Bridge	RFA_135 RFA_136	BR	EBMILLBR
Ebley Mill Weir	RFA_137 RFA_138	WR WR WR	EBMLWR1 EBMLWR2 EBMLWR3
Dudbridge Road Culvert	RFA_145 RFA_146	SL	DUDBRCUL
Redlers Mill Sluices	RFA_147 RFA_148	SL WR WR WR	REDLRSL1 REDLRWR1 REDLRWR2 REDLRWR3

Table 6 Continued

Structure name	Structure cell	Element type	Element label
Fromehall Mill Bypass Sluices	RFA_156 RFA_157	WR WR SL SL WR	FROMLWR1 FROMLWR2 FROMLSL1 FROMLSL2 FROMLWR3
Fromehall Mill Bridge	RFA_159 RFA_160	BR	FRMILLBR
Lodgemore Bridge	RFA_163A RFA_164	BR	LOMILLBR
Lodgemore Mills Sluices	RFA_165 RFA_166	SL WR WR	LODMLSL1 LODMLWR1 LODMLWR2
Lodgemore Mill Culvert	RFA_167 RFA_168	HL	LOMILLCU
Bath Road Bridge	RFA_170 RFA_171	BR	A46BRDBR
Spring Hill Bridge	RFA_002 RFC_003	BR	SPRINGBR
Gloucester & Sharpness Canal East channel Siphon	RFB_003 RFB_004	SY	GSCRHCSY
Whitminster East Channel Weir	RFB_007 RFB_008	SL SL SL SL SL WR	WHIRHSL1 WHIRHSL2 WHIRHSL3 WHIRHSL4 WHIRHSL5 WHIRHWR1
Spring Hill Weir	RFC_001 RFC_001A	WR WR	CARVPWR1 CARVPWR2
Churchend Bridge	RFC_005 RFC_006	BR	CHESCHBR
Churchend Weir	RFC_007 RFC_008	WR WR	CHESCWR1 CHESCWR2
Millend Lane Bridge	RFD_003 RFD_004	BR	MILENDBR
Churchend Sluices	RFD_007 RFD_008	SL SL SL	CHESLSL1 CHESLSL2 CHESLSL3

Table 6 Continued

Structure name	Structure cell	Element type	Element label
Bonds Mill	RFD_019 RFD_020	SL SL	BONCUSL1 BONCUSL2
GWR Embankment Bridge	RFD_025 RFD_026	HL	GWREMBBR
Ocean Pool Bridge	RFD_026 RFD_027	BR	OCPOOLBR
Bridgend Mill Side Weir	RFD_034 RFD_035	SL SL	BRIDGSL1 BRIDGSL2
Bridgend Mill Bridge	RFD_037 RFD_038	BR	BRIDMIBR
Bridgend Kennels Bridge	RFD_043 RFD_044	BR	BRKENNBR
Bridgend Kennels Sluices	RFD_047 RFD_048	SL	BRIKENSL
Downton road Footbridge	RFD_050 RFD_051	BR	DOWNFTBR
Upper Mills Footbridge	RFD_052 RFD_053	BR	UPMIFTBR
Upper Mills Sluices	RFD_054 RFD_055	SL	UPMILLSL
Upper Mills Bridge	RFD_060 RFD_061	BR	UPMILLBR
Ryeford Saw Mills Culvert	RFD_067 RFD_068	SL SL WR	RYEFDSL1 RYEFDSL2 RYEFDWR1
Refuse Tip Weir 3	RFD_078 RFD_079	WR	REFWR1-1
Refuse Tip Weir 2	RFD_080 RFD_081	WR WR	REFWR2-1 REFWR2-2
Market Garden Weir	RFE_004 RFE_005	WR WR	MARGDWR1 MARGDWR2
Beards Mill	RFF_002 RFF_003	WR WR	BEARDWR3 BEARDWR4

Table 6 Continued

Structure name	Structure cell	Element type	Element label
Bonds Mill Side Sluices	RFG_005 RFG_006	SL SL SL SL	BONSLSL1 BONSLSL2 BONSLSL3 BONSLSL4
Ebley Corn Mill Culverts	RFH_003 RFH_004	SL SL	EBCNCUL1 EBCNCUL2
Bridgend Mill Culvert	RFJ_002 RFJ_003	WR	BRIDGCUL
Bridgend Mill Bypass	RFK_003 RFK_004	WR	BRIDGBYP
Banty Ditch Culvert	RFL_010 RFL_011	HL	BANTYCUL
Banty Ditch Weir	RFL_014 RFL_015	WR	BANTYDWR
Fromehall Mill Sluice	RFN_004 RFN_005	SL SL	FRMHLCL1 - FRMHLCL2
Dudbridge Lock Weir	SCA_004 SCA_005	WR	DUDLCKWR
Printing Works Lock Weir	SCA_006 SCA_007	WR	RUSBRKWR
Lodgemore Canal Weir	SCA_012 SCA_013	WR	PSWCKSWR
Cainscross Road Lock Weir	SCA_014 SCA_015	WR WR	CAINSWR1 CAINSWR2

Table 7 Nailsworth Stream sub-model structure elements

Structure name	Structure cell	Element type	Element label
Dudbridge Weir	NSA_001 NSA_002	WR SL	NSOUTFWR NSOUTFSL
Selsley Hill Culvert	NSA_004 NSA_005	BR	SESLILYCV
Erinold Downstream Control Weir	NSA_012 NSA_013	WR	GANTRYWR
Erinold Culvert	NSA_013 NSA_014	HL	ERINODCV
Erinold Bridge	NSA_015 NSA_016	SL	ERINODBR
Car Park Bridge	NSA_018 NSA_019	BR	CARPRKBR
Cotswold House Bridge	NSA_022 NSA_023	HL	COTSHOBR
New Tynings Footbridge	NSA_024 NSA_025	BR	NEWTYNBR
Priory Bridge	NSA_027 NSA_028	HL	PRIORYBR
Rooksmoor Mill Right Channel Culvert	NSA_037 NSA_038	SL	RKSMRCVR
Rooksmoor Mill Weir	NSA_038 NSA_039	WR SL	RKSMRWR1 RKSMRWR2
Selsley road Bridge	NSA_044 NSA_045	BR	SESLILYBR
Selsley Road Weir	NSA_045 NSA_046	WR	SESLILYWR
Paul's Rise Bridge	NSA_047 NSA_048	BR	PAULSRBR
Railway Bridge	NSA_051 NSA_052	BR	NSRAILBR
Forge Weir	NSA_053 NSA_054	WR	FORGEWR
Birds Crossing Bridge	NSA_055 NSA_056	BR	BIRDSXBR

Table 7 Continued

Structure name	Structure cell	Element type	Element label
Station Road Works	NSA_061 NSA_062	SL WR WR SL SL	STRODSL1 STRODWR1 STRODWR2 STRODSL2 STRODSL3
Station Road Bridge	NSA_062 NSA_063	SL WR	STRODSL4 STRODWR3
South Woodchester Works Bridge	NSA_064 NSA_065	BR	STHWODBR
Frogmarsh Lane Bridge	NSA_075 NSA_076	HL	FROGMSBR
Bath Road Bridge	NSA_077 NSA_078	BR	BATHRDBR
Merrett's Mills Bridge	NSA_082 NSA_083	BR	MERRMIBR
Merrett's Mills Culvert	NSA_085 NSA_086	HL	MERRETSLSL
Inchbrook Bridge	NSA_088 NSA_089	BR	INCHBKBR
Inchbrook Culvert	NSA_090 NSA_092	HL	INCHBKSL
Critchley's Bridge 1	NSA_092 NSA_093	BR	CRITHBR1
Critchley's New Culvert	NSA_095 NSA_096	BR	CRITHNCV
Critchley's Bridge 2	NSA_097 NSA_098	BR	CRITHBR2
Dunkirk Mills Culvert	NSA_100 NSA_101	SL	DUNKRSL1
Garage Culvert	NSA_118 NSA_119	BR	GARAGECV
Egypt Mill Weir	NSA_121 NSA_122	WR WR WR	EGYPTWR1 EGYPTWR2 EGYPTWR3
Rooksmoor Mill Left Channel Culvert	NSB_001 NSB_002	SL SL	RKSMRSL1 RKSMRSL2

Table 7 Continued

Structure name	Structure cell	Element type	Element label
Critchley's Left Channel Culvert	NSC_001 NSC_002	WR SL	CRITRDWR CRITHSL2
Critchley's Bridge 3	NSC_007 NSC_008	BR	CRITHBR3
Critchley's Bridge 4	NSC_008 NSC_009	BR	CRITHBR4
Tennis Court Bridge 2	NSC_011 NSC_012	HL	TENISBR2
Dunkirk Mills Bridge 1	NSC_014 NSC_015	BR	DUNKRBR1
Dunkirk Mills Side Spills	NSC_015 NSC_016	WR WR SL	DUNKRWR1 DUNKPWR2 DUNKRSL2
Critchley's Bridge 5	NSD_001 NSD_002	SL	CRITHSL1
Tennis Court Bridge 1	NSD_005 NSD_006	BR	TENNISBR
Elm Brook Bridge	NSD_007 NSD_008	BR	ELMBRKBR
Gables Bridge	NSD_009 NSD_010	BR	GABLESBR
Dunkirk Mills Entrance Bridge	NSD_011 NSD_012	BR	DUNKRBR2
Filling Station Culvert	NSD_018 NSD_019	SL WR	FILSTCV1 FILSTCV2

Table 8 Upper Frome Sub-model sluice gate openings

Element Label	Fixed Opening	Minimum Opening	Maximum Opening
ARUMLSL1	-	0.00	1.30
ARUMLSL2	-	0.00	1.30
THRUPSL1	1.23	-	-
THRUPSL2	1.19	-	-
GRFBYSL1	0.35	-	-
PHXBYSL1	0.50	-	-
PHXESSL1	0.30	-	-
BRIPOS1	0.25	-	-
BRIPOS2	-	0.00	1.00
PTINDSL1	-	0.00	0.80
PHXMLSL1	-	0.00	1.80
BORMSL1	0.80	-	-
BORMSL2	1.15	-	-
MARBYSL1	0.72	-	-
MARBYSL2	0.57	-	-
ILEUPSL1	0.80	-	-
CHINDSL1	0.45	-	-
CHINDSL2	-	0.00	1.20
CHINDSL3	0.10	-	-
RIDLDSL1	0.62	-	-
BAKERSBR	1 1.80	-	-
BAKERSL1	-	0.00	0.60
MARMLSL1	1.34	-	-
ILEMLSL1	0.20	-	-
ILEMLSL2	-	0.00	0.70
ILEBYSL1	-	0.00	0.80
WIMCNSL1	0.10	-	-
CHCANCV1	1 1.20	-	-
CHCANCV2	1 0.55	-	-

Table 8 Continued

Element Label	Fixed Opening	Minimum Opening	Maximum Opening
BAKCNSL1	0.10	-	-
PUCKMSL1	0.10	-	-
WHITESL1	0.10	-	-
CHCHCNCV	1 1.16	-	-
THANHOBR	1 2.35	-	-
PUCKCULV	1 1.31	-	-

Notes:

- 1 These structures are culverts represented using the orifice type flow equation of a sluice gate.

Table 9 Lower Frome Sub-model sluice gate openings

Element Label	Fixed Opening	Minimum Opening	Maximum Opening
NLSOUTSL	1.00	-	-
RIVSEVFL	2 2.75	-	-
UFRAMSL1	2.93	-	-
UFRAMSL2	1.82	-	-
UFRAMSL3	1.24	-	-
UFRAMSL4	0.61	-	-
WHEATESL	-	0.0	1.80
FROMESLS	-	0.0	1.7
MILLESL1	0.50	-	-
MILLESL2	0.50	-	-
MILLESL3	0.90	-	-
MILLESL4	1.10	-	-
MILLESL5	0.90	-	-
STANMSL1	0.69	-	-
STANMSL2	0.66	-	-
STANMSL3	0.74	-	-
STANMSL4	-	0.00	1.30
STANMSL5	-	0.00	1.30
EBCORNSL	1.35	-	-
DUDBRCUL	1 1.55	-	-
REDLRSL1	-	0.00	1.30
FROMSL1	0.40	-	-
FROMSL2	0.30	-	-
LODMLSL1	-	0.00	1.30
WHIRHSL1	1.83	-	-
WHIRHSL2	1.51	-	-
WHIRHSL3	1.19	-	-
WHIRHSL4	0.87	-	-
WHIRHSL5	0.55	-	-

Table 9 Continued

Element Label	Fixed Opening	Minimum Opening	Maximum Opening
CHESLSSL1	1.14	-	-
CHESLSSL2	1.55	-	-
CHESLSSL3	1.58	-	-
BRIDGSL1	0.05	-	-
BRIDGSL2	0.00	-	-
BRIKENSL	1.42	-	-
UPMILLSL	1.30	-	-
RYEFDSL1	-	0.00	1.60
RYEFDSL2	-	0.00	1.85
BONSLSL1	0.00	-	-
BONSLSL2	1.10	-	-
BONSLSL3	1.30	-	-
BONSLSL4	1.30	-	-
EBCNCUL1	1 1.36	-	-
EBCNCUL2	1 1.61	-	-
FRMHLC1	0.68	-	-
FRMHLC2	0.45	-	-
BONCUSL1	1 1.91	-	-
BONCUSL2	1 1.94	-	-

Notes:

- 1 These structures are culverts represented using the orifice type flow equation of a sluice gate.
- 2 This is a flapped outfall.

Table 10 Nailsworth Stream Sub-model sluice gate openings

Element Label	Fixed Opening	Minimum Opening	Maximum Opening
NSOUTFSL	1.00	-	-
RKSMRCVR	1 1.59	-	-
RKSMRWR2	0.326	-	-
STRODSL1	0.90	-	-
STRODSL2	0.40	-	-
STRODSL3	0.00	-	-
STRODSL4	1.72	-	-
DUNKRSL1	0.60	-	-
RKSMRSL1	0.30	-	-
RKSMRSL2	0.39	-	-
CRITHSL1	1.49	-	-
DUNKRSL2	0.70	-	-
CRITHSL2	0.69	-	-
FILSTACV	1 1.06	-	-
ERINODBR	2 1.62	-	-

Notes:

- 1 These structures are culverts represented using the orifice type flow equation of a sluice gate.
- 2 This structure is a bridge represented using the orifice type flow equation of a sluice gate.

Table 11 Embankment and causeway structures included in the River Frome Sub-models

Structure location	Model section	Structure type	Label
Upper Frome sub-model			
Canal link to river upstream of canal siphon	ELA_185	PB PB	CAN2RFA1 CAN2RFA2
Canal link to river upstream of Bourne Mills	ERQ_004	PB	CAN2RFQ1
Link between River Frome and canal d/s of St Marys House	ERA_301A	CV	MARYLINK
Link between Ashmead Mill channel and River Frome	ERA_358	PB	ASHMDPB
Bakers Mill reservoir spills	ERA_369	PB PB	BARESPB1 BARESPB2
Links between the River Frome and Bakers Mill reservoir	ERA_371	PB	BARESPB3
	ERA_372	PB	BARESPB4
	ERA_373	PB	BARESPB5
	ERA_374	PB	BARESPB6
Lower Frome sub-model			
Culverts adjacent to Walk Bridge	CLA_015	CV	WALKCV
	CLA_017	CV	WALKCV2
A38 road bridge left hand culvert	CLA_035	CV	A38CV1
A38 road bridge right hand culverts	CRA_035B	CV CV	A38CV2 A38CV3
	CLA_039	CV	M5CV1

Table 11 Continued

Structure location	Model section	Structure type	Label
M5 road bridge right hand culverts and foot tunnel	CRA_039	CV CV	M5CV2 M5CV3
Millend Lane culvert	CRA_053	CV	MILLEND CV
Railway embankment central culvert	CLD_026	CV	RAILCV1
Ryeford underpass	CRL_011	CV	RYEFDUP
Ryeford Road railway bridge	CLA_067	CV	RYEFDRY
Link between River Frome and Fromehall Mill pond	ERA_161	PB	FRMHL PND
Nailsworth Stream sub-model			
Left channel feed into Dunkirk Mills ponds	ERD_021	PB	PB1
	ERD_018	PB	PB2
Link between Dunkirk Mills ponds	CLA_111	CV	CV1
	CLA_110	CV	CV2
Right channel feed into Dunkirk Mills ponds	ELA_108	CV	CV3

Table 12 Locations of model inflows for the River Frome Sub-models

Inflow name	Type	Location	Scaling factor
Upper Frome sub-model			
Upper Frome	Upstream boundary	RFA_389	-
Upper Middle Frome	Lateral inflow	RFA_279 - RFA_298 RFA_299 - RFA_302 RFA_303 - RFA_307 RFA_308 - RFA_311 RFA_312 - RFA_316 RFA_317 - RFA_389	0.1922 0.0210 0.0275 0.0194 0.0275 0.7124
Toadsmoor Stream	Tributary inflow	RFA_278 - RFA_279	-
Lower Middle Frome	Lateral inflow	RFA_175 - RFA_209 RFA_210 - RFA_218 RFA_219 - RFA_222 RFA_223 - RFA_231 RFA_232 - RFA_271 RFA_272 - RFA_276 RFA_277 - RFA_278	0.2790 0.0734 0.0147 0.0457 0.2741 0.0326 0.0098
Downstream Boundary	Rating section	RFA_175	-
Thames & Severn Canal - Upper reach	Upstream boundary	SCC_070	-
Thames & Severn Canal - Upper reach	Rating section	SCC_001	-
Thames & Severn Canal - Lower reach	Upstream boundary	SCB_024	-

Table 12 Continued

Inflow name	Type	Location	Scaling factor
Thames & Severn Canal - Lower reach	Rating section	SCB_001	-
Lower Frome sub-model			
Lower Frome	Upstream boundary	RFA_175	-
Nailsworth Stream	Upstream boundary	NSA_002	-
Slad Brook	Upstream boundary	SCA_016	-
Painswick Stream	Tributary inflow	SCA_011 - SCA_012	-
Randwick Stream	Tributary inflow	SCC_005 - SCC_006	-
Lower Middle Frome	Lateral inflow	RFA_145 - RFA_153 RFA_154 - RFA_161 RFA_162 - RFA_175	0.0935 0.0581 0.1191

Table 12 Continued

Inflow name	Type	Location	Scaling factor	
Lower Frome	Lateral inflow	RFA_001 - RFA_005 RFA_006 - RFA_013 RFB_001 - RFB_008 RFA_015 - RFA_046 RFC_001 - RFC_009 RFA_050 - RFA_071 RFD_008A - RFD_011 RFD_012 - RFD_017 RFD_021 - RFD_031 RFA_078 - RFA_099 RFA_100 - RFA_119 RFD_040 - RFD_046 RFD_047 - RFD_066 RFD_067 - RFD_081 RFA_128 - RFA_140 RFA_141 - RFA_144		0.0482 0.0487 0.0605 0.2381 0.0230 0.1120 0.0174 0.0263 0.0459 0.1059 0.0835 0.0190 0.0571 0.0599 0.0410 0.0135
Downstream Boundary	Stage boundary	RFA_001	-	
Stanley Mills - mill stream	Upstream boundary	RFM_003	-	
Dudbridge - relict Frome	Upstream boundary	RFX_007	-	
Nailsworth Stream sub-model				
Nailsworth Stream	Upstream boundary	NSA_124	-	

Table 12 Continued

Inflow name	Type	Location	Scaling factor
Lower Nailsworth	Lateral inflow	NSD_002 - NSD_021 NSD_022 - NSD_031 NSA_096 - NSA_101 NSA_102 - NSA_113 NSA_114 - NSA_122 NSC_003 - NSC_004 NSA_001 - NSA_036 NSA_040 - NSA_094	0.03773 0.01802 0.01104 0.02760 0.01711 0.35760 0.22503 0.30587
Egypt Mill - wheel channel	Upstream boundary	NSD_024	-
Downstream boundary	Stage boundary	NSA_001	-

Table 13 Availability of calibration data for the River Frome models

Calibration event	Location	Record type	Equivalent model section
5 January 1994	Ebley Mill gauging station	Continuous level recorder & flows	RFA_139
	C1 - Persimon Homes Nailsworth Stream	Continuous level recorder	NSA_001
	C2 - Dudbridge Weir Stroudwater Canal	Continuous level recorder	SCA_005
	C3 - Thrupp River Frome	Continuous level recorder	RFA_220
	C4 - Golden Valley River Frome	Continuous level recorder	RFA_360 + (RFA_361 - RFA_360)*0.25 81
	C5 - Egypt Mill Nailsworth Stream	Continuous level recorder	NSA_124
	M1 - Eastington River Frome	Peak level recorder	RFA_045 + (RFA_046 - RFA_045)*0.25 75
	M3 - Ryeford Cableways	Peak level recorder	CELL 89A
	M4 - Ryeford South River Frome	Peak level recorder	RFA_109 + (RFA_110 - RFA_109)*0.53 28
	M5 - Wallbridge River Frome	Peak level recorder	RFA_172 + (RFA_173 - RFA_172)*0.79 36
	M6 - Brimscombe River Frome	Peak level recorder	RFA_265 + (RFA_266 - RFA_265)*0.72 57

Table 13 Continued

Calibration event	Location	Record type	Equivalent model section
5 January 1994	M7 - Chalford River Frome	Peak level recorder	
	M8 - Upper Framilode River Frome	Peak level recorder	RFA_006 + (RFA_007 - RFA_006)*0.5806
	M10 - Woodchester Nailsworth Stream	Peak level recorder	NSA_050
30 May 1979	Ebley Mill gauging station	Continuous level recorder & flows	RFA_139
18 December 1965	d/s Red Lion PH	Observed level	RFA_331
	u/s Boume Mill	Observed level	RFA_271
	u/s Brimscombe Mill Pond Culvert	Observed level	RFA_253
	Brimscombe Mill Pond	Observed level	RFA_250
	u/s Thrupp Works	Observed level	RFA_238
	d/s Thrupp Works	Observed level	RFA_236
	u/s Phoenix Mills	Observed level	RFA_232
	d/s Griffin's Mill Bypass Weir	Observed level	RFA_216
	d/s Phoenix Mills	Observed level	RFP_003
	d/s Griffin's Mill	Observed level	RFO_008

Table 13 Continued

Calibration event	Location	Record type	Equivalent model section
18 December 1965	u/s Stafford's Mill	Observed level	RFA_208
	u/s Stanton's Bridge	Observed level	RFA_204
	d/s Butterow Bridge	Observed level	RFA_192
	d/s Eagle Mills	Observed level	RFA_189
	u/s Arundell Mill	Observed level	RFA_187

Table 14 Comparison of SALMON-F model and physical model levels at Ebley Mill

Discharge (m³/s)	Ebley Mill gauging station level (mOD)	Difference (m)
20	32.012	-0.070
25	32.033	-0.018
30	32.074	+0.002
35	32.099	+0.031
40	32.146	+0.030
45	32.200	+0.032
50	32.294	-0.006
55	32.416	-0.057
60	32.519	-0.087
67	32.606	-0.034
75	32.683	+0.041
90	32.799	+0.159

Table 15 Comparison of observed and predicted peak water levels - January 1994 calibration event

Gauge location	Peak water level (mOD)		
	Observed	Predicted	Difference (m)
C1	34.803	34.816	+0.013
C2	34.205	34.233	+0.028
C3	[see text]	48.306	-
C4	[see text]	79.670	-
C5	57.908	57.906	-0.002
M1	13.472	13.547	+0.075
M4	28.150	28.144	-0.006
M5	38.449 / 38.596	38.383	-0.066 / -0.213
M6	56.910 / 57.066	57.029	+0.119 / -0.037
M7	72.384	72.167	-0.217
M8	7.350	7.365	+0.015
M9	8.600	7.637	-0.963
M10	43.670	43.697	+0.027
Ebley Mill	31.686	31.744	+0.058
Peak flow (m ³ /s)			
Ebley Mill	11.84	12.97	11.32

Table 16 Comparison of observed and predicted peak water levels - May 1979 calibration event

Gauge location	Peak water level (mOD)		
	Observed	Predicted	Difference (m)
C1	-	31.588	-
C2	-	34.518	-
C3	-	48.429	-
C4	-	79.818	-
C5	-	58.126	-
M1	-	13.937	-
M3	-	26.590	-
M4	-	28.252	-
M5	-	38.601	-
M6	-	57.166	-
M7	-	72.245	-
M8	-	7.157	-
M9	-	7.546	-
M10	-	44.008	-
Ebley Mill	31.923	32.008	+0.085
Peak flow (m³/s)			
Ebley Mill	19.2	21.3	+1.9

Table 17 Comparison of observed and predicted peak water levels - December 1965 flood event

Gauge location / model section	Peak water level (mOD)		
	Observed level	Predicted level	Difference (m)
C1	-	35.234	-
C2	-	34.570	-
C3	-	48.463	-
C4	-	79.884	-
C5	-	58.136	-
M1	-	14.300	-
M3	-	26.594	-
M4	-	28.240	-
M5	-	38.634	-
M6	-	57.109	-
M7	-	72.328	-
M8	-	7.657	-
M9	-	7.927	-
M10	-	44.012	-
Ebley Mill	-	32.047	-
Peak flow (m³/s)			
Ebley Mill	-	24.133	-
Observed peak water levels (mOD)			
RFA_253 - u/s Brimscombe Mill Pond Culvert	55.960	56.024	+0.064
Ebley Mill	-	32.047	-
Peak flow (m³/s)			
Ebley Mill	-	24.133	-
Observed peak water levels (mOD)			
RFA_253 - u/s Brimscombe Mill Pond Culvert	55.960	56.024	+0.064

Table 17 Continued

Gauge location / model section	Peak water level (mOD)		
	Observed level	Predicted level	Difference (m)
Observed peak water levels (mOD)			
RFA_250 - Brimscombe Mill Pond	55.390	55.425	+0.035
RFA_238 - u/s Thrupp Works	52.020	51.984	-0.036
RFA_236 - d/s Thrupp Works	50.730	50.570	-0.160
RFA_232 - u/s Phoenix Mills	50.250	50.044	-0.206
RFA_216 - d/s Griffin's Mill Bypass Weir	47.860	47.901	+0.041
RFP_003 - d/s Phoenix Mills	48.770	48.611	-0.159
RFO_009 - d/s Griffin's Mill	47.610	47.679	+0.069
RFA_208 - u/s Stafford's Mill	46.900	46.864	-0.036
RFA_204 - u/s Stanton's Bridge	45.880	45.916	+0.036
RFA_192 - d/s Butterow Bridge	44.640	44.509	-0.131
RFA_189 - d/s Eagle Mills	43.410	43.555	+0.145
RFA_187 - u/s Arundell Mill	43.370	43.428	+0.058
RFA_184 - u/s Canal Syphon	42.720	42.461	-0.259
RFA_183 - d/s Canal Syphon	42.160	41.740	-0.420
RFA_182 - u/s Railway Mill	41.290	41.687	+0.397
RFA_175 - George Kent & Co., Wallbridge	39.720	39.314	-0.406

Table 17 Continued

Gauge location / model section	Peak water level (mOD)		
	Observed level	Predicted level	Difference (m)
Observed peak water levels (mOD)			
RFA_172 - Wallbridge	39.980	38.498	-1.482
RFA_146 - u/s Dudbridge Culvert	33.440	32.618	-0.822
RFA_118 - d/s Refuse Tip Weir 1	28.860	28.711	-0.149
RFA_114 - u/s Redhill Culvert	28.490	28.345	-0.145
RFA_106 - u/s Stanley Mills Bridge	28.020	28.124	+0.104
RFA_104 - u/s Stanley Mills Weir	27.830	28.107	+0.277
RFA_087 - d/s Stanley Downton Bridge	22.330	21.738	-0.592
RFA_078 - u/s Beards Mill	20.220	20.197	+0.023
RFA_074 - u/s Beards Mill road bridge	18.640	18.716	+0.076
RFA_054 - u/s Millend Mills	16.810	15.758	-1.052
RFA_053 - d/s Millend Mills	15.670	14.880	-0.790
RFA_046 - d/s Spring Hill Weir	14.470	14.330	-0.140
RFA_044 - u/s Meadow Mill	14.440	14.298	-0.142
RFD_080 - d/s Refuse Tip Weir 2	28.790	28.858	+0.068
RFD_075 - Ryeford North Channel	28.250	28.117	-0.133
RFD_061 - Upper Mills Bridge	25.370	25.060	-0.310
RFD_057 - u/s Upper Mills Sluices	24.980	24.958	-0.022

Table 17 Continued

Gauge location / model section	Peak water level (mOD)		
	Observed level	Predicted level	Difference (m)
Observed peak water levels (mOD)			
RFD_043 - u/s Bridgend Kennels Bridge	22.330	22.339	+0.009
RFD_038 - u/s Bridgend Mill Bridge	22.136	22.034	-0.102
RFD_033 - Lower Mills d/s Sluice	21.220	20.635	-0.585
RFD_025 - North Channel u/s Railway	19.480	19.483	+0.003
RFD_021 - u/s Bonds Mill	19.330	19.197	-0.133
RFD_017 - d/s Bonds Mill	16.880	16.751	-0.129
RFC_004 - Eastington church	14.940	14.765	-0.175
RFC_003 - u/s Eastington road bridge	14.660	14.756	+0.096
RFL_014 - Banty Ditch	25.540	25.018	-0.522
SCA_005 - Dudbridge Lock Weir	34.640	34.570	-0.070
CELL 52 - d/s Railway embankment	19.400	18.417	-0.070
CELL 81 - d/s Ryeford Road	25.950	24.979	-0.971
CELL 89 - Ryeford Saw Mills	26.740	26.604	-0.136
CELL 90 - Ryeford Saw Mills	28.094	27.491	-0.603
CELL 85 - Ryeford Canal	28.350	27.899	-0.451

Table 18 Final roughness parameters for the River Frome models

Model reach	Channel ks	Floodplain ks
Upper Frome sub-model		
RFA_175 - RFA_389	0.60	2.00
RFO_001 - RFO_012	0.60	2.00
RFP_001 - RFP_006	0.60	2.00
RFQ_001 - RFQ_004	0.60	2.00
RFR_001 - RFR_002	0.60	2.00
RFS_001 - RFS_007	0.60	2.00
RFT_001 - RFT_003	0.60	2.00
SCB_001 - SCB_024	0.60	2.00
SCC_001 - SCC_070	0.60	2.00
All Floodplain sections		2.00
Lower Frome sub-model		
NSA_001 - NSA_002	0.60	2.00
RFA_001 - RFA_032	0.60	2.00
RFA_033 - RFA_048	0.80	2.00
RFA_050 - RFA_053	1.50	2.00
RFA_049 - RFA_077	0.60	2.00
RFA_078 - RFA_087	1.50	2.00
RFA_088 - RFA_103	0.60	2.00
RFA_104 - RFA_118	1.00	2.00
RFA_119 - RFA_170	0.60	2.00
RFA_171 - RFA_175	2.00	2.00
RFB_001 - RFB_008	0.60	2.00
RFC_001 - RFC_009	1.50	2.00
RFD_001 - RFD_067	0.60	2.00
RFD_068 - RFD_081	1.00	2.00
RFF_001 - RFF_003	0.60	2.00
RFG_001 - RFG_006	0.60	2.00

Table 18 Continued

Model reach	Channel ks	Floodplain ks
Upper Frome sub-model		
RFJ_001 - RFJ_003	0.60	2.00
RFK_001 - RFK_004	0.60	2.00
RFL_001 - RFL_016	1.00	2.00
RFM_001 - RFM_003	0.60	2.00
RFH_001 - RFH_004	0.60	2.00
RFN_001 - RFN_006	0.60	2.00
RFX_001 - RFX_007	0.60	2.00
SCA_001 - SCA_016	0.60	2.00
RFE_001 - RFE_005	1.00	2.00
All Floodplain	-	2.00
Nailsworth Stream sub-model		
NSA_001 - NSA_124	0.60	2.00
NSB_001 - NSB_002	0.60	2.00
NSC_001 - NSC_016	0.60	2.00
NSD_001 - NSD_024	0.60	2.00
NSE_001 - NSE_002	0.60	2.00

Table 19 Final structure coefficients - Upper Frome sub-model

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Railway Mill Weir	GWRMLWR1	WR	1.50	0.67
	GWRMLWR2	WR	1.50	0.67
	GWRMLWR3	WR	1.50	0.67
	GWRMLWR4	WR	1.50	0.67
	GWRMLWR5	WR	1.50	0.67
Canal Syphon	THSEVSY	SY	0.50	0.67
Arundell Mill Sluices	ARUMLWR1	WR	0.90	0.67
	ARUMLWR2	WR	0.90	0.67
	ARUMLSL1	SL	0.90	0.67
	ARUMLSL2	SL	0.90	0.67
Eagle Mills	CVNWKCUL	BR	10.00	
Butterow Hill Bridge	BUTHILBR	BR	1.00	
Bowbridge Estate Bridge	BOWESBR1	BR	1.00	
Housing Estate Link Bridge	BOWESBR2	BR	1.00	
Stanton's Bridg	BUTFTPBR	BR	0.70	
Stafford Mills	THRUPSL1	SL	0.80	0.67
	THRUPSL2	SL	0.80	0.67
	THRUPWR1	WR	0.80	0.67
	THRUPWR2	WR	0.40	0.67
Griffin's Mill Footbridge	GRFMLBR1	HL	0.73	
Griffin's Mill Bypass Weir	GRFBYSL1	SL	0.90	0.67
	GRFBYWR1	WR	1.00	0.67
	GRFBYWR2	WR	1.00	0.67
	GRFBYWR3	WR	0.40	0.67
Griffin Mill Estate Bridge	GRFACSBR	BR	1.00	

Table 19 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Griffin Mill Estate Bridge 2	GRFMLBR2	BR	1.00	
Phoenix Mill Bypass Channel Bridge	BROOKBR1	BR	1.00	
Phoenix Mill Lock Footbridge	HAMLCKBR	BR	1.00	
Swimming Pool Footbridge	SWMPOLBR	BR	1.00	
Phoenix Mill Bypass Weir	PHXBYWR1	WR	0.70	0.67
	PHXBYWR2	WR	0.40	0.67
	PHXBYWR3	WR	0.50	0.67
	PHXBYSL1	SL	0.70	0.67
Thrupp Works Bridge 1	PHXACSBR	BR	1.00	
Thrupp Works Bridge 2	PHXFTPBR	BR	1.00	
Thrupp Works Sluices	PHXESSL1	SL	0.70	0.67
	PHXESWR1	WR	0.80	0.67
	PHXESWR2	WR	0.50	0.67
	PHXESWR3	WR	0.40	0.40
Thrupp Works Bridge 3	HAKSIDBR	BR	1.00	
Caravan Park Bridge	THPCVNBR	BR	1.00	
Brimsccombe Mill Pond Sluices	BRIPOSL1	SL	1.00	0.67
	BRIPOSL2	SL	1.00	0.67
	BRIPOWR1	WR	0.40	0.40
Brimsccombe Mill Pond Culvert	BRIPOCUL	HL	0.50	
Brimsccombe Hill Bridge	BRIMSCBR	BR	1.00	
Brimsccombe Port Exit Bridge	BURKETBR	BR	1.00	

Table 19 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Brimsccombe Mill Culvert	BENSNBR1	BR	1.00	
Brimsccombe Mill Access Bridge	BENSNBR2	HL	0.15	
Brimsccombe Mill Sluices	PTINDSL1	SL	0.80	0.67
	PTINDWR1	WR	0.80	0.67
	PTINDWR2	WR	0.80	0.67
Brimsccombe Port Bridge	PORTINBR	BR	1.00	
Boume Mill Bypass Sluices	BORMLWR1	WR	0.70	0.67
	BORMLWR2	WR	0.40	0.40
Wimberley Mills Weir	WIMMLWR1	WR	1.00	0.67
	WIMMLWR2	WR	1.00	0.67
	WIMMLWR3	WR	0.90	0.67
	WIMMLWR4	WR	0.40	0.67
	WIMMLWR5	WR	0.40	0.40
Knapp Lane Bridge	WIMBERBR	BR	1.00	
Wimberley Mills Culvert 1	WIMBCUL1	HL	0.04	
Wimberley Mills Culvert 2	WIMBCUL2	HL	0.53	
St Marys Mill Weir	MARCNWR1	WR	1.00	0.67
	MARCNWR2	WR	1.00	0.67
St Marys Mill Bypass Sluices	MARBYSL1	SL	0.70	0.67
	MARBYSL2	SL	0.80	0.67
St Marys House Culvert	MARHSCUL	BR	1.00	
Iles Mill Railway Culvert	ILERLCUL	BR	1.00	
Iles Mill Bridge	ILESMLBR	BR	1.00	

Table 19 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Illes Mill Bypass Weirs	ILEUPWR1	WR	0.80	0.67
	ILEUPSL1	SL	0.80	0.67
Belvedere Mill	BELVEWR1	WR	1.00	0.67
	BELVEWR2	WR	1.00	0.67
Belvedere Pond Bridge	BELVMLBR	BR	1.00	
Chalford Industrial Estate	CHINDSL1	SL	0.70	0.67
	CHINDSL2	SL	0.80	0.67
	CHINDSL3	SL	0.50	0.67
Chalford Chairs Culvert	CHLCHCUL	HL	0.50	
Thanet House Bridge	THANHOBR	SL	1.50	0.80
Red Lion Bridge	REDLINBR	HL	0.32	
Brooklyn Bridge	BRKLYNBR	BR	1.00	
Sub Stn. Bridge	SUBSTNBR	BR	1.00	
Ridley Mill Sluices	RIDLYSL1	SL	1.00	0.67
	RIDLWWR1	WR	0.70	0.67
Harley Lane Culverts	HARLEYBR	BR	1.00	
Ashmeade Sluices	ASHMDWR1	WR	0.90	0.67
	ASHMDWR2	WR	0.90	0.67
	ASHMDWR4	WR	0.70	0.67
Bakers Bridge	BAKERSBR	SL	0.90	0.67
Bakers Mill Sluices	BAKERWR1	WR	0.80	0.67
	BAKERWR2	WR	0.80	0.67
	BAKERSL1	SL	1.00	0.67
Puck Mill Culvert	PUCKCULV	SL	0.50	0.67

Table 19 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Clinton House Footbridge	GRFMLBR3	BR	1.00	
Griffin's Mill d/s Weir	GRFMLWR1	WR	0.90	0.67
	GRFMLWR2	WR	1.00	0.67
	GRFMLWR3	WR	0.40	0.40
Griffin's Mill Culvert	GRFMLCUV	HL	0.35	
Griffin's Mill u/s Weir	GRFMLWR4	WR	0.80	0.67
	GRFMLWR5	WR	0.80	0.67
	GRFMLWR6	WR	0.90	0.67
Phoenix Mill Stream Bridge	BROOKBR2	BR	1.00	
Phoenix Mill	PHXMLSL1	SL	0.80	0.67
Bourne Mill Sluices	BORMLSL1	SL	0.80	0.67
	BORMLSL2	SL	0.80	0.67
St Marys Mill Culvert	MARMLSL1	SL	1.10	0.67
Iles Mill Culvert	ILEMMLSL1	SL	1.00	0.67
	ILEMMLSL2	SL	0.90	0.67
	ILEMMLWR1	WR	0.90	0.67
Iles Mill Bypass Sluices	ILEBYSL1	SL	0.80	0.67
Butterow Hill Canal Bridge	BUTCANBR	HL	1.40	
Bowbridge Lock Weir	BOWLCKWR	WR	1.00	0.67
Griffin's Mill Lock Weir	GRIFMLWR	WR	1.00	0.67
Phoenix Mill Lock Weir	HAMLCKWR	WR	1.00	0.67
Wimberley lock Weir	WIMCNSL1	SL	0.80	0.67
	WIMCNWR1	WR	1.00	0.67
	WIMCNWR2	WR	1.00	0.67

Table 19 Continued

Structure Name	Element label	Element Type	Cd, K, Af	Dr
Iles Mill Lock Weir	ILELCKWR	WR	1.00	0.67
Springside Canal Culvert	BELMLCUL	WR	0.90	0.67
Greystones Canal Culvert	CHCANCV1	SL	0.90	0.67
Chalford Canal Culvert	CHCANCV2	SL	0.90	0.67
Cowcombe Hill Culvert	CHCHCNCV	SL	0.50	0.67
Clowes Lock Weir	CLOWESWR	WR	0.40	0.67
Golden Valley lock Weir	GOLDWWR1	WR	1.00	0.67
	GOLDWWR2	WR	1.00	0.67
Bakers Mill Lower Lock	BAKCNWR1	WR	0.90	0.67
	BAKCNWR2	WR	0.90	0.67
	BAKCNSL1	SL	0.80	0.67
Bakers Mill Upper Lock	BAKCNWR3	WR	1.10	0.67
	BAKCNWR4	WR	1.00	0.67
	BAKCNWR5	WR	1.00	0.67
Puck Mill Lower Lock	PUCKMSL1	SL	0.80	0.67
	PUCKMWR1	WR	0.90	0.67
Puck Mill Upper Lock	PUCKMWR2	WR	0.90	0.67
Whitehall Lower Lock	WHITEHWR	WR	1.00	0.67
	WHITESL1	SL	0.80	0.67

Table 20 Final structure coefficients - Lower Frome sub-model

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Dudbridge Weir	NLSOUTWR	WR	0.90	0.67
	NLSOUTSL	SL	0.90	0.67
River Severn Outfall	RIVSEVFL	FL	0.80	0.67
Upper Framilode Weir	UFRAMSL1	SL	0.90	0.10
	UFRAMSL2	SL	0.40	0.67
	UFRAMSL3	SL	0.40	0.67
	UFRAMSL4	SL	0.40	0.67
G&S canal West Siphon	GSCLHCSY	SY	0.80	0.67
Whitminster West Channel Weir	WHILHWR1	WR	0.90	0.67
	WHILHWR2	WR	0.60	0.67
	WHILHWR3	WR	0.60	0.67
	WHILHWR4	WR	0.60	0.67
Whitminster Bridge	WHITMIBR	BR	1.00	
Wheatenhurst Sluices	WHEATESL	SL	0.80	0.67
	WHEATWR1	WR	0.80	0.67
	WHEATWR2	WR	0.90	0.67
Walk Rhine Bridge	WALKRHBR	BR	1.00	
Fromebridge Mill	FROMEWR1	WR	0.80	0.67
	FROMEWR2	WR	0.80	0.67
	FROMEWR3	WR	0.80	0.67
	FROMESLS	SL	0.80	0.67
A38 Road Bridge	A38RODBR	BR	1.00	
M5 Road Bridge	M5ROADBR	BR	1.00	
Meadow Mill	MEADOWHL	HL	1.50	
Meadow Bridge	MEADOWBR	BR	1.00	

Table 20 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Millend Mills	MILLESL1	SL	0.80	0.67
	MILLESL2	SL	0.80	0.67
	MILLESL3	SL	0.50	0.67
	MILLESL4	SL	0.50	0.67
	MILLESL5	SL	0.50	0.67
Beards Mill Bridge	BEARMIBR	BR	1.00	
Beards Mill Side Weir	BEARDWR1	WR	0.50	0.67
	BEARDWR2	WR	0.20	0.67
Stanley Downton Bridge	STDOWNBR	BR	1.00	
Stanley Mills Weir	STANMSL1	SL	1.10	0.67
	STANMSL2	SL	1.10	0.67
	STANMSL3	SL	1.10	0.67
	STANMSL4	SL	1.10	0.67
	STANMSL5	SL	1.10	0.67
Stanley Mills Bridge	STANMIBR	BR	1.00	
Redhill Culvert	REDHILBR	BR	50.00	
Refuse Tip Weir 1	REFWR3-1	WR	0.90	0.95
	REFWR3-2	WR	0.40	0.40
Ebley Corn Mill Sluices	EBCORNSL	SL	0.80	0.67
Ebley Corn Mill Bridge	EBCORNBR	BR	1.00	
Ebley Mill Bridge	EBMILLBR	BR	1.00	
Ebley Mill Weir	EBMLWR1	WR	1.10	0.67
	EBMLWR2	WR	0.85	0.67
	EBMLWR3	WR	0.60	0.67
Dudbridge Road Culvert	DUDBRCUL	SL	0.90	0.67

Table 20 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Redlers Mill Sluices	REDLRLS1	SL	0.80	0.67
	REDLWR1	WR	0.80	0.67
	REDLWR2	WR	0.80	0.67
	REDLWR2	WR	0.80	0.67
Fromehall Mill Bypass Sluices	FROMLWR1	WR	0.90	0.67
	FROMLWR2	WR	0.90	0.67
	FROMLSL1	SL	0.70	0.67
	FROMLSL2	SL	0.70	0.67
	FROMLWR3	WR	0.80	0.67
Fromehall Mill Bridge	FRMILLBR	BR	1.00	
Lodgemore Bridge	LOMILLBR	BR	1.00	
Lodgemore Mills Sluices	LODMLSL1	SL	0.90	0.67
	LODMLWR1	WR	0.80	0.67
	LODMLWR2	WR	0.70	0.67
Lodgemore Mills Culvert	LOMILLCU	HL	1.00	
Bath Road Bridge	A46BRDBR	BR	5.00	
Spring Hill Bridge	SPRINGBR	BR	50.00	
G&S Canal East Siphon	GSCRHCSY	SY	0.80	0.67
Whitminster East Channel Weir	WHIRHSL1	SL	0.90	0.67
	WHIRHSL2	SL	0.40	0.67
	WHIRHSL3	SL	0.40	0.67
	WHIRHSL4	SL	0.40	0.67
	WHIRHSL5	SL	0.40	0.67
	WHIRHWR1	WR	0.40	0.67
Spring Hill Weir	CARVPWR1	WR	0.60	0.67
	CARVPWR2	WR	0.60	0.67

Table 20 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Churchend Bridge	CHESCHBR	BR	50.00	
Churchend Weir	CHESCWR1	WR	1.00	0.67
	CHESCWR2	WR	1.00	0.67
Millend Lane Bridge	MILENDBR	BR	1.00	
Churchend Sluices	CHESLSL1	SL	0.80	0.67
	CHESLSL2	SL	0.80	0.67
	CHESLSL3	SL	0.80	0.67
Bonds Mill	BONCUSL1	SL	0.40	0.20
	BONCUSL2	SL	0.40	0.20
GWR Embankment Bridge	GWREMBBR	HL	0.30	
Ocean Pool Bridge	OCPOOLBR	BR	10.00	
Bridgend Mill Side Weir	BRIDGSL1	SL	0.60	0.67
	BRIDGSL2	SL	0.70	0.67
Bridgend Mill Bridge	BRIDMIBR	BR	5.00	
Bridgend Kennels Bridge	BRKENNBR	BR	1.00	
Bridgend Kennels Sluice	BRIKNSL	SL	0.70	0.67
Downton Road Footbridge	DOWNFTBR	BR	1.00	
Upper Mills Footbridge	UPMIFTBR	BR	1.00	
Upper Mills Sluices	UPMILLSL	SL	0.70	0.67
Upper Mills Bridge	UPMILLBR	BR	5.00	
Ryeford Saw Mills Culvert	RYEFDSL1	SL	0.60	0.67
	RYEFDSL2	SL	0.60	0.67
	RYEFDWR1	WR	0.20	0.00

Table 20 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Refuse Tip Weir 3	REFWR1-1	WR	0.60	0.67
Refuse Tip Weir 2	REFWR2-1	WR	0.80	0.80
	REFWR2-2	WR	0.80	0.80
	MARGDWR1	WR	0.70	0.67
Market Garden Weir	MARGDWR2	WR	0.40	0.67
	BEARDWR3	WR	0.001	0.67
Beards Mill	BEARDWR4	WR	0.20	0.67
	BONSLSL1	SL	0.40	0.20
Bonds Mill Side Sluices	BONSLSL2	SL	0.40	0.20
	BONSLSL3	SL	0.40	0.20
	BONSLSL4	SL	0.40	0.20
	EBCNCUL1	SL	1.00	0.67
Ebley Corn Mill Culverts	EBCNCUL2	SL	1.00	0.67
	BRIDGCUL	WR	0.70	0.67
Bridgend Mill Bypass	BRIDGBYP	WR	0.60	0.67
Banty Ditch Culvert	BANTYCUL	HL	1.00	
Banty Ditch Weir	BANTYDWR	WR	0.70	0.67
Fromehall Mill Sluice	FRMHLC1	SL	0.90	0.67
	FRMHLC2	SL	0.90	0.67
Dudbridge Lock Weir	DUDLCKWR	WR	1.00	0.67
Printing Works Lock Weir	RUSBRKWR	WR	1.00	0.67
Lodgmore Canal Weir	PSWCKSWR	WR	1.00	0.67
Cainscross Road Lock Weir	CAINSWR1	WR	1.00	0.67
	CAINSWR2	WR	1.00	0.67

Table 21 Final structure coefficients - Nailsworth Stream sub-model

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Dudbridge Weir	NSOUTFWR	WR	1.00	0.67
	NSOUTFSL	SL	0.90	0.67
Selsley Hill Culvert	SESLYCV	BR	1.00	
Erinoid Downstream Control Weir	GANTRYWR	WR	0.90	0.67
Erinoid Culvert	ERINODCV	HL	1.00	
Erinoid Bridge	ERINODBR	SL	0.90	0.67
Car Park Bridge	CARPRKBR	BR	1.00	
Cotswold House Bridge	COTSHOBR	HL	0.04	
New Tynings Footbridge	NEWTYNBR	BR	1.00	
Priory Bridge	PRIORYBR	HL	0.3	
Rooksmoor Mill Right Channel Culvert	RKSMRCVR	SL	1.00	0.67
Rooksmoor Mill Weir	RKSMRWR1	WR	0.80	0.67
	RKSMRWR2	SL	0.80	0.67
Selsley road Bridge	SESLYBR	BR	1.00	
Selsley Road Weir	SESLYWR	WR	0.90	0.67
Paul's Rise Bridge	PAULSRBR	BR	1.00	
Railway Bridge	NSRAILBR	BR	1.00	
Forge Weir	FORGEWR	WR	0.90	0.67
Birds Crossing Bridge	BIRDSXBR	BR	1.00	

Table 21 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Station Road Works	STRODSL1	SL	0.70	0.67
	STRODWR1	WR	0.40	0.67
	STRODWR2	WR	0.40	0.67
	STRODSL2	SL	0.80	0.67
	STRODSL3	SL	0.80	0.67
Station Road Bridge	STRODSL4	SL	0.90	0.67
	STRODWR3	WR	0.40	0.67
South Woodchester Works Bridge	STHWODBR	BR	1.00	
Frogmarsh Lane Bridge	FROGMSBR	HL	0.16	
Bath Road Bridge	BATHRDBR	BR	1.00	
Merritt's Mills Bridge	MERRMIBR	BR	1.00	
Merritt's Mills Culvert	MERRETSL	HL	0.94	
Inchbrook Bridge	INCHBKBR	BR	1.00	
Inchbrook Culvert	INCHBKSL	HL	0.01	
Critchley's Bridge 1	CRITHBR1	BR	1.00	
Critchley's New Culvert	CRITHNCV	BR	1.00	
Critchley's Bridge 2	CRITHBR2	BR	1.00	
Dunkirk Mills Culvert	DUNKRSL1	SL	0.90	0.67
Garage Culvert	GARAGECV	BR	1.00	
Egypt Mill Weir	EGYPTWR1	WR	0.90	0.67
	EGYPTWR2	WR	0.90	0.67
	EGYPTWR3	WR	0.90	0.67

Table 21 Continued

Structure Name	Element label	Element Type	Cd, K, Aff	Dr
Rooksmoor Mill Left Channel Culvert	RKSMRSL1	SL	0.80	0.67
	RKSMRSL2	SL	0.80	0.67
Critchley's Left Channel Culvert	CRITRDWR	WR	0.90	0.40
	CRITHSL2	SL	1.00	0.67
Critchley's Bridge 3	CRITHBR3	BR	1.00	
Critchley's Bridge	CRITHBR4	BR	1.00	
Tennis Court Bridge 2	TENISBR2	HL	0.10	
Dunkirk Mills Bridge 1	DUNKRBR1	BR	1.00	
Dunkirk Mills Side Spills	DUNKRWR1	WR	0.90	0.67
	DUNKRWR2	WR	0.90	0.67
	DUNKRSL2	SL	0.90	0.67
Critchley's Bridge 5	CRITHSL1	SL	0.90	0.67
Tennis Court Bridge 1	TENNISBR	BR	1.00	
Elm Brook Bridge	ELMBRKBR	BR	1.00	
Gables Bridge	GABLESBR	BR	1.00	
Dunkirk Mills Entrance Bridge	DUNKRBR2	BR	1.00	
Filling Station Culvert	FILSTCV1	SL	0.90	0.67
	FILSTCV2	WR	0.40	0.67

Table 22 Design event return period water levels

Location	5 year	10 year	25 year	50 year	100 year	150 year
C1	34.979	35.154	35.407	35.654	35.948	36.306
C2	34.349	34.470	34.667	34.838	35.001	35.105
C3	48.350	48.414	48.515	48.592	48.647	48.684
C4	79.747	79.797	79.836	80.005	80.145	80.239
C5	57.991	58.082	58.228	58.463	58.923	59.264
M1	13.745	14.161	14.276	14.350	14.416	14.437
M3	26.461	26.464	26.500	26.563	26.629	26.785
M4	28.189	28.222	28.259	28.276	28.294	28.302
M5	38.459	38.573	38.726	38.978	39.080	39.161
M6	57.026	57.033	57.168	57.287	57.407	57.494
M7	72.175	72.227	72.288	72.471	72.582	72.642
M8	7.864	7.900	7.985	8.042	8.060	8.156
M9	7.999	8.043	8.150	8.185	8.199	8.336
M10	43.826	43.955	44.161	44.631	45.157	45.669
Ebley Mill	31.859	31.981	32.089	32.158	32.196	32.228
Peak flow (m³/s)						
Ebley Mill						
	16.4	20.4	26.9	31.0	37.2	40.7

Table 23 Additional modelling downstream of Wheatenhurst Sluices - 4.88m peak level tide

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFA_001	4.88	4.88	4.88	4.88	4.88
River Severn Tidal Outfall					
RFA_001A	7.01	7.12	7.13	7.16	7.22
RFA_002	7.26	7.36	7.37	7.40	7.45
Upper Framilode Weir					
RFA_003	8.20	8.32	8.33	8.36	8.42
RFA_004	8.32	8.43	8.44	8.48	8.54
RFA_005	8.44	8.56	8.57	8.60	8.66
Junction with RFB_001					
RFA_006	8.44	8.56	8.57	8.60	8.66
RFA_007	8.52	8.64	8.65	8.68	8.74
RFA_008	8.60	8.70	8.72	8.74	8.80
RFA_008A	8.65	8.75	8.76	8.78	8.83
Gloucester & Sharpness Canal - Left Syphon					
RFA_009	8.70	8.84	8.86	8.88	8.95
RFA_010	8.73	8.88	8.90	8.92	8.99
RFA_011	8.73	8.88	8.90	8.93	9.00
RFA_012	8.74	8.89	8.91	8.93	9.00
Whitminster Weir - Left					
RFA_013	8.78	8.93	8.94	8.97	9.04
Junction with RFB_008					
RFA_014	8.78	8.93	8.94	8.97	9.04
RFA_015	8.78	8.92	8.94	8.96	9.03
RFA_016	8.78	8.92	8.94	8.96	9.04
RFA_017	8.80	8.94	8.96	8.98	9.05
RFA_018	8.81	8.95	8.97	8.99	9.06
Wheatenhurst Sluice					
RFA_019	10.15	10.07	10.09	10.13	10.08

Table 23 Continued

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFB_001	8.44	8.56	8.57	8.60	8.66
RFB_002	8.49	8.60	8.61	8.65	8.71
RFB_003	8.52	8.63	8.64	8.68	8.74
Gloucester & Sharpness Canal - Right Syphon					
RFB_004	8.67	8.82	8.84	8.87	8.94
RFB_005	8.73	8.88	8.90	8.92	8.99
RFB_006	8.74	8.89	8.91	8.93	9.00
RFB_007	8.76	8.90	8.92	8.94	9.01
Whitminster Weir - Right					
RFB_008	8.78	8.93	8.94	8.97	9.04
Floodplain Cells					
Cell 1	8.20	8.48	8.56	8.65	8.71
Cell 2	8.10	8.23	8.56	8.65	8.71
Cell 3	8.73	8.88	8.90	8.92	9.00
Cell 4	8.74	8.88	8.90	8.93	9.00
Cell 5	8.74	8.89	8.91	8.93	9.00
Cell 6	8.20	8.20	8.20	8.20	8.87
Cell 7	8.40	8.40	8.40	8.40	8.87
Cell 8	8.80	8.80	8.80	8.80	8.80
Cell 9	8.37	8.37	8.37	8.37	8.37
Cell 10	8.39	8.39	8.39	8.39	8.39

Table 24 Additional modelling downstream of Wheatenhurst Sluices - 6.00m peak level tide

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFA_001	6.00	6.00	6.00	6.00	6.00
River Severn Tidal Outfall					
RFA_001A	7.01	7.12	7.13	7.16	7.22
RFA_002	7.26	7.36	7.37	7.40	7.45
Upper Framilode Weir					
RFA_003	8.20	8.32	8.33	8.36	8.42
RFA_004	8.32	8.43	8.44	8.48	8.54
RFA_005	8.44	8.56	8.57	8.60	8.66
Junction with RFB_001					
RFA_006	8.44	8.56	8.57	8.60	8.66
RFA_007	8.52	8.64	8.65	8.68	8.74
RFA_008	8.60	8.70	8.72	8.74	8.80
RFA_008A	8.65	8.75	8.76	8.78	8.83
Gloucester & Sharpness Canal - Left Syphon					
RFA_009	8.70	8.84	8.86	8.88	8.95
RFA_010	8.73	8.88	8.90	8.92	8.99
RFA_011	8.73	8.88	8.90	8.93	9.00
RFA_012	8.74	8.89	8.91	8.93	9.00
Whitminster Weir - Left					
RFA_013	8.78	8.93	8.94	8.97	9.04
Junction with RFB_008					
RFA_014	8.78	8.93	8.94	8.97	9.04
RFA_015	8.78	8.92	8.94	8.96	9.03
RFA_016	8.78	8.92	8.94	8.96	9.04
RFA_017	8.80	8.94	8.96	8.98	9.05
RFA_018	8.81	8.95	8.97	8.99	9.06
Wheatenhurst Sluice					
RFA_019	10.15	10.07	10.09	10.13	10.08

Table 24 Continued

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFB_001	8.44	8.56	8.57	8.60	8.66
RFB_002	8.49	8.60	8.61	8.65	8.71
RFB_003	8.52	8.63	8.64	8.68	8.74
Gloucester & Sharpness Canal - Right Syphon					
RFB_004	8.67	8.82	8.84	8.87	8.94
RFB_005	8.73	8.88	8.90	8.92	8.99
RFB_006	8.74	8.89	8.91	8.93	9.00
RFB_007	8.76	8.90	8.92	8.94	9.01
Whitminster Weir - Right					
RFB_008	8.78	8.93	8.94	8.97	9.04
Floodplain Cells					
Cell 1	8.20	8.48	8.56	8.65	8.71
Cell 2	8.10	8.23	8.56	8.65	8.71
Cell 3	8.73	8.88	8.90	8.92	9.00
Cell 4	8.74	8.88	8.90	8.93	9.00
Cell 5	8.74	8.89	8.91	8.93	9.00
Cell 6	8.20	8.20	8.20	8.20	8.87
Cell 7	8.40	8.40	8.40	8.40	8.87
Cell 8	8.80	8.80	8.80	8.80	8.80
Cell 9	8.37	8.37	8.37	8.37	8.37
Cell 10	8.39	8.39	8.39	8.39	8.39

Table 25 Additional modelling downstream of Wheatenhurst Sluices - 8.00m peak level tide

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFA_001	8.00	8.00	8.00	8.00	8.00
River Severn Tidal Outfall					
RFA_001A	8.11	8.14	8.16	8.18	8.22
RFA_002	8.14	8.18	8.20	8.22	8.27
Upper Framilode Weir					
RFA_003	8.43	8.49	8.54	8.57	8.65
RFA_004	8.47	8.54	8.59	8.62	8.71
RFA_005	8.55	8.60	8.65	8.67	8.77
Junction with RFB_001					
RFA_006	8.55	8.60	8.65	8.67	8.77
RFA_007	8.60	8.66	8.71	8.74	8.83
RFA_008	8.66	8.71	8.76	8.79	8.87
RFA_008A	8.70	8.75	8.80	8.82	8.90
Gloucester & Sharpness Canal - Left Syphon					
RFA_009	8.75	8.84	8.88	8.91	8.97
RFA_010	8.77	8.88	8.92	8.95	9.00
RFA_011	8.77	8.89	8.93	8.96	9.00
RFA_012	8.78	8.90	8.94	8.97	9.01
Whitminster Weir - Left					
RFA_013	8.81	8.93	8.97	9.00	9.04
Junction with RFB_008					
RFA_014	8.81	8.93	8.97	9.00	9.04
RFA_015	8.81	8.92	8.96	8.99	9.03
RFA_016	8.81	8.93	8.97	9.00	9.04
RFA_017	8.83	8.95	8.98	9.01	9.06
RFA_018	8.84	8.96	8.99	9.02	9.07
Wheatenhurst Sluice					
RFA_019	10.15	10.07	10.09	10.13	10.08

Table 25 Continued

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFB_001	8.55	8.60	8.65	8.67	8.77
RFB_002	8.58	8.62	8.65	8.68	8.80
RFB_003	8.60	8.64	8.69	8.71	8.81
Gloucester & Sharpness Canal - Right Syphon					
RFB_004	8.72	8.83	8.87	8.90	8.96
RFB_005	8.77	8.88	8.92	8.95	9.00
RFB_006	8.78	8.89	8.94	8.97	9.01
RFB_007	8.79	8.91	8.94	8.97	9.01
Whitminster Weir - Right					
RFB_008	8.81	8.93	8.97	9.00	9.04
Floodplain Cells					
Cell 1	8.20	8.48	8.65	8.68	8.80
Cell 2	8.10	8.46	8.65	8.68	8.80
Cell 3	8.77	8.89	8.93	8.96	9.00
Cell 4	8.77	8.89	8.93	8.96	9.00
Cell 5	8.77	8.89	8.93	8.96	9.01
Cell 6	8.20	8.20	8.20	8.20	8.98
Cell 7	8.40	8.40	8.40	8.40	8.98
Cell 8	8.80	8.80	8.80	8.80	8.97
Cell 9	8.37	8.37	8.37	8.37	8.97
Cell 10	8.39	8.39	8.39	8.39	8.97

Table 26 Additional modelling downstream of Wheatenhurst Sluices - 10.00m peak level tide

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFA_001	10.00	10.00	10.00	10.00	10.00
River Severn Tidal Outfall					
RFA_001A	9.04	9.07	9.13	9.17	9.31
RFA_002	9.04	9.07	9.13	9.17	9.31
Upper Framilode Weir					
RFA_003	9.04	9.07	9.13	9.17	9.31
RFA_004	9.06	9.09	9.15	9.19	9.32
RFA_005	9.09	9.12	9.17	9.22	9.35
Junction with RFB_001					
RFA_006	9.09	9.12	9.17	9.22	9.35
RFA_007	9.11	9.14	9.19	9.23	9.37
RFA_008	9.12	9.14	9.20	9.24	9.37
RFA_008A	9.13	9.16	9.22	9.26	9.39
Gloucester & Sharpness Canal - Left Syphon					
RFA_009	9.16	9.20	9.28	9.32	9.44
RFA_010	9.17	9.22	9.30	9.35	9.46
RFA_011	9.18	9.22	9.31	9.35	9.46
RFA_012	9.18	9.23	9.31	9.36	9.46
Whitminster Weir - Left					
RFA_013	9.19	9.24	9.32	9.37	9.47
Junction with RFB_008					
RFA_014	9.19	9.24	9.32	9.37	9.47
RFA_015	9.19	9.24	9.32	9.37	9.47
RFA_016	9.20	9.24	9.33	9.37	9.48
RFA_017	9.20	9.25	9.33	9.38	9.48
RFA_018	9.21	9.25	9.34	9.38	9.48
Wheatenhurst Sluice					
RFA_019	10.15	10.07	10.10	10.14	10.10

Table 26 Continued

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFB_001	9.09	9.12	9.17	9.22	9.35
RFB_002	9.11	9.13	9.19	9.23	9.36
RFB_003	9.12	9.14	9.19	9.23	9.37
Gloucester & Sharpness Canal - Right Syphon					
RFB_004	9.16	9.21	9.29	9.34	9.45
RFB_005	9.18	9.23	9.31	9.35	9.46
RFB_006	9.18	9.23	9.31	9.36	9.46
RFB_007	9.19	9.23	9.32	9.36	9.46
Whitminster Weir - Right					
RFB_008	9.19	9.24	9.32	9.37	9.47
Floodplain Cells					
Cell 1	9.11	9.14	9.19	9.23	9.37
Cell 2	9.11	9.14	9.19	9.23	9.37
Cell 3	9.18	9.23	9.31	9.35	9.46
Cell 4	9.18	9.23	9.31	9.36	9.46
Cell 5	9.18	9.23	9.31	9.36	9.46
Cell 6	9.17	9.22	9.31	9.35	9.46
Cell 7	9.17	9.22	9.31	9.35	9.46
Cell 8	9.16	9.22	9.31	9.36	9.46
Cell 9	9.07	9.16	9.32	9.37	9.47
Cell 10	9.05	9.14	9.25	9.30	9.42

Table 27 Additional modelling downstream of Wheatenhurst Sluices - 10.50m peak level tide

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFA_001	10.50	10.50	10.50	10.50	10.50
River Severn Tidal Outfall					
RFA_001A	9.15	9.16	9.17	9.19	9.36
RFA_002	9.16	9.18	9.20	9.21	9.36
Upper Framilode Weir					
RFA_003	9.16	9.18	9.21	9.24	9.37
RFA_004	9.16	9.18	9.24	9.26	9.40
RFA_005	9.16	9.19	9.25	9.29	9.44
Junction with RFB_001					
RFA_006	9.16	9.19	9.25	9.29	9.44
RFA_007	9.17	9.21	9.27	9.31	9.45
RFA_008	9.18	9.21	9.28	9.32	9.46
RFA_008A	9.20	9.23	9.30	9.34	9.47
Gloucester & Sharpness Canal - Left Syphon					
RFA_009	9.23	9.27	9.35	9.40	9.52
RFA_010	9.25	9.30	9.38	9.43	9.54
RFA_011	9.25	9.30	9.39	9.43	9.54
RFA_012	9.25	9.30	9.39	9.43	9.54
Whitminster Weir - Left					
RFA_013	9.26	9.32	9.40	9.45	9.55
Junction with RFB_008					
RFA_014	9.26	9.32	9.40	9.45	9.55
RFA_015	9.26	9.31	9.40	9.45	9.55
RFA_016	9.26	9.32	9.41	9.46	9.56
RFA_017	9.27	9.32	9.41	9.46	9.56
RFA_018	9.27	9.33	9.41	9.46	9.57
Wheatenhurst Sluice					
RFA_019	10.15	10.08	10.11	10.14	10.10

Table 27 Continued

Section Label	5 Year Event	10 Year Event	25 Year Event	50 Year Event	100 Year Event
RFB_001	9.16	9.19	9.25	9.29	9.44
RFB_002	9.17	9.20	9.27	9.31	9.45
RFB_003	9.18	9.21	9.27	9.31	9.46
Gloucester & Sharpness Canal - Right Syphon					
RFB_004	9.24	9.28	9.37	9.42	9.53
RFB_005	9.25	9.30	9.39	9.43	9.54
RFB_006	9.25	9.30	9.39	9.44	9.55
RFB_007	9.26	9.31	9.39	9.44	9.55
Whitminster Weir - Right					
RFB_008	9.26	9.32	9.40	9.45	9.55
Floodplain Cells					
Cell 1	9.17	9.21	9.27	9.31	9.45
Cell 2	9.18	9.21	9.27	9.31	9.45
Cell 3	9.25	9.30	9.39	9.43	9.54
Cell 4	9.25	9.30	9.39	9.43	9.54
Cell 5	9.25	9.30	9.39	9.44	9.54
Cell 6	9.25	9.30	9.39	9.43	9.54
Cell 7	9.25	9.30	9.39	9.43	9.54
Cell 8	9.24	9.30	9.39	9.43	9.54
Cell 9	9.21	9.30	9.40	9.45	9.56
Cell 10	9.14	9.24	9.32	9.37	9.48

Table 28 Structure coefficient sensitivity tests - locations where upstream water level increases exceed 0.10m

Structure Name	Upstream section	Water level increase (m) for decrease in coefficients of:	
		10%	20%
Lower Frome Sub-model			
Wheatenhurst Sluices	RFA_019	0.01	0.14
Millend Mill	RFA_054	0.12	0.21
Stanley Downton Mill race	RFA_090	0.05	0.11
Refuse Tip Weir 1	RFA_119	0.08	0.17
Ebley Mill Weir	RFA_138	0.05	0.11
Fromehall Mill Bypass Sluices	RFA_157	0.06	0.12
Lodgemore Mills Sluices	RFA_166	0.05	0.11
Refuse Tip Weir 3	RFD_081	0.08	0.17
Dudbridge Lock Weir	SCA_005	0.09	0.20
Ruscombe Brook Weir	SCA_007	0.08	0.18
Cainscross Road Weir	SCA_015	0.06	0.12
Upper Frome Sub-model			
Thames and Severn Canal Syphon	RFA_184	0.25	0.53
Arundell Mill Sluices	RFA_187	0.14	0.34
Eagle Mills Culvert	RFA_190	0.14	0.30
Butterow Hill Bridge	RFA_193	0.10	0.22
Bowbridge Estate Bridge	RFA_195	0.10	0.21
Bowbridge Estate Bridge 2	RFA_199	0.06	0.14
Griffin Mill Footbridge 1	RFA_215	0.03	0.20
Griffin Mill Bypass	RFA_218	0.03	0.12
Thrupp Caravan Site Bridge	RFA_242	0.11	0.23
Brimscombe Mill Pond Outlet	RFA_250	0.06	0.12
Chalford Industrial Estate Sluices	RFA_324	0.21	0.30
Thanet House Bridge	RFA_331	0.06	0.12
Ridley Mill Sluices	RFA_344	0.06	0.12
Ashmead Sluices	RFA_357	0.06	0.13
Bakers Bridge	RFA_367	0.14	0.41
Puck Mill Culvert	RFA_379	0.12	0.26

Table 28 Continued

Structure Name	Upstream section	Water level increase (m) for decrease in coefficients of:	
		10%	20%
Griffin Mill Weir 2	RFO_012	0.03	0.12
Butterow Hill Canal Bridge	SCB_007	0.08	0.33
Puck Mill Upper Lock Weir	SCC_060	0.07	0.15
Whitehall Lower lock Weir	SCC_062	0.13	0.26
Nailsworth Stream Sub-model			
Erinoid Bridge	NSA_016	0.15	0.33
Car Park Bridge	NSA_019	0.15	0.33
Cotswold House Bridge	NSA_023	0.08	0.19
New Tynings Footbridge	NSA_025	0.06	0.15
Rooksmoor Mill Culvert - Right	NSA_038	0.39	0.84
Rooksmoor Mill Weir	NSA_039	0.38	0.83
Selsley Road Bridge	NSA_045	0.37	0.82
Selsley Road Weir	NSA_046	0.36	0.80
Pauls Rise Bridge	NSA_048	0.31	0.73
Railway Bridge	NSA_052	0.29	0.63
The Forge Weir	NSA_054	0.26	0.57
Birds Crossing	NSA_056	0.21	0.28
Station Road Works	NSA_062	0.22	0.40
Station Road Bridge	NSA_063	0.17	0.35
South Woodchester Works Bridge	NSA_065	0.14	0.30
Frogmarsh Lane Bridge	NSA_076	0.07	0.11
Bath Road Bridge	NSA_078	0.07	0.12
Merretts Mills Bridge	NSA_083	0.08	0.14
Merretts Mills Culvert	NSA_086	0.10	0.17
Inchbrook Bridge	NSA_089	0.09	0.15
Critchleys (New) Culvert	NSA_096	0.06	0.15
Critchleys Bridge 2	NSA_098	0.11	0.23
Dunkirk Mills Culvert	NSA_101	0.09	0.19
Garage Culvert	NSA_119	0.12	0.25
Egypt Mill Weir & Wheel	NSA_122	0.12	0.25

Table 28 Continued

Structure Name	Upstream section	Water level increase (m) for decrease in coefficients of:	
		10%	20%
Rooksmoor Mill Culvert - Left	NSB_002	0.38	0.83
Tennis Court Bridge	NSC_012	0.26	0.06
Dunkirk Mills Bridge 1	NSC_015	0.26	0.12
Dunkirk Mills Side Sluices	NSC_016	0.09	0.19



Figures



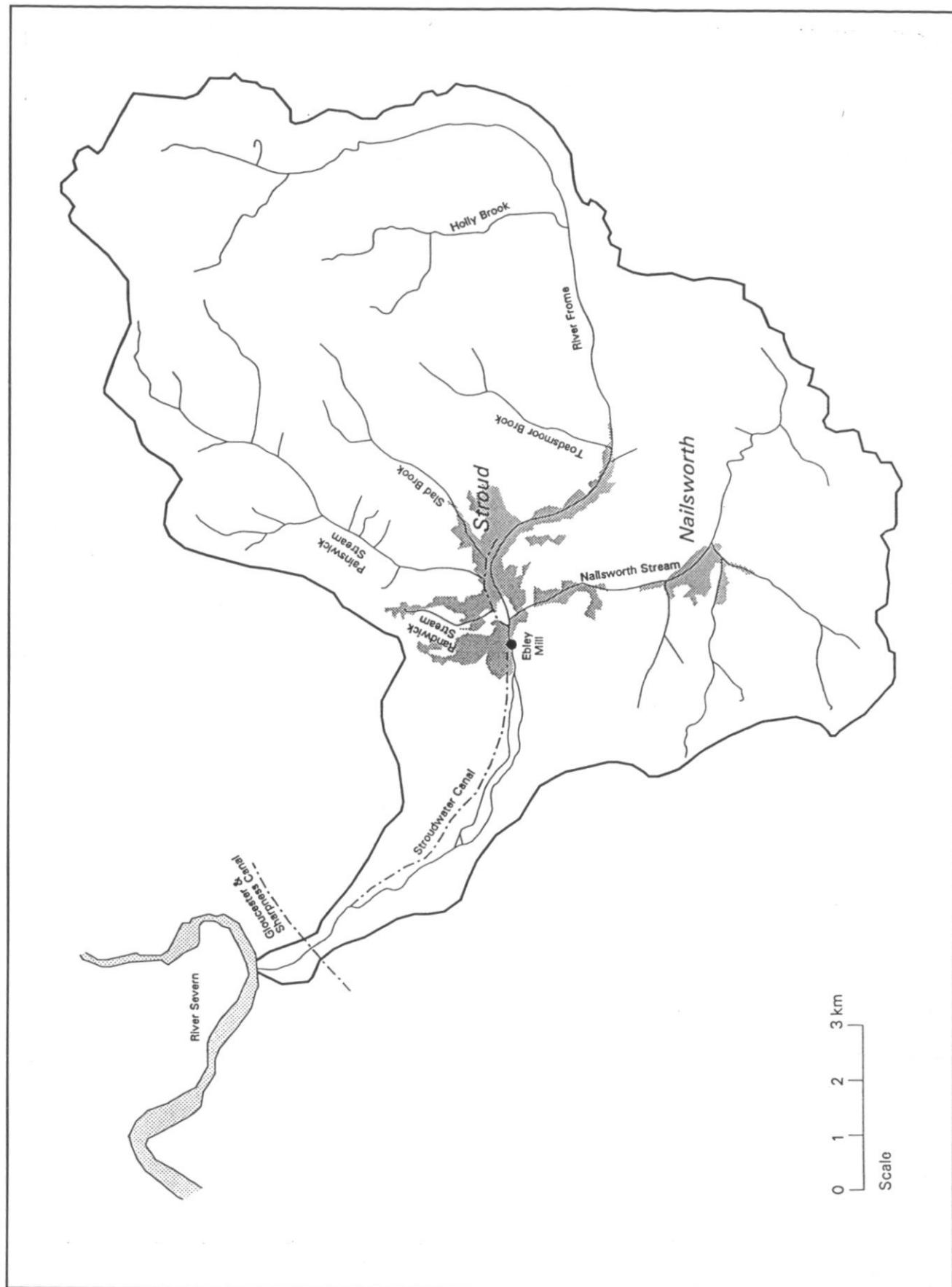


Figure 1 Frome catchment and river system

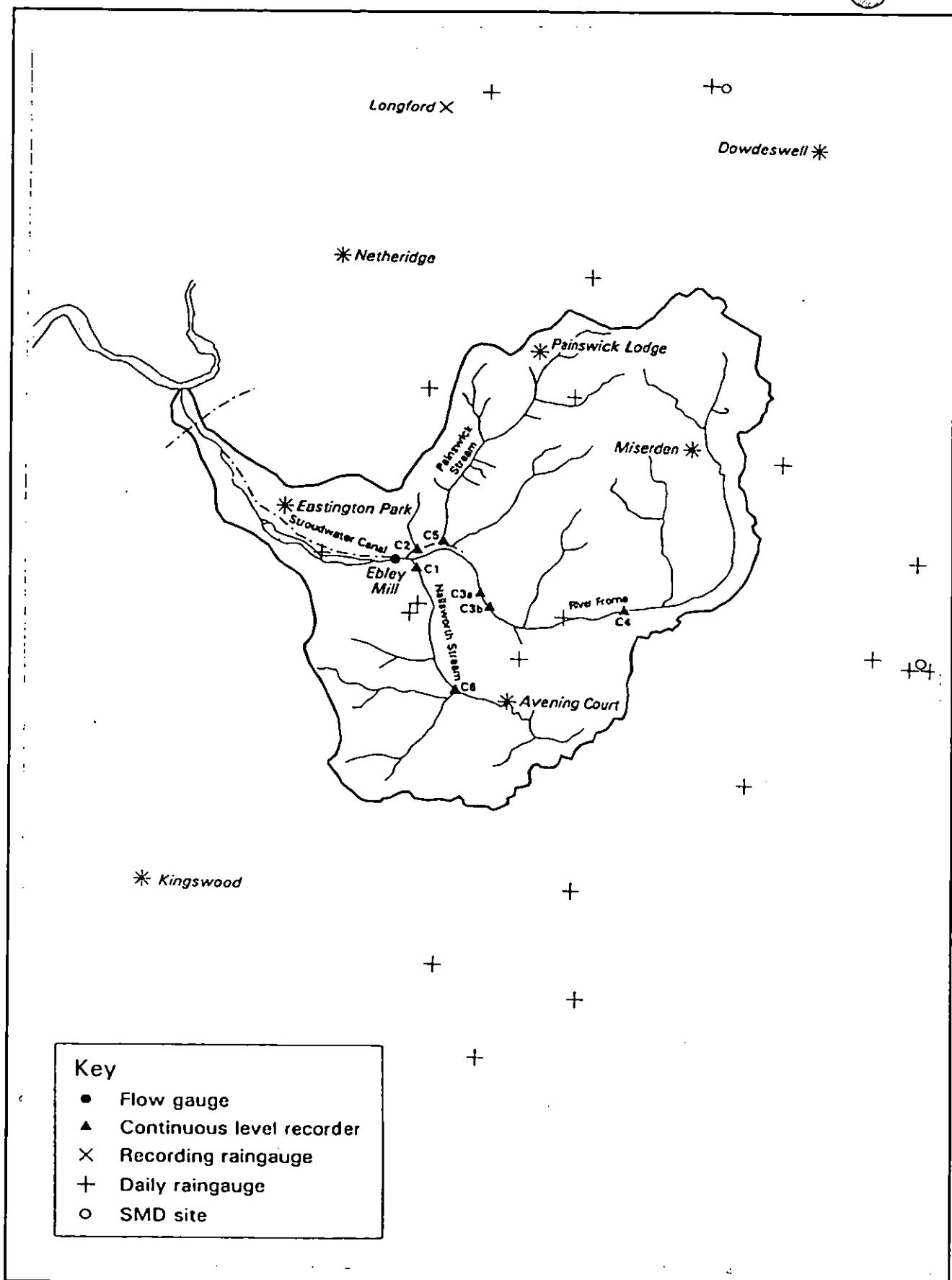


Figure 2 Frome basin showing locations of flow gauging stations and meteorological sites

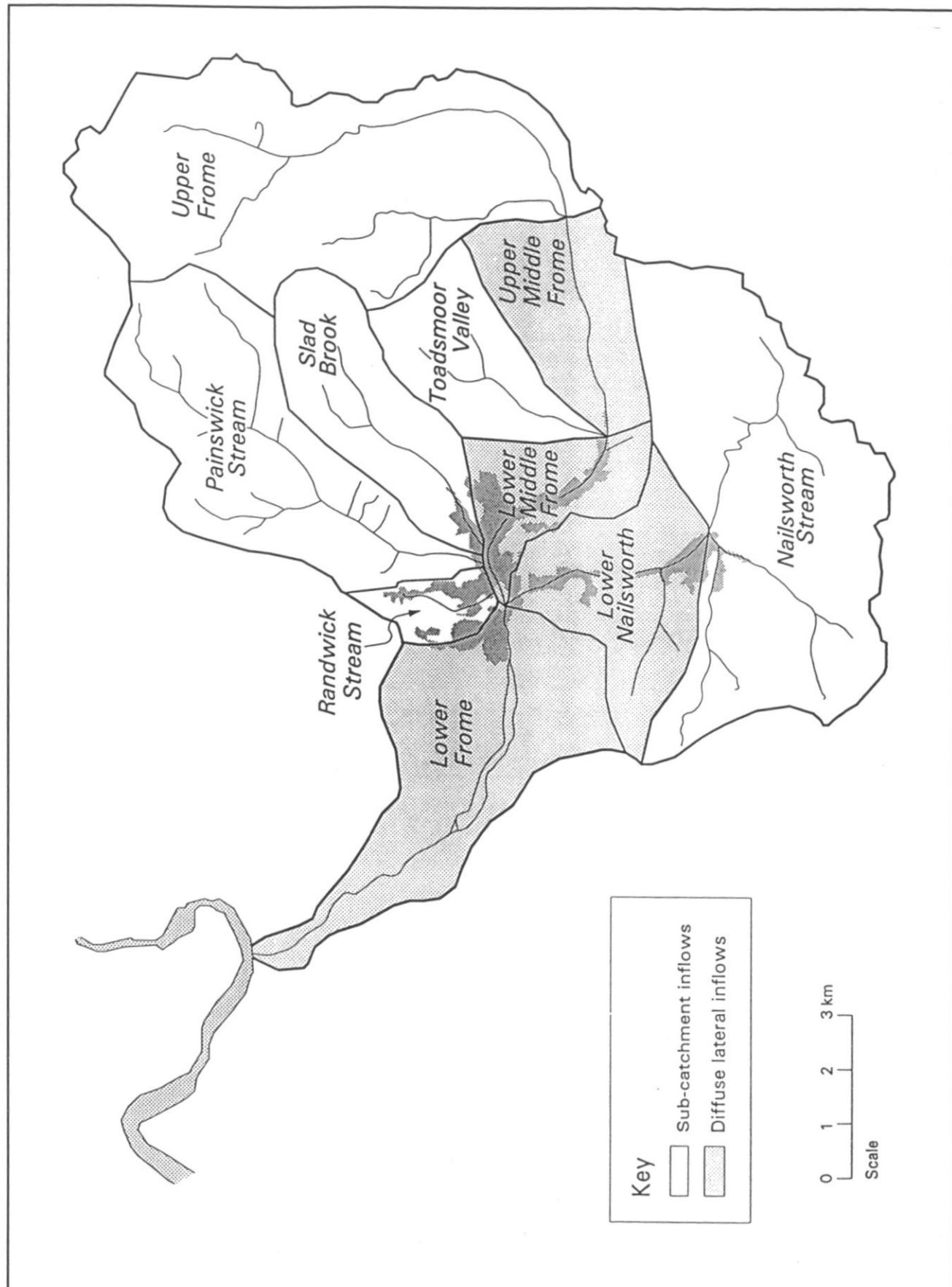


Figure 3 Frome basin showing sub-catchment boundaries

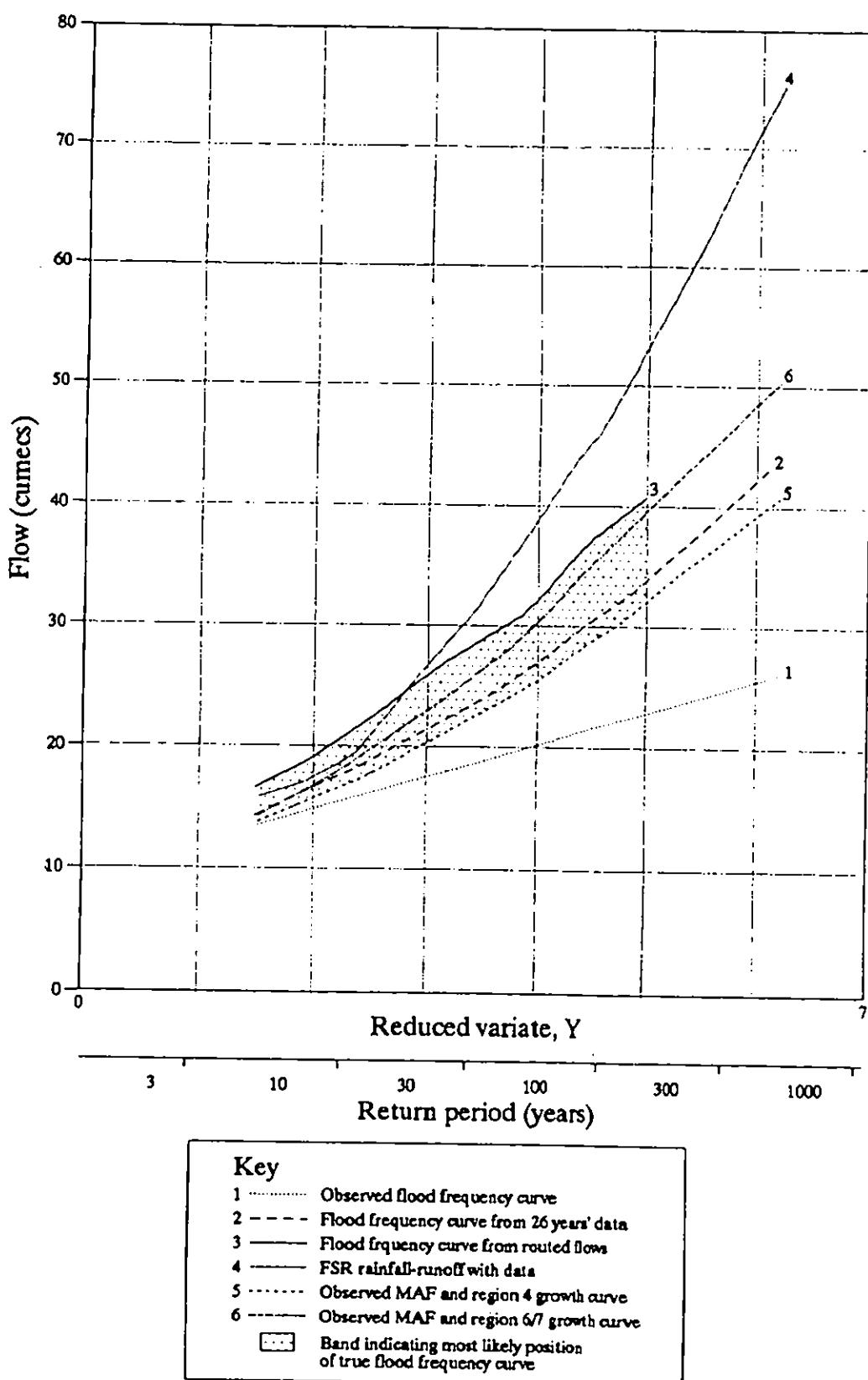


Figure 4 Comparison of flood frequency plots for Ebley Mill

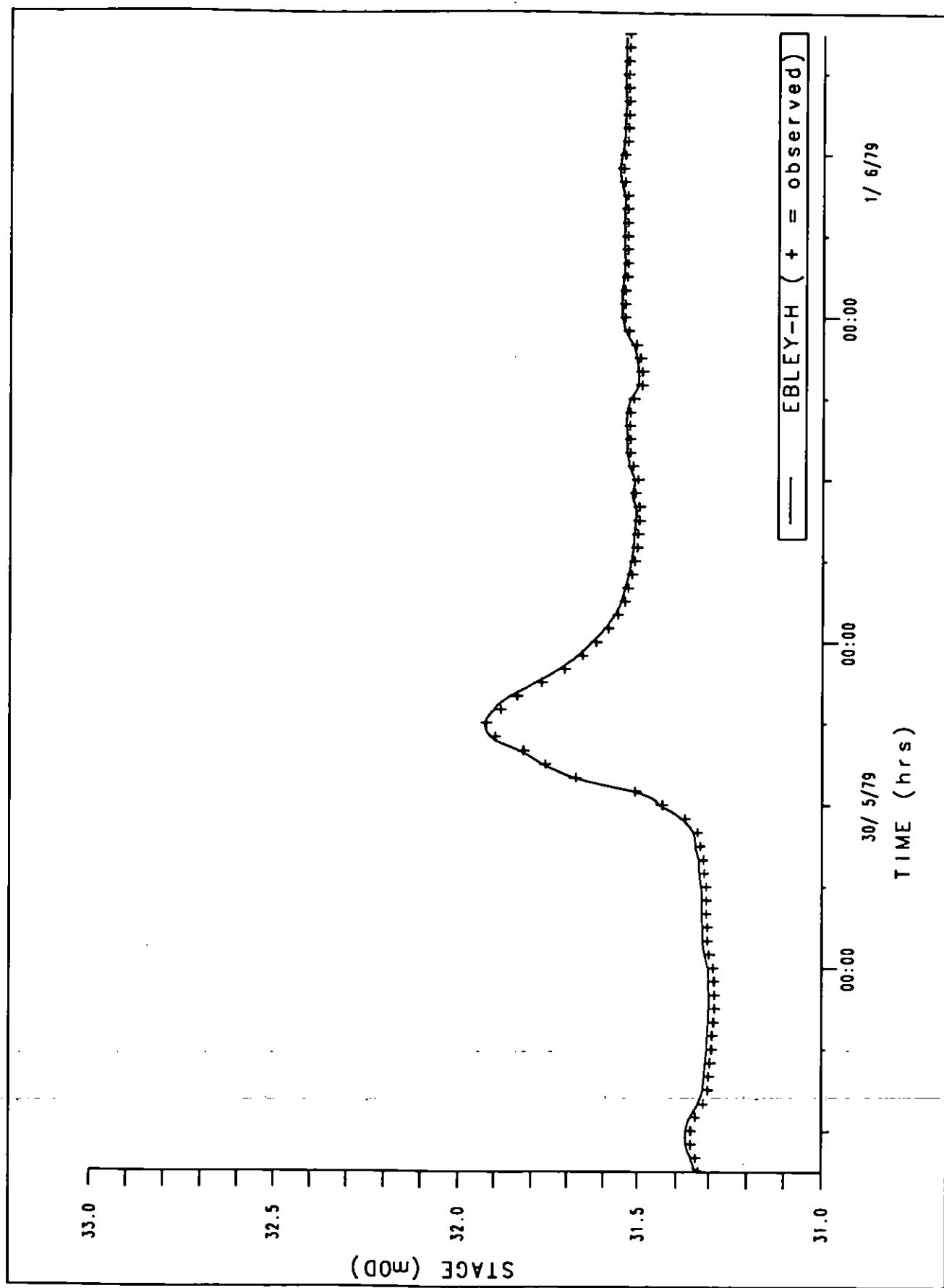


Figure 5 Ebley Mill gauging station calibration results - May 1979 event

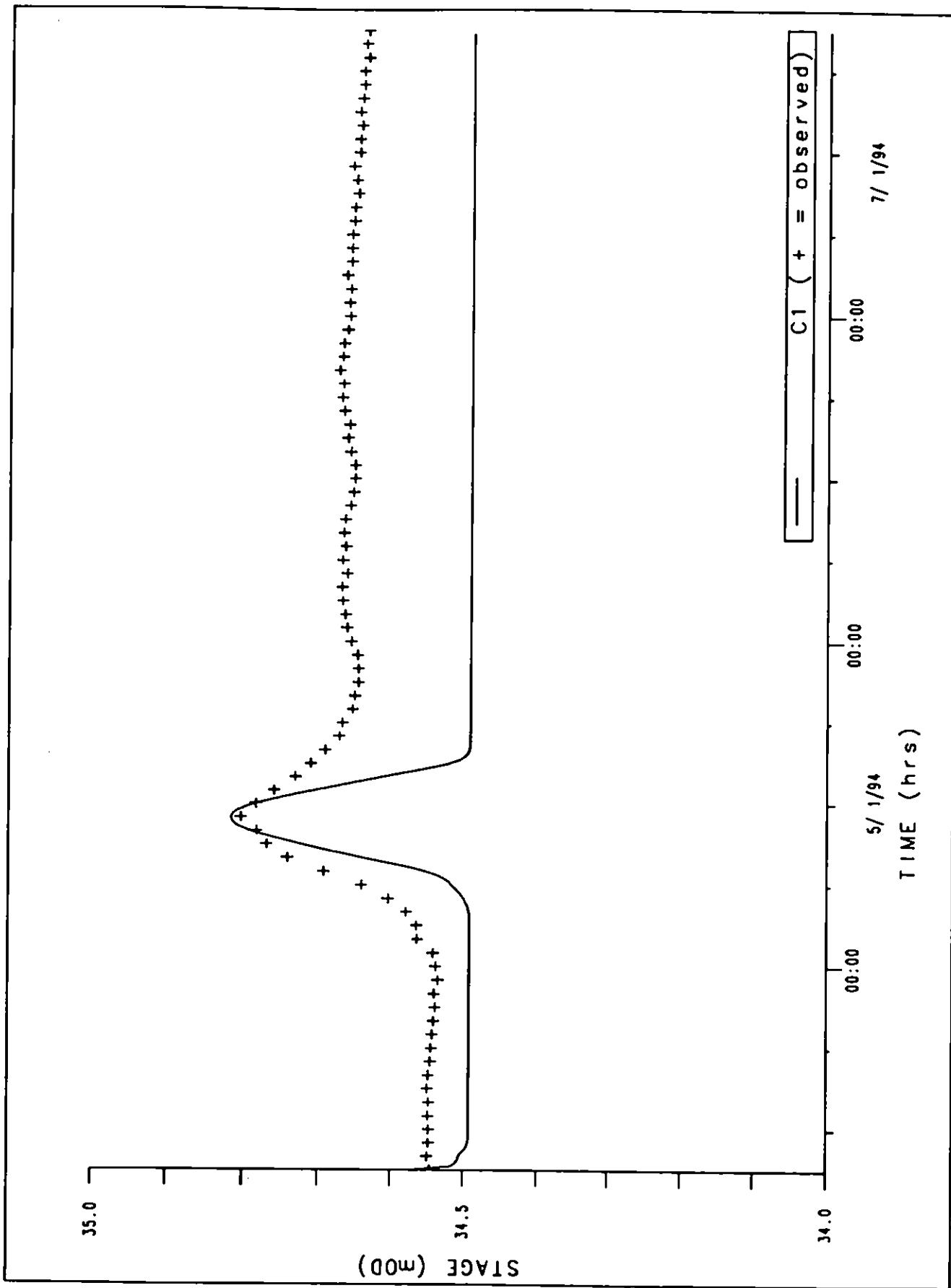


Figure 6 January 1994 calibration results - C1 (Persimon Homes)

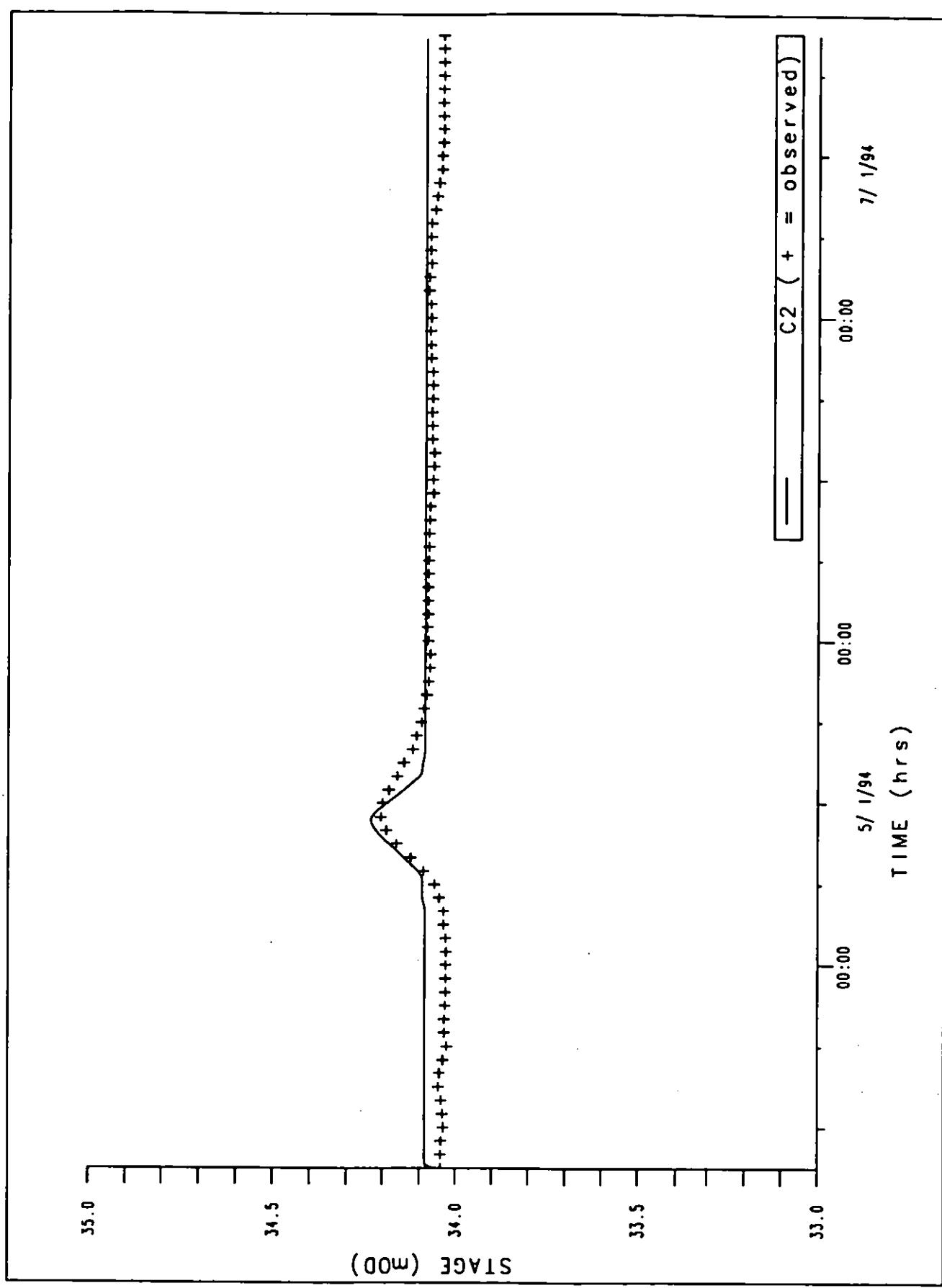


Figure 7 January 1994 calibration results - C2 (Dudbridge Weir)

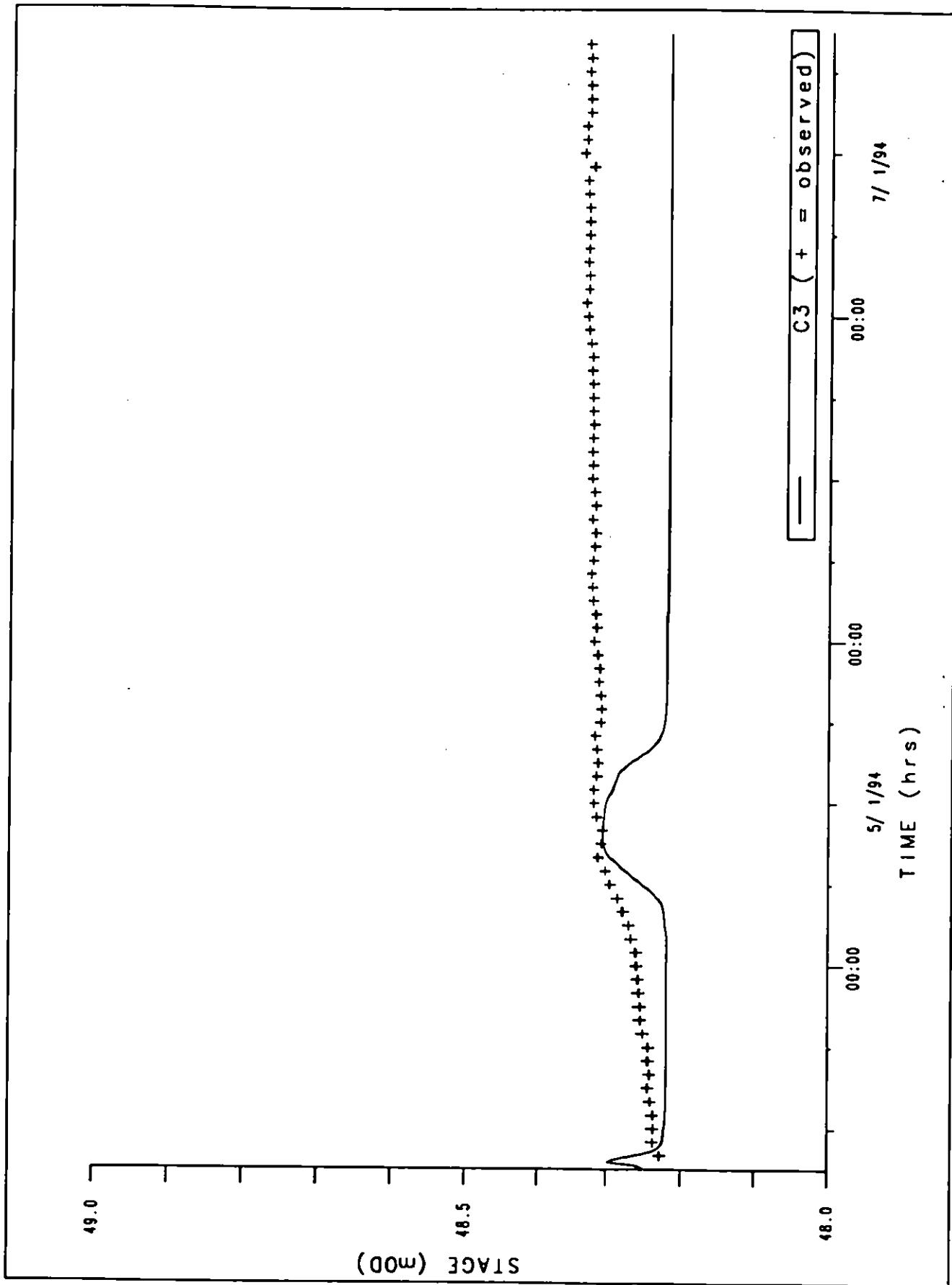


Figure 8 January 1994 calibration results - C3 (Thrupp)

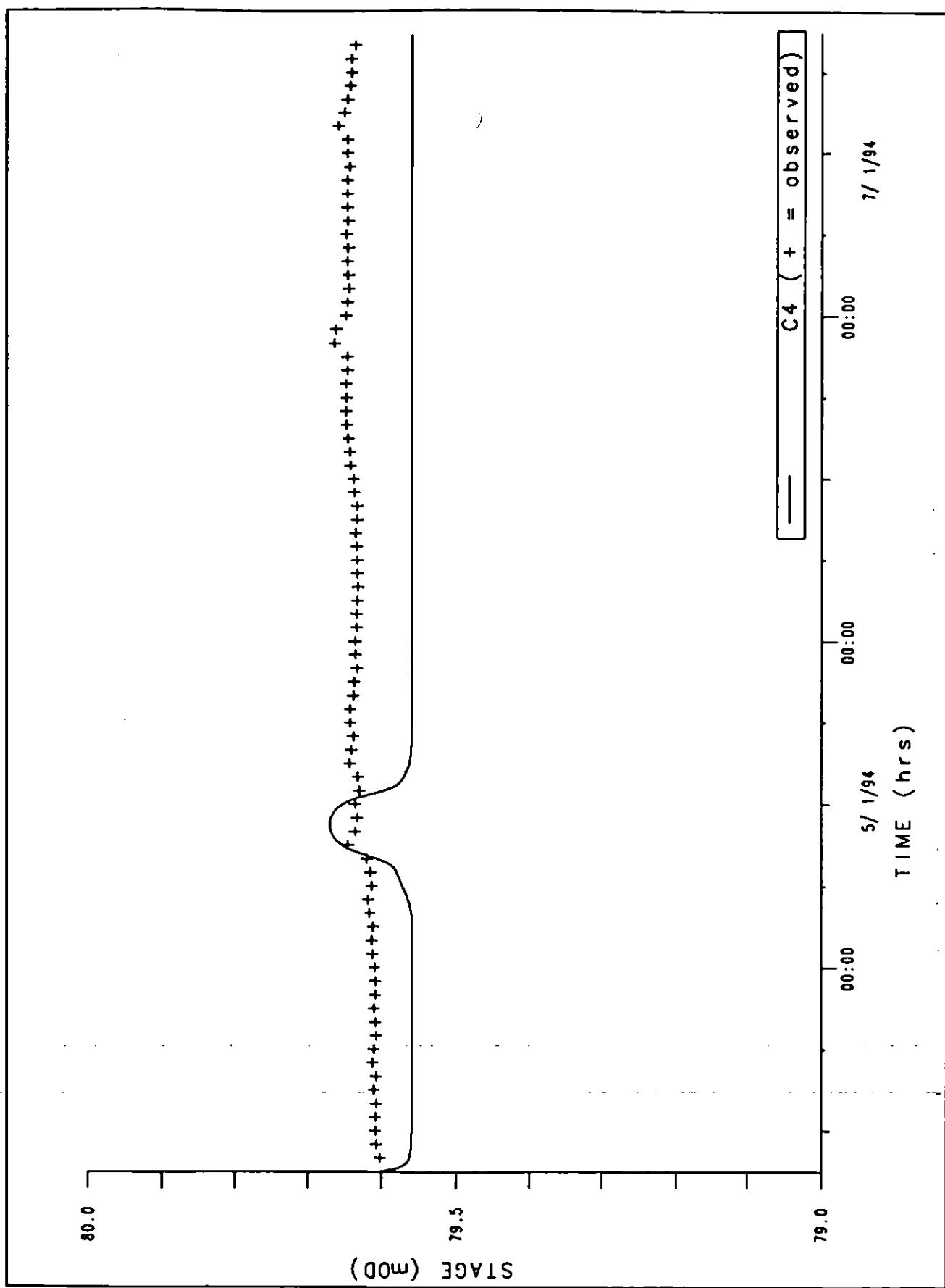


Figure 9 January 1994 calibration results - C4 (Golden Valley)

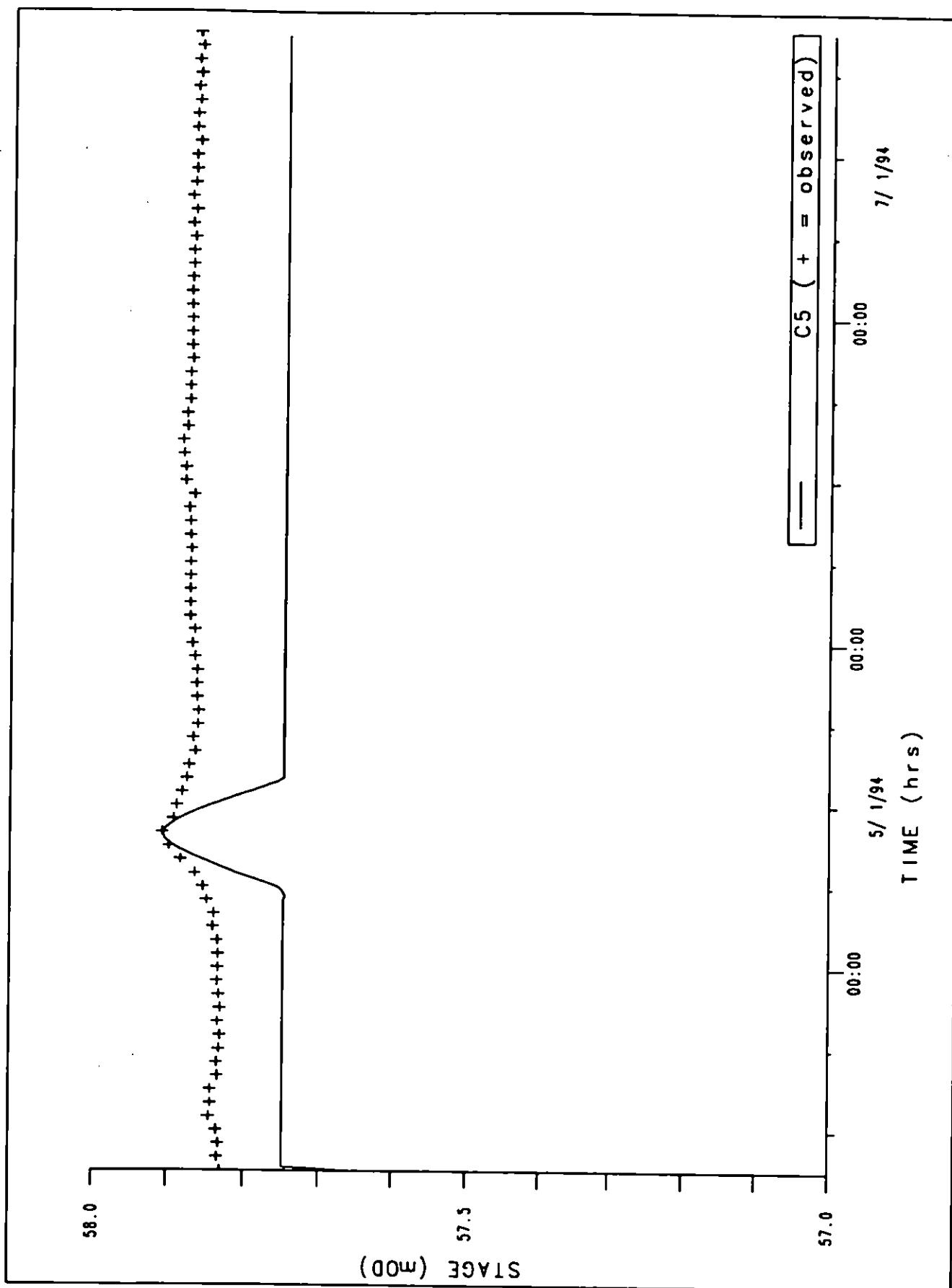


Figure 10 January 1994 calibration results - C5 (Egypt Mill)

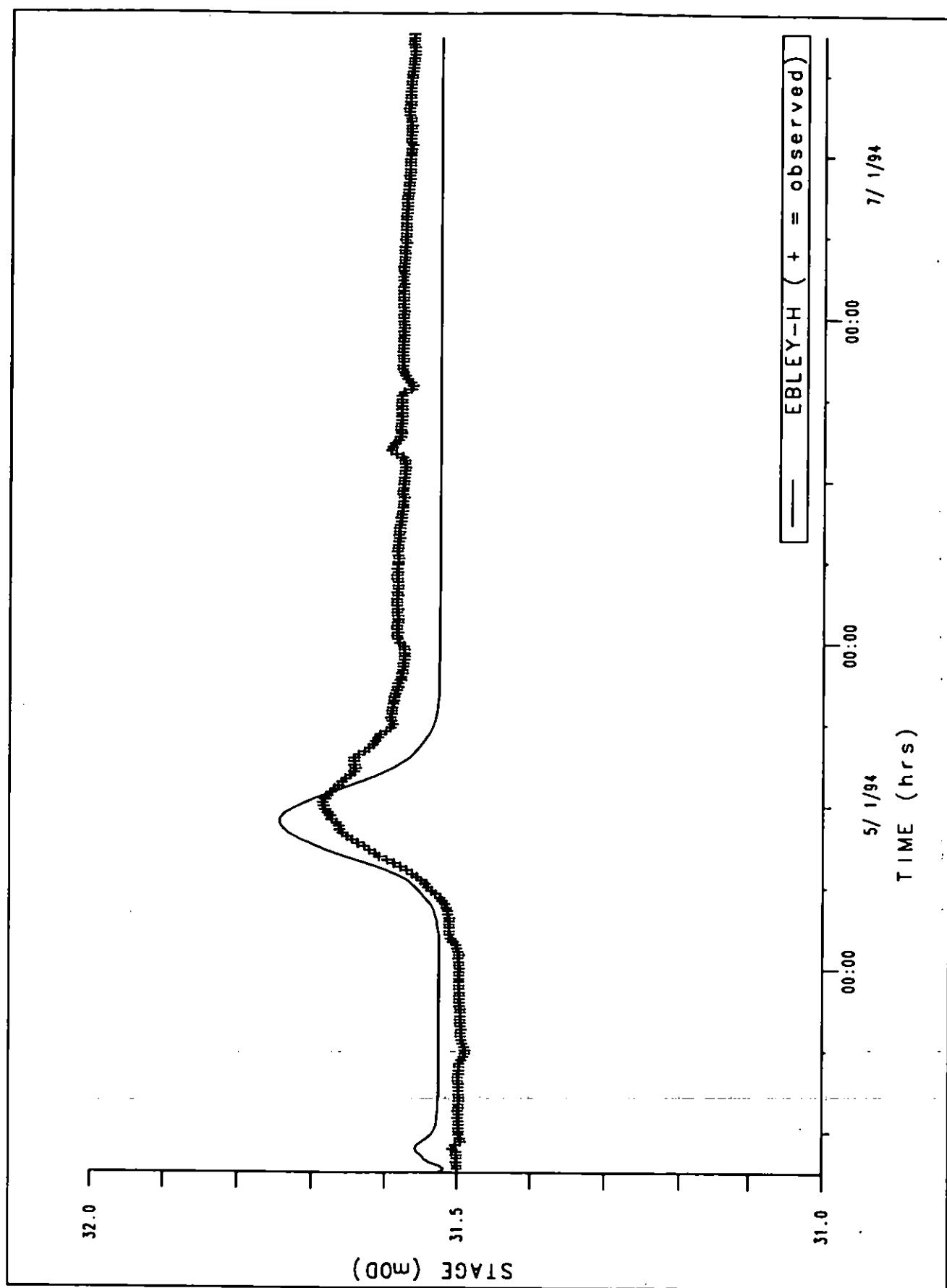


Figure 11 January 1994 calibration results - stage at Ebley Mill

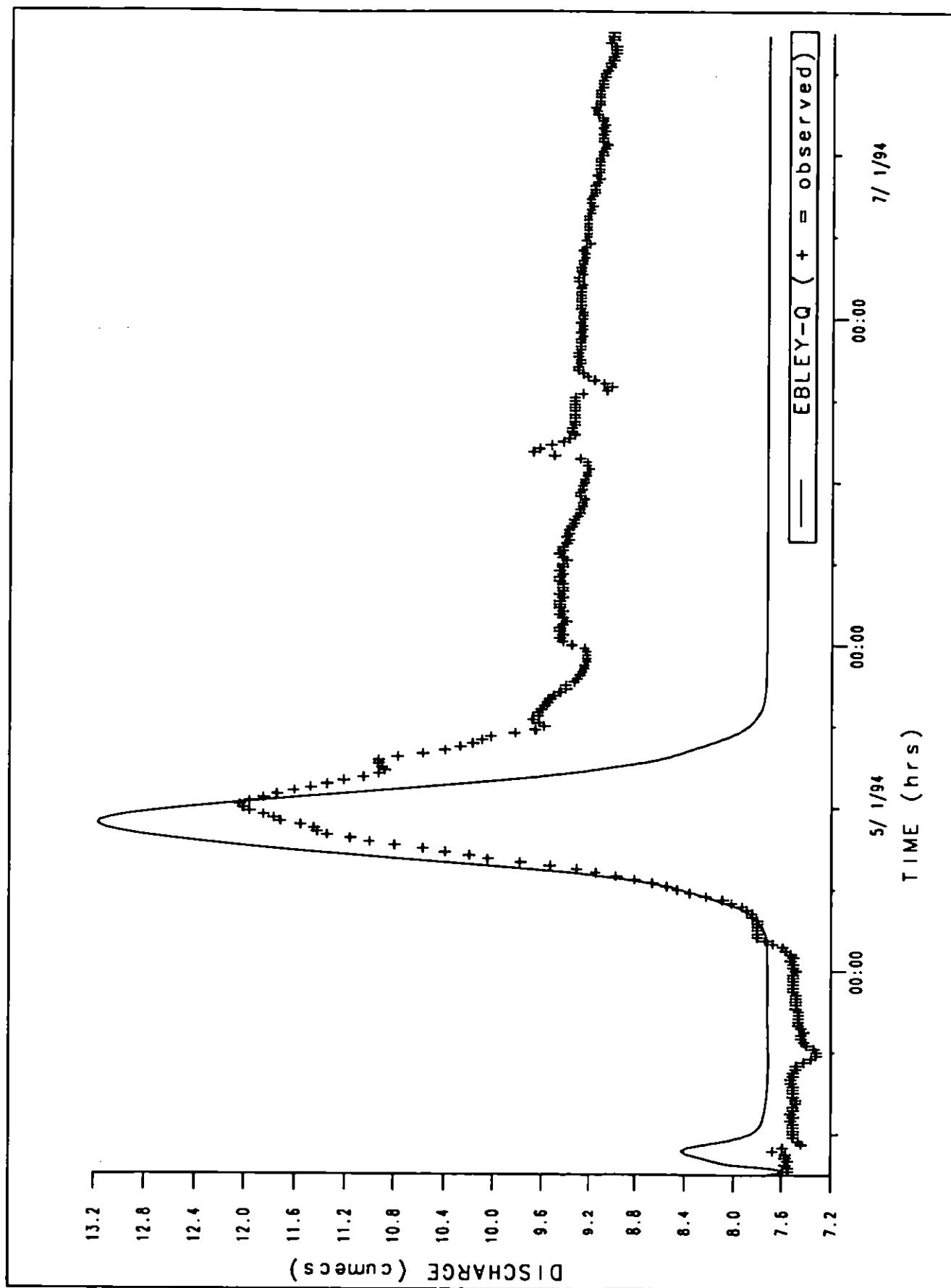


Figure 12 January 1994 calibration results - discharge at Ebley Mill

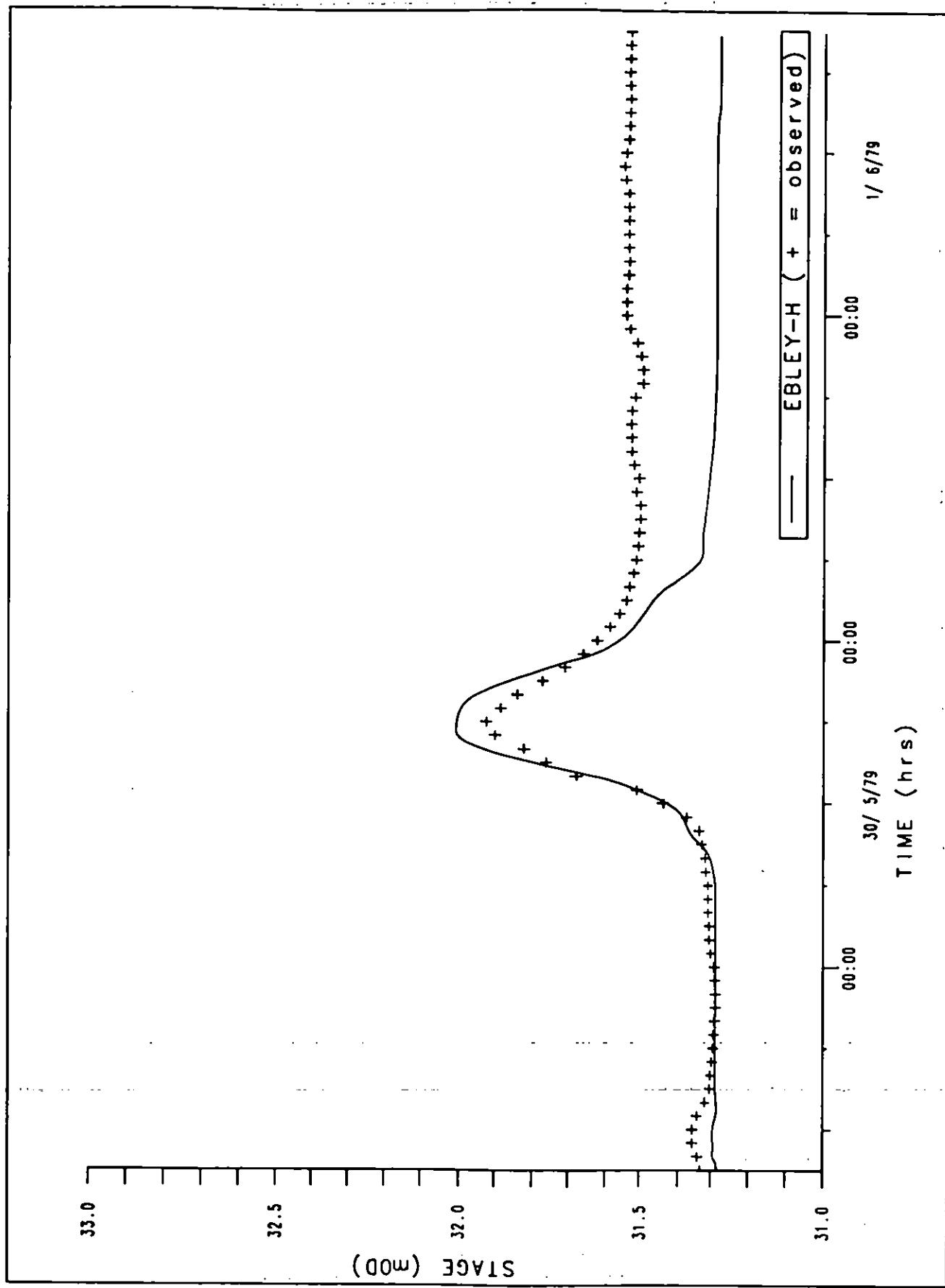


Figure 13 May 1979 calibration results - stage at Ebley Mill

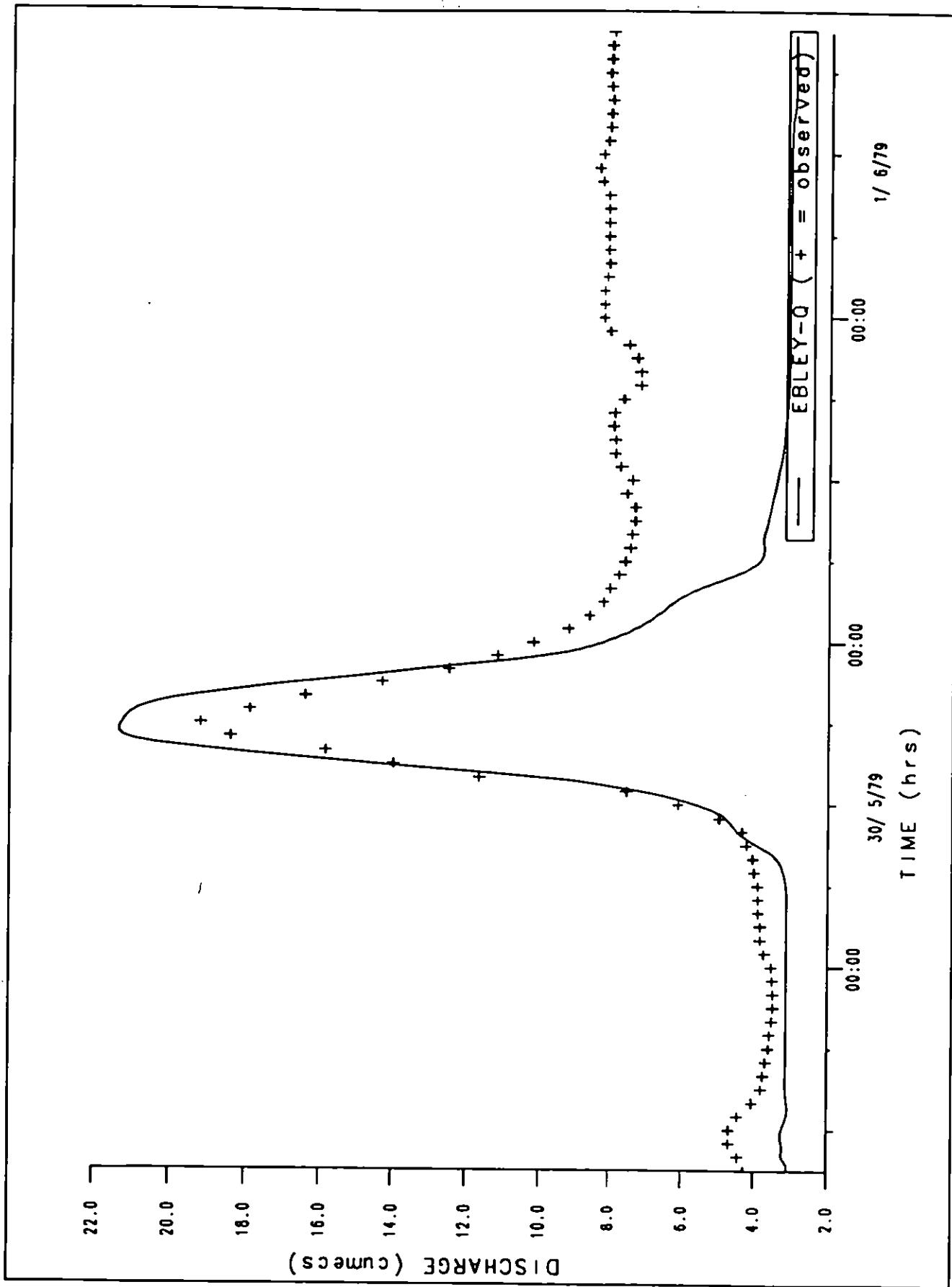


Figure 14 May 1979 calibration results - discharge at Ebley Mill.

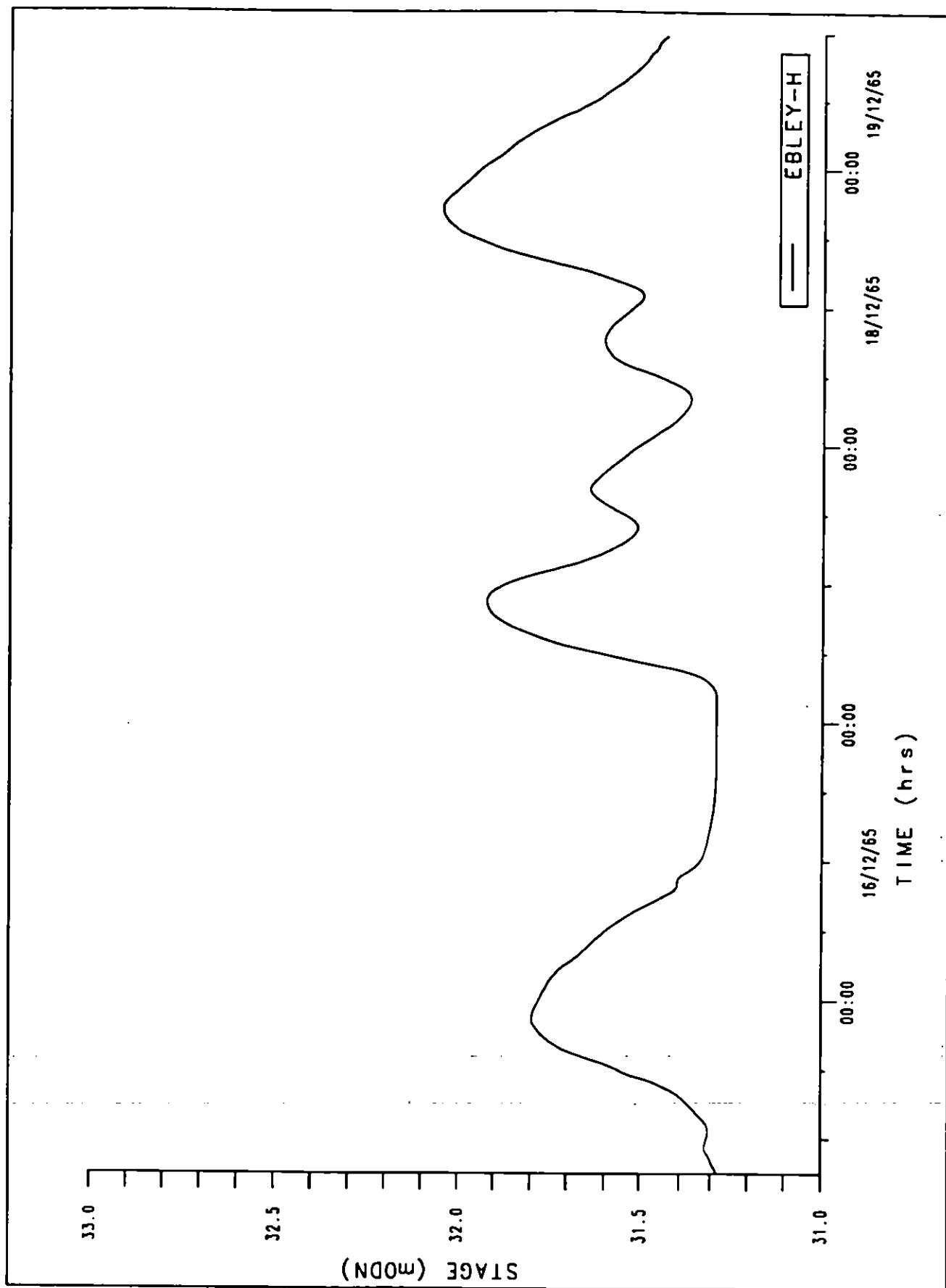


Figure 15 December 1965 calibration results - stage at Ebley Mill

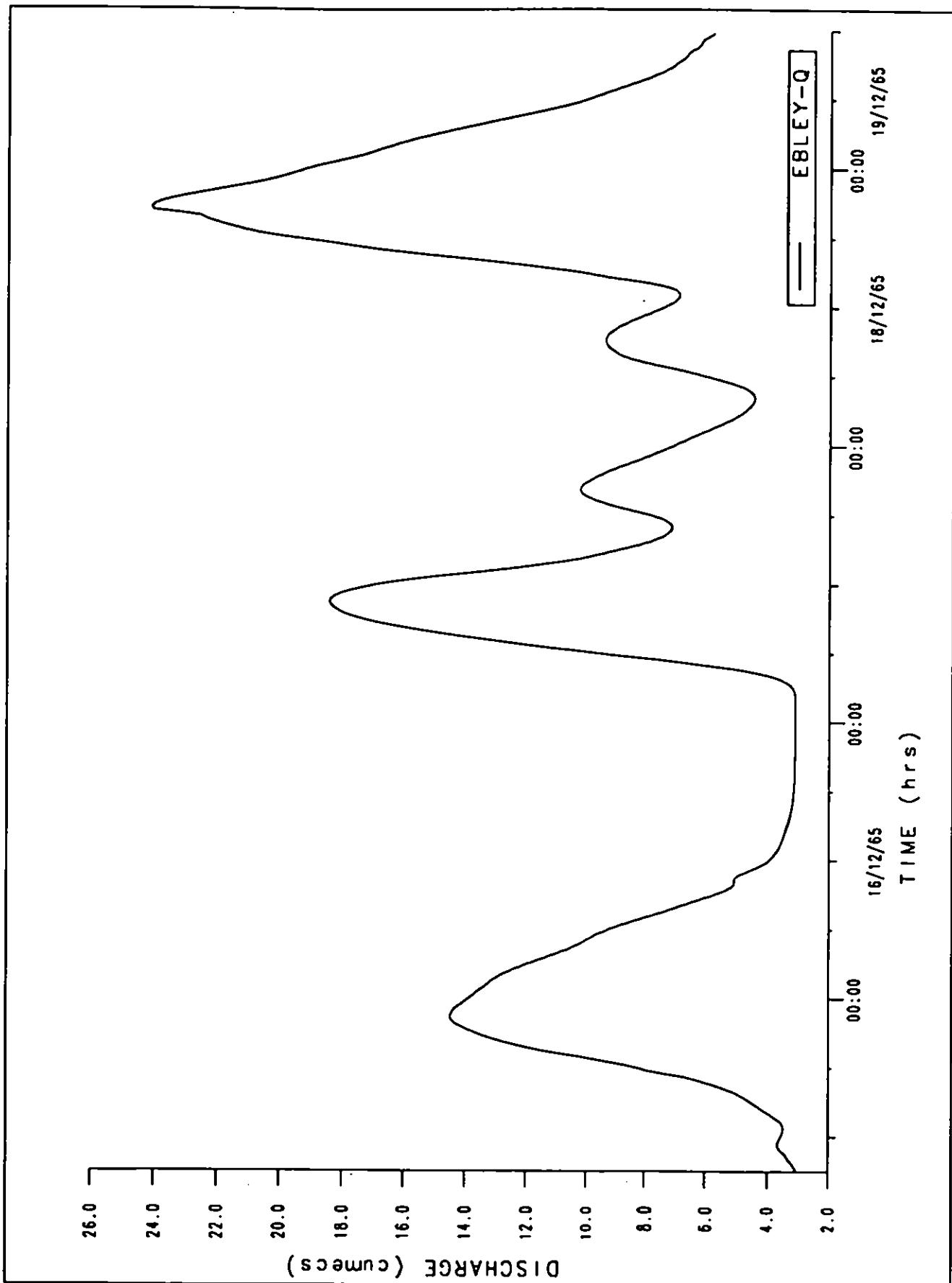


Figure 16 December 1965 calibration results - discharge at Ebley Mill

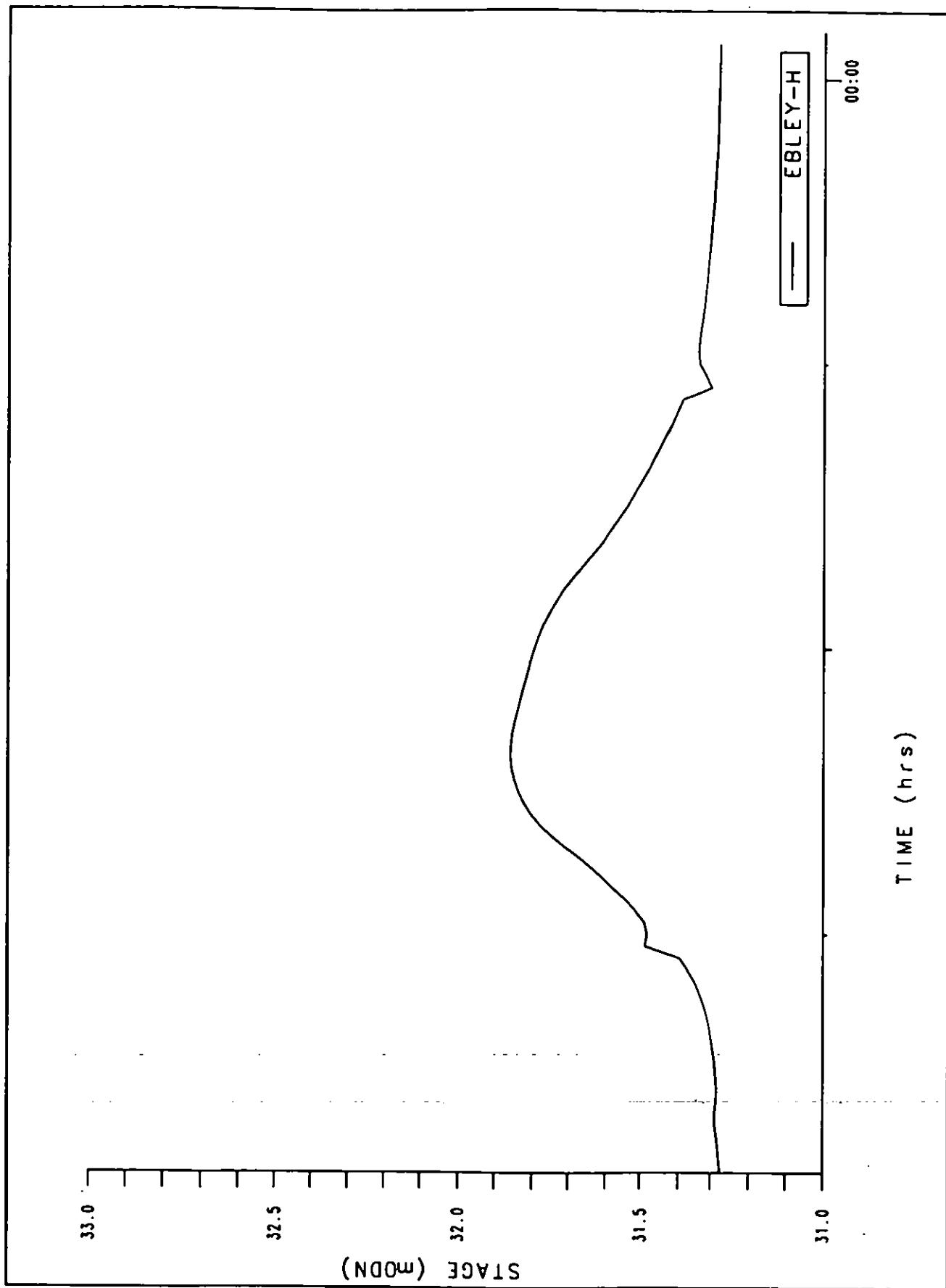


Figure 17 5 year return period flood event - stage at Ebley Mill

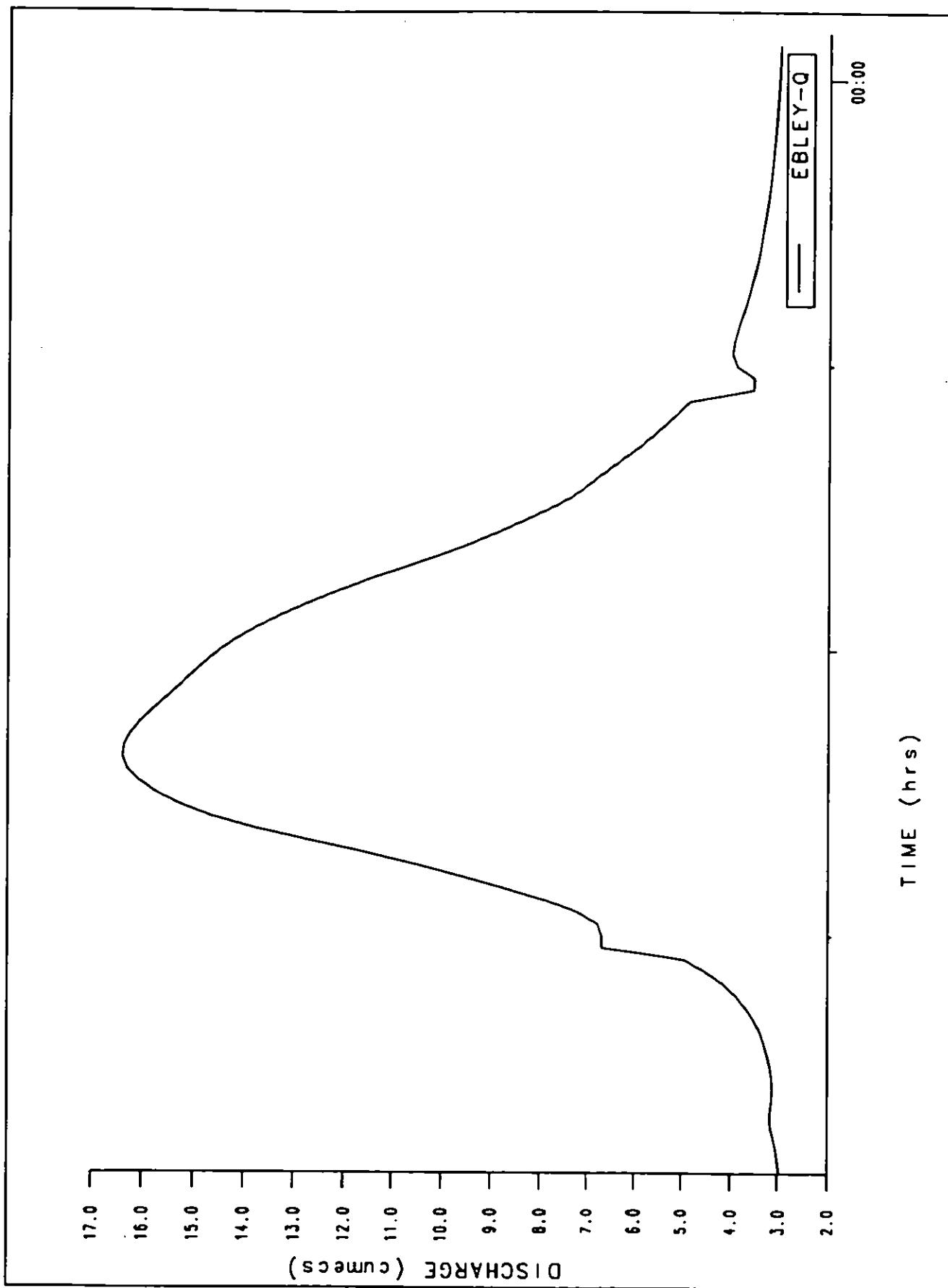


Figure 18 5 year return period flood event - discharge at Ebley Mill

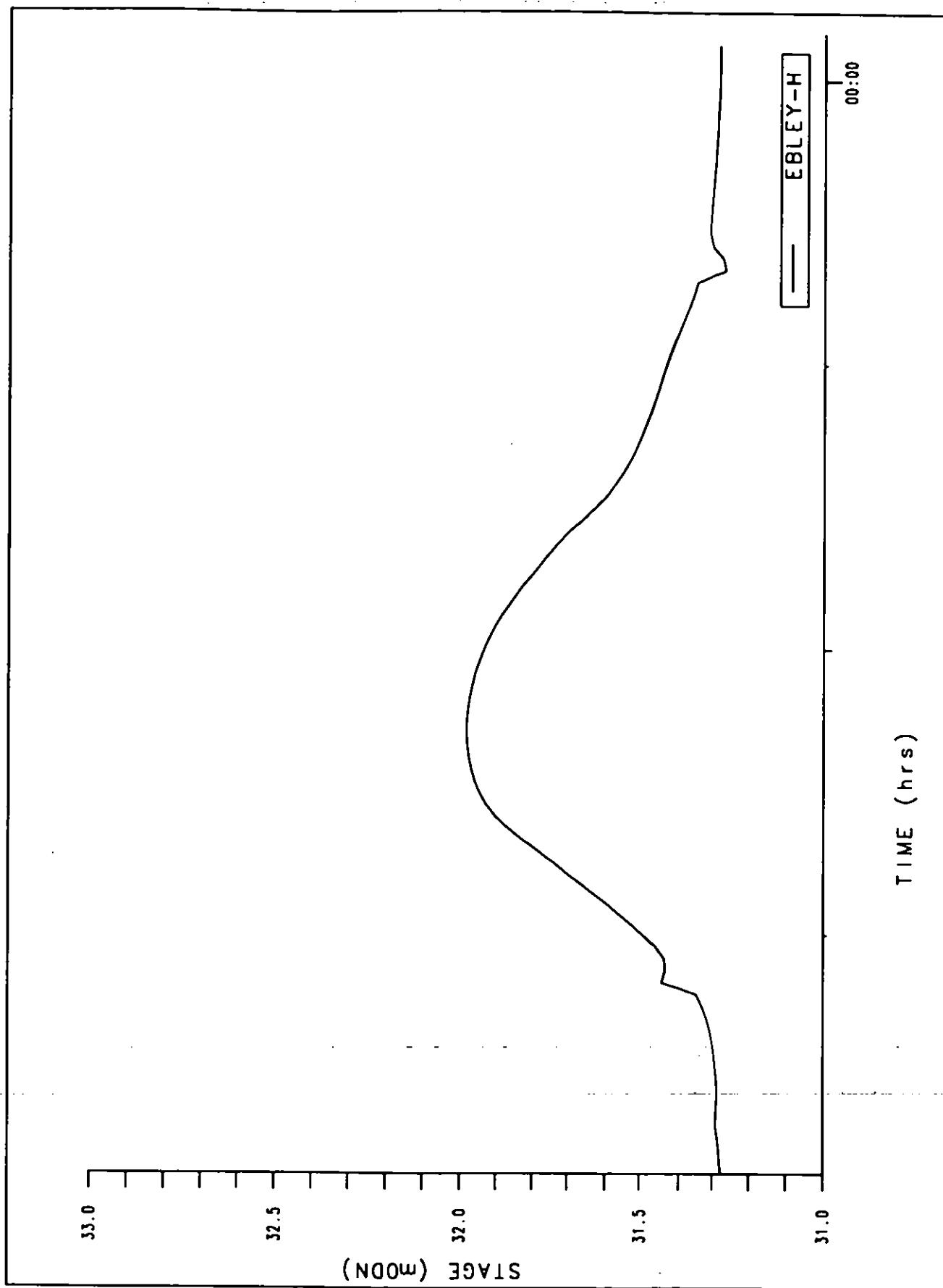


Figure 19 10 year return period flood event - stage at Ebley Mill

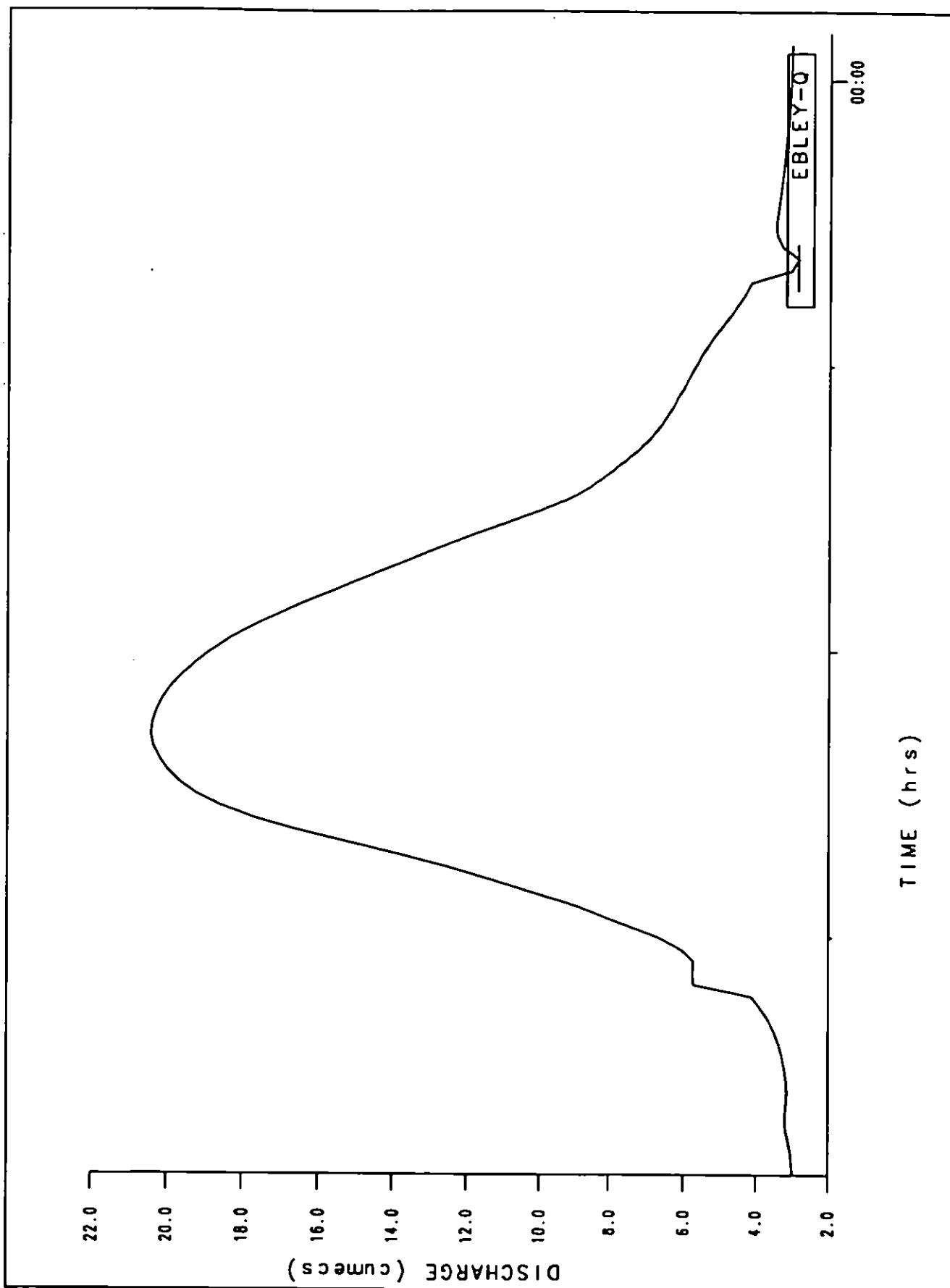


Figure 20 10 year return period flood event - discharge at Ebley Mill

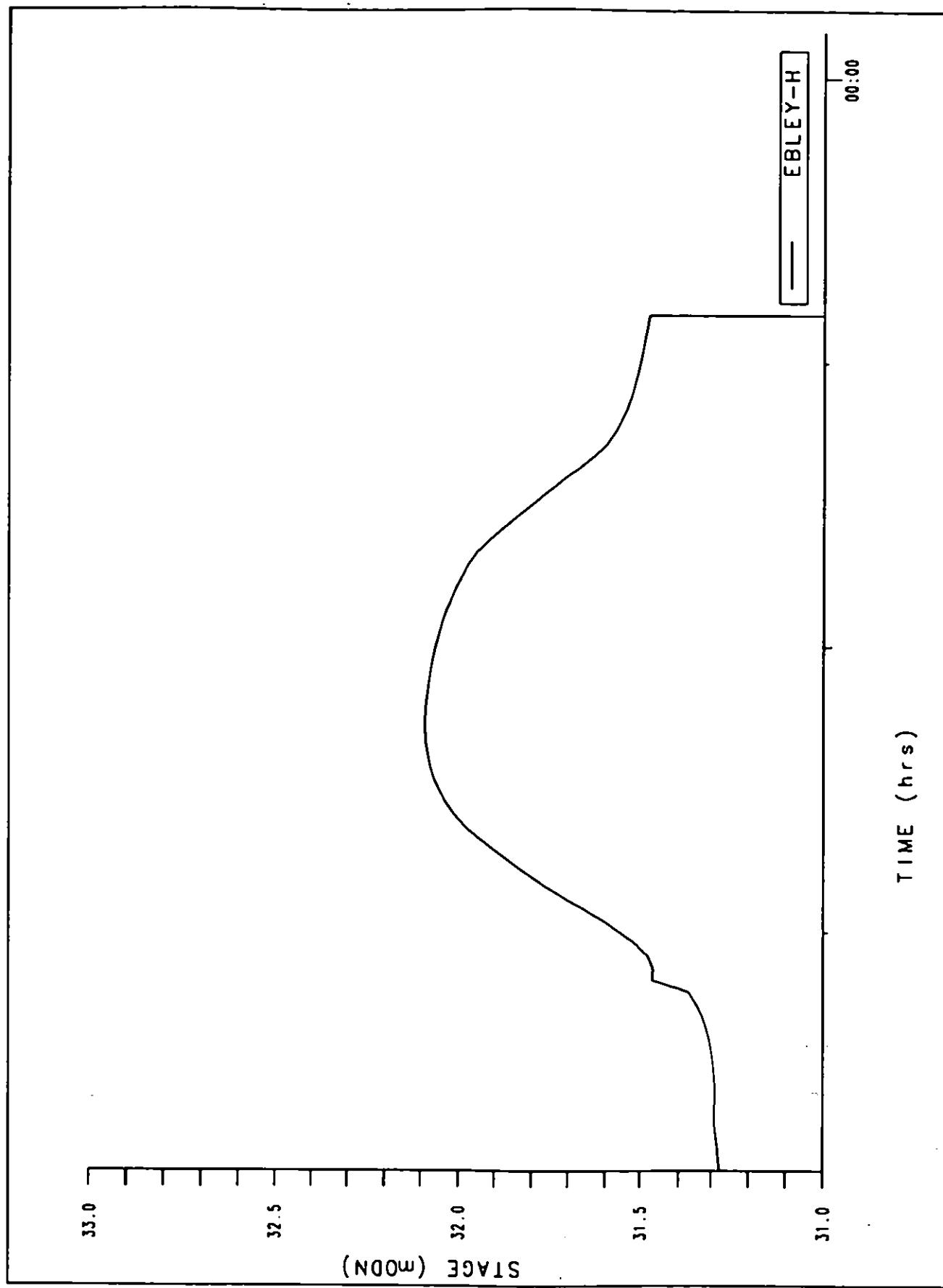


Figure 21 25 year return period flood event - stage at Ebley Mill

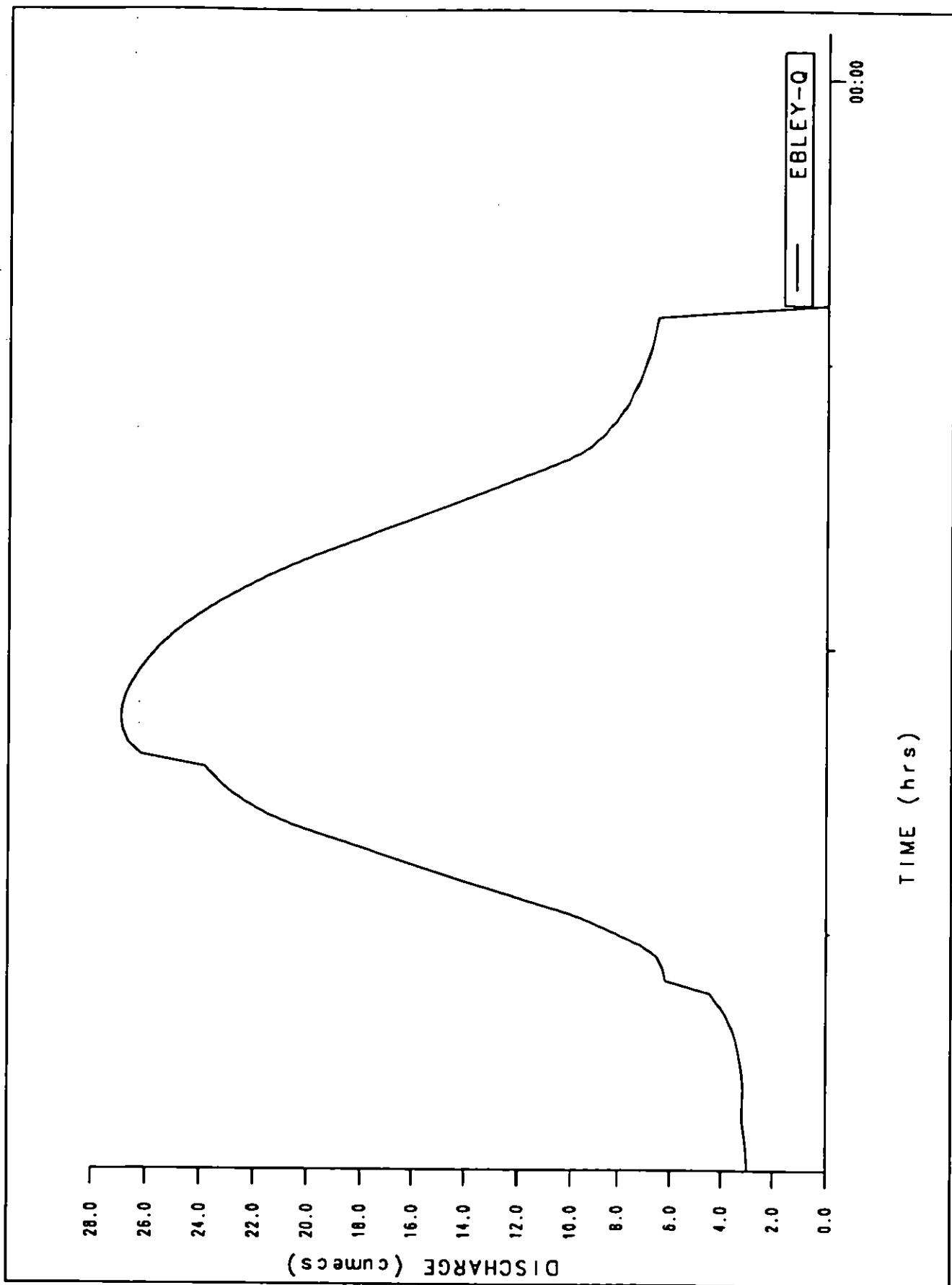


Figure 22 25 year return period flood event - discharge at Ebley Mill

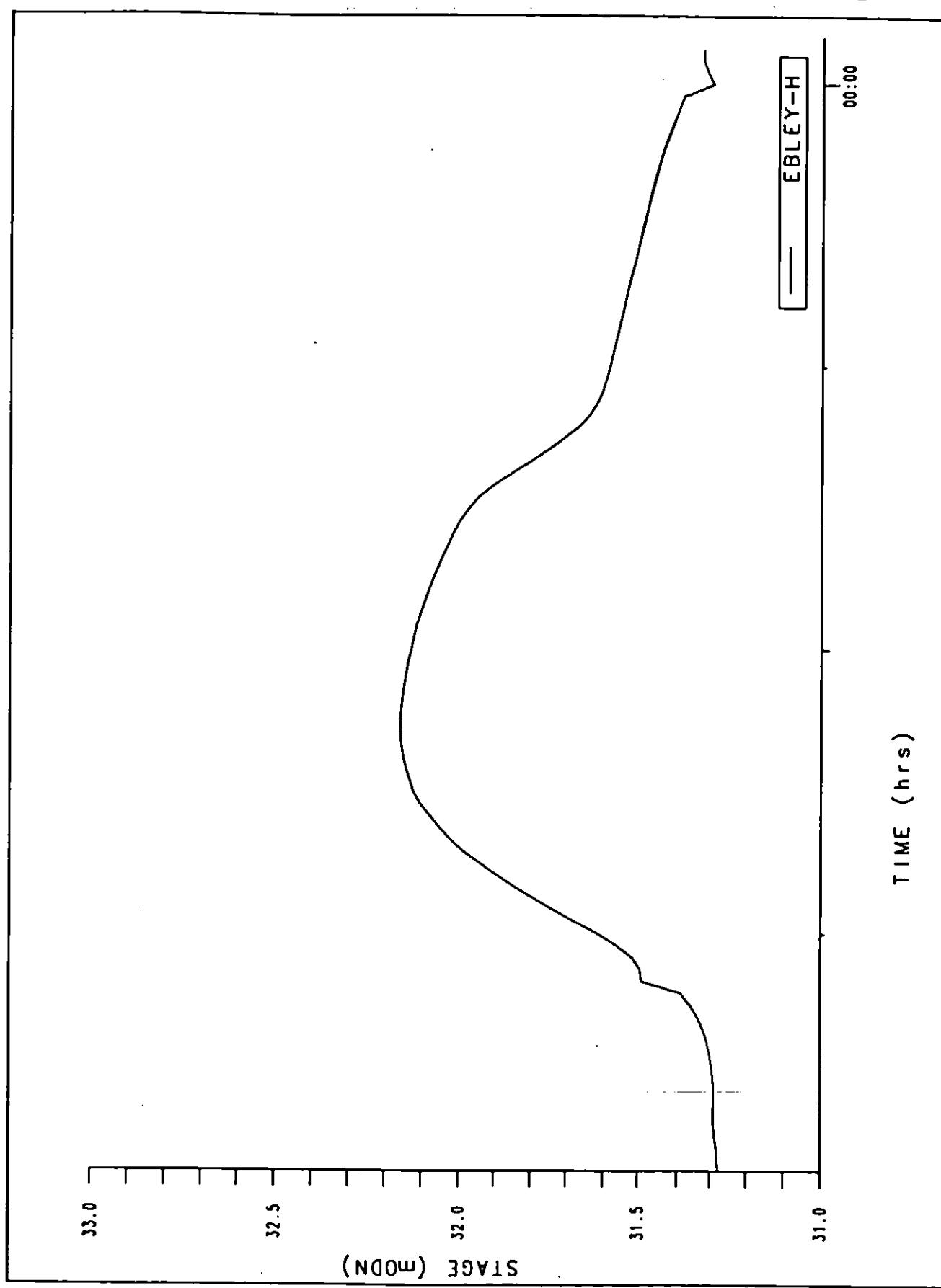


Figure 23 50 year return period flood event - stage at Ebley Mill

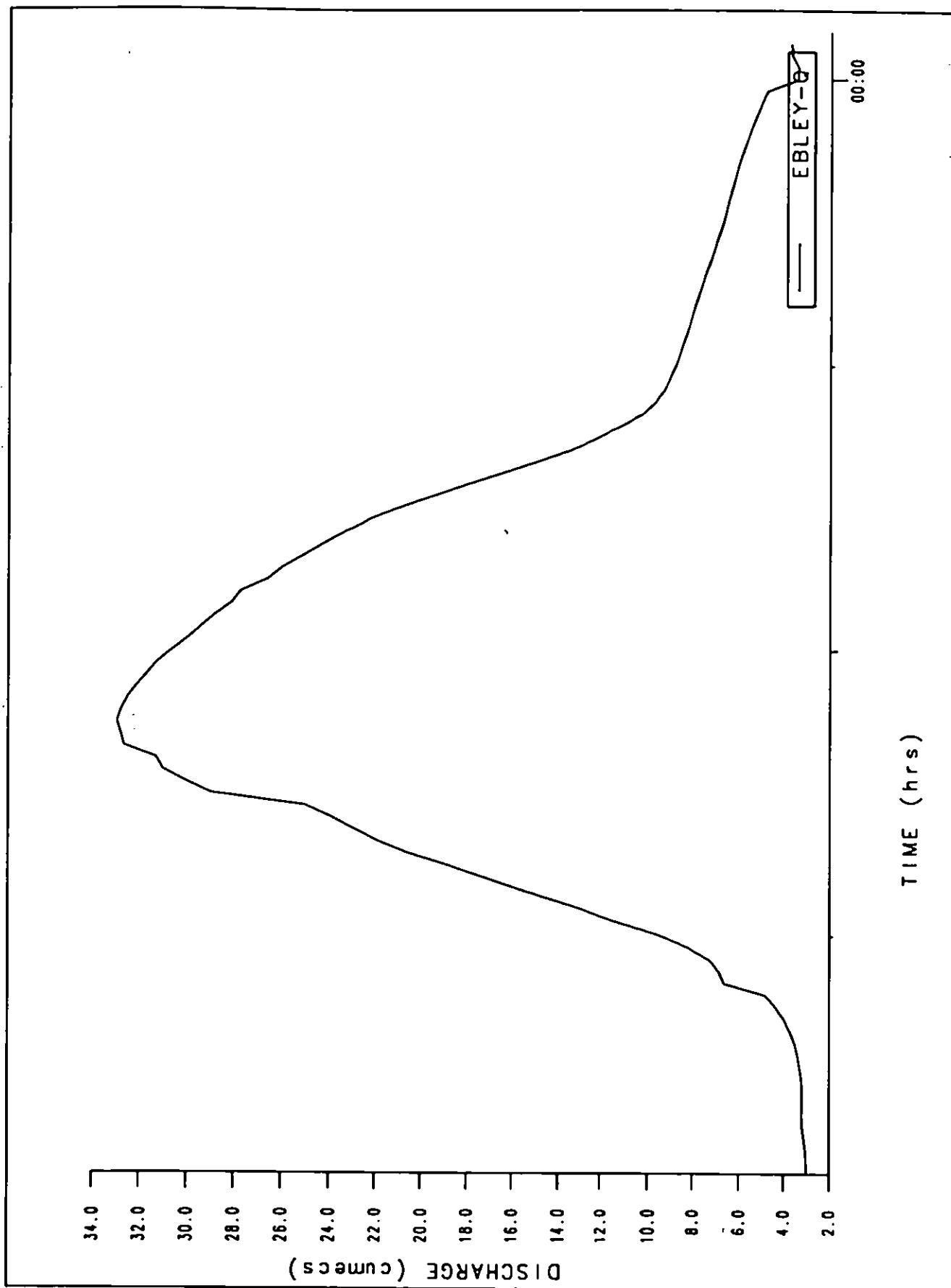


Figure 24 50 year return period flood event - discharge at Ebley Mill

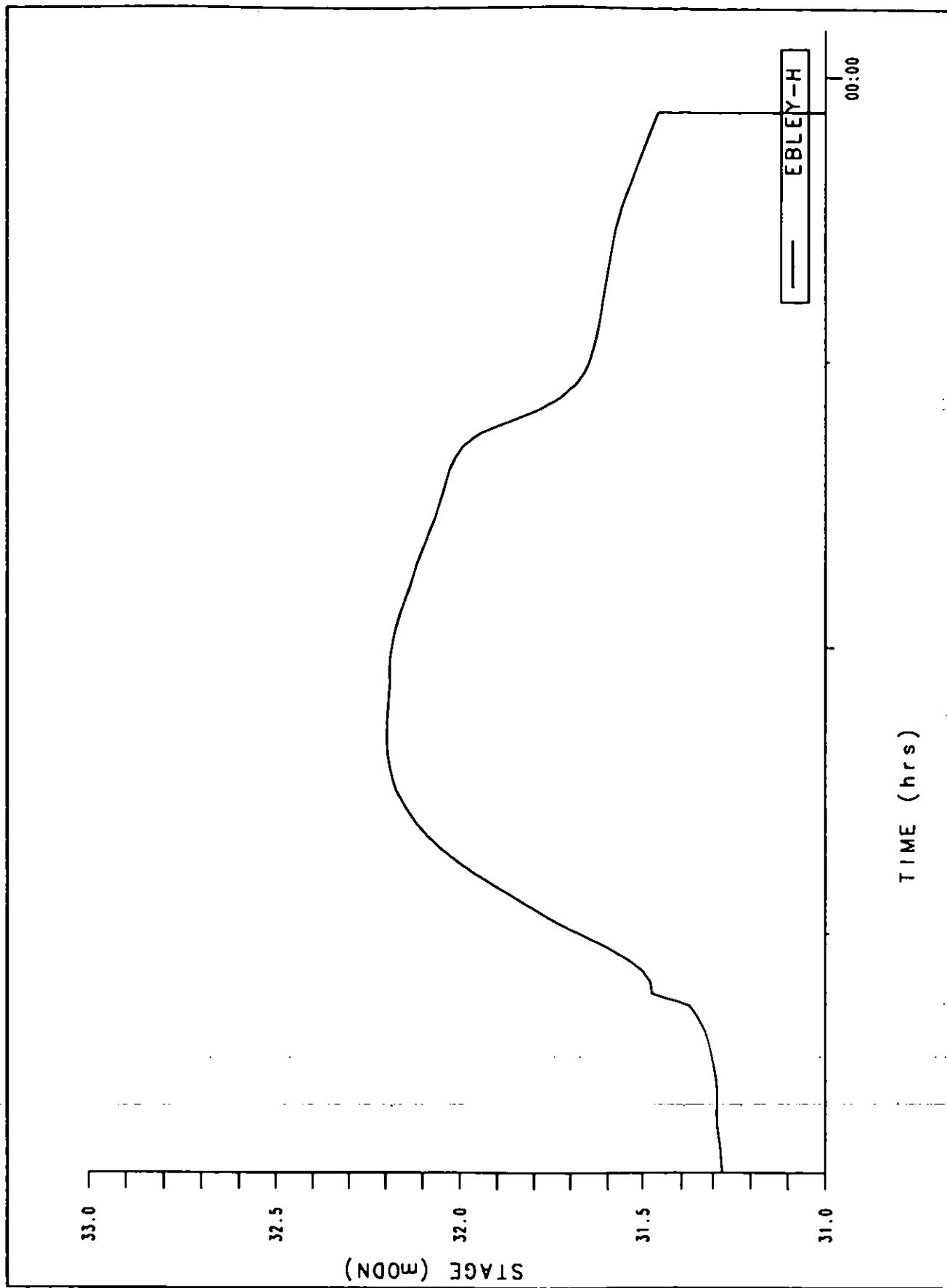


Figure 25 100 year return period flood event - stage at Ebley Mill

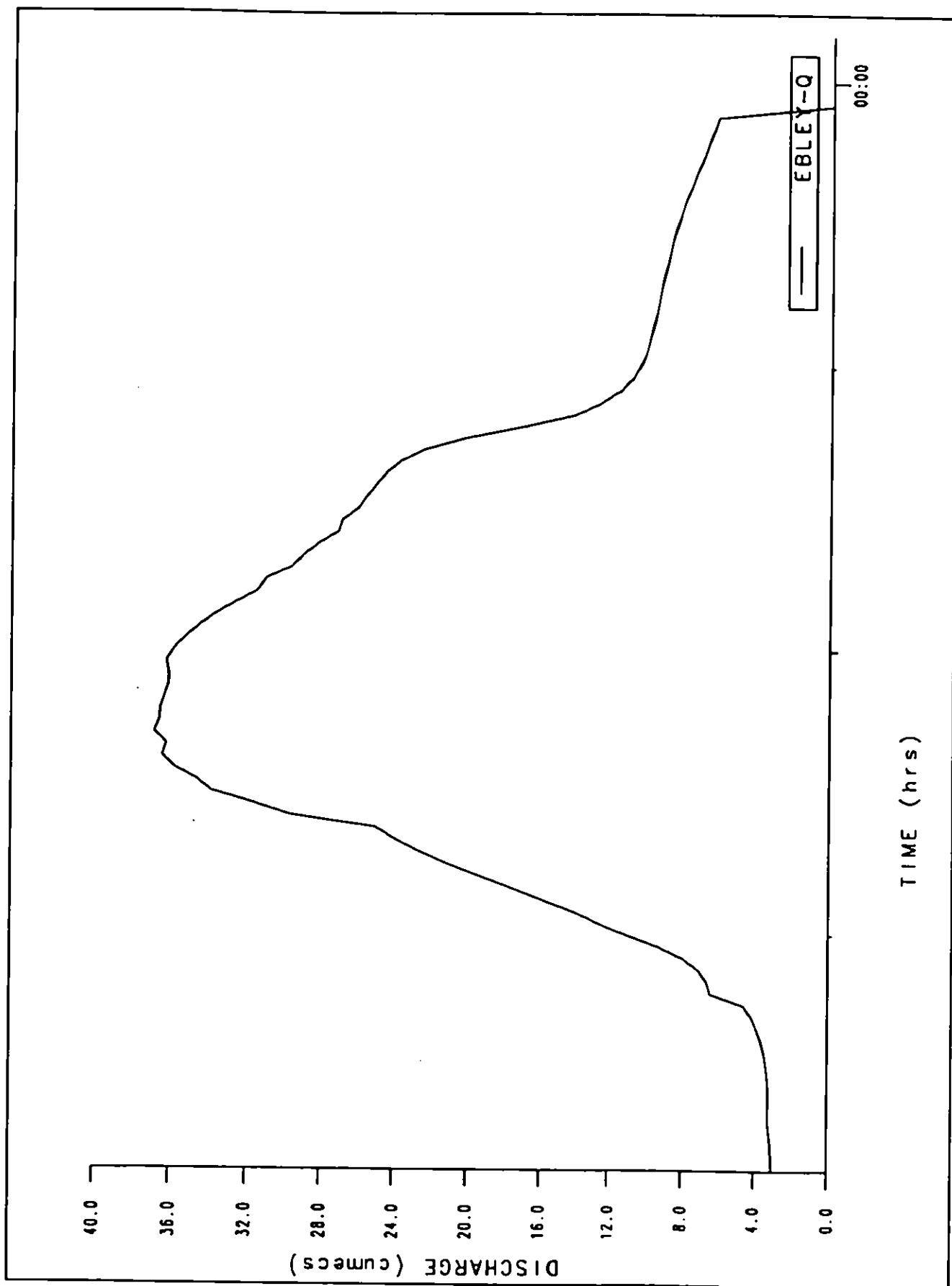


Figure 26 100 year return period flood event - discharge at Ebley Mill

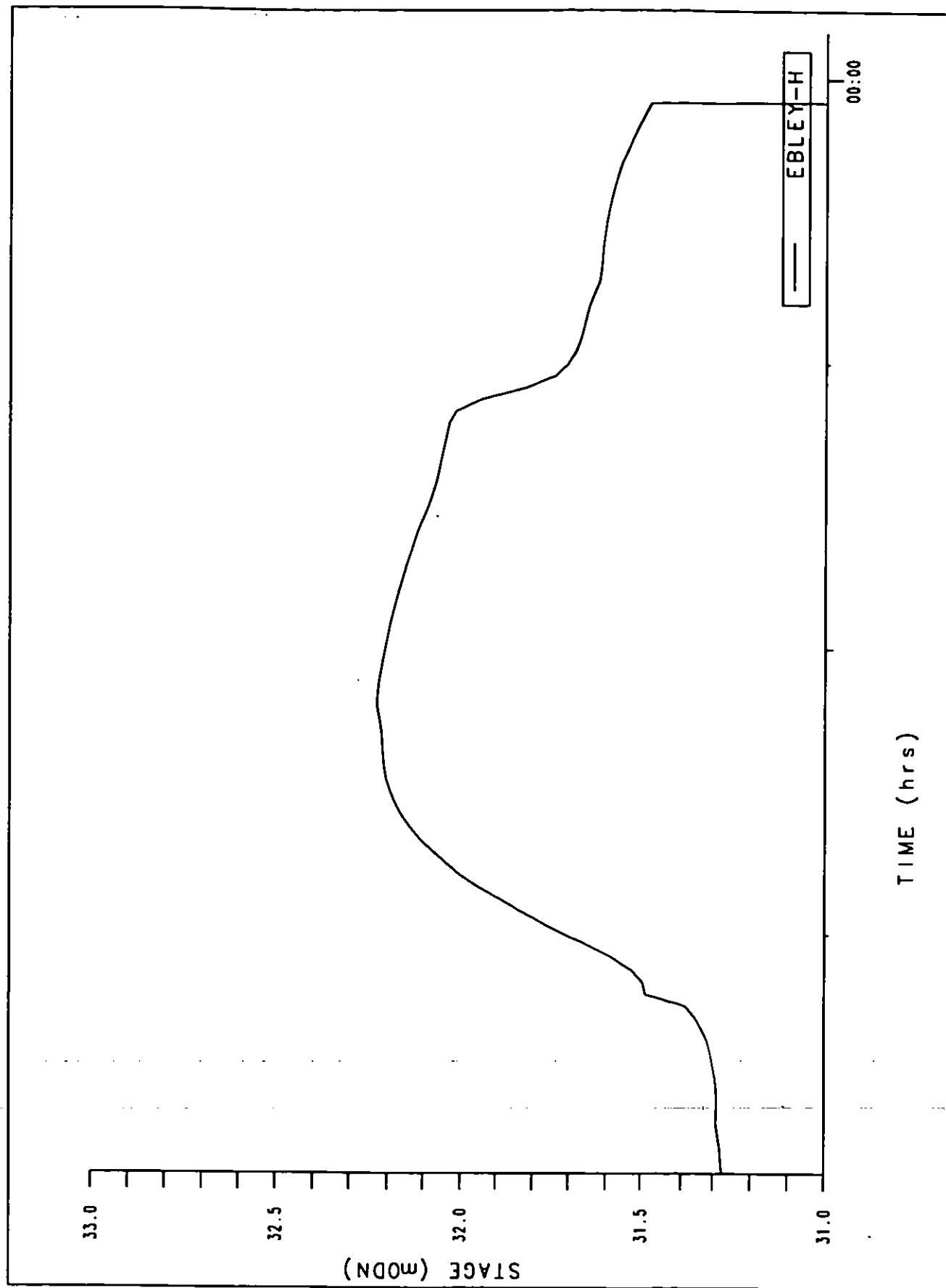


Figure 27 150 year return period flood event - stage at Ebley Mill

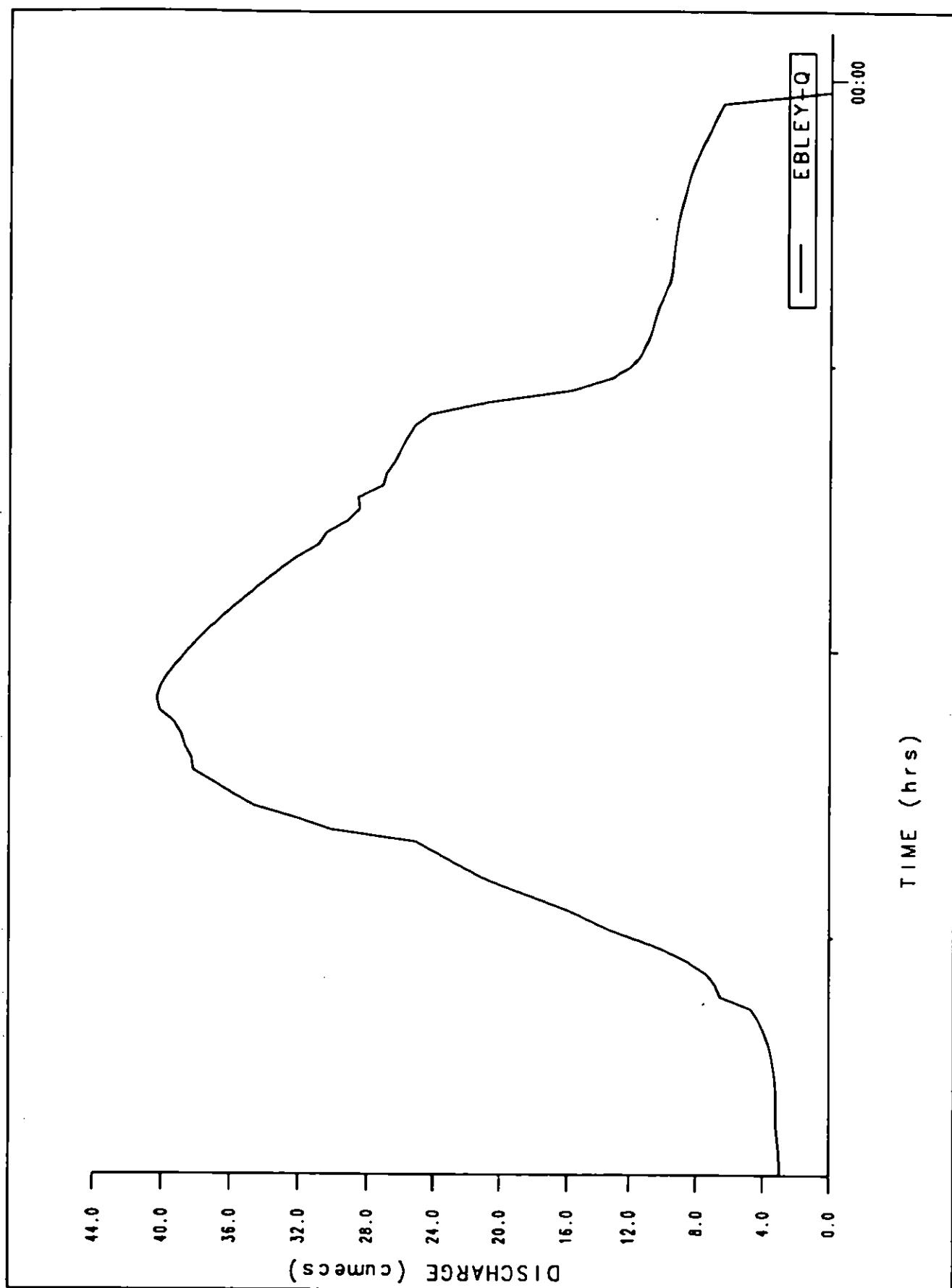


Figure 28 150 year return period flood event - discharge at Ebley Mill

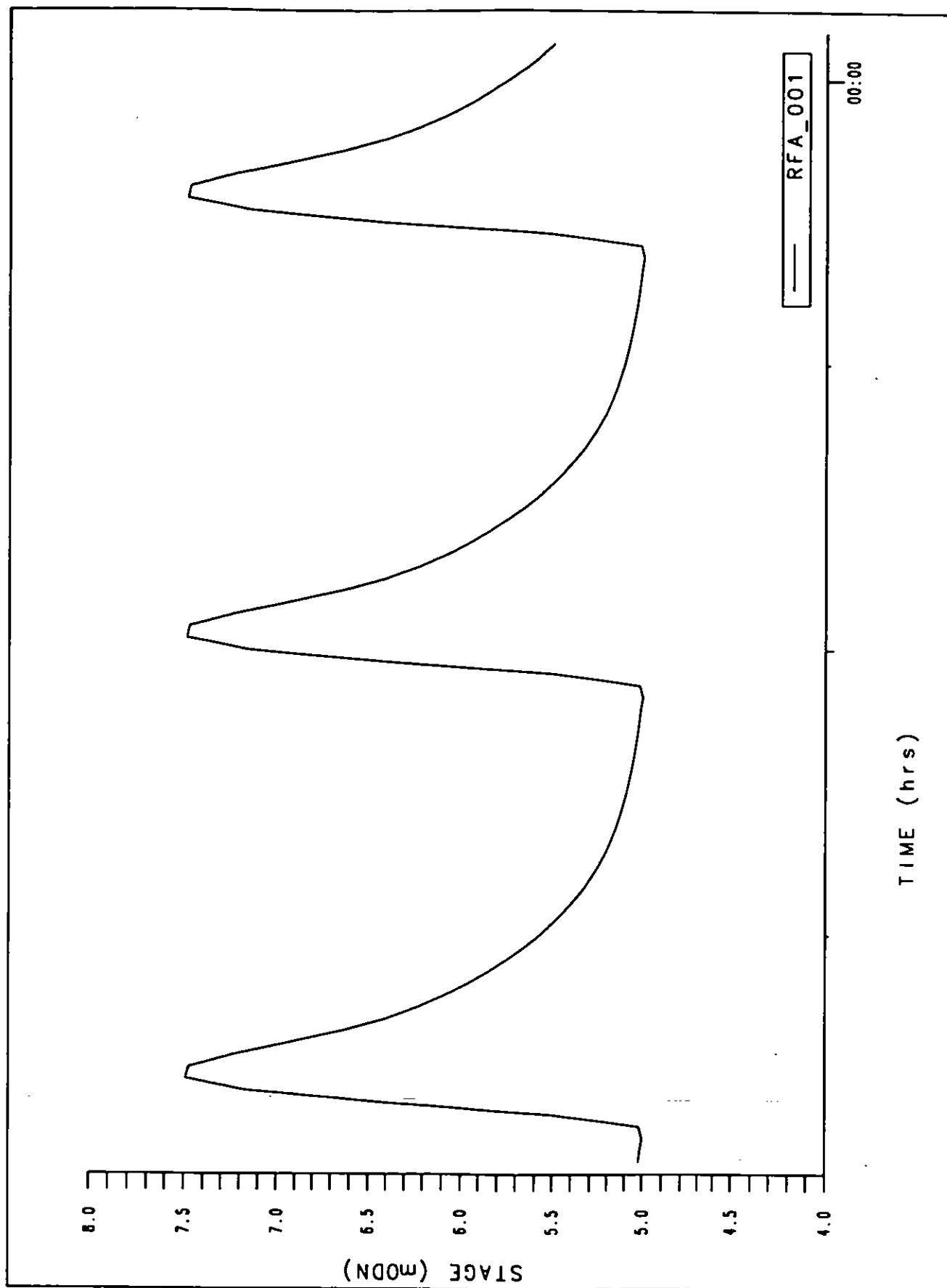


Figure 29 Design event downstream boundary condition

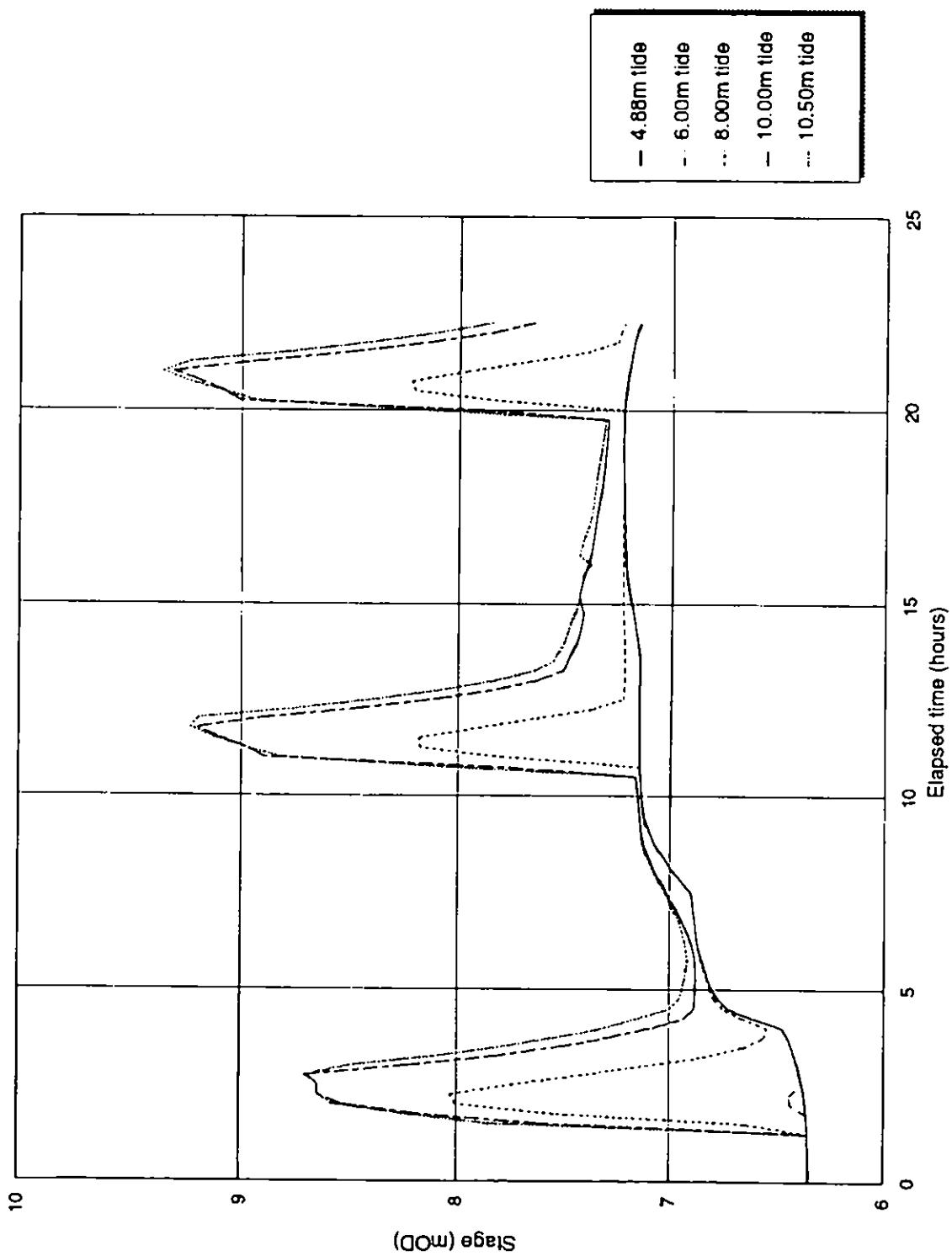


Figure 30 100 year water levels upstream of Framilode outfall

Appendices





Appendix 1

Design event maximum water levels



Section Label	5 Year Event		10 Year Event		25 Year Event		50 Year Event		100 Year Event		150 Year Event	
	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)
RFA_001	7.49	15.0	7.49	16.0	7.49	17.3	7.49	17.5	7.49	17.6	7.49	20.6
River Severn Tidal Outfall												
RFA_001A	7.57	14.9	7.58	15.9	7.61	17.2	7.63	17.4	7.64	17.5	7.68	20.5
RFA_002	7.60	14.5	7.61	15.9	7.65	16.9	7.68	17.1	7.68	17.2	7.73	20.3
Upper Framford Weir												
RFA_003	7.86	14.5	7.90	15.9	7.99	16.9	8.04	17.0	8.06	17.1	8.16	20.3
RFA_004	7.91	14.3	7.95	15.9	8.05	16.8	8.09	16.9	8.11	17.0	8.23	20.2
RFA_005	7.98	13.9	8.02	15.9	8.13	16.6	8.17	16.7	8.18	17.0	8.31	20.0
Junction with RFB_001												
RFA_006	7.98	6.5	8.02	7.4	8.13	7.8	8.17	7.8	8.18	8.0	8.31	9.9
RFA_007	8.01	6.4	8.06	7.4	8.17	7.7	8.20	7.8	8.21	8.0	8.35	9.8
RFA_008	8.05	6.4	8.09	7.4	8.20	7.7	8.24	7.7	8.25	8.0	8.39	9.7
RFA_008A	8.03	6.4	8.08	7.4	8.18	7.7	8.22	7.7	8.22	8.0	8.36	9.7
Gloucester & Sharpness Canal - Left Syphon												
RFA_009	8.11	6.4	8.17	7.4	8.30	7.6	8.33	7.7	8.34	8.0	8.55	9.7
RFA_010	8.18	6.4	8.24	7.4	8.37	7.6	8.41	7.7	8.42	8.0	8.65	9.7
RFA_011	8.20	6.4	8.25	7.4	8.39	7.6	8.42	7.7	8.43	8.0	8.68	8.4
RFA_012	8.25	6.4	8.32	7.4	8.44	7.6	8.47	7.7	8.48	8.0	8.71	8.5
Whitminster Weir - Left												
RFA_013	8.38	6.4	8.49	7.4	8.57	7.6	8.59	7.7	8.60	8.0	8.79	8.5
Junction with RFB_008												
RFA_014	8.38	13.9	8.49	15.9	8.57	16.2	8.59	16.5	8.60	17.5	8.79	19.8
RFA_015	8.38	13.9	8.48	15.9	8.56	16.2	8.58	16.4	8.59	17.5	8.78	19.9

Whitminster Bridge						
	8.38	13.9	8.48	15.9	8.57	16.2
RFA_016	8.38	13.9	8.48	15.9	8.57	16.2
RFA_017	8.42	13.9	8.53	15.9	8.61	16.2
RFA_018	8.44	13.9	8.55	15.9	8.63	16.2

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RFA_019	10.15	13.9	10.07	15.9	10.09	16.2	10.13	16.4	10.11	17.5	10.14	19.9
RFA_020	10.16	13.9	10.07	15.9	10.10	16.2	10.13	16.4	10.11	17.5	10.19	19.9
RFA_021	10.18	13.9	10.18	15.9	10.20	16.2	10.21	16.4	10.25	17.5	10.35	19.9
RFA_022	10.20	13.9	10.29	15.9	10.31	16.2	10.32	16.4	10.37	17.5	10.47	19.9
RFA_023	10.23	13.9	10.34	15.9	10.36	16.2	10.37	16.4	10.42	17.5	10.52	19.9

Walk Rhine Bridge

RFA_024	10.27	13.9	10.39	15.9	10.40	16.2	10.41	16.4	10.47	17.5	10.58	19.9
RFA_025	10.34	13.9	10.47	15.9	10.48	16.2	10.49	16.4	10.55	17.5	10.68	18.0
RFA_026	10.39	13.9	10.51	15.9	10.53	16.2	10.54	16.4	10.60	17.5	10.71	18.0
RFA_027	10.45	14.0	10.58	15.9	10.60	16.2	10.61	16.4	10.66	17.5	10.75	18.0
RFA_028	10.55	14.0	10.67	15.9	10.69	16.2	10.70	16.4	10.76	17.5	10.82	18.0
RFA_029	10.66	14.0	10.76	15.9	10.80	16.2	10.81	16.4	10.86	17.5	10.90	18.0
RFA_030	10.76	14.0	10.88	15.9	10.90	16.2	10.91	16.4	10.97	17.5	11.00	18.0
RFA_031	10.84	14.0	10.95	15.9	10.97	16.2	10.98	16.4	11.03	17.5	11.06	18.0
RFA_032	10.91	14.0	11.03	15.9	11.04	16.2	11.05	16.4	11.11	17.5	11.14	18.0

Fromebridge Hall

RFA_033	12.36	14.0	12.41	15.9	12.42	16.2	12.43	16.4	12.46	17.5	12.48	18.0
RFA_034	12.37	14.0	12.49	15.9	12.44	16.1	12.45	16.4	12.48	17.5	12.50	18.0
A38 Road Bridge												
RFA_035	12.41	14.0	12.49	15.9	12.50	16.1	12.51	16.4	12.56	17.5	12.58	18.0
RFA_036	12.43	14.0	12.51	17.8	12.52	18.6	12.53	19.4	12.58	23.5	12.60	25.0

RFA_037	12.44	14.0	12.54	17.8	12.55	18.6	12.56	19.4	12.61	24.6	12.63	26.7
RFA_038	12.46	14.0	12.57	18.0	12.58	19.2	12.59	20.6	12.66	29.7	12.67	33.9
RFA_039	12.48	14.0	12.59	18.0	12.61	19.2	12.62	20.6	12.71	29.7	12.74	33.9

M5 Road Bridge

RFA_040	12.51	14.0	12.62	18.0	12.64	19.2	12.66	20.6	12.78	29.7	12.83	33.9
RFA_041	12.59	14.1	12.73	18.0	12.75	19.2	12.79	20.6	12.98	28.1	13.07	30.7
RFA_042	12.69	14.1	12.85	18.0	12.89	19.2	12.94	19.9	13.19	21.4	13.29	22.1
RFA_043	12.78	14.1	12.85	18.0	12.99	19.2	13.04	19.9	13.27	21.4	13.36	22.1

Meadow Mill Wall

RFA_044	13.71	14.1	14.14	18.0	14.27	19.2	14.35	19.9	14.43	21.4	14.45	22.1
RFA_045	13.74	14.1	14.15	18.9	14.26	25.2	14.33	30.6	14.40	36.3	14.42	38.8
RFA_046	13.77	14.1	14.19	18.9	14.31	25.3	14.40	30.7	14.48	36.4	14.50	39.3

Junction with RFC_001

RFA_047	13.77	12.2	14.19	17.3	14.31	23.6	14.40	29.1	14.48	34.9	14.50	37.7
RFA_048	13.88	12.2	14.27	17.3	14.44	23.6	14.56	29.2	14.67	34.9	14.72	37.7

Meadow Bridge

RFA_049	13.90	12.2	14.31	17.3	14.49	23.6	14.64	29.2	14.78	34.9	14.92	37.7

Junction with RFD_001

RFA_050	13.90	6.8	14.31	11.2	14.49	14.5	14.64	17.5	14.78	19.3	14.82	19.9
RFA_051	14.07	6.8	14.46	10.5	14.64	11.4	14.78	12.4	14.90	12.7	15.01	12.7
RFA_052	14.25	6.9	14.61	10.6	14.77	11.1	14.89	11.3	15.00	11.4	15.09	11.3
RFA_053	14.46	5.8	14.78	6.3	14.89	6.5	14.97	6.7	15.05	6.8	15.12	6.8

Millend Mills Shulkes

RFA_054	15.66	5.8	15.73	6.3	15.76	6.5	15.79	6.7	15.80	6.8	15.80	6.8
RFA_055	15.90	5.8	15.94	6.3	15.97	6.5	15.98	6.7	15.99	6.7	16.00	6.8
RFA_056	16.10	5.8	16.14	6.3	16.16	6.5	16.17	6.7	16.18	6.7	16.18	6.8

RFA_057	16.24	5.8	16.28	6.3	16.30	6.5	16.31	6.7	16.32	6.7	16.32	6.8
RFA_058	16.36	5.8	16.40	6.3	16.42	6.5	16.43	6.6	16.44	6.7	16.44	6.8
RFA_059	16.47	5.8	16.51	6.2	16.54	6.5	16.55	6.7	16.56	6.8	16.56	6.9
RFA_060	16.57	6.0	16.61	7.2	16.63	7.9	16.64	8.4	16.64	8.8	16.65	8.9
RFA_061	16.67	6.0	16.73	7.2	16.76	7.9	16.78	8.4	16.79	8.8	16.80	8.9
RFA_062	16.79	6.0	16.87	7.2	16.91	7.9	16.93	8.5	16.95	9.0	16.96	9.3
RFA_063	16.91	5.9	16.99	7.2	17.04	7.9	17.07	8.5	17.10	9.2	17.11	9.6
RFA_064	17.03	5.9	17.12	7.1	17.17	7.9	17.21	8.5	17.24	8.9	17.27	9.0
RFA_065	17.20	5.9	17.29	7.1	17.35	8.0	17.38	9.0	17.42	9.2	17.43	9.4
RFA_066	17.34	5.9	17.44	7.1	17.50	7.4	17.56	7.5	17.59	7.5	17.60	7.5
RFA_067	17.48	5.9	17.57	8.0	17.60	8.9	17.62	9.0	17.64	9.1	17.65	9.0
RFA_068	17.58	5.9	17.69	8.9	17.73	10.6	17.74	11.0	17.75	11.3	17.75	11.4
RFA_069	17.73	5.9	17.91	8.9	18.00	10.7	18.02	11.3	18.03	11.7	18.03	11.9
RFA_070	17.90	5.9	18.09	8.9	18.18	13.0	18.20	14.8	18.21	15.8	18.22	16.3
RFA_071	18.08	5.9	18.28	8.9	18.45	13.0	18.52	15.3	18.54	17.1	18.55	18.1
Junction with RFF_001												
RFA_072	18.08	5.9	18.28	8.9	18.45	12.7	18.52	14.9	18.54	16.5	18.55	17.4
RFA_073	18.20	5.9	18.43	8.9	18.64	12.7	18.74	14.9	18.80	16.5	18.83	17.4
RFA_074	18.29	5.9	18.52	8.9	18.74	12.7	18.84	15.0	18.89	17.4	18.91	18.8
Boards Mill Bridge												
RFA_075	18.35	5.9	18.63	8.9	18.92	12.7	19.07	15.0	19.18	17.4	19.27	18.8
RFA_076	18.40	5.2	18.70	7.0	19.00	9.5	19.17	10.9	19.31	12.3	19.39	13.0
Beards Mill Side Wall												
RFA_077	19.85	5.2	20.02	7.0	20.22	9.5	20.33	10.9	20.44	12.3	20.49	13.0
Junction with RFF_003												
RFA_078	19.85	5.2	20.02	7.1	20.22	9.7	20.33	11.3	20.44	12.9	20.49	13.7

RFA_078A	19.91	5.2	20.08	7.1	20.29	9.5	20.40	11.0	20.51	12.9	20.56	14.2
RFA_079	20.12	5.6	20.25	5.8	20.44	6.0	20.55	6.0	20.66	6.1	20.72	6.1
RFA_080	20.28	5.6	20.34	6.0	20.47	6.3	20.58	6.4	20.69	6.5	20.75	6.6
RFA_081	20.42	5.6	20.47	6.0	20.55	6.3	20.62	6.4	20.71	6.5	20.77	6.5
RFA_082	20.62	5.6	20.65	6.0	20.69	6.5	20.72	6.9	20.77	7.1	20.81	7.3
RFA_083	20.79	5.6	20.83	6.0	20.87	6.5	20.89	6.8	20.92	7.1	20.95	7.3
RFA_084	20.94	5.5	20.98	6.0	21.03	6.5	21.05	6.8	21.08	7.1	21.09	7.3
RFA_085	21.06	5.5	21.10	6.0	21.14	6.5	21.17	6.8	21.19	7.0	21.21	7.2
RFA_086	21.34	5.5	21.37	5.9	21.42	6.4	21.44	6.7	21.46	7.0	21.48	7.2
RFA_087	21.66	5.5	21.70	5.9	21.74	6.4	21.76	6.7	21.78	7.0	21.79	7.2

Stanley Downton Bridge

RFA_088	21.70	5.5	21.73	5.9	21.77	6.4	21.80	6.7	21.82	7.0	21.83	7.2
RFA_089	21.96	5.5	22.00	5.9	22.04	6.4	22.07	6.7	22.09	7.0	22.11	7.1

Stanley Downton Mill Race

RFA_090	22.40	5.5	22.44	5.9	22.49	6.4	22.52	6.7	22.55	7.0	22.57	7.1
RFA_091	22.58	5.5	22.64	5.9	22.70	6.4	22.73	6.7	22.77	6.9	22.79	7.1
RFA_092	22.68	5.5	22.73	5.9	22.79	6.4	22.82	6.7	22.85	6.9	22.87	7.1
RFA_093	22.77	5.5	22.82	5.9	22.87	6.4	22.90	6.6	22.93	6.9	22.95	7.0
RFA_094	22.86	5.5	22.90	5.9	22.96	6.4	22.99	6.6	23.02	6.9	23.03	7.0
RFA_095	22.96	5.5	23.00	5.9	23.06	6.3	23.09	6.6	23.12	6.8	23.13	7.0
RFA_096	23.04	5.5	23.09	5.9	23.14	6.3	23.17	6.6	23.20	6.8	23.21	6.9
RFA_097	23.15	5.5	23.19	5.9	23.24	6.3	23.27	6.5	23.29	6.8	23.31	6.9
RFA_098	23.26	5.5	23.30	5.8	23.35	6.3	23.37	6.5	23.39	6.7	23.41	6.9
RFA_099	23.33	5.4	23.36	5.8	23.41	6.3	23.43	6.5	23.45	6.7	23.47	6.8

Junction with RFM_001

RFA_100	23.33	5.4	23.36	5.8	23.41	6.3	23.43	6.5	23.45	6.7	23.47	6.8
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RFA_101	23.51	5.4	23.55	5.8	23.59	6.3	23.61	6.5	23.63	6.7	23.64	6.8
RFA_102	23.80	5.4	23.83	5.8	23.87	6.2	23.89	6.5	23.91	6.7	23.91	6.8
RFA_103	24.11	5.4	24.14	5.8	24.18	6.2	24.19	6.4	24.21	6.6	24.22	6.7
Stanley Mills Weir												
RFA_104	28.08	5.4	28.11	5.8	28.13	6.2	28.15	6.4	28.16	6.6	28.17	6.7
RFA_105	28.09	5.4	28.12	5.8	28.14	6.2	28.16	6.4	28.17	6.6	28.18	6.7
Stanley Mills Bridge												
RFA_106	28.09	5.4	28.12	5.8	28.15	6.2	28.16	6.4	28.18	6.6	28.18	6.7
RFA_107	28.15	5.4	28.18	5.8	28.21	6.2	28.22	6.4	28.24	6.6	28.25	6.7
RFA_108	28.17	5.4	28.20	5.8	28.23	6.2	28.25	6.4	28.27	6.6	28.27	6.7
RFA_109	28.18	5.4	28.22	5.8	28.25	6.2	28.27	6.4	28.29	6.5	28.29	6.7
RFA_110	28.20	5.4	28.23	5.8	28.27	6.2	28.28	6.4	28.30	6.6	28.31	6.6
RFA_111	28.21	5.4	28.25	5.7	28.29	6.1	28.31	6.4	28.32	6.6	28.33	6.6
RFA_112	28.24	5.4	28.27	5.7	28.32	5.9	28.34	5.9	28.35	5.9	28.36	5.9
RFA_113	28.25	4.4	28.29	4.5	28.33	4.7	28.35	4.8	28.37	4.9	28.38	4.8
RFA_114	28.28	5.6	28.32	5.8	28.36	6.4	28.38	7.0	28.40	7.5	28.41	7.8
Redhill Bridge												
RFA_115	28.38	5.6	28.42	5.8	28.48	6.4	28.52	7.0	28.56	7.5	28.58	7.8
RFA_116	28.42	5.6	28.47	5.8	28.53	6.4	28.57	7.0	28.61	7.5	28.64	7.8
RFA_117	28.46	6.0	28.51	7.5	28.59	10.8	28.65	13.8	28.70	16.7	28.73	18.8
RFA_118	28.54	6.0	28.62	7.5	28.77	10.8	28.80	13.8	28.92	15.9	29.11	17.6
Refuse Tip Weir 1												
RFA_119	28.91	6.0	29.05	7.5	29.23	10.8	29.37	13.8	29.45	15.9	29.52	17.6
Junction with RFD_081												
RFA_120	28.91	15.9	29.05	20.0	29.23	26.9	29.37	32.9	29.45	37.0	29.52	40.2
RFA_121	29.16	15.9	29.32	20.0	29.54	26.9	29.70	32.9	29.80	37.0	29.87	40.2

Junction with RFH_001							
RFA_122	29.16	8.4	29.32	10.6	29.54	14.8	29.70
RFA_123	29.20	8.4	29.36	10.6	29.59	14.0	29.75
RFA_124	29.24	8.4	29.40	10.6	29.63	14.0	29.80
RFA_125	29.31	8.4	29.47	9.6	29.72	10.7	29.90
Ebley Corn Mill Bypass							
RFA_126	29.86	8.4	29.97	9.6	30.14	10.7	30.21
Junction with RFH_004							
RFA_127	29.86	15.9	29.97	19.0	30.14	23.5	30.21
RFA_128	29.98	16.4	30.07	20.0	30.18	25.7	30.24
Ebley Corn Mill Bridge							
RFA_129	30.07	16.4	30.19	20.0	30.34	25.7	30.40
RFA_130	30.20	16.4	30.33	20.0	30.53	23.4	30.59
RFA_131	30.31	16.4	30.43	20.0	30.61	23.6	30.79
RFA_132	30.48	16.4	30.60	20.4	30.72	26.9	30.77
RFA_133	30.61	16.4	30.76	20.4	30.93	26.9	31.05
RFA_134	30.71	16.4	30.88	20.4	31.08	26.9	31.23
RFA_135	30.66	16.4	30.80	20.4	31.01	24.3	31.18
Ebley Mill Bridge							
RFA_136	30.67	16.4	30.82	20.4	31.03	24.3	31.20
RFA_137	30.82	16.4	30.99	20.4	31.20	24.3	31.36
Ebley Mill Wall							
RFA_138	31.81	16.4	31.93	20.4	32.04	24.3	32.11
RFA_139	31.86	16.4	31.98	20.4	32.09	24.3	32.16
RFA_140	32.02	16.4	32.17	20.4	32.30	24.3	32.37
Junction with SCA_001							
RFA_136	30.67	16.4	30.82	20.4	31.03	24.3	31.20
RFA_137	30.82	16.4	30.99	20.4	31.20	24.3	31.36
Ebley Mill Wall							
RFA_138	31.81	16.4	31.93	20.4	32.04	24.3	32.11
RFA_139	31.86	16.4	31.98	20.4	32.09	24.3	32.16
RFA_140	32.02	16.4	32.17	20.4	32.30	24.3	32.37

RFA_141	32.02	11.7	32.17	14.7	32.30	16.6	32.37	17.9	32.40	19.5	32.43	20.3
RFA_142	32.13	11.7	32.28	14.7	32.38	18.7	32.43	21.8	32.46	23.8	32.48	24.4
RFA_143	32.29	11.6	32.45	14.6	32.59	18.7	32.68	22.0	32.73	24.5	32.74	25.7
RFA_144	32.29	11.6	32.43	14.6	32.57	18.7	32.65	22.0	32.69	24.5	32.71	25.7
Junction with RFX_001												
RFA_145	32.29	5.3	32.43	6.3	32.57	7.9	32.65	10.0	32.69	10.9	32.71	11.7

Dudbridge Road Culvert

RFA_146	32.38	5.3	32.53	6.3	32.68	7.9	32.80	9.9	32.85	10.8	32.89	11.6
RFA_147	32.50	5.3	32.62	6.3	32.76	7.9	32.88	9.9	32.93	10.8	32.97	11.6

Redlens Mill Sluices

RFA_148	34.40	5.3	34.37	6.3	34.49	7.9	34.65	9.9	34.71	10.8	34.74	11.6
RFA_149	34.40	5.3	34.37	6.3	34.49	7.9	34.65	9.9	34.71	10.8	34.74	11.6
RFA_150	34.40	5.2	34.37	6.3	34.51	7.9	34.66	9.9	34.72	10.8	34.75	11.6
RFA_151	34.43	5.2	34.53	6.3	34.68	7.9	34.84	9.9	34.91	10.8	34.95	11.6
RFA_152	34.61	5.2	34.72	6.2	34.87	7.8	35.04	9.8	35.10	10.7	35.15	11.6
RFA_153	34.65	5.2	34.76	6.2	34.91	7.8	35.08	9.8	35.15	10.7	35.20	11.5

Junction with RFN_001

RFA_154	34.65	3.8	34.76	4.6	34.91	5.9	35.08	7.7	35.15	8.6	35.20	9.4
RFA_155	34.75	3.7	34.86	4.5	35.01	5.9	35.18	7.7	35.25	8.6	35.30	9.3
RFA_156	34.87	3.7	34.97	4.5	35.12	5.8	35.28	7.7	35.35	8.5	35.40	9.3

Fromehall Mill Bypass Sluices

RFA_157	36.09	3.7	36.17	4.5	36.28	5.8	36.39	7.6	36.44	8.5	36.48	9.3
RFA_158	36.12	3.7	36.20	4.4	36.32	5.8	36.46	5.9	36.53	5.9	36.58	6.0
RFA_159	36.14	3.6	36.23	4.4	36.35	5.8	36.48	5.9	36.55	5.9	36.60	5.9

Fromehall Mill Bridge

RFA_160	36.26	3.6	36.41	4.4	36.66	5.8	36.78	5.9	36.83	5.9	36.86	5.9
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RFA_161	36.27	3.8	36.41	4.6	36.66	5.8	36.78	6.5	36.83	6.7	36.86	7.0
Junction with RFN_006												
RFA_162	36.27	5.2	36.41	6.3	36.66	7.8	36.78	8.6	36.83	8.8	36.86	9.1
RFA_163	36.32	5.2	36.46	6.3	36.71	7.8	36.82	9.7	36.86	10.6	36.88	11.4
RFA_163A	36.40	5.2	36.52	6.3	36.75	7.8	36.87	9.7	36.91	10.6	36.94	11.4
Lodgemore Mills Bridge												
RFA_164	36.44	5.2	36.56	6.2	36.78	7.8	36.91	9.7	36.95	10.6	36.99	11.4
RFA_165	36.45	5.2	36.57	6.2	36.79	7.8	36.92	9.7	36.96	10.6	37.00	11.4
Lodgemore Mills Sluices												
RFA_166	38.00	5.2	38.08	6.2	38.17	7.8	38.21	9.7	38.25	10.6	38.18	11.4
RFA_167	38.00	5.2	38.07	6.2	38.17	7.8	38.21	9.6	38.24	10.6	38.17	11.4
Lodgemore Mills Culvert												
RFA_168	38.15	5.2	38.28	6.2	38.45	7.8	38.79	9.6	38.90	10.6	39.00	11.3
RFA_169	38.17	5.1	38.29	6.2	38.46	7.7	38.79	9.6	38.91	10.6	39.00	11.3
RFA_170	38.25	5.1	38.37	6.2	38.54	7.7	38.85	9.6	38.96	10.7	39.05	11.3
Bath Road Bridge												
RFA_171	38.27	5.1	38.39	6.2	38.56	7.7	38.86	9.6	38.97	10.7	39.06	11.3
RFA_172	38.29	5.1	38.41	6.2	38.57	7.7	38.86	9.6	38.97	10.7	39.06	11.3
RFA_173	38.50	5.1	38.62	6.2	38.77	7.7	39.01	9.6	39.11	10.7	39.19	11.3
RFA_174	38.73	5.1	38.83	6.2	38.97	7.7	39.16	9.6	39.25	10.7	39.31	11.3
RFA_175	39.18	5.1	39.28	6.2	39.36	7.7	39.49	9.6	39.56	10.7	39.60	11.3
RFB_001	7.98	7.5	8.02	8.5	8.13	8.8	8.17	8.9	8.18	9.1	8.31	10.2
RFB_002	8.06	7.5	8.10	8.5	8.21	8.8	8.24	8.8	8.25	9.1	8.39	10.1
RFB_003	8.10	7.5	8.15	8.5	8.26	8.7	8.29	8.8	8.30	9.1	8.43	10.0
Gloucester & Sharpness Canal - Right Syphon												
RFB_004	8.20	7.5	8.26	8.5	8.39	8.7	8.42	8.8	8.43	9.1	8.63	10.0

Whitminster Weir - Right												
RFB_005	8.28	7.5	8.36	8.5	8.47	8.7	8.49	8.8	8.50	9.0	8.71	9.1
RFB_006	8.33	7.5	8.43	8.5	8.52	8.8	8.53	8.3	8.54	9.6	8.73	12.5
RFB_007	8.36	7.5	8.46	8.5	8.54	8.8	8.56	9.3	8.57	9.6	8.76	12.5
Caravan Park Weir												
RFC_001A	13.82	2.0	14.21	2.8	14.34	2.9	14.42	3.1	14.50	2.9	14.52	2.7
RFC_002	13.85	1.9	14.22	2.8	14.34	2.9	14.42	3.0	14.50	2.8	14.52	2.7
Spring Hill Bridge												
RFC_003	13.88	1.9	14.64	2.7	14.73	2.8	14.80	3.0	14.85	2.8	14.87	2.7
RFC_004	14.05	1.9	14.65	2.4	14.74	2.6	14.80	2.5	14.85	2.6	14.87	2.5
RFC_005	14.15	1.9	14.66	2.3	14.75	2.6	14.81	2.4	14.86	2.6	14.88	2.5
Churchend School Bridge												
RFC_006	14.51	1.9	15.37	2.3	15.41	2.6	15.44	2.3	15.47	2.5	15.47	2.4
RFC_007	14.60	1.9	15.38	1.9	15.42	1.9	15.44	1.9	15.47	1.9	15.48	1.9
Millend Lane Bridge												
RFD_004	14.08	5.4	14.43	5.7	14.66	5.9	14.82	6.0	14.99	6.1	15.14	6.2
RFD_005	14.13	5.4	14.45	5.7	14.67	5.9	14.83	6.0	15.00	6.1	15.14	6.2

Junction with RFE_001

RFD_006	14.13	3.5	14.45	3.5	14.67	3.6	14.83	3.6	15.00	3.6	15.14	3.6
RFD_007	14.13	3.5	14.44	3.5	14.66	3.6	14.81	3.6	14.99	3.6	15.13	3.6
RFD_008	15.69	3.5	15.70	3.5	15.71	3.6	15.71	3.6	15.71	3.6	15.72	3.6

Junction with RFQ_009

RFD_009A	15.69	5.4	15.70	5.4	15.71	5.4	15.71	5.4	15.71	5.4	15.72	5.4
RFD_009	15.77	6.4	15.78	6.5	15.78	6.6	15.78	6.6	15.78	6.6	15.78	6.6
RFD_010	15.89	6.7	15.90	6.8	15.90	6.9	15.90	7.0	15.90	7.0	15.90	7.0
RFD_011	15.89	6.7	15.99	6.8	16.00	6.9	16.00	6.9	16.00	7.0	16.00	7.0

Junction with RFE_005

RFD_012	15.99	7.3	15.99	7.4	16.00	7.5	16.00	7.6	16.00	7.6	16.00	7.6
RFD_013	16.09	8.3	16.10	8.7	16.10	8.9	16.10	9.1	16.10	9.1	16.11	9.2
RFD_014	16.20	8.3	16.22	8.7	16.23	8.9	16.23	9.1	16.23	9.1	16.23	9.2
RFD_015	16.37	8.3	16.39	8.7	16.40	8.9	16.41	9.0	16.41	9.1	16.41	9.1
RFD_016	16.54	8.3	16.56	8.7	16.57	8.9	16.58	9.0	16.58	9.1	16.59	9.1
RFD_017	16.71	8.3	16.74	8.7	16.75	8.9	16.76	9.0	16.76	9.1	16.76	9.1

Junction with RFQ_001

RFD_018	16.71	6.3	16.74	6.6	16.75	6.8	16.76	6.8	16.76	6.9	16.76	6.9
RFD_019	16.94	6.3	16.97	6.6	16.98	6.8	16.99	6.8	16.99	6.9	16.99	6.9

Bonds Mill Culvert

RFD_020	19.12	6.3	19.17	6.6	19.20	6.8	19.21	6.8	19.22	6.8	19.22	6.9
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Junction with RFQ_006

RFD_021	19.12	8.3	19.17	8.7	19.20	8.9	19.21	9.0	19.22	9.1	19.22	9.1
RFD_022	19.20	8.3	19.25	8.7	19.27	8.9	19.28	9.0	19.28	9.1	19.30	9.1
RFD_023	19.27	8.3	19.31	8.7	19.34	8.9	19.35	9.0	19.36	9.2	19.36	9.2
RFD_024	19.35	8.3	19.39	8.9	19.41	9.5	19.42	9.8	19.43	10.1	19.43	10.3
RFD_025	19.42	8.6	19.46	10.1	19.49	11.2	19.50	11.8	19.50	12.3	19.51	12.6

QWR Bridge							
RFD_026	19.70	8.6	19.78	10.1	19.86	11.2	19.89
Ocean Pool Bridge							
RFD_027	20.01	8.6	20.23	10.1	20.44	11.2	20.55
RFD_028	20.07	8.3	20.27	9.7	20.47	11.6	20.58
RFD_029	20.09	10.0	20.28	13.8	20.47	16.6	20.59
RFD_030	20.16	9.5	20.37	12.4	20.54	14.2	20.62
RFD_031	20.21	9.5	20.41	12.4	20.57	15.5	20.64
Junction with RFJ_001							
RFD_032	20.21	6.2	20.41	8.9	20.57	11.9	20.64
RFD_033	20.27	6.2	20.48	9.0	20.65	11.9	20.73
Junction with RFK_001							
RFD_034	20.27	3.5	20.48	3.8	20.65	4.0	20.73
Bridgeend Mill Side Sluices							
RFD_035	21.46	3.5	21.49	3.8	21.52	4.0	21.55
Junction with RFJ_003							
RFD_036	21.46	6.8	21.49	7.2	21.52	7.6	21.55
RFD_037	21.48	6.8	21.51	7.2	21.54	7.6	21.57
Bridgeend Mill Bridge							
RFD_038	21.90	6.8	21.98	7.2	22.06	7.6	22.14
RFD_039	21.91	6.1	22.00	6.5	22.08	6.9	22.16
Junction with RFK_004							
RFD_040	21.91	8.7	22.00	9.5	22.08	10.1	22.16
RFD_041	21.92	9.6	22.01	10.5	22.09	11.2	22.17
RFD_042	21.94	10.2	22.03	11.7	22.10	12.2	22.18
RFD_043	21.99	10.2	22.08	11.4	22.16	11.4	22.23

Bridgend Kennels Bridge							
RFD_044	22.08	10.2	22.28	11.4	22.37	11.5	22.44
RFD_045	22.10	10.3	22.30	11.1	22.39	11.4	22.45
RFD_046	22.12	10.3	22.31	11.1	22.40	11.4	22.47
Junction with RFL_001							
RFD_047	22.12	6.3	22.31	6.4	22.40	6.4	22.47
Bridgend Kennels Stulices							
RFD_048	22.79	6.3	22.80	6.4	22.82	6.4	22.85
RFD_049	22.88	6.6	22.89	6.8	22.90	6.9	22.92
RFD_050	22.95	6.6	22.96	6.8	22.97	6.9	22.98
Downton Road Footbridge							
RFD_051	22.97	6.6	22.98	6.8	22.99	6.9	23.00
RFD_052	23.08	6.6	23.09	6.8	23.10	6.9	23.11
Upper Mill's Footbridge							
RFD_053	23.18	6.6	23.21	6.8	23.23	6.9	23.25
RFD_054	24.04	6.6	24.05	6.8	24.06	6.9	24.07
Upper Mill's Stulices							
RFD_055	24.99	6.6	25.07	6.8	25.10	6.9	25.10
RFD_056	25.04	6.6	25.11	6.9	25.14	7.1	25.14
RFD_057	25.07	6.6	25.13	8.3	25.16	9.3	25.16
RFD_058	25.13	6.8	25.20	8.3	25.24	9.3	25.24
RFD_059	25.15	6.8	25.23	8.3	25.27	9.3	25.28
RFD_060	25.17	6.8	25.26	8.3	25.30	9.3	25.31
Upper Mill's Bridge							
RFD_061	25.20	6.8	25.30	8.3	25.35	9.3	25.36
RFD_062	25.24	6.8	25.33	8.3	25.39	9.3	25.40

RFD_063	25.27	6.8	25.37	8.3	25.43	9.2	25.44	9.4	25.44	9.5	25.45	9.6
RFD_064	25.32	6.8	25.43	8.3	25.49	9.2	25.49	9.4	25.50	9.5	25.51	9.6
RFD_065	25.37	6.7	25.48	8.8	25.53	10.9	25.54	11.2	25.54	11.5	25.55	11.6
RFD_066	25.40	6.7	25.52	9.4	25.57	12.5	25.58	13.0	25.58	13.5	25.59	13.7
Junction with RFL_016												
RFD_067	25.40	10.5	25.52	14.0	25.57	16.6	25.58	17.0	25.58	17.4	25.59	17.5
Ryeford Saw Mills Culvert												
RFD_068	27.74	10.5	27.74	14.0	27.57	16.6	27.73	17.0	27.65	17.4	27.67	17.5
RFD_069	27.74	10.5	27.74	14.0	27.63	16.6	27.73	16.9	27.72	17.0	27.73	17.1
RFD_070	27.75	10.4	27.74	14.0	27.76	17.6	27.81	18.7	27.84	19.1	27.84	19.3
RFD_071	27.75	10.4	27.75	14.0	27.82	17.6	27.86	18.6	27.88	19.2	27.89	19.4
RFD_072	27.76	10.4	27.75	13.9	27.93	18.1	27.96	20.1	27.97	21.0	27.98	21.6
RFD_073	27.77	10.4	27.77	13.9	28.01	18.1	28.04	20.0	28.06	21.0	28.08	21.6
RFD_074	27.77	10.4	27.83	13.9	28.07	18.1	28.12	20.0	28.14	21.0	28.16	21.6
RFD_075	27.78	10.4	27.88	13.9	28.12	18.1	28.17	20.0	28.20	20.9	28.22	21.5
RFD_076	27.80	9.9	28.03	12.5	28.29	15.9	28.36	17.8	28.39	18.6	28.41	19.2
RFD_077	27.86	9.9	28.12	12.5	28.37	16.2	28.43	18.1	28.46	20.5	28.48	21.3
RFD_078	27.95	9.9	28.20	12.5	28.45	16.2	28.53	19.1	28.57	20.4	28.59	21.4
Refuse Tip Wall 2												
RFD_079	28.59	9.9	28.73	12.5	28.92	16.2	29.06	19.1	29.12	20.4	29.17	21.4
RFD_080	28.61	9.9	28.75	12.5	28.93	16.2	29.06	19.1	29.11	21.1	29.15	22.7
Refuse Tip Wall 3												
RFD_081	28.91	9.9	28.95	12.5	29.23	16.2	29.37	18.1	29.45	21.1	29.52	22.7
RFE_001	14.13	1.9	14.45	2.2	14.67	2.3	14.83	2.4	15.00	2.5	15.14	2.6
RFE_002	14.70	0.9	14.73	1.0	14.81	1.1	14.93	1.1	15.07	1.1	15.19	1.1
RFE_003	14.72	0.6	14.75	0.6	14.83	0.6	14.94	0.7	15.08	0.7	15.20	0.7

RFE_004	14.73	0.6	14.76	0.6	14.84	0.6	14.95	0.6	15.09	0.6	15.21	0.6
Market Garden Wall												
RFF_005	15.99	0.6	15.99	0.6	16.00	0.6	16.00	0.6	16.00	0.6	16.00	0.6
RFF_001	18.08	0.0	18.28	0.1	18.45	0.3	18.52	0.4	18.54	0.6	18.55	0.7
RFF_002	18.08	0.0	18.28	0.1	18.45	0.3	18.52	0.4	18.54	0.6	18.56	0.7
Beards Mill Culvert												
RFQ_003	19.85	0.0	20.02	0.1	20.22	0.3	20.33	0.4	20.44	0.6	20.49	0.7
RFQ_001	16.71	2.0	16.74	2.1	16.75	2.2	16.76	2.2	16.76	2.2	16.76	2.2
RFQ_002	16.77	2.0	16.80	2.1	16.81	2.2	16.82	2.2	16.82	2.2	16.82	2.2
RFQ_003	16.88	2.0	16.90	2.1	16.91	2.2	16.91	2.2	16.92	2.2	16.92	2.2
RFQ_004	17.07	2.0	17.08	2.1	17.09	2.2	17.10	2.2	17.10	2.2	17.10	2.2
RFQ_005	17.20	2.0	17.22	2.1	17.23	2.2	17.23	2.2	17.23	2.2	17.23	2.2
Bonds Mill Side Sluices												
RFQ_006	19.12	2.0	19.17	2.1	19.20	2.2	19.21	2.2	19.22	2.2	19.22	2.2
RFH_001	28.16	7.5	29.32	9.4	29.54	12.1	29.70	13.9	29.80	15.9	29.87	16.8
RFH_002	29.24	7.5	29.40	9.4	29.61	13.0	29.77	14.3	29.86	16.4	29.93	16.9
RFH_003	29.34	7.5	29.50	9.4	29.72	13.0	29.85	14.4	29.95	16.6	30.01	16.9
Ebley Corn Mill Culverts												
RFH_004	29.86	7.5	29.97	9.4	30.14	13.0	30.21	14.4	30.32	16.6	30.36	16.9
RFJ_001	20.21	3.3	20.41	3.5	20.57	3.6	20.64	3.8	20.74	4.0	20.79	4.2
RFJ_002	20.25	3.3	20.44	3.5	20.60	3.6	20.66	3.8	20.76	4.0	20.81	4.2
Bridgend Mill Culverts												
RFJ_003	21.46	3.3	21.49	3.5	21.52	3.6	21.55	3.8	21.58	4.0	21.60	4.2
RFK_001	20.27	2.7	20.48	5.2	20.65	7.8	20.73	9.3	20.81	10.6	20.85	11.2
RFK_002	20.52	2.7	20.73	3.0	20.95	3.2	21.04	3.5	21.12	3.9	21.16	4.1
RFK_003	20.81	2.7	20.85	3.0	21.00	3.2	21.08	3.5	21.15	3.9	21.18	4.1

Bridgeland Mill Bypass Culvert

RFK_004	21.91	2.7	22.00	3.0	22.08	3.2	22.16	3.5	22.24	3.9	22.29	4.1
RFL_001	22.12	4.0	22.31	4.7	22.40	4.9	22.47	5.0	22.53	5.0	22.56	5.0
RFL_002	22.26	3.7	22.40	4.4	22.48	5.2	22.55	6.1	22.61	6.8	22.65	7.4
RFL_003	22.47	2.7	22.58	3.2	22.68	4.9	22.76	6.0	22.83	7.1	22.87	7.7
RFL_004	22.71	2.7	22.78	2.9	22.94	3.1	23.02	3.2	23.09	3.5	23.13	3.6
RFL_005	23.18	3.2	23.19	3.5	23.23	4.4	23.28	5.1	23.34	6.0	23.36	6.9
RFL_006	23.43	3.5	23.46	3.8	23.49	3.9	23.52	3.9	23.57	3.9	23.59	3.9
RFL_007	23.75	3.7	23.77	4.7	23.85	10.7	23.87	11.5	23.89	12.1	23.91	12.3
RFL_008	23.99	2.6	24.11	2.6	24.16	2.6	24.20	2.6	24.22	2.6	24.23	2.6
RFL_009	24.29	3.4	24.31	3.5	24.34	4.2	24.36	4.5	24.38	4.7	24.39	4.8
RFL_010	24.40	3.4	24.41	3.6	24.47	4.2	24.50	4.4	24.52	4.5	24.53	4.6

Banty Ditch Culvert

RFL_011	25.11	3.4	25.16	3.6	25.33	4.5	25.35	4.6	25.37	4.7	25.38	4.7
RFL_012	25.11	3.7	25.16	4.3	25.34	4.6	25.36	4.6	25.38	4.6	25.39	4.6
RFL_013	25.12	3.7	25.17	4.6	25.35	4.8	25.36	4.8	25.38	4.8	25.39	4.8
RFL_014	25.17	3.7	25.23	4.6	25.37	4.6	25.38	4.8	25.40	4.8	25.41	4.8

Banty Ditch Wall

RFL_015	25.40	3.7	25.51	4.6	25.58	4.8	25.57	4.8	25.58	4.8	25.58	4.8
RFL_016	25.40	3.7	25.52	4.6	25.57	4.8	25.58	4.8	25.58	4.8	25.59	4.8
RFM_001	23.33	0.1	23.36	0.1	23.41	0.1	23.43	0.1	23.45	0.1	23.47	0.1
RFM_002	23.33	0.0	23.36	0.0	23.41	0.0	23.43	0.0	23.45	0.0	23.47	0.0
RFM_003	23.33	0.0	23.36	0.0	23.41	0.0	23.43	0.0	23.45	0.0	23.47	0.0
RFN_001	34.65	1.4	34.76	1.7	34.91	2.0	35.08	2.1	35.15	2.2	35.20	2.2
RFN_002	34.69	1.4	34.79	1.7	34.93	2.0	35.09	2.1	35.16	2.1	35.21	2.2
RFN_003	34.76	1.4	34.85	1.7	34.97	2.0	35.12	2.1	35.18	2.1	35.23	2.2

	RFN_004	34.80	1.4	34.88	1.7	35.00	2.0	35.13	2.1	35.19	2.1	35.24	2.2
Framehall Mill Sluice													
RFN_005	36.27	1.4	36.41	1.7	36.66	2.0	36.78	2.1	36.83	2.1	36.86	2.2	
RFN_006	36.27	1.4	36.41	1.7	36.66	2.0	36.78	2.1	36.83	2.1	36.86	2.2	
RFX_001	32.29	6.7	32.43	8.5	32.57	10.9	32.65	13.0	32.69	14.3	32.71	15.2	
RFX_002	32.29	6.7	32.44	8.5	32.58	10.9	32.67	13.0	32.71	14.3	32.73	15.2	
RFX_003	32.31	6.7	32.46	8.5	32.61	10.9	32.70	13.0	32.75	14.3	32.77	15.2	
Junction with NSA_001													
RFX_004	32.31	0.0	32.46	0.0	32.61	0.1	32.70	0.1	32.75	0.2	32.77	0.3	
RFX_005	32.31	0.0	32.46	0.0	32.61	0.0	32.70	0.1	32.75	0.1	32.77	0.2	
RFX_006	32.31	0.0	32.46	0.0	32.61	0.0	32.70	0.0	32.75	0.1	32.77	0.1	
RFX_007	32.31	0.0	32.46	0.0	32.61	0.0	32.70	0.0	32.75	0.0	32.77	0.0	
NSA_001	32.31	6.7	32.46	8.4	32.61	10.9	32.70	13.0	32.75	14.3	32.77	15.2	
NSA_002	34.20	6.7	34.33	8.4	34.49	10.9	34.63	13.0	34.71	14.3	34.77	15.2	
SCA_001	32.02	4.7	32.17	6.2	32.30	8.8	32.37	11.3	32.40	13.9	32.43	15.8	
SCA_002	32.02	4.7	32.16	6.2	32.28	8.8	32.34	11.3	32.37	13.9	32.38	15.8	
SCA_003	32.07	4.7	32.22	6.2	32.37	8.8	32.47	11.3	32.55	13.9	32.61	15.7	
SCA_004	32.20	4.7	32.37	6.2	32.59	8.8	32.76	11.3	32.91	13.8	33.01	15.7	
Dudbridge Lock Weir													
SCA_005	34.35	4.7	34.47	6.2	34.67	8.8	34.84	11.3	35.00	13.9	35.11	15.7	
SCA_006	36.09	3.9	36.16	5.2	36.28	7.6	36.39	9.9	36.49	12.3	36.56	13.9	
Ruscombe Brook Weir													
SCA_007	36.94	3.9	37.05	5.2	37.24	7.6	37.40	9.9	37.56	12.3	37.66	13.9	
SCA_008	37.10	3.9	37.25	5.2	37.47	7.6	37.66	9.9	37.83	12.3	37.93	13.9	
SCA_009	37.20	3.9	37.36	5.2	37.60	7.6	37.80	9.9	37.97	12.3	38.07	13.9	
SCA_010	37.23	3.9	37.40	5.2	37.66	7.6	37.87	9.9	38.05	12.3	38.17	13.9	

SCA_011	37.37	3.9	37.54	5.2	37.80	7.6	38.01	9.9	38.19	12.3	38.31	13.9
SCA_012	37.43	2.2	37.61	2.8	37.91	3.7	38.14	4.6	38.34	5.5	38.47	6.1
Painswick Stream Weir												
SCA_013	37.75	2.2	37.81	2.8	37.99	3.7	38.21	4.6	38.41	5.5	38.53	6.1
SCA_014	37.76	2.2	37.82	2.8	38.01	3.8	38.22	4.7	38.42	5.6	38.54	6.3
Cainscross Road Weir												
SCA_015	39.87	2.2	39.94	2.8	40.05	3.8	40.14	4.7	40.23	5.7	40.29	6.3
SCA_016	40.02	2.2	40.11	2.8	40.23	3.8	40.33	4.7	40.43	5.7	40.49	6.3

Model Cell	5 Year Event		10 Year Event		25 Year Event		50 Year Event		100 Year Event		150 Year Event	
	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)
Cell 1	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00
Cell 2	8.10	0.00	8.10	0.00	8.10	0.00	8.10	0.00	8.10	0.00	8.10	0.00
Cell 3	7.70	0.00	7.70	0.00	7.86	0.16	8.09	0.39	8.51	0.81	8.71	1.01
Cell 4	8.10	0.00	8.10	0.00	8.31	0.21	8.33	0.23	8.51	0.41	8.71	0.61
Cell 5	8.40	0.00	8.40	0.00	8.40	0.00	8.40	0.00	8.40	0.00	8.71	0.32
Cell 6	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00
Cell 7	8.40	0.00	8.40	0.00	8.40	0.00	8.40	0.00	8.40	0.00	8.40	0.00
Cell 8	8.80	0.00	8.80	0.00	8.80	0.00	8.80	0.00	8.80	0.00	8.80	0.00
Cell 9	8.37	0.00	8.37	0.00	8.37	0.00	8.37	0.00	8.37	0.00	8.37	0.00
Cell 10	8.38	0.09	8.38	0.09	8.38	0.09	8.38	0.09	8.38	0.09	8.38	0.09
Cell 11	9.00	0.00	9.00	0.00	9.33	0.33	9.68	0.68	10.39	1.39	10.74	1.74
Cell 12	9.00	0.00	9.00	0.00	9.33	0.33	9.68	0.68	10.39	1.39	10.74	1.74
Cell 13	9.00	0.00	9.00	0.00	9.46	0.46	9.68	0.68	10.39	1.39	10.74	1.74
Cell 14	8.90	0.00	8.90	0.00	9.47	0.57	9.68	0.78	10.39	1.49	10.75	1.85
Cell 15	9.30	0.00	9.30	0.00	9.66	0.36	9.68	0.38	10.39	1.09	10.75	1.45
Cell 16	9.50	0.00	10.23	0.73	10.44	0.94	10.44	0.94	10.47	0.97	10.75	1.25
Cell 17	9.40	0.00	10.23	0.83	10.44	1.04	10.44	1.04	10.47	1.07	10.75	1.35
Cell 18	9.40	0.00	10.23	0.83	10.44	1.04	10.44	1.04	10.47	1.07	10.76	1.36
Cell 19	10.60	0.00	10.60	0.00	10.60	0.00	10.60	0.00	10.60	0.00	10.60	0.00
Cell 20	11.50	0.00	11.50	0.00	12.03	0.53	12.59	1.09	12.65	1.15	12.67	1.17
Cell 21	10.40	0.00	10.88	0.48	10.94	0.54	11.00	0.60	11.32	0.92	11.58	1.18
Cell 21A	11.00	0.00	11.31	0.31	11.32	0.32	11.32	0.32	11.36	0.36	11.59	0.59
Cell 22	11.50	0.00	11.50	0.00	12.03	0.53	12.59	1.09	12.65	1.15	12.67	1.17

Cell 23	10.40	0.00	10.40	0.00	10.40	0.00	10.40	0.00	11.32	0.92	11.58	1.18
Cell 24	11.00	0.00	11.00	0.00	12.03	1.03	12.59	1.59	12.65	1.65	12.67	1.67
Cell 25	10.90	0.00	10.90	0.00	10.90	0.00	10.90	0.00	11.64	0.74	11.67	0.77
Cell 26	11.00	0.00	11.32	0.32	12.03	1.03	12.59	1.59	12.65	1.65	12.67	1.67
Cell 27	11.50	0.00	11.50	0.00	11.50	0.00	11.50	0.00	11.50	0.00	11.50	0.00
Cell 28	11.50	0.00	11.50	0.00	12.03	0.53	12.59	1.09	12.65	1.15	12.67	1.17
Cell 29	12.00	0.00	12.00	0.00	12.00	0.00	12.00	0.00	12.00	0.00	12.00	0.00
Cell 30	11.50	0.00	11.50	0.00	12.87	1.37	13.44	1.94	13.53	2.03	13.55	2.05
Cell 31	12.50	0.00	12.50	0.00	12.50	0.00	12.50	0.00	12.50	0.00	12.50	0.00
Cell 32	12.00	0.00	12.00	0.00	12.87	0.87	13.44	1.44	13.53	1.53	13.56	1.56
Cell 33	13.20	0.00	13.20	0.00	13.20	0.00	13.20	0.00	13.20	0.00	13.20	0.00
Cell 34	12.50	0.00	12.50	0.00	12.93	0.43	13.45	0.94	13.54	1.04	13.56	1.06
Cell 35	13.50	0.00	13.61	0.11	14.26	0.76	14.33	0.89	14.40	0.90	14.42	0.92
Cell 36	12.50	0.00	13.03	0.53	13.12	0.62	13.45	0.95	13.55	1.05	13.58	1.08
Cell 37	13.50	0.00	13.50	0.00	13.61	0.11	14.40	0.90	14.47	0.97	14.50	1.00
Cell 38	13.50	0.00	13.50	0.00	13.50	0.00	13.50	0.00	13.70	0.20	13.82	0.32
Cell 39	14.30	0.00	14.30	0.00	14.30	0.00	14.30	0.00	14.30	0.00	14.30	0.00
Cell 40	14.25	0.00	14.25	0.00	14.25	0.00	14.25	0.00	14.25	0.00	14.30	0.06
Cell 41	14.50	0.00	14.81	0.31	14.90	0.40	14.95	0.45	15.02	0.52	15.10	0.60
Cell 42	14.60	0.70	14.81	0.91	14.91	1.01	14.98	1.08	15.05	1.15	15.12	1.22
Cell 43	14.75	0.35	14.84	0.44	14.94	0.54	15.02	0.61	15.09	0.69	15.16	0.76
Cell 44	15.11	0.61	15.14	0.64	15.17	0.67	15.19	0.69	15.22	0.72	15.26	0.76
Cell 45	15.67	1.27	15.70	1.30	15.73	1.33	15.74	1.34	15.76	1.36	15.77	1.37
Cell 46	15.76	1.38	15.81	1.41	15.84	1.44	15.87	1.47	15.90	1.50	15.92	1.52
Cell 47	16.16	0.41	16.20	0.45	16.23	0.47	16.25	0.50	16.27	0.52	16.28	0.53
Cell 48	16.35	0.35	16.38	0.38	16.41	0.41	16.43	0.43	16.45	0.45	16.47	0.47

Cell 49	16.91	0.17	16.94	0.19	16.97	0.22	16.99	0.24	17.01	0.26	17.02	0.27
Cell 60	17.21	0.21	17.24	0.24	17.27	0.27	17.29	0.29	17.30	0.30	17.31	0.31
Cell 61	17.71	0.26	17.72	0.27	17.75	0.30	17.77	0.32	17.78	0.33	17.79	0.34
Cell 52	18.42	0.52	18.43	0.53	18.44	0.54	18.45	0.55	18.47	0.57	18.48	0.58
Cell 53	17.20	0.00	17.20	0.00	17.34	0.14	17.39	0.19	17.45	0.25	17.47	0.27
Cell 64	17.00	0.00	17.00	0.00	17.56	0.56	17.64	0.64	17.68	0.68	17.69	0.69
Cell 55	17.75	0.00	17.75	0.00	17.79	0.04	17.82	0.07	17.86	0.11	17.88	0.13
Cell 56	18.25	0.00	18.25	0.00	18.30	0.05	18.33	0.08	18.36	0.10	18.37	0.12
Cell 57	19.00	0.00	19.00	0.00	19.76	0.76	19.78	0.78	19.80	0.80	19.80	0.81
Cell 58	20.07	1.07	20.26	1.26	20.45	1.45	20.57	1.57	20.68	1.68	20.74	1.74
Cell 59	20.07	1.07	20.27	1.27	20.46	1.46	20.57	1.57	20.69	1.69	20.75	1.75
Cell 60	20.07	0.67	20.27	0.87	20.46	1.06	20.58	1.18	20.70	1.29	20.76	1.36
Cell 61	20.50	0.00	20.50	0.00	20.55	0.05	20.61	0.11	20.72	0.22	20.78	0.28
Cell 62	20.80	0.00	21.16	0.36	21.23	0.43	21.26	0.46	21.29	0.48	21.30	0.50
Cell 63	21.20	0.00	21.55	0.35	21.59	0.40	21.63	0.43	21.66	0.46	21.67	0.47
Cell 64	20.09	0.29	20.28	0.48	20.47	0.67	20.59	0.79	20.70	0.90	20.77	0.97
Cell 65	20.22	0.22	20.38	0.38	20.55	0.55	20.63	0.63	20.73	0.73	20.79	0.79
Cell 66	21.56	1.16	21.59	1.19	21.61	1.21	21.62	1.23	21.64	1.25	21.66	1.26
Cell 67	21.92	0.42	22.00	0.50	22.08	0.58	22.16	0.66	22.25	0.75	22.30	0.80
Cell 68	21.94	0.39	22.02	0.47	22.10	0.55	22.18	0.63	22.27	0.72	22.32	0.77
Cell 69	21.89	0.09	22.30	0.50	22.39	0.59	22.46	0.66	22.52	0.72	22.55	0.75
Cell 70	21.90	0.00	22.31	0.41	22.41	0.51	22.49	0.59	22.56	0.66	22.59	0.69
Cell 71	22.31	0.31	22.41	0.41	22.47	0.47	22.54	0.54	22.60	0.60	22.64	0.64
Cell 72	23.00	0.00	23.00	0.00	23.02	0.02	23.28	0.28	23.33	0.33	23.34	0.34
Cell 73	23.45	0.25	23.48	0.28	23.55	0.35	23.61	0.41	23.70	0.50	23.75	0.55
Cell 74	22.82	0.82	22.83	0.83	22.84	0.83	22.84	0.84	22.85	0.85	22.86	0.86

Cell 75	22.83	0.33	22.92	0.42	23.00	0.50	23.08	0.58	23.15	0.65	23.18	0.68
Cell 76	23.12	0.12	23.16	0.16	23.21	0.21	23.26	0.26	23.32	0.32	23.35	0.35
Cell 77	23.40	0.30	23.44	0.34	23.47	0.37	23.50	0.40	23.54	0.43	23.56	0.46
Cell 78	24.09	0.19	24.16	0.26	24.20	0.29	24.21	0.31	24.23	0.33	24.24	0.34
Cell 79	23.84	0.04	24.11	0.31	24.20	0.40	24.30	0.50	24.35	0.55	24.38	0.57
Cell 80	24.25	0.00	24.25	0.00	24.50	0.25	24.54	0.29	24.57	0.32	24.59	0.34
Cell 81	24.84	0.44	24.84	0.44	24.90	0.50	24.95	0.55	24.99	0.59	25.01	0.61
Cell 82	23.60	0.00	23.60	0.00	23.60	0.00	23.94	0.34	24.57	0.97	24.59	0.99
Cell 83	24.26	0.26	25.01	1.01	25.34	1.34	25.36	1.36	25.38	1.38	25.39	1.39
Cell 84	24.21	0.11	25.09	0.99	25.36	1.26	25.38	1.28	25.40	1.30	25.41	1.31
Cell 85	27.01	0.11	27.00	0.10	27.44	0.54	27.82	0.92	27.84	0.94	27.85	0.95
Cell 86	27.10	0.00	27.10	0.00	27.10	0.00	27.10	0.00	27.10	0.00	27.10	0.00
Cell 87	26.40	0.00	26.40	0.00	26.40	0.00	26.40	0.00	26.40	0.00	26.40	0.00
Cell 88	24.70	0.00	24.70	0.00	25.27	0.57	25.89	1.29	26.39	1.69	26.68	1.98
Cell 88A	25.72	0.32	25.96	0.56	26.46	1.06	26.54	1.14	26.61	1.21	26.78	1.38
Cell 89	26.46	0.21	26.46	0.21	26.51	0.26	26.57	0.32	26.63	0.38	26.79	0.54
Cell 89A	26.46	0.21	26.46	0.21	26.50	0.25	26.56	0.31	26.63	0.38	26.79	0.54
Cell 90	26.75	0.00	27.24	0.49	27.48	0.73	27.63	0.88	27.67	0.92	27.71	0.96
Cell 90A	26.75	0.00	27.24	0.49	27.48	0.73	27.62	0.88	27.66	0.91	27.70	0.95
Cell 91A	27.50	0.00	27.50	0.00	27.50	0.00	27.50	0.00	27.50	0.00	27.50	0.00
Cell 92	28.27	0.38	28.32	0.41	28.35	0.45	28.39	0.49	28.42	0.52	28.44	0.54
Cell 93	29.25	0.00	29.25	0.00	29.61	0.36	29.77	0.52	29.86	0.61	29.93	0.68
Cell 93A	28.27	0.87	28.31	0.91	28.35	0.95	28.37	0.97	28.39	0.99	28.40	1.00
Cell 94	30.00	0.00	30.33	0.33	30.55	0.55	30.62	0.62	30.68	0.68	30.72	0.72
Cell 94A	28.27	1.01	28.30	1.05	28.34	1.09	28.36	1.11	28.38	1.13	28.39	1.14
Cell 95	29.30	0.00	30.55	1.25	30.63	1.33	30.75	1.45	30.78	1.48	30.79	1.49

Cell 95A	28.00	0.00	28.00	0.00	28.00	0.00	28.28	0.28	28.30	0.30	28.31	0.31
Cell 96	29.97	0.47	30.04	0.54	30.12	0.62	30.23	0.73	30.26	0.76	30.29	0.79
Cell 97	29.97	0.22	30.04	0.29	30.12	0.37	30.24	0.49	30.27	0.52	30.30	0.55
Cell 98	30.90	0.00	30.90	0.00	31.77	0.87	31.89	0.99	31.96	1.06	32.03	1.13
Cell 99	31.50	0.00	31.50	0.00	32.15	0.65	32.19	0.69	32.21	0.71	32.23	0.73
Cell 100	32.00	0.00	32.02	0.02	32.16	0.16	32.21	0.21	32.23	0.23	32.26	0.26
Cell 101	32.00	0.00	32.00	0.00	32.00	0.00	32.27	0.27	32.60	0.60	32.62	0.62
Cell 102	36.40	0.00	36.40	0.00	36.66	0.26	36.77	0.37	36.81	0.41	36.84	0.43
Cell 103	36.24	0.24	36.41	0.41	36.66	0.66	36.77	0.78	36.81	0.81	36.84	0.84
Cell 104	38.35	0.00	38.35	0.00	38.35	0.00	38.35	0.00	38.96	0.61	39.05	0.70

RFA_193	44.56	4.8	44.68	5.8	44.89	7.5	45.10	9.2	45.58	10.4	45.82	11.0
RFA_194	44.56	4.8	44.68	5.8	44.89	7.5	45.11	9.2	45.58	10.4	45.81	11.0

Bowbridge Estate Bridge

RFA_195	44.61	4.8	44.73	5.8	44.94	7.5	45.15	9.2	45.61	10.3	45.84	11.0
RFA_196	44.59	4.8	44.70	5.8	44.91	7.5	45.12	9.2	45.59	10.3	45.83	11.0
RFA_197	44.96	4.8	45.07	5.8	45.24	7.5	45.41	9.1	45.73	10.3	45.93	11.0
RFA_198	45.09	4.8	45.20	5.8	45.37	7.4	45.53	9.1	45.80	10.3	45.98	11.0

Bowbridge Estate Bridge 2

RFA_199	45.08	4.8	45.19	5.8	45.37	7.4	45.54	9.1	45.83	10.3	46.03	11.0
RFA_200	45.14	4.8	45.24	5.8	45.41	7.4	45.58	9.1	45.85	10.3	46.04	11.0
RFA_201	45.27	4.8	45.37	5.7	45.54	7.4	45.69	9.1	45.92	10.3	46.10	11.0
RFA_202	45.35	4.8	45.45	5.7	45.61	7.4	45.77	9.1	45.98	10.3	46.14	10.9
RFA_203	45.38	4.8	45.47	5.7	45.63	7.4	45.78	9.1	45.99	10.3	46.15	10.9

Butterow Footpath Bridge

RFA_204	45.59	4.8	45.73	5.7	46.06	7.4	46.14	9.1	46.25	10.3	46.34	10.9
RFA_205	45.72	4.7	45.83	5.7	46.10	7.4	46.18	9.0	46.28	10.2	46.37	10.9
RFA_206	45.82	4.7	45.90	5.7	46.11	7.4	46.19	9.0	46.28	10.2	46.36	10.9
RFA_207	46.06	4.7	46.13	5.7	46.26	7.4	46.35	9.0	46.42	10.2	46.48	10.9

Thripp Works Well

RFA_208	46.61	4.7	46.74	5.7	46.89	7.4	47.13	9.0	47.20	10.2	47.25	10.9
RFA_209	46.61	4.7	46.74	5.7	46.99	7.4	47.12	9.0	47.20	10.2	47.24	10.9

Junction with RFO_001

RFA_210	46.61	2.4	46.74	2.9	46.99	3.5	47.12	4.2	47.20	4.7	47.24	5.0
RFA_211	46.64	2.4	46.77	2.9	47.00	3.6	47.14	4.1	47.21	4.6	47.26	4.8
RFA_212	46.73	2.4	46.85	2.9	47.06	3.6	47.18	4.4	47.25	5.1	47.30	5.5
RFA_213	46.77	2.4	46.89	2.9	47.09	3.6	47.21	4.4	47.29	5.1	47.33	5.5

RFA_214	46.85	2.4	47.03	2.9	47.19	3.6	47.30	4.4	47.37	5.1	47.41	5.4
Griffin Mill Footbridge 1												
RFA_215	47.66	2.4	47.82	2.9	47.96	3.6	48.15	4.4	48.33	5.1	48.41	5.4
RFA_216	47.69	2.4	47.83	2.9	47.98	3.6	48.17	4.4	48.34	5.1	49.42	5.4
RFA_217	47.72	2.3	47.86	2.8	48.00	3.6	48.19	4.4	48.36	5.1	48.43	5.4
Griffin Mill Bypass												
RFA_218	48.33	2.3	48.38	2.8	48.48	3.6	48.55	4.4	48.60	5.0	48.64	5.4
Junction with RFO_012												
RFA_219	48.33	4.8	48.38	5.8	48.48	7.4	48.55	8.9	48.60	10.0	48.64	10.7
Griffin Mill Access Bridge												
RFA_220	48.35	4.8	48.41	5.8	48.52	7.4	48.59	8.9	48.65	10.0	48.68	10.7
RFA_221	48.48	4.7	48.54	5.7	48.65	7.4	48.73	8.8	48.79	10.0	48.82	10.7
Griffin Mill Footbridge 2												
RFA_222	48.49	4.7	48.56	5.7	48.66	7.4	48.74	8.8	48.80	10.0	48.84	10.7
Junction with RFP_001												
RFA_223	48.49	4.4	48.56	5.4	48.66	5.9	48.74	6.9	48.80	7.8	48.84	8.3
RFA_224	48.61	4.4	48.68	5.4	48.75	5.9	48.84	6.8	48.90	7.8	48.94	8.3
Brookside Bridge 1												
RFA_225	48.76	4.4	48.85	5.3	48.90	5.9	49.02	6.8	49.12	7.8	49.17	8.3
RFA_226	48.82	4.4	48.91	5.3	48.96	5.9	49.08	6.8	49.18	7.8	49.23	8.3
Ham Lock Footbridge												
RFA_227	48.86	4.4	48.98	5.3	49.04	5.9	49.20	6.8	49.38	7.8	49.47	8.3
RFA_228	48.85	4.4	49.04	5.3	49.10	5.9	49.24	6.8	49.41	7.8	49.48	8.3
Swimming Pool Bridge												
RFA_229	49.16	4.4	49.25	5.3	49.31	5.9	49.44	6.8	49.51	7.8	49.98	8.3
RFA_230	49.52	4.4	49.61	5.2	49.65	5.8	49.74	6.8	49.95	7.8	50.09	8.0

Phoenix Mill Bypass Stiles

RFA_231	49.83	4.4	49.99	5.2	50.03	5.8	50.09	6.8	50.19	7.7	50.27	8.0
Junction with RFP_006												
RFA_232	49.93	4.9	49.99	5.8	50.03	7.3	50.09	8.8	50.19	9.9	50.27	10.6
RFA_233	50.12	5.0	50.17	5.8	50.23	7.3	50.30	8.7	50.37	9.9	50.43	10.6

Phoenix Estate Access Bridges

RFA_234	50.22	5.0	50.27	5.8	50.35	7.3	50.43	8.7	50.56	9.9	50.60	10.6
RFA_235	50.38	5.0	50.45	5.8	50.55	7.3	50.65	8.7	50.71	9.9	50.76	10.6

Phoenix Estate Footbridge

RFA_236	50.44	5.0	50.52	5.8	50.64	7.3	50.74	8.7	50.81	9.9	50.86	10.6
RFA_237	50.59	5.0	50.67	5.8	50.79	7.3	50.90	8.7	50.98	9.9	51.03	10.5

Phoenix Estate Stiles

RFA_238	51.86	5.0	51.94	5.8	52.05	7.2	52.13	8.7	52.18	9.8	52.21	10.5
RFA_239	51.89	5.0	51.96	5.8	52.08	7.2	52.16	8.7	52.22	9.8	52.25	10.5

Hawker Slidderley Bridge

RFA_240	51.89	5.0	51.97	5.8	52.08	7.2	52.16	8.7	52.22	9.8	52.25	10.5
RFA_241	51.95	5.0	52.03	5.9	52.15	7.2	52.24	8.6	52.30	9.8	52.33	10.5

Thrupp Caravan Site Bridge

RFA_242	52.02	5.0	52.12	5.9	52.26	7.2	52.51	8.6	52.91	9.8	53.17	10.5
RFA_243	52.12	4.9	52.21	5.9	52.35	7.2	52.58	8.6	52.95	9.8	53.19	10.5
RFA_244	52.23	4.9	52.31	5.9	52.43	7.2	52.63	8.6	52.97	9.8	53.20	10.5
RFA_245	52.44	4.8	52.52	5.8	52.63	7.2	52.77	8.6	53.03	9.8	53.24	10.5
RFA_246	52.77	4.7	52.85	5.8	52.95	7.2	53.04	8.5	53.19	9.7	53.33	10.5
RFA_247	53.02	4.7	53.11	5.7	53.22	7.1	53.32	8.5	53.41	9.7	53.50	10.4
RFA_248	53.19	4.6	53.28	5.7	53.39	7.1	53.49	8.5	53.58	9.7	53.64	10.4
RFA_249	53.32	4.6	53.41	5.7	53.54	6.6	53.66	7.2	53.77	7.7	53.83	7.9

Brimacombe Mill Pond Outlet							
RFA_260	55.44	4.6	55.55	5.7	55.38	6.6	55.52
RFA_261	55.44	4.5	55.55	5.5	55.38	6.6	55.52
RFA_262	55.44	4.5	55.55	5.5	55.40	6.6	55.53
Brimacombe Mill Chemical Works Culvert							
RFA_263	55.60	4.5	55.85	5.4	56.11	6.6	56.24
RFA_264	55.71	4.5	55.94	5.4	56.18	7.1	56.30
Brimacombe Hill Bridge							
RFA_265	55.72	4.5	55.94	5.4	56.19	7.1	56.30
RFA_266	55.72	4.5	55.93	5.4	56.18	7.1	56.29
Burket Bridge (Port Industrial Estate)							
RFA_267	55.78	4.5	55.95	5.4	56.17	7.1	56.27
RFA_268	55.89	4.5	56.02	5.4	56.23	7.1	56.33
Benson's Culvert							
RFA_269	56.33	4.5	56.45	5.4	56.66	7.0	56.82
RFA_270	56.38	4.6	56.50	5.4	56.72	7.0	56.89
Benson's Bridge							
RFA_271	56.39	4.5	56.51	5.4	56.73	7.0	56.96
RFA_272	56.41	4.5	56.54	5.4	56.76	7.0	56.98
Port Industrial Estate Sluices							
RFA_273	56.89	4.5	57.00	5.4	57.08	7.0	57.18
Port Industrial Estate Bridge							
RFA_284	57.00	4.5	57.01	5.4	57.11	7.0	57.23
RFA_285	57.01	4.5	57.02	5.4	57.14	7.0	57.25
RFA_286	57.03	4.4	57.04	5.4	57.18	7.0	57.30
RFA_287	57.08	4.4	57.09	5.4	57.23	6.9	57.35

RFA_268	57.09	4.4	57.15	5.3	57.29	6.9	57.40	8.2	57.51	9.3	57.59	10.0
RFA_269	57.11	4.4	57.17	5.3	57.29	6.9	57.39	8.2	57.49	9.3	57.56	10.0
RFA_270	57.31	4.4	57.40	5.3	57.54	6.9	57.64	8.2	57.73	9.3	57.78	10.0
RFA_271	57.37	4.4	57.46	5.3	57.60	6.9	57.70	8.2	57.78	9.3	57.84	9.9

Junction with RFQ_001

RFA_272	57.37	2.3	57.46	3.1	57.60	4.4	57.70	5.5	57.78	6.5	57.84	7.1
RFA_273	57.59	2.3	57.68	3.0	57.80	4.4	57.88	5.5	57.95	6.5	57.98	7.1
RFA_274	58.00	2.2	58.06	2.4	58.15	2.8	58.20	3.2	58.24	3.5	58.26	3.6
RFA_275	58.06	2.2	58.12	2.4	58.20	2.8	58.25	3.2	58.29	3.4	58.31	3.6

Bourne Mills Bypass

RFA_276	58.40	2.2	58.44	2.4	58.49	2.8	58.52	3.2	58.55	3.4	58.56	3.6
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Junction with RFQ_004

RFA_277	58.40	4.4	58.44	5.3	58.49	6.8	58.52	8.1	58.55	9.2	58.56	9.8
RFA_278	58.51	4.4	58.56	5.3	58.63	6.8	58.69	8.1	58.73	9.1	58.76	9.8
RFA_279	58.68	3.6	58.73	4.3	58.82	5.2	58.88	6.2	58.93	7.6	58.97	8.7
RFA_280	58.81	3.6	58.86	4.3	58.94	5.1	58.99	6.2	59.07	7.6	59.12	8.7

Wimberley Mills Well

RFA_281	59.84	3.6	59.92	4.3	60.01	5.1	60.08	6.2	60.16	7.6	60.22	8.7
RFA_282	59.86	3.6	59.93	4.2	60.02	5.1	60.10	6.2	60.19	7.6	60.24	8.7
RFA_283	59.87	3.6	59.94	4.2	60.03	5.1	60.11	6.2	60.19	7.6	60.25	8.7

Wimberley Mills Bridge

RFA_284	59.99	3.6	60.07	4.2	60.16	5.1	60.26	6.2	60.37	7.6	60.45	8.7
RFA_285	60.04	3.6	60.11	4.2	60.20	5.1	60.30	6.2	60.40	7.6	60.47	8.7
RFA_286	60.16	3.6	60.23	4.2	60.30	5.1	60.39	6.2	60.49	7.6	60.55	8.7

Wimberley Mills Cutout 1

RFA_287	60.60	3.6	60.67	4.2	60.74	5.1	60.84	6.2	60.96	7.6	61.04	8.7
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RFA_288	60.61	3.6	60.67	4.2	60.75	5.1	60.85	6.2	60.97	7.6	61.08	8.1
Wimberley Mills Culvert 2												
RFA_289	61.32	3.6	61.47	4.2	61.67	5.0	61.92	6.2	62.20	7.6	62.23	8.1
RFA_290	61.37	3.6	61.51	4.2	61.69	5.0	61.94	6.2	62.22	7.8	62.25	8.7
RFA_291	61.48	3.6	61.59	4.2	61.75	5.0	61.97	6.2	62.24	7.8	62.27	8.7
RFA_292	61.57	3.6	61.68	4.2	61.80	5.0	62.00	6.2	62.25	7.8	62.29	8.7
RFA_293	61.65	3.6	61.73	4.1	61.85	4.9	62.04	6.2	62.28	7.8	62.31	8.6
RFA_294	61.88	3.6	61.92	4.1	62.01	4.9	62.16	6.2	62.36	7.8	62.40	8.6
RFA_295	62.00	3.6	62.05	4.1	62.13	4.9	62.26	6.2	62.44	7.8	62.48	8.6
RFA_296	62.13	3.7	62.18	4.1	62.25	4.9	62.37	6.2	62.53	7.8	62.58	8.6
RFA_297	62.24	3.7	62.29	4.1	62.37	4.8	62.49	6.2	62.63	7.8	62.69	8.6
RFA_298	62.35	3.8	62.39	4.1	62.46	4.8	62.59	6.2	62.73	7.8	62.79	8.6
Junction with RFR_001												
RFA_299	62.35	1.4	62.39	1.5	62.46	1.8	62.59	2.2	62.73	2.6	62.79	2.8
RFA_300	62.83	1.4	62.93	1.5	62.93	1.7	62.93	2.2	62.93	2.6	62.93	2.8
St Marys Mill Canal Control Wall												
RFA_301	63.08	1.4	63.09	1.5	63.12	1.7	63.17	2.2	63.21	2.6	63.23	2.8
RFA_301A	63.08	1.4	63.09	1.5	63.12	1.8	63.17	2.2	63.22	2.7	63.23	2.9
St Marys Mill Bypass Shelves												
RFA_302	64.16	1.4	64.19	1.5	64.26	1.8	64.40	2.2	64.54	2.7	64.62	2.9
Junction with RFR_002												
St Marys House Culvert												
RFA_303	64.16	3.8	64.19	4.1	64.26	4.8	64.40	6.2	64.54	7.9	64.62	8.7
RFA_304	64.29	3.8	64.32	4.1	64.40	4.8	64.54	6.2	64.70	7.8	64.78	8.7
RFA_305	64.39	3.8	64.42	4.1	64.50	4.8	64.66	6.2	64.82	7.8	64.90	8.7

RFA_324	70.00	3.3	69.86	3.9	69.86	4.6	70.04	6.2	70.32	7.8	70.60	8.6
RFA_325	70.02	3.3	69.87	3.9	69.87	4.5	70.05	6.2	70.35	7.8	70.61	8.8
RFA_326	70.11	3.3	70.06	3.9	70.11	4.5	70.24	6.2	70.48	7.8	70.68	8.8

Chalford Chaire Cultvert

RFA_327	71.03	3.3	71.23	3.9	71.42	4.5	71.86	6.2	71.95	7.8	71.96	8.9
RFA_328	71.04	3.3	71.24	3.9	71.43	4.5	71.87	6.2	71.97	7.8	71.98	8.9
RFA_329	71.40	3.3	71.49	3.9	71.59	4.5	71.91	6.2	72.00	7.8	72.00	8.9
RFA_330	72.51	3.3	72.55	3.9	72.59	4.5	72.72	6.2	72.84	7.8	72.82	8.9

Thonet house Bridge

RFA_331	73.20	3.3	73.26	3.9	73.33	4.5	73.51	6.2	73.66	7.8	73.76	8.9
RFA_332	73.32	3.3	73.39	3.9	73.46	4.5	73.62	6.2	73.77	7.8	73.86	8.9

Red Lion Bridge

RFA_333	73.98	3.3	74.13	3.9	74.30	4.5	74.69	6.2	75.01	7.8	75.20	8.9
RFA_334	74.03	3.3	74.19	3.8	74.35	4.5	74.73	6.2	75.05	7.8	75.25	8.9
RFA_335	74.05	3.3	74.21	3.8	74.37	4.5	74.75	6.2	75.07	7.8	75.26	8.9

Brooklyn Bridge

RFA_336	74.14	3.3	74.29	3.8	74.41	4.5	74.77	6.2	75.08	7.8	75.27	8.9
RFA_337	74.15	3.3	74.30	3.8	74.42	4.5	74.77	6.2	75.08	7.8	75.28	8.9

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RFA_344	76.89	3.2	77.07	3.8	77.16	4.5	77.34	6.2	77.49	7.8	77.59	9.0
RFA_345	76.99	3.2	77.07	3.8	77.16	4.5	77.34	6.2	77.49	7.8	77.59	9.0
RFA_346	77.17	3.2	77.23	3.8	77.31	4.5	77.48	6.2	77.62	7.9	77.71	9.0
RFA_347	77.51	3.2	77.57	3.7	77.65	4.5	77.82	6.2	77.95	7.9	78.04	9.0

Hanley Lane Bridge

RFA_348	77.78	3.2	77.83	3.7	78.14	4.5	78.70	6.2	79.25	7.9	79.58	9.0
RFA_349	77.82	3.2	77.95	3.7	78.15	4.5	78.70	6.3	79.25	6.9	79.59	7.9
RFA_350	77.89	3.2	78.00	3.7	78.18	4.5	78.70	6.3	79.26	7.0	79.59	7.1
RFA_351	78.03	3.2	78.11	3.7	78.25	4.5	78.72	6.3	79.26	7.0	79.59	7.1
RFA_352	78.10	3.2	78.18	3.7	78.32	4.1	78.75	4.5	79.27	4.8	79.60	5.7
RFA_353	78.18	2.5	78.26	2.5	78.38	2.6	78.76	3.2	79.27	5.2	79.60	6.0
RFA_354	78.20	2.5	78.28	2.6	78.40	2.7	78.77	4.0	79.28	6.2	79.61	7.3
RFA_355	78.25	3.2	78.32	3.7	78.41	4.1	78.78	6.0	79.28	8.0	79.61	9.2
RFA_356	78.43	2.5	78.49	2.8	78.56	3.2	78.86	4.6	79.31	6.2	79.61	7.5

Ashmead Mill Sluices

RFA_357	79.26	2.5	79.31	2.8	79.35	3.1	79.53	4.6	79.70	6.2	79.88	7.5
RFA_358	79.31	3.1	79.35	3.6	79.39	4.0	79.57	6.0	79.73	8.0	79.89	9.4
RFA_359	79.43	3.1	79.49	3.6	79.53	4.0	79.71	6.0	79.87	8.0	80.00	9.4
RFA_360	79.68	3.1	79.73	3.8	79.77	4.0	79.94	6.0	80.09	8.0	80.18	9.4
RFA_361	79.95	3.1	80.00	3.8	80.04	4.0	80.19	6.0	80.32	8.0	80.40	9.4
RFA_362	80.28	3.1	80.32	3.6	80.36	4.0	80.51	6.0	80.63	7.9	80.70	9.3
RFA_363	80.64	3.1	80.69	3.5	80.74	4.0	80.93	5.9	81.10	7.9	81.20	9.3
RFA_364	80.84	3.1	80.89	3.5	80.94	4.0	81.13	5.9	81.30	7.9	81.40	9.3
RFA_365	81.13	3.1	81.19	3.5	81.24	3.9	81.44	5.3	81.60	7.0	81.70	8.2
RFA_366	81.24	3.1	81.30	3.5	81.34	3.9	81.53	5.3	81.69	7.0	81.79	8.2

Bakers Bridge

RFA_367	82.28	3.0	82.39	3.5	82.47	3.9	82.77	5.3	83.08	7.0	83.35	8.2
RFA_368	82.34	3.0	82.45	3.5	82.53	3.9	82.82	5.3	83.13	7.0	83.40	8.2
RFA_369	82.47	1.4	82.59	1.5	82.68	1.5	83.03	1.8	83.39	2.0	83.67	2.2

Bakers Mill Slulces

RFA_370	85.28	1.4	85.30	1.5	85.31	1.6	85.36	1.7	85.40	2.0	85.43	2.2
RFA_371	85.28	1.4	85.30	1.5	85.31	1.6	85.36	1.8	85.41	1.9	85.44	2.0
RFA_372	85.29	1.5	85.31	1.7	85.32	1.8	85.36	1.8	85.41	1.9	85.44	2.0
RFA_373	85.31	1.7	85.33	1.9	85.34	2.1	85.38	2.2	85.42	2.4	85.46	2.9
RFA_374	85.32	3.0	85.35	3.6	85.36	4.1	85.40	4.3	85.44	4.7	85.48	5.6
RFA_375	85.39	3.0	85.42	3.5	85.46	4.0	85.49	4.3	85.53	4.7	85.59	5.6
RFA_376	85.49	3.0	85.53	3.5	85.56	4.0	85.58	4.3	85.61	4.6	85.67	5.6
RFA_377	85.88	3.0	86.01	3.5	86.04	4.0	86.05	4.3	86.07	4.6	86.11	5.6
RFA_378	86.62	2.9	86.86	3.5	86.89	4.0	86.71	4.3	86.73	4.4	86.77	4.6

Puck Mill Culvert

RFA_379	90.78	2.9	91.65	3.5	92.55	4.0	93.01	4.2	93.38	4.4	93.80	4.5
RFA_380	90.80	2.9	91.65	3.5	92.55	4.0	93.01	4.2	93.38	4.4	93.80	4.5
RFA_381	91.04	2.9	91.67	3.5	92.55	4.0	93.02	4.3	93.38	4.5	93.60	4.6
RFA_382	91.32	2.9	91.70	3.5	92.55	4.0	93.02	4.8	93.38	5.2	93.60	5.5
RFA_383	91.34	2.3	91.71	2.3	92.55	3.7	93.02	5.1	93.38	5.7	93.60	5.9
RFA_384	91.38	1.3	91.72	2.0	92.56	3.6	93.02	5.0	93.38	5.7	93.60	5.9
RFA_385	91.42	2.9	91.73	3.9	92.56	5.7	93.02	6.5	93.38	7.1	93.61	7.4
RFA_386	91.57	0.2	91.77	0.8	92.56	2.8	93.02	4.5	93.39	5.2	93.61	5.5
RFA_387	91.65	1.4	91.79	1.4	92.57	2.6	93.03	4.2	93.39	5.1	93.61	5.8
RFA_388	91.96	2.8	92.00	4.0	92.58	5.5	93.03	6.2	93.39	6.3	93.61	6.5
RFA_389	92.50	2.8	92.62	3.9	92.76	6.1	93.08	8.2	93.40	10.4	93.62	11.9
RFO_001	46.61	2.3	46.74	2.8	46.89	3.9	47.12	4.8	47.20	5.5	47.24	5.9

RFO_002	46.62	2.4	46.76	2.9	47.00	3.8	47.14	4.8	47.22	5.6	47.26	6.1
RFO_003	46.69	2.4	46.82	2.9	47.04	3.8	47.18	4.5	47.25	5.0	47.29	5.4
RFO_004	46.79	2.4	46.89	2.9	47.08	3.8	47.21	4.5	47.28	5.0	47.32	5.4
RFO_005	46.86	2.4	46.94	2.9	47.12	3.8	47.23	4.5	47.30	5.0	47.34	5.4

Griffin Mill Footbridge 3

RFO_006	46.90	2.4	46.97	2.8	47.14	3.8	47.25	4.5	47.33	5.0	47.40	5.4
RFO_007	46.95	2.4	47.02	2.9	47.16	3.8	47.27	4.5	47.34	5.0	47.40	5.4

Griffin Mill Weir 1

RFO_008	47.56	2.4	47.61	2.9	47.71	3.8	47.77	4.5	47.81	5.0	47.83	5.4
RFO_009	47.57	2.4	47.63	2.9	47.73	3.8	47.79	4.5	47.82	5.0	47.85	5.4

Griffin Mill Culvert

RFO_010	47.81	2.4	47.87	2.9	48.00	3.8	48.10	4.5	48.17	5.0	48.22	5.4
RFO_011	47.89	2.4	47.94	2.9	48.05	3.8	48.14	4.5	48.21	5.0	48.26	5.4

Griffin Mill Weir 2

RFO_012	48.33	2.4	48.38	2.8	48.48	3.8	48.55	4.5	48.60	5.0	48.64	5.4
RFP_001	48.49	0.3	48.56	0.4	48.66	1.8	48.74	2.0	48.80	2.2	48.84	2.4
RFP_002	48.49	0.3	48.56	0.4	48.68	1.8	48.76	2.0	48.81	2.2	48.85	2.4

Brookdale Bridge 2

RFP_003	48.49	0.3	48.56	0.4	48.68	1.8	48.76	2.0	48.82	2.2	48.86	2.4
RFP_004	48.49	0.3	48.56	0.4	48.71	1.8	48.78	2.0	48.84	2.2	48.88	2.4

Phoenix Mill Culvert

RFP_005	49.93	0.3	49.99	0.4	50.03	1.8	50.09	2.0	50.19	2.2	50.27	2.4
RFP_006	49.93	0.5	49.99	0.5	50.03	1.8	50.09	2.0	50.19	2.2	50.27	2.8
RFO_001	57.37	2.1	57.46	2.3	57.60	2.5	57.70	2.6	57.78	2.8	57.84	2.8
RFO_002	57.65	2.1	57.67	2.3	57.73	2.5	57.78	2.6	57.84	2.8	57.88	2.8

Bourne Mill Sluice

RFQ_003	58.38	2.1	58.40	2.3	58.45	2.5	58.48	2.6	58.51	2.8	58.53	2.8
RFQ_004	58.40	2.2	58.44	2.9	58.49	4.0	58.52	4.9	58.55	5.7	58.56	6.2
RFR_001	62.35	2.4	62.39	2.6	62.46	3.1	62.59	4.0	62.73	5.2	62.79	5.8

St Marys Mill Culvert

RFR_002	64.16	2.4	64.19	2.6	64.26	3.1	64.40	4.0	64.54	5.2	64.62	5.8
RFS_001	64.48	1.6	64.52	1.6	64.60	1.7	64.76	2.0	64.93	2.2	65.01	2.3
RFS_002	64.55	1.6	64.58	1.6	64.65	1.7	64.79	2.0	64.94	2.2	65.02	2.3

Iles Mill Culvert

RFS_003	66.09	1.6	66.10	1.6	66.11	1.7	66.14	2.0	66.16	2.2	66.18	2.3
RFS_004	66.08	1.6	66.09	1.6	66.10	1.7	66.13	2.0	66.15	2.2	66.16	2.3

Junction with RFT_003

RFS_005	66.08	1.6	66.09	1.6	66.10	1.7	66.13	2.0	66.15	2.2	66.16	2.3
RFS_006	66.10	2.5	66.10	2.8	66.12	3.3	66.15	4.5	66.18	5.8	66.19	6.4
RFS_007	66.12	2.4	66.13	2.8	66.15	3.3	66.21	4.5	66.26	5.8	66.28	6.4
RFT_001	64.96	0.0	64.98	0.0	65.05	0.0	65.18	0.0	65.40	0.0	65.58	0.0
RFT_002	64.96	0.0	64.98	0.0	65.05	0.0	65.18	0.0	65.40	0.0	65.58	0.0

Iles Mill Bypass Sluices

RFT_003	66.08	0.0	66.09	0.0	66.10	0.0	66.13	0.0	66.15	0.0	66.16	0.0
SCB_001	43.84	0.0	43.84	0.0	43.84	0.0	43.84	0.1	43.91	0.0	44.02	0.0
SCB_002	43.84	0.1	43.84	0.1	43.84	0.1	43.84	0.1	43.91	0.4	44.02	1.1
SCB_003	43.84	0.1	43.84	0.1	43.84	0.1	43.84	0.1	43.91	0.4	44.02	1.1
SCB_004	43.84	0.1	43.84	0.1	43.84	0.1	43.84	0.1	43.91	0.4	44.02	1.1
SCB_005	43.84	0.1	43.84	0.1	43.84	0.1	43.84	0.1	43.91	0.4	44.02	1.1
SCB_006	43.84	0.1	43.84	0.1	43.84	0.1	43.84	0.1	43.92	0.1	44.03	0.1

Butterow Mill Canal Bridge

SCB_007	43.85	0.1	43.85	0.1	43.85	0.1	43.85	0.1	43.92	0.1	44.03	0.1
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SCB_008	43.85	0.1	43.85	0.1	43.85	0.1	43.85	0.1	43.92	0.1	44.03	0.1
Bowbridge Lock Weir												
SCB_009	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_010	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_011	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_012	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_013	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_014	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_015	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
Grimsthorpe Mill Lock Weir												
SCB_016	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1
SCB_017	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1
SCB_018	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1
SCB_019	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1
Ham Lock Weir												
SCB_020	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1
SCB_021	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1
SCB_022	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1
SCB_023	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1	52.03	0.1
SCB_024	52.76	0.1	52.76	0.1	52.76	0.1	52.76	0.1	52.76	0.1	52.76	0.1
SCC_001	59.71	0.0	59.73	0.0	59.75	0.0	59.76	0.0	59.78	0.0	59.80	0.0
SCC_002	59.72	0.0	59.73	0.0	59.76	0.0	59.78	0.0	59.81	0.1	59.82	0.1
SCC_003	59.73	0.0	59.74	0.0	59.77	0.0	59.80	0.0	59.84	0.1	59.86	0.1
SCC_004	59.73	0.0	59.75	0.0	59.78	0.0	59.81	0.0	59.85	0.1	59.86	0.1
SCC_005	59.73	0.0	59.75	0.0	59.78	0.0	59.81	0.0	59.85	0.1	59.86	0.1

Wimberley Canal Weir

SCC_006	62.96	0.0	62.98	0.0	63.02	0.0	63.06	0.0	63.09	0.1	63.10	0.1
SCC_007	62.98	0.0	62.98	0.0	63.02	0.0	63.06	0.0	63.09	0.1	63.10	0.1
SCC_008	62.96	0.0	62.98	0.0	63.02	0.0	63.06	0.0	63.09	0.1	63.10	0.1
SCC_009	62.96	0.0	62.98	0.0	63.02	0.0	63.06	0.0	63.09	0.1	63.10	0.1
SCC_010	62.96	0.0	62.98	0.0	63.02	0.0	63.06	0.1	63.09	0.1	63.10	0.1
SCC_011	62.96	0.0	62.98	0.0	63.02	0.0	63.06	0.1	63.09	0.1	63.10	0.1
SCC_012	62.96	0.0	62.98	0.0	63.02	0.0	63.06	0.0	63.09	0.0	63.10	0.0
SCC_013	62.96	0.0	62.98	0.0	63.02	0.0	63.06	0.0	63.09	0.0	63.10	0.0

Iles Mill Canal Culvert

SCC_014	64.56	0.0	64.57	0.0	64.58	0.0	64.58	0.0	64.58	0.0	64.58	0.0
SCC_015	64.57	0.0	64.64	0.0	64.73	0.0	64.76	0.0	64.77	0.0	64.77	0.0

Iles Lock Weir

SCC_016	67.34	0.0	67.35	0.0	67.36	0.0	67.37	0.0	67.37	0.0	67.37	0.0
SCC_017	67.34	0.0	67.35	0.0	67.38	0.0	67.40	0.0	67.40	0.0	67.40	0.0

Bolvesthorpe Mill Canal Culvert

SCC_018	70.12	0.0	70.13	0.0	70.15	0.0	70.16	0.0	70.16	0.0	70.16	0.0
SCC_019	70.12	0.0	70.13	0.0	70.16	0.0	70.17	0.0	70.18	0.0	70.18	0.0

Chafford Canal Culvert 1

SCC_020	70.44	0.0	70.46	0.0	70.49	0.0	70.51	0.0	70.51	0.0	70.51	0.0
SCC_021	70.44	0.0	70.46	0.0	70.50	0.0	70.51	0.0	70.52	0.0	70.52	0.0

Chafford Canal Culvert 2

SCC_022	71.99	0.0	72.01	0.0	72.04	0.0	72.05	0.0	72.06	0.0	72.06	0.0
SCC_023	71.99	0.0	72.02	0.0	72.10	0.0	72.13	0.0	72.15	0.0	72.15	0.0

Chafford Chalres Canal Culvert

SCC_024	74.01	0.0	74.04	0.0	74.10	0.0	74.11	0.0	74.12	0.0	74.12	0.0
SCC_025	74.02	0.0	74.12	0.0	74.27	0.0	74.32	0.0	74.34	0.0	74.34	0.0

	74.03	0.0	74.15	0.0	74.35	0.0	74.42	0.0	74.44	0.0	74.45	0.0
Clowes Bridge Lock Wall												
SCC_026	76.81	0.0	76.82	0.0	76.84	0.0	76.84	0.0	76.85	0.0	76.85	0.0
SCC_027	76.81	0.0	76.84	0.0	76.91	0.0	76.92	0.0	76.92	0.0	76.93	0.0
SCC_028	76.81	0.0	76.84	0.0	76.89	0.0	77.03	0.0	77.05	0.0	77.05	0.0
SCC_029	76.81	0.0	76.84	0.0	76.91	0.0	77.05	0.0	77.08	0.0	77.09	0.0
SCC_030	76.81	0.0	76.91	0.0	77.05	0.0	77.08	0.0	77.08	0.0	77.09	0.0
SCC_032	79.71	0.0	79.73	0.0	79.77	0.0	79.77	0.0	79.78	0.0	79.78	0.0
SCC_033	79.71	0.0	79.73	0.0	79.77	0.0	79.77	0.0	79.78	0.0	79.78	0.0
SCC_034	79.71	0.0	79.73	0.0	79.77	0.0	79.77	0.0	79.78	0.0	79.78	0.0
SCC_035	79.71	0.0	79.73	0.1	79.77	0.1	79.77	0.6	79.78	0.7	79.78	0.8
SCC_036	79.71	0.0	79.73	0.1	79.78	0.6	79.79	0.7	79.80	0.8	79.80	0.8
SCC_037	79.71	0.0	79.73	0.1	79.78	0.6	79.80	0.7	79.81	0.8	79.81	0.8
SCC_038	79.71	0.0	79.73	0.1	79.79	0.6	79.81	0.7	79.82	0.8	79.83	0.8
SCC_039	79.71	0.0	79.73	0.1	79.83	0.6	79.86	0.7	79.88	0.8	79.88	0.8
SCC_040	79.71	0.0	79.73	0.1	79.85	0.6	79.89	0.7	79.90	0.8	79.91	0.8
SCC_041	79.71	0.0	79.73	0.1	79.86	0.6	79.90	0.7	79.91	0.8	79.92	0.8
SCC_042	79.71	0.0	79.73	0.1	79.88	0.6	79.92	0.7	79.94	0.8	79.95	0.8
SCC_043	79.71	0.0	79.74	0.1	79.92	0.6	79.96	0.7	79.98	0.8	79.99	0.8
SCC_044	79.71	0.0	79.75	0.1	79.96	0.6	80.01	0.7	80.02	0.8	80.03	0.8
SCC_045	79.71	0.0	79.75	0.1	79.99	0.6	80.03	0.7	80.05	0.8	80.06	0.8
SCC_046	79.71	0.0	79.76	0.1	80.00	0.6	80.04	0.7	80.06	0.8	80.07	0.8
Bakers Mill Lower Lock Wall												
SCC_047	82.01	0.0	82.39	0.1	83.11	0.6	83.15	0.7	83.17	0.8	83.17	0.8
SCC_048	82.01	0.0	82.39	0.1	83.11	0.7	83.15	1.3	83.17	1.7	83.17	1.9
SCC_049	82.01	0.0	82.39	0.1	83.11	0.7	83.15	1.3	83.17	1.7	83.17	1.9
SCC_050	82.01	0.0	82.39	0.1	83.11	0.7	83.15	1.3	83.17	1.7	83.17	1.9

Bakers Mill Upper Lock Weir							
SCC_051	84.51	0.0	84.71	0.1	85.25	0.7	85.38
SCC_052	84.51	0.0	84.71	0.0	85.25	0.5	85.38
SCC_053	84.51	0.0	84.71	0.0	85.25	0.5	85.38
SCC_054	84.51	0.0	84.71	0.0	85.25	0.5	85.39
SCC_055	84.51	0.0	84.71	0.0	85.25	0.5	85.39
SCC_056	84.51	0.0	84.71	0.0	85.25	0.5	85.39
SCC_057	84.51	0.0	84.71	0.0	85.25	0.6	85.41

Puck Mill Lower Lock Weir

Puck Mill Lower Lock Weir							
SCC_058	86.61	0.0	86.61	0.0	87.78	0.6	88.06
SCC_059	86.61	0.0	86.61	0.0	87.78	0.6	88.06
Puck Mill Upper Lock Weir							
SCC_060	90.40	0.0	90.40	0.0	90.57	0.6	90.82
SCC_061	90.40	0.0	90.40	0.0	90.88	0.6	91.63

Whitchall Lower Lock Weir

Whitchall Lower Lock Weir							
SCC_062	91.71	0.0	91.71	0.0	92.55	0.6	93.00
SCC_063	91.71	0.0	91.71	0.0	92.55	2.3	93.01
SCC_064	91.71	0.0	91.71	0.0	92.55	0.5	93.02
SCC_065	91.71	0.0	91.71	0.0	92.56	0.4	93.02
SCC_066	91.71	0.0	91.71	0.0	92.56	0.2	93.02
SCC_067	91.71	0.0	91.71	0.0	92.56	0.1	93.02
SCC_068	91.71	0.0	91.71	0.0	92.56	0.1	93.02
SCC_069	91.71	0.0	91.71	0.0	92.56	0.0	93.02
SCC_070	91.71	0.0	91.71	0.0	92.56	0.0	93.02

Cell 130	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00
Cell 131	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00
Cell 132	80.40	0.00	80.40	0.00	80.40	0.00	80.40	0.00	80.40	0.00	80.40	0.00
Cell 133	80.95	0.00	80.95	0.00	80.95	0.00	80.95	0.00	80.95	0.00	81.20	0.25
Cell 134	81.10	0.00	81.10	0.00	81.10	0.00	81.10	0.00	81.10	0.00	81.10	0.00
Cell 135	81.60	0.00	81.60	0.00	81.60	0.00	81.60	0.00	81.60	0.00	81.60	0.00
Cell 137	85.28	2.10	85.30	2.12	85.31	2.13	85.36	2.18	85.40	2.22	85.44	2.26
Cell 138	85.28	2.19	85.30	2.20	85.32	2.22	85.36	2.26	85.41	2.31	85.44	2.34
Cell 139	85.29	1.81	85.31	1.83	85.32	1.84	85.37	1.89	85.42	1.94	85.45	1.97
Cell 140	85.29	1.49	85.31	1.51	85.33	1.52	85.37	1.57	85.42	1.62	85.45	1.66
Cell 141	91.38	0.72	91.71	1.05	92.55	1.89	93.02	2.36	93.38	2.72	93.60	2.94
Cell 142	91.38	0.64	91.72	0.98	92.56	1.82	93.02	2.28	93.38	2.64	93.60	2.86
Cell 143	91.39	0.59	91.72	0.92	92.56	1.76	93.02	2.22	93.38	2.58	93.60	2.80
Cell 144	91.10	0.15	91.72	0.77	92.56	1.61	93.02	2.07	93.38	2.43	93.61	2.65
Cell 145	91.62	0.42	91.79	0.59	92.57	1.37	93.03	1.83	93.39	2.19	93.61	2.41
Cell 146	91.63	0.43	91.79	0.59	92.57	1.37	93.03	1.83	93.39	2.19	93.61	2.41
Cell 147	91.95	0.55	91.98	0.58	92.58	1.18	93.04	1.64	93.39	1.99	93.61	2.21

5 Year Event		10 Year Event		25 Year Event		50 Year Event		100 Year Event		150 Year Event	
Section Label	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)	Level (mOD)						
NSA_001	31.59	6.7	31.59	8.4	31.59	10.9	31.59	13.0	31.59	14.3	31.59
Nalsworth Stream Outfall Well											
NSA_002	34.16	6.7	34.28	8.4	34.43	10.9	34.56	13.0	34.63	14.3	34.69
NSA_003	34.28	6.7	34.38	8.4	34.52	10.9	34.63	13.0	34.70	14.3	34.74
NSA_004	34.53	6.7	34.64	8.4	34.78	10.8	34.89	13.0	34.96	14.3	35.00
Selsley Hill Culvert											
NSA_005	34.98	6.6	35.15	8.4	35.41	10.8	35.65	13.0	35.85	14.3	36.31
NSA_006	35.01	6.6	35.19	8.4	35.44	10.8	35.68	12.9	35.98	14.3	36.31
NSA_007	35.06	6.6	35.24	8.4	35.50	10.8	35.74	12.9	36.01	14.3	36.34
NSA_008	35.05	6.6	35.24	8.4	35.49	10.8	35.73	12.9	36.00	14.3	36.34
NSA_009	35.13	6.6	35.31	8.4	35.56	10.8	35.79	12.9	36.05	14.3	36.36
NSA_010	35.16	6.6	35.34	8.4	35.59	10.8	35.82	12.8	36.07	13.3	36.38
NSA_011	35.19	6.6	35.37	8.3	35.62	10.8	35.84	13.0	36.08	13.6	36.38
NSA_012	35.21	6.6	35.39	8.3	35.64	10.7	35.86	13.0	36.09	14.5	36.39
Variable Created Well											
NSA_013	35.52	6.6	35.73	8.3	36.01	10.7	36.25	13.0	36.47	14.5	36.73
Ernold Culvert											
NSA_014	37.33	6.5	37.52	8.3	37.82	10.7	38.12	12.9	38.31	14.4	38.42
NSA_015	37.54	6.5	37.69	8.2	37.93	10.7	38.20	12.9	38.37	14.4	38.48
Ernold Bridge											
NSA_016	38.22	6.5	38.44	8.2	38.74	10.7	39.28	12.9	39.71	14.4	40.06
NSA_017	38.27	6.5	38.48	8.2	38.77	10.6	39.30	12.9	39.72	14.4	40.06
NSA_018	38.33	6.5	38.54	8.2	38.82	10.6	39.32	12.9	39.73	14.4	40.07

Car Park Bridge

NSA_018	38.82	6.5	38.52	8.2	38.79	10.6	39.29	12.9	39.70	14.4	40.04	15.5
NSA_020	38.41	6.5	38.61	8.2	38.88	10.6	39.35	12.9	39.74	14.4	40.08	15.5
NSA_021	38.59	6.5	38.75	8.2	38.97	10.6	39.39	12.9	39.77	14.4	40.10	15.5
NSA_022	39.02	6.4	39.11	8.2	39.22	10.6	39.47	12.9	39.80	14.4	40.12	15.5

Cotswold House Bridge

NSA_023	39.41	6.4	39.56	8.2	39.72	10.6	39.80	12.8	39.96	14.3	40.21	15.5
NSA_024	39.45	6.4	39.59	8.2	39.75	10.6	39.83	12.8	39.98	14.3	40.21	15.5

New Tyning's Footbridge

NSA_025	39.48	6.4	39.63	8.2	39.81	10.6	39.90	12.8	40.05	14.3	40.28	15.5
NSA_026	39.55	6.4	39.70	8.2	39.87	10.6	39.97	12.8	40.11	14.3	40.32	15.5
NSA_027	39.65	6.4	39.80	8.1	39.97	10.6	40.09	12.8	40.20	14.3	40.37	15.5

The Phrye Bridge

NSA_028	39.84	6.4	40.02	8.1	40.25	10.5	40.42	12.8	40.55	14.3	40.67	15.5
NSA_029	39.87	6.4	40.06	8.1	40.28	10.5	40.46	12.8	40.58	14.3	40.71	15.5
NSA_030	39.93	6.4	40.12	8.1	40.35	10.5	40.53	12.8	40.65	14.3	40.77	15.5
NSA_031	39.97	6.4	40.16	8.1	40.38	10.5	40.56	12.8	40.68	14.3	40.80	15.5
NSA_032	40.00	6.4	40.19	8.1	40.42	10.5	40.60	12.8	40.72	14.3	40.84	15.5
NSA_033	40.05	6.4	40.24	8.1	40.46	10.5	40.63	12.7	40.75	14.3	40.86	15.5
NSA_034	40.10	6.3	40.29	8.1	40.51	10.5	40.68	12.7	40.80	14.3	40.90	15.5
NSA_035	40.17	6.3	40.35	8.1	40.57	10.5	40.75	12.7	40.86	14.3	40.97	15.5
NSA_036	40.21	6.3	40.37	8.1	40.58	10.5	40.74	12.7	40.85	14.2	40.95	15.5

Junction with NSB_001

NSA_037	40.21	4.2	40.37	5.5	40.58	7.0	40.74	8.5	40.85	9.5	40.95	10.3
NSA_038	42.28	4.2	42.61	5.5	43.35	7.0	44.20	8.5	44.88	9.5	45.49	10.3

Rookemoor Mill Culvert - Right

Rookhamoor Mill Weir							
NSA_039	42.37	4.2	42.68	5.5	43.39	7.0	44.24
Junction with NSB_002							
NSA_040	42.37	6.3	42.68	8.1	43.39	10.5	44.24
NSA_041	42.41	6.3	42.71	8.0	43.40	10.5	44.24
NSA_042	42.42	6.3	42.71	8.0	43.40	10.5	44.24
NSA_043	42.45	6.3	42.73	8.0	43.40	10.5	44.24
NSA_044	42.56	6.3	42.81	8.0	43.42	10.5	44.24
Selsley Road Bridge							
NSA_045	42.61	6.3	42.84	8.0	43.54	10.5	44.34
Selsley Road Weir							
NSA_046	43.13	6.3	43.28	8.0	43.78	10.5	44.50
NSA_047	43.43	6.3	43.55	8.0	43.88	10.5	44.52
Pauls Rites Bridge							
NSA_048	43.65	6.2	43.78	8.0	44.03	10.5	44.59
NSA_049	43.73	6.2	43.86	8.0	44.08	10.4	44.60
NSA_050	43.83	6.2	43.96	8.0	44.16	10.4	44.63
NSA_051	43.96	6.2	44.08	8.0	44.26	10.4	44.66
Railway Bridge							
NSA_052	44.09	6.2	44.23	8.0	44.41	10.4	44.75
NSA_053	44.22	6.2	44.37	7.9	44.55	10.4	44.85
The Forge Weir							
NSA_054	44.58	6.2	44.74	7.9	44.94	10.4	45.24
NSA_055	44.66	6.2	44.81	7.9	45.00	10.4	45.28
Birds Crossing							
NSA_056	44.74	6.2	44.89	7.9	45.11	10.4	45.58

NSA_057	44.80	6.2	44.97	7.9	45.20	10.4	45.64	13.1	46.15	15.1	46.44	17.8
NSA_058	44.84	6.2	45.01	7.9	45.23	10.3	45.66	13.1	46.15	15.2	46.44	17.7
NSA_059	44.86	6.1	45.03	7.9	45.25	10.3	45.67	13.1	46.16	15.3	46.45	17.6
NSA_060	44.82	6.1	45.09	7.9	45.31	10.3	45.70	13.1	46.17	15.3	46.45	17.6
NSA_061	45.03	6.1	45.18	7.9	45.39	10.3	45.72	13.1	46.17	15.4	46.45	17.5

Station Road Works

NSA_062	45.60	6.1	45.75	7.9	46.00	10.3	46.39	13.1	46.80	15.4	47.14	17.5
Station Road Bridge												
NSA_063	46.40	6.1	46.60	7.9	46.86	10.3	47.10	13.1	47.36	15.4	47.62	17.5
NSA_064	46.43	6.1	46.63	7.8	46.87	10.3	47.11	13.1	47.36	15.4	47.62	17.5

South Woodchester Works Bridge

NSA_065	46.45	6.1	46.76	7.8	47.03	10.3	47.24	13.1	47.45	15.4	47.67	17.5
NSA_066	46.49	6.1	46.79	7.8	47.06	10.3	47.26	13.1	47.47	15.4	47.68	17.6
NSA_067	46.52	6.1	46.82	7.8	47.08	10.3	47.29	13.1	47.49	15.4	47.70	17.6
NSA_068	46.58	6.1	46.85	7.8	47.11	10.2	47.32	13.0	47.52	15.4	47.73	17.6
NSA_069	46.58	6.1	46.86	7.8	47.12	10.2	47.33	13.0	47.52	15.5	47.73	17.7
NSA_070	46.60	6.0	46.88	7.8	47.13	10.2	47.34	13.0	47.53	15.5	47.74	17.8
NSA_071	46.60	6.0	46.88	7.9	47.14	10.2	47.34	13.0	47.53	15.5	47.74	17.8
NSA_072	46.70	6.0	46.94	7.9	47.18	10.2	47.37	13.0	47.55	15.5	47.75	17.9
NSA_073	46.88	6.0	47.09	7.9	47.32	10.2	47.52	13.0	47.70	15.5	47.88	17.9
NSA_074	47.12	6.0	47.25	7.9	47.43	10.2	47.60	13.0	47.76	15.5	47.92	17.8
NSA_075	47.50	6.0	47.63	7.8	47.73	10.2	47.85	13.0	47.95	15.5	48.05	17.8

Frogmarch Lane Bridge

NSA_076	48.16	6.0	48.38	7.8	48.70	10.1	49.02	12.9	49.28	15.4	49.48	17.8
Bath Road Bridge												
NSA_077	48.19	6.0	48.42	7.8	48.74	10.1	49.06	12.9	49.31	15.4	49.52	17.8

NSA_078	48.19	6.0	48.42	7.8	48.74	10.1	49.07	12.9	49.33	15.4	49.55	17.8
NSA_079	48.22	6.0	48.44	7.8	48.76	10.1	49.08	12.9	49.34	15.4	49.56	17.8
NSA_080	48.27	6.0	48.50	7.8	48.81	10.1	49.13	12.9	49.38	15.4	49.59	17.8
NSA_081	48.33	5.9	48.54	7.8	48.83	10.1	49.14	12.9	49.38	15.4	49.59	17.8
NSA_082	48.38	5.9	48.59	7.8	48.87	10.1	49.17	12.9	49.40	15.4	49.61	17.8

Meretta Mills Bridge

NSA_083	48.33	5.9	48.54	7.8	48.84	10.1	49.22	12.9	49.62	15.4	49.86	17.8
NSA_084	48.57	5.9	48.74	7.7	48.98	10.1	49.32	12.9	49.66	15.4	49.88	17.8
NSA_085	48.65	5.9	48.82	7.7	49.05	10.0	49.37	12.8	49.70	15.3	49.91	17.8

Meretta Mills Culvert

NSA_086	50.23	5.9	50.56	7.7	50.78	10.0	50.87	12.7	50.92	15.3	50.93	17.8
NSA_087	50.23	5.9	50.57	7.7	50.79	10.0	50.87	12.7	50.93	15.2	50.93	17.8
NSA_088	50.23	5.9	50.56	7.7	50.78	10.0	50.86	12.7	50.92	15.2	50.93	17.7

Inchbrook Bridge

NSA_089	50.23	5.9	50.63	7.7	50.86	10.0	50.95	12.7	51.00	15.2	51.02	17.7
NSA_090	50.24	5.9	50.64	7.7	50.87	10.0	50.95	12.7	51.01	15.2	51.03	17.7
NSA_092	51.21	5.8	51.35	7.6	51.48	9.9	51.56	12.6	51.63	15.1	51.72	17.6

Critchleye Bridge 1

NSA_093	51.47	5.8	51.56	7.6	51.68	9.9	51.81	12.6	52.05	15.1	52.35	17.6
NSA_094	51.58	5.8	51.69	7.6	51.82	9.9	51.95	12.6	52.15	15.1	52.42	17.8

Junction with NSC_001

NSA_095	51.58	1.0	51.69	1.5	51.82	2.7	51.95	4.2	52.15	6.2	52.42	8.6
NSA_096	51.62	1.0	51.74	1.5	51.92	2.7	52.10	4.2	52.34	6.2	52.82	8.6

Critchleye 2

NSA_089	51.67	1.0	51.78	1.1	51.88	1.2	52.20	1.2	52.51	2.3	53.08	4.0
NSA_099	51.74	1.0	51.82	1.1	51.89	1.2	52.21	1.2	52.52	2.3	53.09	3.8
NSA_100	51.85	1.0	51.90	1.1	52.04	1.1	52.23	1.2	52.56	1.3	53.12	1.3

Dunkirk Mills Culvert

NSA_101	55.52	1.0	55.64	1.1	55.75	1.1	55.85	1.2	55.96	1.2	56.12	1.3
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Junction with NSC_016

NSA_102	55.52	2.8	55.64	3.9	55.75	5.0	55.85	6.1	55.96	7.3	56.12	9.3
NSA_103	55.52	2.8	55.64	3.9	55.76	5.0	55.86	6.0	55.97	7.3	56.13	9.3
NSA_104	55.54	2.8	55.67	3.9	55.78	5.0	55.88	6.0	55.99	7.3	56.15	9.3
NSA_105	55.58	2.8	55.71	3.9	55.83	5.0	55.93	6.0	56.04	7.3	56.20	9.3
NSA_106	55.70	2.8	55.82	3.8	55.94	5.0	56.04	6.0	56.14	7.3	56.29	9.3
NSA_107	55.77	2.8	55.90	3.8	56.02	4.9	56.12	6.0	56.25	6.6	56.43	7.3
NSA_108	55.84	2.8	55.97	3.8	56.09	5.1	56.19	6.7	56.30	7.8	56.48	8.2
NSA_109	55.91	2.8	56.04	3.8	56.16	5.1	56.26	6.7	56.34	8.2	56.49	8.9
NSA_110	55.85	2.8	56.08	3.8	56.21	5.1	56.33	6.8	56.40	8.6	56.52	9.6
NSA_111	56.02	2.8	56.16	3.8	56.29	5.1	56.43	6.8	56.52	8.6	56.62	9.6
NSA_112	56.09	2.8	56.22	3.8	56.36	5.0	56.51	6.8	56.62	8.6	56.71	9.6
NSA_113	56.13	2.8	56.26	3.8	56.40	5.0	56.55	7.1	56.66	9.3	56.75	10.5

Junction with NSE_001

NSA_114	56.13	5.1	56.26	6.7	56.40	8.4	56.55	10.8	56.66	11.9	56.75	12.9
NSA_115	56.31	5.1	56.44	6.7	56.61	9.5	56.68	11.7	56.75	13.6	56.81	14.8
NSA_116	56.44	5.1	56.57	6.6	56.75	9.5	56.84	12.1	56.90	14.8	56.83	16.6
NSA_117	56.54	5.1	56.68	6.6	56.87	9.5	56.99	12.1	57.10	14.8	57.16	16.6
NSA_118	56.65	5.1	56.78	6.6	56.96	9.5	57.09	12.1	57.20	14.8	57.29	16.6

Garge Culvert

NSA_119	56.87	5.0	57.05	6.6	57.63	9.5	58.20	12.1	58.76	14.8	59.14	16.5
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NSA_120	56.91	5.0	57.09	6.6	57.64	9.5	58.20	12.1	58.74	14.8	59.13	16.5
NSA_121	57.01	5.0	57.20	6.6	57.72	9.5	58.26	12.1	58.79	14.8	59.15	16.5

Egypt Mill Weir & Wheel

NSA_122	57.99	5.0	58.08	6.6	58.23	9.4	58.48	12.1	58.94	14.8	59.28	16.6
NSA_124	57.99	5.0	58.08	6.6	58.23	9.5	58.46	12.1	58.92	14.8	59.26	16.6
NSB_001	40.21	2.1	40.37	2.6	40.58	3.4	40.74	4.2	40.85	4.8	40.95	5.2

Rookmoor Mill Culvert - Left

NSB_002	42.37	2.1	42.68	2.6	43.39	3.4	44.24	4.2	44.82	4.8	45.52	5.2
NSC_001	51.58	4.8	51.69	6.1	51.82	7.2	51.95	8.4	52.15	9.0	52.42	9.1

Critchley's Left Hand Culvert

NSC_002	52.61	4.8	52.83	6.1	52.96	7.2	53.08	8.4	53.16	9.0	53.23	9.2
NSC_003	52.63	4.8	52.84	6.1	52.97	7.2	53.09	8.4	53.16	9.0	53.23	9.2
NSC_004	52.69	4.1	52.90	5.2	53.03	6.2	53.15	7.1	53.22	7.6	53.28	7.7
NSC_005	52.76	4.2	52.97	5.2	53.10	6.2	53.22	7.1	53.29	7.5	53.34	7.5
NSC_006	52.79	4.2	52.99	5.6	53.11	7.8	53.22	10.1	53.29	11.4	53.33	12.0

Junction with NSD_001

NSC_007	52.79	1.8	52.98	2.8	53.11	3.8	53.22	5.0	53.29	6.1	53.33	6.6
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Critchley's Bridge 3

NSC_008	52.79	1.8	53.00	2.8	53.13	3.8	53.24	5.0	53.31	6.1	53.35	6.6
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Critchley's Bridge 4

NSC_009	52.80	1.8	53.03	2.8	53.19	3.8	53.34	5.0	53.45	6.1	53.54	6.6
NSC_010	52.81	1.8	53.04	2.8	53.20	3.8	53.36	5.0	53.47	6.1	53.55	6.8
NSC_011	52.82	1.8	53.05	2.8	53.21	3.8	53.37	5.0	53.47	7.1	53.55	9.3

Tennis Court Bridge 2

NSC_012	52.83	1.8	53.07	2.8	53.23	3.8	53.39	5.0	53.50	7.1	53.59	9.3
NSC_013	52.83	1.8	53.07	2.8	53.23	3.8	53.38	5.0	53.50	7.1	53.58	9.3

NSC_014	52.85	1.8	53.09	2.8	53.25	3.9	53.42	4.9	53.56	6.1	53.67	8.0
Dunkirk Mills Bridge 1												
NSC_016	52.86	1.8	53.10	2.8	53.30	3.9	53.49	4.9	53.68	6.1	53.88	8.0
NSD_001	52.79	2.4	52.99	2.8	53.11	4.2	53.22	5.1	53.29	5.4	53.33	5.4
Dunkirk Mills Side Sluices												
NSC_018	55.52	1.8	55.64	2.8	55.75	3.9	55.85	4.9	55.96	6.1	56.12	8.0
NSD_002	53.10	2.4	53.28	2.8	53.48	4.2	53.65	5.1	53.72	5.4	53.76	5.4
NSD_003	53.19	2.4	53.32	2.8	53.54	4.1	53.71	5.1	53.77	5.4	53.80	5.4
NSD_004	53.28	2.4	53.40	2.8	53.61	4.1	53.77	5.1	53.83	5.3	53.85	5.4
NSD_005	53.36	2.4	53.46	2.8	53.67	4.1	53.82	5.1	53.88	5.3	53.90	5.4
Critchleye Bridge 5												
NSD_006	53.41	2.4	53.52	2.8	53.90	4.1	54.14	5.1	54.22	5.3	54.25	5.4
NSD_007	53.53	2.3	53.61	2.8	53.94	4.1	54.16	5.3	54.22	6.3	54.23	6.7
Tennis Court Bridge 1												
NSD_008	53.63	2.3	53.73	2.8	54.26	4.1	54.51	5.3	54.59	6.3	54.61	6.7
NSD_009	53.66	2.3	53.75	2.8	54.27	4.1	54.52	5.3	54.60	6.3	54.62	6.6
Elm Brook Bridge 1												
NSD_010	53.70	2.3	53.91	2.8	54.34	4.1	54.55	5.3	54.63	6.3	54.65	6.6
NSD_011	53.83	2.3	53.99	2.8	54.38	4.1	54.58	5.3	54.66	6.3	54.68	6.6
The Gables Bridge												
NSD_012	54.15	2.3	54.38	2.8	55.13	4.1	55.72	5.3	56.29	6.3	56.47	6.6
NSD_013	54.19	2.3	54.40	2.8	55.13	4.1	55.72	5.3	56.29	6.3	56.47	7.1
NSD_014	54.25	2.3	54.42	2.8	55.13	4.3	55.72	5.6	56.29	6.4	56.47	7.5
NSD_015	54.32	2.3	54.48	2.8	55.14	3.5	55.72	4.0	56.29	5.3	56.47	6.3
NSD_016	54.41	2.3	54.55	2.8	55.15	3.5	55.72	4.2	56.30	4.9	56.48	5.8

NSD_017	54.48	2.3	54.61	2.8	55.16	3.6	55.72	4.3	56.30	4.8	56.48	5.4
NSD_018	54.60	2.3	54.73	2.8	55.20	3.3	55.73	4.0	56.30	4.2	56.48	4.3

Filling Station Culvert

NSD_019	56.00	2.3	56.16	2.8	56.30	3.3	56.49	4.0	56.63	4.2	56.73	4.3
NSD_021	56.10	2.3	56.24	2.9	56.38	4.5	56.54	5.1	56.66	5.6	56.75	6.1

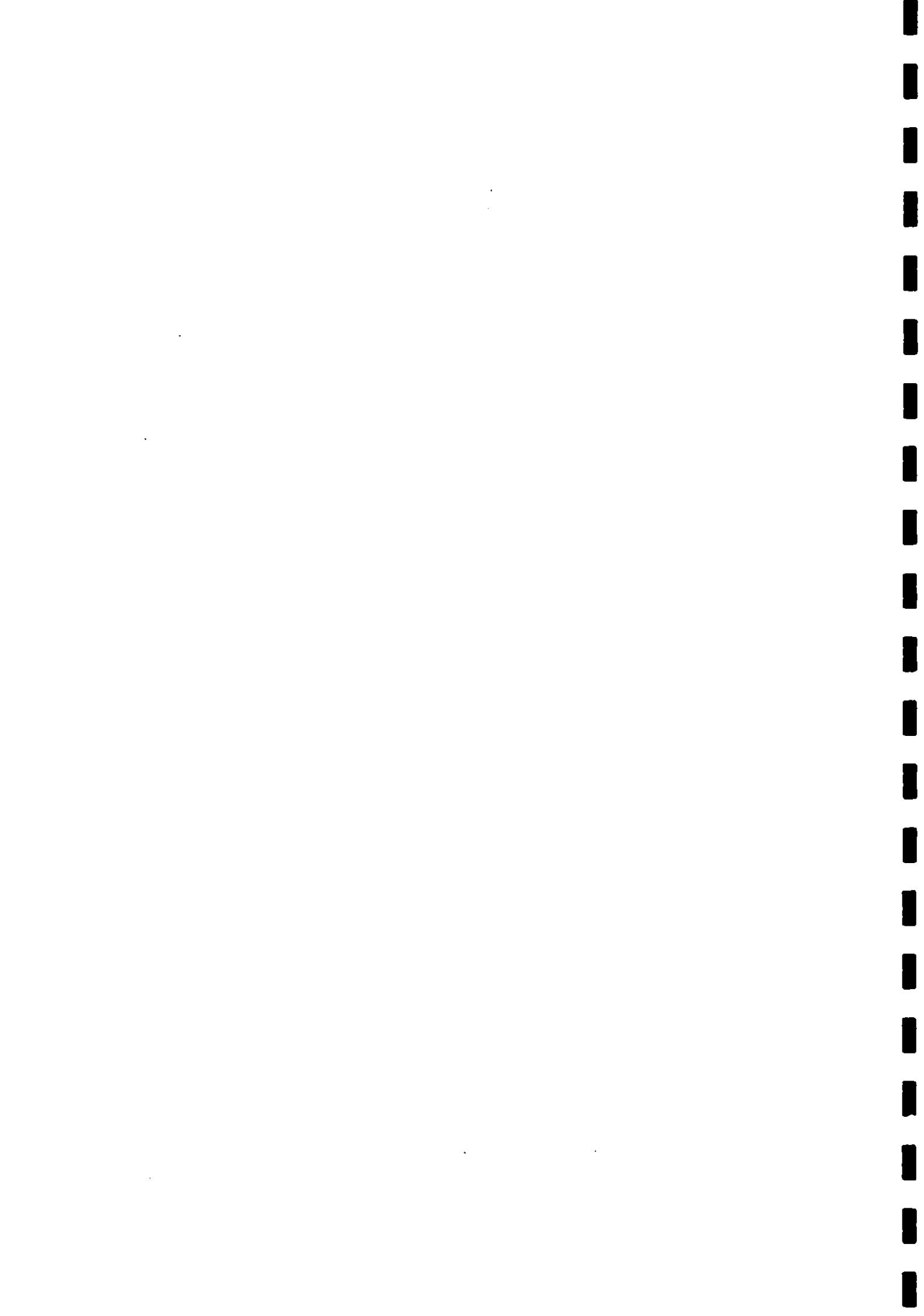
Junction with NSE_002

NSD_022	56.10	0.0	56.24	0.0	56.38	0.1	56.54	1.3	56.66	2.8	56.75	3.7
NSD_023	56.10	0.0	56.24	0.0	56.38	0.0	56.55	0.4	56.68	1.2	56.78	1.8
NSD_024	56.10	0.0	56.24	0.0	56.38	0.0	56.55	0.0	56.69	0.0	56.79	0.0
NSE_001	56.13	2.3	56.26	2.9	56.40	4.4	56.55	4.6	56.66	4.7	56.75	4.7
NSE_002	56.10	2.3	56.24	2.9	56.38	4.4	56.54	4.6	56.66	4.6	56.75	4.7

Model Cell	5 Year Event		10 Year Event		25 Year Event		50 Year Event		100 Year Event		150 Year Event	
	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)
Cell 201	35.50	0.00	35.50	0.00	35.50	0.00	35.82	0.32	36.08	0.58	36.38	0.88
Cell 202	54.00	0.00	54.40	0.40	55.13	1.13	55.72	1.72	56.29	2.29	56.47	2.47
Cell 203	55.06	0.06	55.29	0.29	55.63	0.63	55.74	0.74	56.30	1.30	56.48	1.48
Cell 204	55.07	0.07	55.29	0.29	55.84	0.84	55.99	0.99	56.31	1.31	56.49	1.49
Cell 205	55.50	0.25	55.62	0.36	56.32	1.07	56.53	1.28	56.65	1.40	56.74	1.49

Appendix 2

Properties at risk of flooding in the 100 year return period event



20 Industrial	379180	205250	1250	683	22.48	Door
19 Private	380270	204590	68	1382	22.93	D.P.C.
20 Private	380845	204585	70	1610	22.83	D.P.C.
20 Private	378400	205080	47	707	22.63	Door
20 Private	380180	204730	78	1412	22.68	D.P.C.
20 Private	380200	204720	75	1410	22.71	D.P.C.
20 Commercial	379270	205240	30	672	22.72	Door
20 Private	380160	204750	78	1415	22.73	D.P.C.
20 Private	380180	204740	78	1413	22.74	D.P.C.
20 Private	380170	204740	78	1414	22.74	D.P.C.
20 Private	380190	204580	95	1395	22.75	D.P.C.
20 Private	380210	204730	78	1411	22.75	D.P.C.
20 Private	380220	204710	73	1408	22.82	D.P.C.
20 Private	380200	204350	70	1000	22.86	Door
20 Private	380190	204320	180	1001	22.88	Door
20 Farm	378480	205830	275	759	22.87	Door
20 Private	380210	204710	78	1409	22.88	D.P.C.
20 Private	380230	204700	78	1407	22.89	D.P.C.
20 Private	380220	204650	432	1389	22.90	D.P.C.
20 Industrial	380240	204690	78	1405	23.18	D.P.C.
20 Private	378480	205820	275	760	23.01	Door
20 Farm	380150	204770	72	1417	23.10	D.P.C.
20 Private	380160	204760	72	1418	23.07	D.P.C.
20 Commercial	379300	205280	388	670	23.07	Door
20 Farm	378480	205720	225	761	23.08	Door
18 Old Peoples Home	378550	205720	200	783	23.11	Door
20 Private	380250	204680	78	1404	23.18	D.P.C.
20 Private	380160	204310	120	1002	23.18	Door
20 Private	380060	204650	114	1387	23.19	Door
20 Private	380145	204615	75	1412	23.22	Door
20 Private	380160	204310	102	1003	23.21	Door
20 Private	380270	204680	78	1402	23.28	D.P.C.
20 Private	380055	204625	60	1611	23.30	Door
20 Private	380260	204630	78	1405	23.31	D.P.C.
20 Private	380270	204660	78	1401	23.37	D.P.C.
20 Private	380280	204660	78	1400	23.39	D.P.C.
19 Private	380290	204610	78	1386	23.39	D.P.C.
19 Private	380200	204620	78	1397	23.39	D.P.C.
20 Private	380140	204780	72	1419	23.41	D.P.C.
20 Private	380150	204780	72	1418	23.42	D.P.C.
20 Commercial	380280	204700	102	1004	23.42	Door
20 Private	380290	204660	78	1390	23.48	Door
20 Private	380280	204660	78	1398	23.52	D.P.C.
20 Private	380290	204640	78	1399	23.54	D.P.C.
20 Private	380235	204735	50	1512	23.57	D.P.C.
20 Private	380245	204735	50	1513	23.59	D.P.C.
20 Private	380245	204750	50	1510	23.59	D.P.C.
20 Private	380215	204783	60	1520	23.60	D.P.C.
20 Private	380170	204290	102	1005	23.59	Door
20 Private	380315	204715	39	1527	23.60	D.P.C.
20 Private	380245	204745	50	1511	23.61	D.P.C.
20 Private	380435	204745	60	1478	23.62	D.P.C.
20 Private	380345	204725	45	1529	23.63	D.P.C.
20 Private	380320	204670	50	1454	23.66	D.P.C.
20 Private	380325	204735	50	1454	23.73	D.P.C.
20 Private	380325	204745	45	1534	23.86	D.P.C.
20 Private	380320	204650	40	1451	23.86	D.P.C.
20 Private	380325	204765	40	1452	23.77	D.P.C.
20 Private	380310	204670	50	1453	23.89	D.P.C.
20 Private	380315	204725	40	1450	23.74	D.P.C.
20 Private	380325	204725	45	1531	23.77	D.P.C.
20 Private	380325	204735	35	1535	23.75	D.P.C.
19 Old Peoples Home	380150	204800	78	1420	23.73	D.P.C.
20 Private	380375	204725	45	1532	23.76	D.P.C.
20 Private	380320	204630	40	1450	23.78	D.P.C.
20 Private	380110	204800	60	1421	23.78	D.P.C.
20 Private	380340	204680	50	1455	23.88	D.P.C.
20 Private	380235	204765	20	1509	23.88	D.P.C.
20 Private	380370	204680	35	1450	23.88	D.P.C.
20 Private	380370	204680	35	1450	23.88	D.P.C.

8 Wharfdale Way	Stanley Downton	Bridgend	20 Private	49 1168	24.78 D.P.C.
13 Crescent Close	(bam)	Bridgend	19 Private	380140 204330	152 1006 24.83 Door
Stanley Downton Farm	Stanley Downton	Bridgend	20 Private	380110 204330	100 1426 24.81 D.P.C.
Stanley Downton Farm (bam)	Stanley Downton	Bridgend	19 Private	380130 204360	250 1009 24.81 Door
22 Wharfdale Way	Upper Mts Industrial Estate	Bridgend	20 Private	380100 204340	35 1010 24.82 Door
CAS Jack Toolmaking		Bridgend	19 Industrial	380061 204690	84 1334 24.85 Door
15 Crescent Close	Bridgend	Bridgend	20 Private	38010 204840	100 1427 24.87 D.P.C.
2 Wharfdale Close	Bridgend	Bridgend	20 Private	380055 204745	42 1574 24.92 D.P.C.
1 Wharfdale Close	Bridgend	Bridgend	20 Private	380045 204745	42 1573 24.93 D.P.C.
3 Wharfdale Close	Bridgend	Bridgend	20 Private	380055 204745	42 1575 24.93 D.P.C.
19 Wharfdale Way	Bridgend	Bridgend	20 Private	380205 204795	49 1505 24.89 D.P.C.
5 Wharfdale Close	Bridgend	Bridgend	20 Private	380325 204745	48 1577 24.95 D.P.C.
4 Wharfdale Close	Bridgend	Bridgend	20 Private	380515 204745	48 1578 24.96 D.P.C.
37 Wharfdale Way	Bridgend	Bridgend	20 Private	380205 204785	49 1504 25.04 D.P.C.
22 Wharfdale Close	Bridgend	Bridgend	20 Private	380305 204785	42 1591 25.21 D.P.C.
8 Wharfdale Close	Bridgend	Bridgend	20 Private	380555 204745	42 1580 25.22 D.P.C.
23 Wharfdale Close	Bridgend	Bridgend	20 Private	380305 204785	42 1590 25.23 D.P.C.
6 Wharfdale Close	Bridgend	Bridgend	20 Private	380335 204745	48 1578 25.24 D.P.C.
7 Wharfdale Close	Bridgend	Bridgend	20 Private	380545 204745	63 1579 25.24 D.P.C.
9 Wharfdale Close	Bridgend	Bridgend	20 Private	380565 204745	42 1581 25.24 D.P.C.
Amcan	Upper Mts Industrial Estate	Bridgend	19 Industrial	380430 204690	143 1336 25.29 Door
14 Wharfdale Way	Stanley Downton	Bridgend	20 Private	380405 204815	42 1571 25.31 D.P.C.
Stanley Downton	Bridgend	Bridgend	19 Private	380110 204320	200 1008 25.32 Door
11 Wharfdale Close	Bridgend	Bridgend	20 Private	380545 204745	54 1583 25.38 D.P.C.
10 Wharfdale Close	Bridgend	Bridgend	20 Private	380575 204745	42 1582 25.39 D.P.C.
4 Fleuce Cottage	Stanley Downton	Bridgend	20 Private	380090 204210	40 1012 25.42 Door
King Stanley	King Stanley	Bridgend	20 Private	381155 204355	80 1184 25.42 Door
Stanley Downton	Stanley Downton	Bridgend	20 Private	380090 204230	72 1015 25.45 D.P.C.
Bridgeend	Stanley Downton	Bridgend	20 Private	380095 204855	42 1580 25.47 D.P.C.
16 Wharfdale Way	Stanley Downton	Bridgend	20 Private	380090 204220	77 1013 25.48 Door
2 Fleuce Cottage	Bridgend	Bridgend	20 Private	380090 204220	40 1014 25.48 Door
21 Wharfdale Way	Bridgend	Bridgend	20 Private	380275 204805	42 1494 25.49 D.P.C.
23 Wharfdale Way	Bridgend	Bridgend	20 Private	380265 204805	42 1495 25.49 D.P.C.
Concord Vehicles Ltd	Upper Mts Industrial Estate	Bridgend	20 Industrial	380060 204730	375 1338 25.53 Door
19 Stanley Mts Cottages	King Stanley	Bridgend	18 Private	380115 204345	83 1183 25.522 Door
Concord Vehicles Ltd	Upper Mts Industrial Estate	Bridgend	20 Private	380355 204825	42 1560 25.53 D.P.C.
Concord Vehicles Ltd	Vakas Ltd	Bridgend	20 Industrial	380060 204710	130 1340 25.53 Door
18 Wharfdale Close	Upper Mts Industrial Estate	Bridgend	20 Industrial	380545 204775	65 1588 25.6 D.P.C.
17 Wharfdale Close	Bridgend	Bridgend	20 Private	380525 204785	50 1586 26.61 D.P.C.
Amcan Ltd	Upper Mts Industrial Estate	Bridgend	20 Industrial	380565 204845	50 1586 26.61 D.P.C.
3 Nothe Ark	King Stanley	Bridgend	19 Private	380690 204690	1175 1341 25.54 D.P.C.
2 The Limes	King Stanley	Bridgend	19 Private	380205 204730	375 1337 25.57 Door
17 Stanley Mts Cottages	King Stanley	Bridgend	18 Private	381155 204355	48 1785 25.57 Door
Wayne Precision Engineering	Upper Mts Industrial Estate	Bridgend	19 Industrial	380040 204710	150 1335 25.57 Door
Concord Vehicles Ltd	Upper Mts Industrial Estate	Bridgend	20 Industrial	380070 204740	391 1339 25.59 Door
18 Wharfdale Close	Bridgend	Bridgend	20 Private	380545 204785	48 1787 25.65 Door
17 Wharfdale Close	Bridgend	Bridgend	20 Private	381115 204465	58 1788 25.65 Door
1 Nothe Ark	Upper Mts Industrial Estate	Bridgend	19 Private	381155 204465	58 1781 25.7 Door
Mad Industrial Vehicles	King Stanley	Bridgend	19 Industrial	380690 204690	1175 1341 25.61 Door
34 Wharfdale Way	King Stanley	Bridgend	19 Private	381315 204475	47 1582 25.76 D.P.C.
30 Wharfdale Way	King Stanley	Bridgend	19 Private	381285 204435	70 1785 25.83 Door
Stanley Cottage	King Stanley	Bridgend	19 Private	381165 204385	48 1788 25.83 Door
27 Wharfdale Way	King Stanley	Bridgend	18 Private	380245 204905	42 1497 25.79 D.P.C.
25 Wharfdale Way	Bonds Estate	Bridgend	20 Disused	378200 205250	140 0865 25.82 Door
Empty Building	T	Bridgend	19 Industrial	380061 204700	150 1323 25.84 Door
C Tools & Estate office	U M I E	Bridgend	20 Private	380315 204825	42 1535 25.86 D.P.C.
1 Nothe Ark	Bridgend	Bridgend	20 Private	380325 204925	42 1557 25.88 D.P.C.
46 Wharfdale Way	Bridgend	Bridgend	20 Private	380395 204835	42 1569 25.91 D.P.C.
44 Wharfdale Way	Bridgend	Bridgend	20 Private	380110 204860	100 1423 25.92 D.P.C.
42 Wharfdale Way	Bridgend	Bridgend	20 Private	380565 204785	42 1587 25.95 D.P.C.
18 Wharfdale Way	Bridgend	Bridgend	20 Private	380515 204813	58 1590 25.95 D.P.C.
14 Wharfdale Close	Bridgend	Bridgend	20 Private	380515 204813	58 1592 25.95 D.P.C.
2 Crescent Close	Bridgend	Bridgend	20 Private	379250 205260	375 865 25.95 Door
19 Crescent Close	Bridgend	Bridgend	20 Private	380575 204785	42 1586 25.96 D.P.C.
4 Crescent Close	Bridgend	Bridgend	20 Private	380160 204830	60 1423 25.98 D.P.C.
50 Wharfdale Way	Bridgend	Bridgend	20 Private	380295 204835	42 1553 26.04 D.P.C.
48 Wharfdale Way	Bridgend	Bridgend	20 Private	380140 204850	70 1503 26.15 D.P.C.
50 Wharfdale Way	Riola	Bridgend	20 Industrial	380720 204710	749 1343 26.17 D.P.C.
Upper Mts Industrial Estate					

6 Court Farm Mews	Stonehouse	Stroud	Stanley Downton	19 Private	723	28.44	Door
6 Books Drive	Ravenhill Cottages	Stroud	Private	380153	204955	45	29.98 D.P.C.
10 Books Drive	Spring Cottages	Stroud	Private	380040	204210	285	20.17 29.99 D.P.C.
6 Books Drive	Bloomfield House	Stroud	Private	380155	204985	32	28.99 D.P.C.
5 Spring Cottages	Ebley	Ryleford	Private	380165	205055	40	28.99 D.P.C.
4 Spring Cottages	Ryleford	Ryleford	Private	3801345	204585	32	30.01 Door
3 Spring Cottages	Ryleford	Ryleford	Private	381345	204605	32	18.13 30.03 Door
2 Spring Cottages	Plot 17	Books Drive	Private	380155	204605	22	18.14 30.04 Door
Stonehouse Court Hotel	Plot 16	Books Drive	Private	380215	204965	58	30.05 Door
Urbannen Address	Ebley	Stroud	Empty	380315	204985	55	30.25 D.P.C.
Berian Construction Ltd	Books Drive	Stroud	Commercial	380700	204800	100	1349 30.06 Door
Arthur Smiths	Ebley	Stroud	Commercial	382320	204530	50	30.29 Door
Plot 21 Books Drive	Books Drive	Stroud	Commercial	380245	204985	469	30.33 Door
Plot 17	Stonehouse	Stroud	Commercial	382340	204580	100	30.37 D.P.C.
Frogmiree Compaq	Court Garden	Stroud	Private	378470	205110	131	613 30.38 Door
7 Barlow Close	Stroud	Stroud	Private	380095	205045	72	1720 30.56 D.P.C.
Stroudwater Cottage	Stroud	Stroud	Private	378870	205170	62	30.57 Door
Berian Construction Ltd	Books Drive	Stroud	Commercial	382340	204520	75	620 30.58 Door
Broadfield	Ebley	Stroud	Private	382340	204580	62	614 30.59 Door
Ryleford (offices)	Ryleford	Stroud	Commercial	381325	204555	30	1811 30.6 Door
Stonehouse	Stroud	Stroud	Private	378980	205180	100	730 30.68 Door
11 Barlow Close	Stroud	Stroud	Empty	380125	205035	90	30.61 D.P.C.
1 Barlow Close	Stroud	Stroud	Private	380410	204910	75	1763 30.61 Door
17 Barlow Close	Stroud	Stroud	Private	380045	205085	72	1727 30.64 D.P.C.
Plot 18	Books Drive	Stroud	Private	380223	205005	80	1743 30.69 D.P.C.
Unknown Address	Books Drive	Stroud	Private	380225	205005	98	1742 30.7 D.P.C.
1 Barlow Close	Stroud	Stroud	Empty	380870	204810	64	1348 30.72 D.P.C.
Barri	Stroud	Stroud	Commercial	380115	205045	72	1717 30.73 D.P.C.
Address's Unknown	Books Drive	Stroud	Private	380750	204510	150	731 30.73 Door
5 Barlow Close	Ebley	Stroud	Private	378890	205120	187	732 30.74 Door
Water Edge	Stroud	Stroud	Private	380115	205035	70	1719 30.75 D.P.C.
Stonehouse Court Hotel	Stroud	Stroud	Private	382480	204550	112	612 30.75 Door
2 Barlow Close	Ryleford	Stroud	Hold N	378950	205090	300	738 30.76 Door
Westward Motions	Ebley	Stroud	Private	380115	205075	80	1723 30.76 D.P.C.
4 Books Drive	Stroud	Stroud	Commercial	382750	204550	47	615 30.78 Door
1 Barlow Close	Stroud	Stroud	Private	380145	205025	65	1715 30.81 D.P.C.
Court Larena	Stroud	Stroud	Private	380135	205025	85	1718 30.81 D.P.C.
Plot 2 Barlow Close (Show Home)	Plotting Cottage	Stroud	Private	378970	205090	169	734 31.03 D.P.C.
15 Barlow Close	Ebley	Stroud	Private	380155	205085	72	1728 30.84 D.P.C.
Canal Cottage	Ryleford	Stroud	Private	381455	204635	60	1842 31.03 Door
Westward Motions	Ryleford	Stroud	Private	380075	205075	205115	72 1729 31.06 D.P.C.
9 Barlow Close	Ebley	Stroud	Private	380665	205095	72	1728 31.07 D.P.C.
4 Books Drive	Stroud	Stroud	Private	380075	205095	85	1722 31.08 D.P.C.
1 Barlow Close	Stroud	Stroud	Private	380075	205105	72	1731 31.11 Door
Plot 1 Barlow Close	Stroud	Stroud	Private	380075	205105	94	1840 31.11 Door
Plot 2 Barlow Close	Ebley	Stroud	Private	380665	205095	63	1843 31.12 D.P.C.
12 Barlow Close	Ryleford	Stroud	Private	380105	205095	72	1735 31.12 D.P.C.
13 Barlow Close	Ryleford	Stroud	Private	382910	204610	1881	565 31.12 D.P.C.
14 Barlow Close	Ebley	Stroud	Private	382910	204610	75	610 31.12 D.P.C.
1 Ryeford house	Stroud	Stroud	Private	380105	205075	72	1724 31.12 D.P.C.
1 Canal Side Cottage	Ebley	Stroud	Private	382600	204570	37	621 31.15 Door
1 Holly Tree Garden	Ryleford	Stroud	Private	380085	205085	72	1730 31.41 D.P.C.
Plot 6 Barlow Close: Stroud	Ebley	Stroud	Private	382540	204610	75	609 32.44 D.P.C.
6 Barlow Close: Stroud	Ebley	Stroud	Private	380115	205105	72	1734 32.549 D.P.C.
3 Holly Tree Garden	Stroud	Stroud	Private	382910	204670	225	555 32.61 D.P.C.
1 Holly Tree Garden	Ebley	Stroud	Private	382910	204520	56	556 32.69 D.P.C.
16 Barlow Close	Stroud	Stroud	Private	382910	204870	137	534 32.71 D.P.C.
17 Barlow Close	Ebley	Stroud	Commercial	382960	204630	475	556 32.8 Door
1 Holly Tree Garden	Stroud	Stroud	Commercial	382960	204630	475	556 32.8 Door

Mazda Motor House	Stroud
Mazda Motor House	Stroud
1 Gladstone Gardens	Durdidge
5 Gladstone Gardens	Durdidge
4 Gladstone Gardens	Durdidge
2 Gladstone Gardens	Durdidge
7 Gladstone Gardens	Durdidge
8 Gladstone Gardens	Durdidge
Grenavay	Ebley
3 Gladstone Gardens	Durdidge
10 Gladstone Gardens	Durdidge
Greenvale	Stroud
Tarnwood Building Supplies	Ebley
Holly Tree House	Stroud
11 Gladstone Gardens	Ebley
Stroud Plant Hire	Stroud
Hoopers of Ebley	Stroud
32 Frome Gardens	Stroud
33 Frome Gardens	Stroud
7 Frome Gardens	Stroud
Bridge Road Motors	Stroud
2 Frome Gardens	Stroud
3 Frome Gardens	Stroud
Stroud Plant Hire	Stroud
30 Frome Gardens	Stroud
4 Frome Gardens	Stroud
1 Baytree Compta	Stroud
6 Frome Gardens	Stroud
8 Frome Gardens	Stroud
1 Baytree House	Flyadro
Ebley Training School	Stroud
34 Frome Gardens	Stroud
5 Frome Gardens	Stroud
1 Frome Graders	Stroud
2 Baytree House	Durdidge
The Bunglow	Stroud
2 Baytree Cottage	Stroud
Vale House	Stroud
Ebley Coach Services	Durdidge
187 Westward Road	Ebley
Kennedy's garden Center	Stroud
Rutter	Durdidge
Ebley Coach Services	Durdidge
9 Frome Gardens	Stroud
Frome Graders	Durdidge
1 Jay Bee Plant Sales Ltd	Ebley
Lower Durdidge House	Stroud
Autosport	Ebley
Stroud Plant Hire	Stroud
26 Frome Gardens	Stroud
Rutter	Stroud
Mars Enterprise	Durdidge
33 Frome Gardens	Stroud
Lews & Hite	Durdidge
29 Frome Gardens	Stroud
Jay Bee Plant Sales Ltd	Ebley
305 Westward Road	Durdidge
Kannara Mill Cottage	Stroud
4 Park View	Stroud
11 Frome Gardens	Stroud
Reiter	Ebley
10 Frome Gardens	Stroud
Mede Motor House	Stroud
Reiter	Durdidge
213 Westward Road	Ebley
11 Bridge-Side	Stroud
1 Gladiators	Ebley
10 Bridge Side	Stroud
Cotswold Owl	Ebley
9 Bridge-Side	Stroud
12 Bridge-Side	Stroud
13 Bridge-Side	Stroud
3 Gladstone	Ebley
303 Westward Road	Stroud
2 Gladstone	Ebley
Stroud Mail Co	Lis
Jay Bee Plant Sales Ltd	Ebley
Stroud Metal Co	Lis

382920 204700 1044 552 32.81 Door	
382900 204700 131 561 32.87 Door	
19 Private	Stroud
20 Commercial	Stroud
382940 204800 71 1238 32.95 Door	
382920 204760 42 1236 32.96 Door	
382940 204760 100 1237 32.98 Door	
382940 204760 71 1239 32.97 Door	
382920 204760 32 1235 33.02 Door	
382940 204760 47 1234 33.03 Door	
382930 204660 344 563 33.05 Door	
382940 204790 50 1240 33.18 Door	
382950 204360 90 1242 33.19 Door	
382910 204650 562 557 33.23 Door	
382920 204660 87 604 33.27 Door	
18 Private	Stroud
19 Private	Stroud
20 Commercial	Stroud
382940 204650 125 611 33.33 D.P.C.	
19 Private	Stroud
20 Commercial	Stroud
382910 204810 150 1101 33.35 Door	
20 Private	Stroud
382900 204790 60 1304 33.38 D.P.C.	
20 Private	Stroud
382950 204690 66 1305 33.39 D.P.C.	
20 Private	Stroud
382910 204770 40 1241 33.32 Door	
382930 204650 112 603 33.43 Door	
382940 204750 54 1274 33.45 D.P.C.	
382920 204780 62 631 33.47 D.P.C.	
382940 204800 119 1102 33.48 Door	
382980 204700 78 1302 1251 D.P.C.	
20 Private	Stroud
382960 204790 68 1278 33.52 D.P.C.	
19 Ancty	Stroud
20 Private	Stroud
20 Private	Stroud
382940 204770 54 1278 33.54 D.P.C.	
19 Emcy	Stroud
20 Commercial	Stroud
382980 204690 45 1248 33.56 Door	
20 Private	Stroud
382900 204690 225 558 33.57 Door	
20 Private	Stroud
382950 204790 72 1306 33.59 D.P.C.	
20 Private	Stroud
382920 204790 68 1277 33.61 D.P.C.	
19 Empt	Stroud
20 Private	Stroud
382940 204690 100 1245 33.62 Door	
382940 204690 78 1844 33.63 Door	
382980 204690 21 1242 33.64 Door	
382940 204690 40 1247 33.63 Door	
382950 204670 60 1281 33.64 D.P.C.	
20 Commercial	Stroud
382940 204690 62 582 33.71 Door	
20 Commercial	Stroud
382940 204735 250 1839 33.72 Door	
20 Commercial	Stroud
382940 204700 200 1097 33.73 Door	
382940 204620 62 580 33.76 Door	
382950 204530 2100 1229 33.79 Door	
382940 204670 72 1246 33.80 D.P.C.	
20 Commercial	Stroud
382940 204790 68 1273 33.88 D.P.C.	
382940 204670 94 1271 33.94 Door	
382950 204535 1221 2221 33.96 Window	
382980 204790 204 1097 33.97 Door	
382910 204700 537 623 34.07 Door	
382950 204690 261 1098 33.98 Door	
382950 204700 54 1200 33.99 Door	
383020 204760 60 1281 33.99 D.P.C.	
20 Industrial	Stroud
382920 204760 68 1280 33.99 D.P.C.	
382950 204670 66 1280 33.99 D.P.C.	
20 Industrial	Stroud
382940 204690 62 582 34.12 Door	
19 Private	Stroud
20 Industrial	Stroud
382940 204670 98 1307 34.12 D.P.C.	
19 Private	Stroud
382950 204730 2270 1233 34.13 Door	
20 Industrial	Stroud
382940 204700 54 1301 34.14 D.P.C.	
20 Industrial	Stroud
382970 204670 537 623 34.17 Door	
20 Industrial	Stroud
382940 204670 57 623 34.18 D.P.C.	
20 Industrial	Stroud
382940 204700 86 1085 34.19 D.P.C.	
19 Private	Stroud
382910 204790 60 1283 34.20 Door	
382940 204690 72 1084 34.21 D.P.C.	
20 Industrial	Stroud
382940 204670 62 600 34.22 Door	
20 Industrial	Stroud
382940 204690 78 1085 34.23 D.P.C.	
20 Industrial	Stroud
382940 204700 68 1282 34.24 Door	
382950 204700 86 1085 34.25 D.P.C.	
19 Private	Stroud
382940 204700 37 578 34.26 Door	
382940 204690 72 1084 34.27 D.P.C.	
19 Private	Stroud
382920 204790 62 600 34.28 Door	
382950 204690 70 1085 34.29 D.P.C.	
20 Private	Stroud
382940 204670 36 628 34.30 D.P.C.	
20 Private	Stroud
382940 204670 38 1067 34.31 D.P.C.	
19 Private	Stroud
382940 204690 62 601 34.33 D.P.C.	
20 Industrial	Stroud
382910 204790 2623 1980 34.34 D.P.C.	
20 Commercial	Stroud
382920 204650 225 624 34.35 D.P.C.	
20 Industrial	Stroud
382910 204760 600 1081 34.37 D.P.C.	

PROF

PROF

PROF

Wyndale Junior School
 40 Stanley View
 38 Stanley View
 209 Washward Road
 1 Stanley View
 5-8 The Grove
 3 Stanley View
 Enviro Technology
 68 Stanley View
 44 Stanley View
 34 Durdidge Meadow
 22 Durdidge Meadow
 3 Meadow End
 32 Durdidge Meadow
 24 Durdidge Meadow
 28 Durdidge Meadow
 28 Durdidge Meadow
 42 Stanley View
 B-12 The Grove
 20 Durdidge Meadow
 30 Durdidge Meadow
 44 Stanley View
 62 Stanley View
 58 Stanley View
 64 Durdidge Meadow
 60 Stanley View
 19 Durdidge Meadow
 36-42 (flats) Durdidge Meadow
 44-50 (flats) Durdidge Meadow
 52 Stanley View
 17 Durdidge Meadow
 5 Stanley View
 310 Washward Road
 48 Stanley View
 54 Stanley View
 50 Stanley View
 48 Stanley View
 6 Stanley View
 8 Stanley View
 36 Stanley View
 41 Stanley View
 32 Stanley View
 Enviro Technology (garages)
 34 Stanley View
 43 Stanley View
 8 Durdidge Meadow
 30 Stanley View
 41 Stanley View
 11 Durdidge Meadow
 Building under construction
 2 Stanley View
 43 Stanley View
 39 Stanley View
 4 Stanley View
 17 Stanley View
 45 Stanley View
 14 Stanley View
 18 Stanley View
 15 Stanley View
 Tanwood Building Supplies
 13 Durdidge Meadow
 18 Stanley View
 22 Stanley View
 7 Durdidge Meadow
 5 Durdidge Meadow
 24 Stanley View
 13 Durdidge Meadow
 18 Stanley View
 26 Stanley View
 20 Stanley View
 10 Stanley View
 15 Durdidge Meadow
 26 Stanley View
 Rhionne
 11 Stanley View
 13 Stanley View
 9 Stanley View
 35 Stanley View
 37 Stanley View
 7 Stanley View
 27 Stanley View

19 School	900	1832	35.88	Door		
20 Private	385710	204360	35	1158	35.95	D.P.C.
20 Private	383710	204370	40	1155	35.98	D.P.C.
19 Private	382180	204730	58	579	35.98	Door
20 Private	383630	204410	35	1135	35.97	D.P.C.
20 Private	382540	204710	109	598	35.945	Door
20 Private	383630	204410	35	1136	35.99	D.P.C.
20 Private	383630	204460	198	1072	35.99	Door
20 Private	383720	204350	35	1157	36	D.P.C.
20 Private	383720	204360	35	1158	36	D.P.C.
20 Private	383630	204460	30	1124	36.02	D.P.C.
20 Private	383630	204490	40	1123	36.03	D.P.C.
20 Private	383630	204500	45	1256	36.006	D.P.C.
20 Private	3832370	204450	35	1156	36.01	Door
20 Private	383630	204460	28	1126	36.02	D.P.C.
20 Private	383630	204490	110	1122	36.02	D.P.C.
20 Private	383560	204480	35	1158	36.06	D.P.C.
20 Private	383710	204340	40	1159	36.07	D.P.C.
20 Private	383710	204350	35	1161	36.11	D.P.C.
20 Private	383350	204450	40	1159	36.03	D.P.C.
20 Private	383710	204700	109	598	36.03	Door
20 Private	383560	204500	40	1120	36.04	D.P.C.
20 Private	383640	204480	40	1125	36.04	D.P.C.
20 Private	383630	204350	35	1158	36.09	D.P.C.
20 Private	383160	204440	110	1182	36.09	D.P.C.
20 Private	383710	204440	110	1183	36	D.P.C.
20 Private	383630	204330	35	1164	36.11	D.P.C.
20 Private	383630	204420	35	1194	36.08	D.P.C.
20 Private	383710	204390	35	1160	36.06	D.P.C.
20 Private	383410	204420	35	1195	36.17	D.P.C.
20 Private	383670	204340	35	1168	36.14	D.P.C.
20 Private	383700	204320	35	1162	36.14	D.P.C.
20 Private	383680	204330	35	1165	36.14	D.P.C.
20 Private	383670	204350	40	1167	36.15	D.P.C.
20 Private	383150	204400	25	1186	36.15	D.P.C.
20 Private	383710	204670	47	626	36.11	Door
20 Private	382390	204670	35	1155	36.11	Door
20 Private	383450	204400	110	1182	36.09	D.P.C.
20 Private	383670	204440	110	1183	36.09	D.P.C.
20 Private	383620	204340	35	1168	36.14	D.P.C.
20 Private	383700	204320	35	1173	36.19	D.P.C.
20 Private	383680	204330	35	1174	36.19	D.P.C.
20 Private	383670	204370	40	1170	36.23	D.P.C.
20 Private	383670	204320	40	1163	36.18	D.P.C.
20 Private	383650	204420	35	1157	36.26	D.P.C.
20 Private	383670	204400	40	1187	36.15	D.P.C.
20 Private	383580	204370	45	1176	36.17	D.P.C.
20 Private	383680	204360	35	1173	36.19	D.P.C.
20 Private	383670	204370	40	1169	36.23	D.P.C.
26 Empty	383150	204420	98	1205	36.24	D.P.C.
20 Private	383570	204400	40	1170	36.25	D.P.C.
20 Private	383700	204320	40	1163	36.18	D.P.C.
20 Private	383650	204420	35	1157	36.18	D.P.C.
20 Private	383670	204420	35	1157	36.19	D.P.C.
20 Private	383670	204470	35	1171	36.26	D.P.C.
20 Private	383710	204440	50	1142	36.27	D.P.C.
20 Private	383740	204370	48	1154	36.22	D.P.C.
20 Private	383620	204420	35	1163	36.3	D.P.C.
20 Private	383630	204390	35	1181	36.28	D.P.C.
20 Private	383710	204420	50	1143	36.28	D.P.C.
19 Commercial	383730	204390	35	1151	36.31	D.P.C.
20 Private	383870	204400	35	1171	36.32	D.P.C.
20 Private	383710	204440	50	1142	36.31	D.P.C.
20 Private	383730	204390	40	1155	36.32	D.P.C.
20 Private	383680	204430	35	1179	36.32	D.P.C.
20 Private	383650	204410	45	1180	36.33	D.P.C.
20 Private	383680	204420	35	1181	36.33	D.P.C.
20 Private	383640	204420	35	1191	36.37	D.P.C.
19 Private	383650	204370	40	1177	36.33	D.P.C.
20 Private	383410	204500	40	1131	36.34	Door
20 Private	383620	204420	40	1182	36.35	D.P.C.
20 Private	383560	204370	35	1178	36.35	D.P.C.
20 Private	383720	204430	40	1140	36.36	D.P.C.
20 Private	383720	204410	40	1139	36.36	D.P.C.
20 Private	383750	204390	40	1150	36.38	D.P.C.
20 Private	383750	204390	35	1138	36.39	D.P.C.
20 Private	383740	204430	50	1145	36.42	D.P.C.

29 Stanley View	Stroud	20 Private	383486	204460	40	1129	36.44	D.P.C.	
4 Durdidge Meadow	Stroud	20 Private	383486	204460	35	1130	36.44	D.P.C.	
2 Durdidge Meadow	Stroud	20 Disused	384050	204970	618	449	36.51	Door	
Empty Warehouse	Stroud	20 Private	385350	204450	35	1203	36.51	D.P.C.	
66 Durdidge Meadow	Stroud	20 Private	385340	204440	35	1204	36.52	D.P.C.	
68 Durdidge Meadow	Stroud	20 Private	3853670	204470	55	1128	36.53	D.P.C.	
6 Durdidge Meadow	Stroud	20 Private	3853750	204410	45	1148	36.54	D.P.C.	
35 Stanley View	Stroud	20 Private	3853860	204460	40	1132	36.54	D.P.C.	
1 Durdidge Meadow	Stroud	20 Private	3853750	204410	45	1147	36.56	Door	
1 Durdidge Meadow	A Whelan/Henward	20 Private	385700	204430	50	1131	36.56	D.P.C.	
Riveter & Coche Ltd/Copy shop/C	Riveter	19 Commercial	384160	204900	1360	463	36.56	Door	
Wayside	Durdidge	19 Private	3853500	204830	144	1080	36.57	Door	
14 Durdidge Meadow	Stroud	20 Private	3853410	204510	60	1232	36.61	D.P.C.	
19-25 Stanley View (flats)	Stroud	20 Private	3853486	204460	40	1117	36.63	D.P.C.	
12 Durdidge Meadow	Stroud	20 Private	3853730	204450	103	1144	36.63	D.P.C.	
10 Durdidge Meadow	Stroud	20 Private	3853680	204460	40	1118	36.64	D.P.C.	
18 Durdidge Meadow	Stroud	20 Private	3853700	204460	28	1115	36.64	D.P.C.	
The M.J Shop	Stroud	20 Industrial	385670	204500	40	1119	36.65	D.P.C.	
16 Durdidge Meadow	Stroud	20 Industrial	384110	204940	200	458	36.65	Door	
8 Durdidge Meadow	Stroud	20 Industrial	3853680	204500	35	1118	36.65	D.P.C.	
Frome Hall Lodge	Stroud	20 Private	385700	204480	21	1114	36.65	D.P.C.	
Empty	Stroud	19 Private	384200	204960	80	482	36.69	Door	
L	B Bently Fibres Ltd	Stroud	19 Private	384120	204930	1340	487	36.7	Door
Sewem Instruments Ltd	Stroud	19 Industrial	384160	204900	682	484	36.72	Door	
235a Westward Road (children's home) Ebley	Stroud	20 Industrial	384170	204900	360	485	36.74	Door	
Mount Pleasant	Stroud	20 Industrial	384140	204880	548	486	36.76	Door	
Winterbottom	Stroud	19 children's home	382780	204730	175	580	36.85	Door	
Maison Decor	Durdidge	20 Private	380010	204770	158	1018	37	Door	
Winterbottom	Stroud	19 Industrial	384340	205000	752	458	37.05	Door	
Stone Meadow Lane	Stroud	20 Commercial	382440	204460	300	1230	37.07	Door	
Wyedale Junior School	Ebley	20 Industrial	384380	204900	120	455	37.2	Door	
3 Lodgemore Cottages	Stroud	20 Industrial	384270	204990	600	481	37.22	Door	
2 Lodgemore Cottages	Stroud	20 Industrial	386350	204520	42	1248	37.23	Door	
Winterbottom	Stroud	20 Store	381445	204895	260	1825	37.27	Door	
Stone Meadow Lane	Stroud	20 School	384320	205020	9	459	37.29	Door	
Wyedale Junior School	Ebley	20 Private	384300	205020	60	458	37.35	Door	
1 Lodgemore Cottage	Stroud	20 Industrial	384340	205020	35	1207	37.32	Door	
Kimbale	Stroud	20 Private	382600	204730	180	437	37.33	Door	
1 Blue Row	Stroud	20 Private	383150	204800	49	1068	37.34	Door	
Treganite	Stroud	19 Private	383170	204530	135	2043	37.35	Door	
323 Westward Road	Ebley	20 Private	383250	204530	135	1253	37.44	D.P.C.	
Lawn Cottage	Stroud	20 Private	382350	204970	61	637	37.49	Door	
2 Blue Row	Stroud	20 Private	383150	204800	19	1068	37.55	Door	
Dolphin Mundy Sunsets Ltd	Ebley	19 Private	382610	204520	35	1250	37.6	Door	
Woodbeckens	Stroud	20 Industrial	382600	204730	275	584	37.64	Door	
25 Westward Road	Ebley	20 Private	382100	204890	50	656	37.74	Door	
3 Blue Row	Stroud	19 Private	382350	204870	94	638	37.78	D.P.C.	
The Western Pattern Making Co	Ebley	19 Private	385310	204520	35	1251	37.83	Door	
31 Durdidge Meadow	Stroud	20 Industrial	382160	204720	262	585	37.84	Door	
4 Blue Row	Stroud	20 Empty	383500	204400	35	1207	37.85	D.P.C.	
Martoe	Ebley Rd	19 Private	382310	204510	55	1222	37.87	Door	
Buckhurst	Ebley Rd	20 Private	381193	204885	90	1843	37.92	Door	
Wyedale Junior School	Ebley Rd	20 Private	381535	204835	90	1846	37.96	Door	
281 Westward Road	Ryleford	20 School	381425	204735	130	1837	38.02	Door	
Wyedale Junior School	Ebley	20 Hair salon	382160	204740	150	593	38.04	Door	
Chapel Cottage	Stroud	20 School	381435	204725	210	1838	38.08	Door	
75-81 (flats) Durdidge Meadow	Stroud	20 Private	380310	205050	56	533	38.12	Door	
13-19 (flats) Durdidge Meadow	Stroud	20 Private	382000	204890	240	682	38.23	C.F.	
25-41 (flats) Durdidge Meadow	Stroud	20 Private	382350	204370	117	1211	38.32	D.P.C.	
51-61 (flats) Durdidge Meadow	Stroud	20 Private	383550	204360	117	1210	38.35	D.P.C.	
Orchardton	Ebley Rd	20 Private	384310	204360	35	1206	38.37	D.P.C.	
Whitelocken	Ebley Rd	20 Private	381545	204350	117	1213	38.37	D.P.C.	
Whiteford	Ebley Rd	20 Offices	381585	204845	70	1847	38.37	Door	
19 Industrial	Stroud	20 Private	381585	204885	117	1214	38.37	D.P.C.	
28 Westward Road	Ryleford	20 Private	384530	205040	440	452	38.43	Door	
25 Westward Road	Ebley Rd	20 Private	382120	204680	50	654	38.44	Door	
5 Ebley Rd	Ebley	19 children's home	3811825	204635	80	1853	38.47	Door	
Seven Trent Water Depot	Ebley Rd	20 Private	381605	204695	60	1850	38.47	Door	
63-73 (flats) Durdidge Meadow	Ebley	20 Private	384770	205040	50	434	38.51	Door	
Westward Road	Stroud	20 Above	382130	204690	50	653	38.71	Door	
21 Westward Road	Ebley	20 Private	382080	204680	50	659	38.73	Door	

F	Town	Stroud
Vakosa	Stroud	Stroud
20 Bridge Street	Stroud	Stroud
19 Bridge Street	Stroud	Stroud
127 Westward Road	Stroud	Stroud
11 Fort View Terrace	Stroud	Stroud
12 Fort View Terrace	Stroud	Stroud
10 Fort View Terrace	Stroud	Stroud
9 Fort View Terrace	Stroud	Stroud
6 Fort View Terrace	Stroud	Stroud
7 Fort View Terrace	Stroud	Stroud
125 Westward Road	Stroud	Stroud
Coleverne	Chestnut Lane	Stroud
4 Port View Terrace	Stroud	Stroud
18 Bridge Street	Stroud	Stroud
3 Port View Terrace	Stroud	Stroud
1 Port View Terrace	Stroud	Stroud
Springfield Cottage	Stroud	Stroud
1A Port View Terrace	Stroud	Stroud
H & L Motors	Stroud	Stroud
Lodgemore House	Stroud	Stroud
Address Unknown	Stroud	Stroud
139 Calmcross Road	Stroud	Stroud
Railtown Products	Stroud	Stroud
1A Port View Terrace	Stroud	Stroud
Red Cross	Stroud	Stroud
5 Port View Terrace	Stroud	Stroud
8 Fort View Terrace	Stroud	Stroud
Motorcycles MOT Centre	Stroud	Stroud
3 Lodgeomore Close	Stroud	Stroud
Patis' Autos	Stroud	Stroud
4 Lodgeomore Close	Stroud	Stroud
5 Lodgeomore Close	Stroud	Stroud
6 Lodgeomore Close	Stroud	Stroud
Sunny Glen	Stroud	Stroud
T	Stroud R A O B Social Club	Stroud
5 Bridge Street	Chestnut Lane	Stroud
Coopers	Stroud	Stroud
Waltonde House	Stroud	Stroud
T	4 Bridge Street	Stroud
H & L Motors	Westward Road	Stroud
Stroud Precision	Westward Road	Stroud
Graham Reeves Building Merchant	Stroud	Stroud
Tropic House	Westward Road	Stroud
3 Bridge Street	Westward Road	Stroud
10 Anchor Terrace	Westward Road	Stroud
Calmcross Filling Station	Stroud	Stroud
8 Anchor Terrace	Stroud	Stroud
2 Bridge Street	Stroud	Stroud
14 Anchor Terrace	Stroud	Stroud
12 Anchor Terrace	Stroud	Bull & Sons
T	1-5 Bowbridge Lock (Mals)	Stroud
St Luke's Therapy Centre	Calmcross Road	Stroud
The Gables	Chestnut Lane	Stroud
Karandy	Stroud	Stroud
79 Westward Road	Stroud	Stroud
1 Bridge Street	Stroud	Stroud
1 Anchor Mill Cottage	Stroud	Stroud
2 Arnold Mill Cottage	Stroud	Stroud
75 Westward Road	Stroud	Stroud
77 Westward Road	Stroud	Calmcross Rd
Christian Community Centre	Stroud	Stroud
Graham Reeves Building Merchant	Stroud	Stroud
C Dragon Fish & Chips	Stroud	Stroud
71a Westward Rd	Stroud	Stroud
Double D Bootmakers	Stroud	Stroud
The Ball Hotel	Stroud	Stroud
John Sturley Services	Stroud	Stroud
69 Westward Road	Stroud	Stroud
Stroud Furniture Makers	Stroud	Stroud
20 Industrial	Stroud	Stroud
394600 205080	180	449
394610 205090	30	537
394610 205090	30	538
394610 205090	41.55	Door
394610 205090	41.59	Door
383540 204920	29	1047
383540 204920	41.77	Door
383100 204810	35	1046
383100 204810	41.78	Door
382480 204910	32	1043
382480 204910	41.82	Door
382470 204910	32	1044
382470 204910	41.83	Door
382470 204920	32	1042
382470 204920	41.87	Door
382470 204920	32	1041
382470 204920	41.89	Door
383500 204920	32	1038
383500 204920	41.93	Door
383500 204920	32	1039
383500 204920	42.09	Door
382100 204810	130	1323
382100 204810	42.17	Door
381970 205090	84	1353
381970 205090	42.24	D.P.C.
383150 204930	32	1036
383150 204930	42.27	Door
383150 204930	38	1045
383150 204930	42.28	D.P.C.
383150 204930	32	1035
383150 204930	42.28	Door
383150 204930	30	1034
383150 204930	42.31	Door
383150 204930	30	1033
383150 204930	42.45	Door
383150 204930	90	1320
383150 204930	42.53	Door
388510 204930	32	1037
388510 204930	42.67	Door
388510 204930	80	1318
388510 204930	42.74	Door
388140 204770	66	1321
388140 204770	42.79	Door
388140 204770	96	1363
388140 204770	42.85	D.P.C.
388140 204800	140	1319
388140 204800	42.89	Door
388130 204800	80	1320
388130 204800	42.93	Door
388130 204830	36	1340
388130 204830	42.95	Door
388130 204830	36	1341
388130 204830	42.98	D.P.C.
388130 204830	36	1342
388130 204830	43.01	Door
388130 204830	36	1343
388130 204830	43.12	Door
388130 204830	36	1344
388130 204830	43.12	D.P.C.
388130 205130	36	1353
388130 205130	43.28	D.P.C.
388130 204930	36	1354
388130 204930	43.39	D.P.C.
388120 205130	65	1314
388120 205130	43.46	Door
388110 204780	72	1416
388110 204780	43.57	Door
388100 205030	72	1414
388100 205030	43.58	Door
388100 205010	224	175
388100 205010	44.03	C.V.
383570 204940	28	1031
383570 204940	44.07	Door
383570 205110	140	1354
383570 205110	44.07	D.P.C.
384820 204860	1000	1413
384820 204860	44.07	Door
384720 204970	140	1419
384720 204970	44.08	C.F.
384800 205020	48	415
384800 205020	44.14	Door
384930 205050	78	412
384930 205050	44.26	Door
384530 204940	44	1030
384530 204940	44.28	Door
383220 204820	180	1313
383220 204820	44.37	Door
383210 204810	200	1312
383210 204810	44.38	Door
383180 204700	194	1316
383180 204700	44.39	Door
383180 204700	72	1317
383180 204700	44.40	D.P.C.
384190 205020	48	1362
384190 205020	44.56	D.P.C.
384930 204940	38	1028
384560 205000	54	470
384560 205000	44.57	Door
383350 204980	758	1022
383350 204980	44.63	Door
383480 205010	54	474
383480 205010	44.68	Window
383180 204820	48	1322
383180 204820	44.69	Door
384580 205000	54	473
384580 205000	44.72	Window
384570 205000	54	471
384570 205000	44.75	Window
384570 205000	54	472
384570 205000	44.77	Window
384570 204920	12	411
385775 204265	117	353
384400 205150	512	518
383190 205120	88	1355
384000 205120	64	539
383580 204880	48	1272
384320 205160	140	520
384320 205160	45.87	Door
384860 205050	72	436
385775 204265	117	356
385580 205150	512	518
385580 205150	45.88	Door
383370 204580	40	397
383370 204580	45.74	Door
383370 204580	42	1270
383360 204850	68	1271
383360 204850	45.85	Door
384320 205160	140	520
384320 205160	45.88	Door
383370 204860	40	398
383370 204860	45.73	Door
383380 204800	54	1268
383380 204800	45.86	Door
384850 205100	120	435
384850 205100	45.89	Door
385010 204920	400	400
385010 204920	46.02	Door
383190 204880	122	1266
383190 204880	46.03	Door
383470 204930	48	1026
PROF		

White House	Stroud	Stroud		
Murphy Kitchens	Westward Road	Westward Road		
63 Westward Road	Stroud	Stroud		
63 Westward Road	Stroud	Stroud		
25 Westward Road	Stroud	Stroud		
Raymonds Electrics	Stroud	Stroud		
61 Westward Road	Stroud	Stroud		
H	G Motor Components	Stroud		
John Davies	Accident Repair Workshop	Stroud		
George Dickenson Tyre & Exhaust Centre	Thripp	Stroud		
Presto Gaing	Westward Road	Stroud		
45 Westward Road	Stroud	Stroud		
Vendi	Outbridge Hill	Stroud		
41 Westward Road	Stroud	Stroud		
Walbridge House	(cottage)	Stroud		
Stroud Architectural Systems Ltd	Thripp	Stroud		
47 Westward Road	Stroud	Stroud		
B & H Engineering (Stroud)	Stroud	Stroud		
37 Westward Place	J Agnew Motor Engineer	Stroud		
R	S & R Scrap	Stroud		
Warwick Car Company	Stroud	Stroud		
21 Bowbridge Lock	Stroud	Stroud		
12 Bowbridge Lock	Stroud	Stroud		
8 Bowbridge Lock	Stroud	Stroud		
10 Bowbridge Lock	Stroud	Stroud		
13 Bowbridge Lock	Stroud	Stroud		
20 Bowbridge Lock	Stroud	Stroud		
18 Bowbridge Lock	Stroud	Stroud		
14 Bowbridge Lock	Stroud	Stroud		
6 Bowbridge Lock	Stroud	Stroud		
Warwick Car Company	Stroud	Stroud		
7 Bowbridge Lock	Stroud	Stroud		
S & R Scrap	26 Bowbridge Lock	Stroud		
Stroud Architectural Supplies Ltd	Stroud	Stroud		
36 Bowbridge Lock	Stroud	Stroud		
37 Bowbridge Lock	Stroud	Stroud		
22 Bowbridge Lock	Stroud	Stroud		
31 Bowbridge Lock	Stroud	Stroud		
29 Bowbridge Lock	Stroud	Stroud		
9-11 Bowbridge Lock (flats)	Stroud	Stroud		
15-17 Bowbridge Lock (flats)	D	Stroud		
32 Bowbridge Lock	Camerross Rd	Stroud		
30 Bowbridge Lock	Tyre & Exhaust Centre (empty)	Stroud		
Warehouse (empty) Stroud	Thripp	Stroud		
Cycle Sport	N Foundsales	Stroud		
Arundell Mill Cottage	Stroud	Stroud		
33-35 Bowbridge Lock (flats)	D	Stroud		
24 Bowbridge Lock	Stroud	Stroud		
25-27 Bowbridge Lock (flats)	Stroud	Stroud		
23 Bowbridge Lock (flats)	Stroud	Stroud		
Berry Hunt Windows Thripp	Stroud	Stroud		
Jackanory	Chester Lane	Stroud		
Chez Nous	S W	Stroud		
J	Calncross Road	Stroud		
Robert Timms	Calncross Road	Stroud		
Bistro Cafeteria Extensions	Thripp	Stroud		
Arnolda Car Sales	Calncross Road	Stroud		
Private Workshop	Calncross Road	Stroud		
The Cedars	Stroud	Stroud		
Lacey & Thompson Garage	Stroud	Stroud		
(no address unknown) Outbridge Hill	E	Stroud		
M	Whittington House	Stroud		
Stroud District Council	Outbridge Hill	Stroud		
C	Dubbridge	Stroud		
Stroud District Council	V Austral Toomaking	Stroud		
J	Lowdham Mailworks	Stroud		
Stroud District Council	Dubbridge	Stroud		
I	123 Calncross Road	Stroud		
PROF				
19 Private				
19 Commercial				
383480 204960	204930	100	1023	46.18 Door
383480 204960	204900	36	1265	46.25 Door
383390 204960	204900	36	1254	46.28 Door
383480 204960	204940	98	1024	46.28 Door
19 Empty				
20 Commercial				
383240 204910	204910	98	1262	46.29 Door
20 Private				
383480 204960	204900	36	1263	46.32 Door
20 Industrial				
385120 204920	180	401	46.35 Door	46.35 D.P.C.
385120 204900	180	402	46.35 Door	46.35 D.P.C.
20 Private				
384700 204970	36	418	46.34 Door	46.34 D.P.C.
20 Industrial				
385920 204980	240	338	46.38 Door	46.42 D.P.C.
20 Commercial				
385960 205930	2000	334	46.55 Door	46.52 D.P.C.
20 Private				
383410 204910	40	1258	46.56 Door	46.54 D.P.C.
19 Industrial				
383420 204910	40	1250	46.54 Door	46.54 D.P.C.
20 Private				
383170 204530	100	1112	46.54 Door	46.54 D.P.C.
20 Commercial				
385240 204890	90	404	46.62 Door	46.62 D.P.C.
20 Private				
385040 204890	90	403	46.63 Door	46.63 D.P.C.
19 Empty				
385940 204920	220	1021	46.64 Door	46.64 D.P.C.
20 Industrial				
385960 204850	90	408	46.65 Door	46.65 D.P.C.
20 Commercial				
385140 204840	400	1020	46.66 Door	46.66 D.P.C.
20 Industrial				
385050 204880	98	408	46.68 Door	46.68 D.P.C.
20 Private				
385815 204105	45	365	46.68 Door	46.68 D.P.C.
20 Commercial				
385050 204930	180	405	46.70 Door	46.70 D.P.C.
20 Private				
385740 204940	220	1021	46.71 Door	46.71 D.P.C.
20 Industrial				
385680 204870	90	407	46.72 Door	46.72 D.P.C.
20 Private				
385795 204215	35	357	46.78 Door	46.78 D.P.C.
20 Commercial				
385195 204215	30	364	46.78 Door	46.78 D.P.C.
20 Private				
385795 204215	30	360	46.79 Door	46.79 D.P.C.
20 Private				
385825 204205	43	363	46.79 Door	46.79 D.P.C.
20 Private				
385905 204215	35	363	46.79 Door	46.79 D.P.C.
20 Private				
385795 204215	30	361	46.79 Door	46.79 D.P.C.
20 Private				
385795 204245	32	354	46.79 Door	46.79 D.P.C.
20 Industrial				
385070 204170	90	407	46.80 Door	46.80 D.P.C.
20 Private				
385195 204185	30	356	46.80 Door	46.80 D.P.C.
20 Commercial				
385195 204170	227	1022	46.80 Door	46.80 D.P.C.
20 Private				
385840 204150	227	1022	46.80 Door	46.80 D.P.C.
20 Private				
385805 204185	30	367	46.80 Door	46.80 D.P.C.
20 Private				
385945 204155	27	373	46.80 Door	46.80 D.P.C.
20 Private				
385920 204170	254	1024	46.81 Door	46.81 D.P.C.
20 Private				
385960 203960	440	1345	46.82 Door	46.82 D.P.C.
20 Industrial				
385785 204220	77	352	46.84 Door	46.84 D.P.C.
20 Private				
385930 203780	192	130	46.85 Door	46.85 D.P.C.
19 Industrial				
385940 204150	227	1027	46.86 Door	46.86 D.P.C.
20 Private				
385950 204170	372	1378	46.86 Door	46.86 D.P.C.
20 Commercial				
385945 204170	204	915	46.87 Door	46.87 D.P.C.
20 Private				
385825 204170	227	1027	46.87 Door	46.87 D.P.C.
20 Private				
385785 204225	77	358	46.88 Door	46.88 D.P.C.
20 Private				
385870 203850	40	1348	46.89 Door	46.89 D.P.C.
19 Industrial				
385610 204560	48	208	46.90 Door	46.90 D.P.C.
19 Private				
385780 203780	192	130	46.92 Door	46.92 D.P.C.
20 Private				
385920 204170	227	1027	46.92 Door	46.92 D.P.C.
20 Private				
385170 204170	204	915	46.96 Door	46.96 D.P.C.
20 Private				
385110 204390	240	1170	46.97 Door	46.97 D.P.C.
19 Private				
385970 204150	360	1360	46.98 Door	46.98 D.P.C.
20 Private				
385825 204170	204	915	46.98 Door	46.98 D.P.C.
20 Private				
385980 203890	90	340	47.03 Door	47.03 D.P.C.
19 Industrial				
386180 205110	84	316	47.07 Door	47.07 D.P.C.
20 Private				
386000 205140	98	307	47.07 Door	47.07 D.P.C.
20 Private				
386270 204940	154	510	47.08 Door	47.08 D.P.C.
19 Private				
386270 204940	154	510	47.08 Door	47.08 D.P.C.
20 Private				
386970 203820	200	333	47.11 Door	47.11 D.P.C.
20 Commercial				
386570 205120	240	517	47.12 Door	47.12 D.P.C.
19 Offices				
385980 203890	90	340	47.18 Door	47.18 D.P.C.
20 Commercial				
386180 205110	84	316	47.27 Door	47.27 D.P.C.
20 Private				
386000 205140	98	307	47.34 Door	47.34 D.P.C.
19 Private				
386270 204940	154	510	47.36 Door	47.36 D.P.C.
20 Industrial				
386970 203890	120	378	47.38 Door	47.38 D.P.C.
20 Office				
386840 204610	162	1086	47.42 Door	47.42 D.P.C.
20 Store				
386370 205150	124	519	47.43 Door	47.43 D.P.C.
19 Industrial				
386980 203780	520	329	47.54 Door	47.54 D.P.C.
20 Private				
386730 204650	460	1082	47.55 Door	47.55 D.P.C.
19 Industrial				
386980 203810	460	1093	47.62 Door	47.62 D.P.C.
20 Stroud				
386730 204640	630	1093	47.62 Door	47.62 D.P.C.
20 Private				
386410 205140	80	542	47.65 Door	47.65 D.P.C.

New Building (recently built)	Name Building (Unknown name & number)
ARC	Thruop
Coulter Garage	Stroud
Graham Roberts Building Merchant	Stroud
40 Bath Road	Stroud
42 Bath Road	Stroud
Brookside	Stroud
Emily House (under construction)	Stroud
Eagle Man Carpenters	Stroud
Anthony's	Stroud
Brookville	Stroud
44 Bath Road	Stroud
Hawker Siddley	Stroud
50 Bath Road	Stroud
48 Bath Road	Stroud
J	Stroud
Hawker Siddley	Stroud
52 Bath Road	Stroud
Carpets of Worth	Stroud
54 Bath Road	Stroud
Norman & Ballinger	Stroud
Normal Structures	Stroud
EZE Whealoe	Stroud
Rose Cottage	Stroud
E	Stroud
The Clonkens Arms	Stroud
Norman Machinery	Stroud
Stroud Bus Depot	Stroud
Filed House	Stroud
Hawker Siddley	Stroud
Regan Machinery Ltd	Stroud
Eagle Man Carpets	Stroud
Straight Eight Precision	Stroud
Topo Ltd	Stroud
UHL F1	Stroud
Howard Tannery	Stroud
Clarke Automation Ltd	Stroud
Widewdene	Stroud
Coutere Orange	Stroud
Weston Ltd	Stroud
Jet Pac Ltd	Stroud
Plant	Stroud
Unit B2	Stroud
9 Thruop Industrial Estate - Caravan site	Stroud
Phoenix	Stroud
Whistley Plant	Stroud
Emily Unit	Stroud
Whitton	Stroud
101 Engineering Ltd	Stroud
West Country Metal Products	Stroud
A	Stroud
Roy's Vphonables	Stroud
A1 Motoring Services	Stroud
Bell Fitter Ltd	Stroud
Colour Business Firms	Stroud
Coughs & Matthews Ltd	Stroud
Combury	Stroud
Laurel Cottage	Stroud
Corner Cottage	Stroud
Unit 2	Stroud
1 Thruop Industrial Estate	Stroud
Unit 3 Thruop Industrial Estate - Caravan site	Stroud
Graham Roberts Building Merchant	Stroud
10 Thruop Industrial Estate - Caravan site	Stroud
2 Thruop Industrial Estate - Caravan site	Stroud
27 Cheladale	Stroud
3 Thruop Industrial Estate - Caravan site	Stroud
Brooklyn	Stroud
17 Thruop Industrial Estate - Caravan park	Stroud
Ex-Clothing Factory	Stroud

20 Private	51.13 Door
20 Private	51.18 Door
19 Industrial	51.2 Door
20 Commercial	51.22 Door
20 Commercial	51.31 Door
20 Private	51.45 Door
20 Private	51.46 Door
20 Private	51.5 Door
20 Private	51.61 Door
20 Commercial	51.65 Door
20 Private	51.8 Door
20 Private	51.87 Door
20 Private	51.91 Door
20 Industrial	51.95 Door
20 Industrial	51.97 Door
20 Private	51.99 Door
20 Industrial	52.03 Door
20 Industrial	52.06 Door
20 Industrial	52.07 Door
20 Private	52.07 Door
20 Industrial	52.1 Door
20 Industrial	52.11 Door
20 Private	52.12 Door
20 Industrial	52.24 Door
20 Industrial	52.31 Door
20 Industrial	52.33 Door
18 Public House	52.35 Door
20 Industrial	52.35 Door
20 Bus Depot	52.42 Door
20 Private	52.42 Door
20 Industrial	52.44 Door
20 Industrial	52.46 Door
20 Industrial	52.48 Door
20 Industrial	52.51 Door
20 Industrial	52.53 Door
18 Private	52.53 Door
20 Industrial	52.55 Door
20 Industrial	52.56 Door
20 Industrial	52.57 Door
20 Industrial	52.58 Door
20 Industrial	52.59 Door
20 Industrial	52.61 Door
20 Industrial	52.62 Door
20 Industrial	52.63 Door
20 Industrial	52.64 Door
20 Industrial	52.65 Door
20 Industrial	52.66 Door
20 Industrial	52.67 Door
20 Industrial	52.68 Door
20 Industrial	52.69 Door
20 Industrial	52.72 Door
20 Industrial	52.73 Door
20 Industrial	52.74 Door
20 Industrial	52.75 Door
20 Industrial	52.76 Door
20 Industrial	52.77 Door
20 Industrial	52.78 Door
20 Industrial	52.79 Door
20 Industrial	52.81 Door
20 Industrial	52.82 Door
20 Industrial	52.83 Door
20 Industrial	52.84 Door
20 Industrial	52.85 Door
20 Industrial	52.86 Door
20 Industrial	52.87 Door
20 Industrial	52.88 Door
20 Industrial	52.89 Door
20 Industrial	52.90 Door
20 Industrial	52.91 Door
20 Industrial	52.92 Door
20 Industrial	52.93 Door
20 Industrial	52.94 Door
20 Industrial	52.95 Door
20 Industrial	52.96 Door
20 Industrial	52.97 Door
20 Industrial	52.98 Door
20 Industrial	52.99 Door
20 Industrial	53.00 Door
20 Industrial	53.01 Door
20 Industrial	53.02 Door
20 Industrial	53.03 Door
20 Industrial	53.04 Door
20 Industrial	53.05 Door
20 Industrial	53.06 Door
20 Industrial	53.07 Door
20 Industrial	53.08 Door
20 Industrial	53.09 Door
20 Industrial	53.10 Door
20 Industrial	53.11 Door
20 Industrial	53.12 Door
20 Industrial	53.13 Door
20 Industrial	53.14 Door
20 Industrial	53.15 Door
20 Industrial	53.16 Door
20 Industrial	53.17 Door
20 Industrial	53.18 Door
20 Industrial	53.19 Door
20 Industrial	53.20 Door
20 Industrial	53.21 Door
20 Industrial	53.22 Door
20 Industrial	53.23 Door
20 Industrial	53.24 Door
20 Industrial	53.25 Door
20 Industrial	53.26 Door
20 Industrial	53.27 Door
20 Industrial	53.28 Door
20 Industrial	53.29 Door
20 Industrial	53.30 Door
20 Industrial	53.31 Door
20 Industrial	53.32 Door
20 Industrial	53.33 Door
20 Industrial	53.34 Door
20 Industrial	53.35 Door
20 Industrial	53.36 Door
20 Industrial	53.37 Door
20 Industrial	53.38 Door

Appendix 3

Sensitivity test maximum water levels



RFA_016	8.59	17.5	8.74	19.0	9.03	23.4	8.59	16.3	8.61	15.6
RFA_017	8.64	17.5	8.78	19.0	9.06	23.5	8.63	16.3	8.64	15.6
RFA_018	8.65	17.5	8.80	19.0	9.08	23.5	8.65	16.3	8.66	15.6

Wheatenhurst Sluices

RFA_019	10.11	17.5	10.21	19.0	10.35	23.5	10.12	16.3	10.25	15.6
RFA_020	10.11	17.5	10.22	19.0	10.37	23.5	10.13	16.3	10.26	15.6
RFA_021	10.25	17.5	10.31	19.0	10.47	23.5	10.25	16.3	10.29	15.6
RFA_022	10.37	17.5	10.44	19.0	10.61	23.5	10.35	16.3	10.35	15.6
RFA_023	10.42	17.5	10.49	19.0	10.66	23.5	10.40	16.3	10.40	15.6

Walk Rhine Bridge

RFA_024	10.47	17.5	10.54	19.0	10.73	23.5	10.44	16.3	10.44	15.6
RFA_025	10.55	17.5	10.63	17.9	10.84	18.4	10.52	16.3	10.51	15.2
RFA_026	10.60	17.5	10.67	17.9	10.87	18.4	10.56	16.3	10.54	15.2
RFA_027	10.66	17.5	10.71	18.0	10.90	18.4	10.62	16.3	10.59	15.2
RFA_028	10.76	17.5	10.78	18.0	10.95	18.5	10.71	16.4	10.67	15.2
RFA_029	10.86	17.5	10.89	18.0	11.02	18.5	10.82	16.4	10.77	15.2
RFA_030	10.97	17.5	10.99	18.0	11.09	18.5	10.92	16.4	10.86	15.2
RFA_031	11.03	17.5	11.06	18.0	11.13	18.5	10.98	16.4	10.93	15.2
RFA_032	11.11	17.5	11.14	18.0	11.20	18.5	11.06	16.4	11.00	15.2

Frombridge Mill

RFA_033	12.46	17.5	12.47	18.0	12.49	18.5	12.48	16.4	12.50	15.2
RFA_034	12.48	17.5	12.49	18.0	12.51	18.5	12.50	16.4	12.52	15.2
A38 Road Bridge										
RFA_035	12.56	17.5	12.58	18.0	12.60	18.5	12.58	16.4	12.59	15.2
RFA_036	12.58	23.5	12.60	24.9	12.62	25.5	12.59	23.2	12.59	23.1
RFA_037	12.61	24.6	12.63	26.6	12.65	27.5	12.62	24.6	12.63	24.9

RFA_038	12.66	29.7	12.67	33.6	12.69	35.5	12.66	30.2	12.67	30.2	12.67	31.3
RFA_039	12.71	29.7	12.74	33.6	12.75	35.5	12.72	30.1	12.73	30.1	12.73	31.3

M5 Road Bridge

RFA_040	12.78	29.7	12.83	33.6	12.85	35.4	12.79	30.1	12.81	30.1	12.81	31.3
RFA_041	12.98	28.1	13.06	30.5	13.10	31.3	12.99	28.8	13.02	28.8	13.02	28.3
RFA_042	13.19	21.4	13.28	22.0	13.32	22.2	13.21	22.4	13.23	22.4	13.23	19.9
RFA_043	13.27	21.4	13.35	22.0	13.39	22.2	13.29	22.5	13.29	22.5	13.29	19.9

Meadow Mill Wall

RFA_044	14.43	21.4	14.45	22.0	14.46	22.2	14.41	22.5	14.44	22.5	14.44	19.9
RFA_045	14.40	36.3	14.41	38.6	14.42	39.4	14.38	36.5	14.41	36.5	14.41	35.8
RFA_046	14.48	36.4	14.50	39.0	14.51	40.1	14.47	36.6	14.48	36.6	14.48	36.0

Junction with RFC_001

RFA_047	14.48	34.9	14.50	37.5	14.51	38.6	14.47	35.1	14.48	35.1	14.48	34.5
RFA_048	14.67	34.9	14.72	37.5	14.73	38.6	14.67	35.1	14.68	35.1	14.68	34.5

Meadow Bridge

RFA_049	14.78	34.9	14.91	37.5	14.97	38.6	14.79	35.1	14.79	35.1	14.79	34.5
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Junction with RFD_001

RFA_050	14.78	19.3	14.91	20.0	14.97	19.9	14.79	19.5	14.79	19.5	14.79	19.3
RFA_051	14.90	12.7	15.00	12.7	15.05	13.0	14.91	12.7	14.91	12.7	14.91	12.6
RFA_052	15.00	11.4	15.08	11.3	15.12	11.2	15.00	11.3	15.00	11.3	15.00	11.2
RFA_053	15.05	6.8	15.11	6.8	15.15	6.8	15.05	6.7	15.05	6.7	15.05	6.6

Millend Mills Sluices

RFA_054	15.80	6.8	15.80	6.8	15.81	6.8	15.92	6.7	16.01	6.6	16.01	6.6
RFA_055	15.99	6.7	16.00	6.8	16.00	6.8	16.05	6.7	16.11	6.6	16.11	6.6
RFA_056	16.18	6.7	16.18	6.8	16.18	6.8	16.20	6.7	16.23	6.6	16.23	6.6
RFA_057	16.32	6.7	16.32	6.8	16.32	6.8	16.33	6.7	16.34	6.6	16.34	6.6

	16.44	6.7	16.44	6.8	16.44	6.8	16.44	6.7	16.45	6.6
RFA_058	16.44	6.7	16.44	6.8	16.56	6.9	16.56	6.9	16.56	6.8
RFA_059	16.56	6.8	16.56	6.9	16.65	9.0	16.65	8.9	16.65	8.9
RFA_060	16.64	8.8	16.65	8.9	16.80	9.0	16.80	8.8	16.80	8.9
RFA_061	16.79	8.8	16.80	8.9	16.96	9.3	16.95	9.2	16.96	9.2
RFA_062	16.95	9.0	16.96	9.3	17.11	9.5	17.10	9.4	17.10	9.4
RFA_063	17.10	9.2	17.11	9.5	17.26	9.0	17.28	9.1	17.25	9.0
RFA_064	17.24	8.9	17.43	9.3	17.44	9.4	17.42	9.3	17.43	9.3
RFA_065	17.42	9.2	17.60	7.5	17.61	7.5	17.60	7.5	17.60	7.4
RFA_066	17.59	7.5	17.65	9.0	17.65	9.0	17.64	9.0	17.64	8.9
RFA_067	17.64	9.1	17.75	11.3	17.75	11.4	17.75	11.2	17.75	11.2
RFA_068	17.75	11.3	18.03	11.7	18.03	11.9	18.03	12.0	18.03	11.5
RFA_069	18.03	11.7	18.21	15.8	18.21	16.2	18.21	16.5	18.21	15.4
RFA_070	18.21	15.8	18.55	17.1	18.55	18.0	18.54	18.6	18.53	16.3
RFA_071	18.54	17.1								
Junction with RFF_001										
RFA_072	18.54	16.5	18.55	17.3	18.56	17.8	18.54	16.2	18.53	15.7
RFA_073	18.80	16.5	18.82	17.3	18.84	17.8	18.79	16.2	18.77	15.7
RFA_074	18.89	17.4	18.91	18.6	18.92	19.5	18.88	17.0	18.86	16.2
Beards Mill Bridge										
RFA_075	19.19	17.4	19.26	18.6	19.31	19.5	19.21	17.0	19.19	16.2
RFA_076	19.31	12.3	19.38	12.9	19.43	13.4	19.32	11.6	19.30	10.8
Beards Mill Side Weir										
RFA_077	20.44	12.3	20.49	12.9	20.52	13.4	20.49	11.6	20.52	10.8
Junction with RFF_003										
RFA_078	20.44	12.9	20.49	13.6	20.52	14.2	20.49	12.3	20.52	11.4

RFA_078A	20.51	12.9	20.55	14.0	20.59	14.8	20.54	13.0	20.56	12.8
RFA_079	20.66	6.1	20.71	6.1	20.75	6.1	20.68	6.0	20.69	5.9
RFA_080	20.69	6.5	20.75	6.6	20.79	6.6	20.71	6.4	20.72	6.3
RFA_081	20.71	6.5	20.76	6.5	20.80	6.6	20.73	6.4	20.74	6.3
RFA_082	20.77	7.1	20.81	7.3	20.84	7.5	20.78	6.9	20.78	6.6
RFA_083	20.92	7.1	20.95	7.3	20.98	7.4	20.92	6.9	20.91	6.6
RFA_084	21.08	7.1	21.09	7.2	21.11	7.4	21.06	6.9	21.04	6.6
RFA_085	21.19	7.0	21.21	7.2	21.22	7.4	21.18	6.9	21.16	6.6
RFA_086	21.46	7.0	21.47	7.2	21.48	7.3	21.45	6.8	21.42	6.5
RFA_087	21.78	7.0	21.79	7.1	21.80	7.3	21.77	6.8	21.74	6.5

Stanley Downton Bridge

RFA_088	21.82	7.0	21.83	7.1	21.84	7.3	21.81	6.8	21.78	6.5
RFA_089	22.09	7.0	22.11	7.1	22.12	7.2	22.08	6.8	22.05	6.5

Stanley Downton Mill Race

RFA_090	22.55	7.0	22.56	7.1	22.58	7.2	22.60	6.8	22.66	6.5
RFA_091	22.77	6.9	22.78	7.1	22.80	7.2	22.79	6.8	22.81	6.4
RFA_092	22.85	6.9	22.87	7.1	22.88	7.2	22.86	6.7	22.88	6.4
RFA_093	22.93	6.9	22.95	7.0	22.96	7.1	22.94	6.7	22.94	6.4
RFA_094	23.02	6.9	23.03	7.0	23.05	7.1	23.02	6.7	23.01	6.3
RFA_095	23.12	6.8	23.13	7.0	23.14	7.1	23.11	6.6	23.10	6.3
RFA_096	23.20	6.8	23.21	6.9	23.23	7.0	23.19	6.6	23.17	6.3
RFA_097	23.29	6.8	23.30	6.9	23.32	7.0	23.28	6.6	23.26	6.2
RFA_098	23.39	6.7	23.41	6.8	23.42	6.9	23.38	6.5	23.36	6.2
RFA_099	23.45	6.7	23.47	6.8	23.47	6.9	23.44	6.5	23.42	6.2

Junction with RFM_001

RFA_100	23.45	6.7	23.47	6.8	23.47	6.9	23.44	6.5	23.42	6.2
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RFA_101	23.63	6.7	23.64	6.8	23.64	6.9	23.61	6.5	23.59	6.2
RFA_102	23.91	6.7	23.91	6.8	23.92	6.9	23.89	6.5	23.86	6.1
RFA_103	24.21	6.6	24.22	6.7	24.23	6.8	24.19	6.4	24.17	6.1

Stanley Mills Weir

RFA_104	28.16	6.6	28.17	6.7	28.17	6.8	28.19	6.4	28.22	6.1
RFA_105	28.17	6.6	28.18	6.7	28.18	6.8	28.20	6.4	28.23	6.1

Stanley Mills Bridge

RFA_106	28.18	6.6	28.18	6.7	28.19	6.8	28.21	6.4	28.24	6.1
RFA_107	28.24	6.6	28.25	6.7	28.25	6.8	28.26	6.4	28.28	6.0
RFA_108	28.27	6.6	28.27	6.7	28.28	6.7	28.29	6.3	28.30	6.1
RFA_109	28.29	6.5	28.29	6.6	28.30	6.7	28.30	6.3	28.32	6.1
RFA_110	28.30	6.6	28.31	6.6	28.32	6.7	28.32	6.3	28.33	6.1
RFA_111	28.32	6.6	28.33	6.6	28.34	6.7	28.34	6.3	28.35	6.1
RFA_112	28.35	5.9	28.36	5.9	28.37	5.9	28.37	5.6	28.38	5.2
RFA_113	28.37	4.9	28.38	4.8	28.38	4.7	28.38	4.7	28.39	4.3
RFA_114	28.40	7.5	28.41	7.8	28.42	8.0	28.41	7.5	28.42	7.5

Rodhill Bridge

RFA_115	28.56	7.5	28.58	7.8	28.60	8.0	28.58	7.5	28.60	7.5
RFA_116	28.61	7.5	28.63	7.8	28.65	8.0	28.63	7.4	28.65	7.5
RFA_117	28.70	16.7	28.73	18.5	28.75	20.0	28.72	17.6	28.74	18.8
RFA_118	29.02	15.9	29.10	17.2	29.16	18.7	29.07	16.1	29.13	16.4

Refuse Tip Weir 1

RFA_119	29.45	15.9	29.50	17.2	29.56	18.6	29.53	16.1	29.62	16.4
Junction with RFD_081										
RFA_120	29.45	37.0	29.50	39.6	29.56	42.3	29.53	36.8	29.62	36.7
RFA_121	29.80	37.0	29.85	39.7	29.91	42.3	29.81	36.8	29.85	36.7

Junction with RFH_001						
RFA_122	29.80	21.2	29.85	23.0	29.91	25.0
RFA_123	29.85	19.0	29.90	20.4	29.95	22.1
RFA_124	29.89	19.2	29.95	20.3	30.01	21.8
RFA_125	29.98	10.9	30.04	10.9	30.09	11.0
Ebley Corn Mill Bypass						
RFA_126	30.32	11.0	30.35	11.0	30.38	11.0
Junction with RFH_004						
RFA_127	30.32	26.4	30.35	26.9	30.38	26.9
RFA_128	30.30	29.0	30.32	30.0	30.35	30.1
Ebley Corn Mill Bridge						
RFA_129	30.48	29.1	30.52	30.3	30.59	30.3
RFA_130	30.66	26.8	30.69	27.5	30.73	28.0
RFA_131	30.82	56.4	30.82	55.5	30.82	55.6
RFA_132	30.83	36.9	30.86	37.8	30.89	39.7
RFA_133	31.11	36.8	31.14	39.8	31.17	42.3
RFA_134	31.31	37.4	31.36	39.7	31.40	42.3
RFA_135	31.28	28.5	31.34	29.8	31.39	30.4
Ebley Mill Bridge						
RFA_136	31.30	28.5	31.36	29.9	31.41	30.4
RFA_137	31.45	28.4	31.52	29.5	31.57	30.4
Ebley Mill Weir						
RFA_138	32.15	28.4	32.17	29.5	32.20	30.4
RFA_139	32.20	28.4	32.22	29.4	32.25	30.4
RFA_140	32.40	30.7	32.43	32.8	32.44	34.6

Junction with SCA_001

RFA_141	32.40	19.5	32.43	20.2	32.44	20.7	32.42	19.2	32.43	18.7
RFA_142	32.46	23.6	32.47	24.3	32.49	25.3	32.46	23.6	32.47	23.5
RFA_143	32.73	24.5	32.74	25.6	32.76	27.0	32.73	24.5	32.73	24.4
RFA_144	32.69	24.5	32.71	25.6	32.72	27.0	32.69	24.5	32.69	24.4
Junction with RFX_001										
RFA_145	32.69	10.9	32.71	11.6	32.72	12.1	32.69	10.9	32.69	11.0
Dudbridge Road Culvert										
RFA_146	32.85	10.8	32.89	11.6	32.91	12.1	32.88	10.9	32.92	10.9
RFA_147	32.93	10.8	32.97	11.6	32.99	12.1	32.95	10.9	32.98	10.9
Reddles Mill Sluices										
RFA_148	34.71	10.8	34.74	11.6	34.76	12.1	34.76	10.8	34.80	10.9
RFA_149	34.71	10.8	34.74	11.6	34.75	12.1	34.75	10.8	34.80	10.9
RFA_150	34.72	10.8	34.75	11.6	34.77	12.1	34.76	10.8	34.81	10.8
RFA_151	34.91	10.8	34.95	11.5	34.97	12.0	34.93	10.8	34.96	10.8
RFA_152	35.10	10.7	35.15	11.5	35.18	12.0	35.12	10.7	35.14	10.8
RFA_153	35.15	10.7	35.20	11.5	35.23	12.0	35.16	10.7	35.18	10.8
Junction with RFN_001										
RFA_154	35.15	8.6	35.20	9.3	35.23	9.8	35.16	8.6	35.16	9.0
RFA_155	35.25	8.6	35.30	9.3	35.33	9.8	35.26	8.7	35.28	9.0
RFA_156	35.35	8.5	35.40	9.3	35.43	9.7	35.36	8.7	35.38	8.9
Fromehall Mill Bypass Sluices										
RFA_157	36.44	8.5	36.48	9.3	36.51	9.7	36.50	8.6	36.56	8.9
RFA_158	36.53	5.9	36.58	6.0	36.61	6.0	36.58	5.6	36.64	5.4
RFA_159	36.55	5.9	36.60	5.9	36.63	5.9	36.60	5.6	36.65	5.4
Fromehall Mill Bridge										
RFA_160	36.83	5.9	36.86	5.9	36.88	5.9	36.86	5.6	36.88	5.4

RFA_161	36.83	6.7	36.86	7.0	36.88	7.2	36.85	6.6	36.87	6.5
Junction with RFN_006										
RFA_162	36.83	8.8	36.86	9.1	36.88	9.5	36.85	8.5	36.87	8.2
RFA_163	36.86	10.6	36.88	11.4	36.90	12.0	36.87	10.6	36.89	10.5
RFA_163A	36.91	10.6	36.94	11.3	36.96	12.0	36.92	10.5	36.94	10.5
Lodgemore Mills Bridge										
RFA_164	36.95	10.6	36.99	11.3	37.01	12.1	36.97	10.5	36.98	10.5
RFA_165	36.96	10.6	37.00	11.3	37.02	12.0	36.98	10.5	36.99	10.5
Lodgemore Mills Sluices										
RFA_166	38.25	10.6	38.35	11.3	38.41	12.0	38.30	10.5	38.36	10.5
RFA_167	38.24	10.6	38.34	11.3	38.40	12.0	38.29	10.5	38.35	10.5
Lodgemore Mills Culvert										
RFA_168	38.90	10.6	38.99	11.3	39.05	11.9	38.89	10.5	38.87	10.5
RFA_169	38.91	10.6	39.00	11.3	39.06	12.0	38.89	10.5	38.88	10.5
RFA_170	38.96	10.7	39.05	11.3	39.11	11.8	38.95	10.7	38.93	10.7
Bath Road Bridge										
RFA_171	38.97	10.7	39.06	11.3	39.11	11.8	38.96	10.7	38.94	10.7
RFA_172	38.97	10.7	39.05	11.3	39.11	11.8	38.96	10.7	38.94	10.7
RFA_173	39.11	10.7	39.19	11.3	39.24	11.7	39.10	10.7	39.09	10.7
RFA_174	39.25	10.7	39.31	11.3	39.35	11.7	39.24	10.7	39.24	10.7
RFA_175	39.56	10.7	39.60	11.2	39.63	11.7	39.56	10.7	39.55	10.7
RFB_001	8.18	9.1	8.27	10.0	8.49	11.7	8.19	8.6	8.19	8.4
RFB_002	8.25	9.1	8.35	9.9	8.57	11.7	8.25	8.6	8.25	8.4
RFB_003	8.30	9.1	8.40	9.8	8.62	11.6	8.29	8.6	8.28	8.4
Gloucester & Sharpness Canal - Right Syphon										
RFB_004	8.43	9.1	8.58	9.8	8.89	11.6	8.44	8.6	8.45	8.4

RFB_005	8.50	9.0	8.66	9.1	8.96	10.3	8.50	8.6	8.52	8.1
RFB_006	8.54	9.6	8.68	11.7	8.98	14.7	8.54	9.2	8.55	9.1
RFB_007	8.57	9.6	8.71	11.7	8.99	15.5	8.56	9.2	8.58	9.1
Whitminster Weir - Right										
RFB_008	8.60	9.6	8.75	11.7	9.03	15.5	8.60	9.2	8.61	9.1
RFC_001	14.48	2.9	14.50	2.9	14.51	2.7	14.47	2.8	14.48	2.6
Caravan Park Weir										
RFC_001A	14.50	2.9	14.52	2.9	14.53	2.7	14.49	2.8	14.51	2.6
RFC_002	14.50	2.8	14.52	2.8	14.53	2.7	14.49	2.7	14.51	2.6
Spring Hill Bridge										
RFC_003	14.85	2.8	14.86	2.8	14.87	2.7	14.85	2.7	14.86	2.6
RFC_004	14.85	2.6	14.87	2.5	14.88	2.5	14.85	2.3	14.87	2.2
RFC_005	14.86	2.6	14.87	2.5	14.88	2.5	14.86	2.3	14.87	2.2
Churchend School Bridge										
RFC_006	15.47	2.5	15.47	2.4	15.48	2.5	15.48	2.2	15.48	2.2
RFC_007	15.47	1.9	15.48	1.9	15.48	1.9	15.48	1.8	15.49	1.7
Churchend School Weir										
RFC_008	15.65	1.9	15.65	1.9	15.66	1.9	15.68	1.8	15.70	1.7
RFC_009	15.71	1.9	15.72	1.9	15.72	1.9	15.73	1.8	15.75	1.7
RFD_001	14.78	15.6	14.91	17.5	14.97	18.7	14.79	15.6	14.79	15.3
RFD_002	14.87	6.7	14.99	8.4	15.05	9.5	14.88	6.6	14.88	6.3
RFD_003	14.88	6.1	15.01	6.2	15.07	6.2	14.89	5.9	14.89	5.7
Millend Lane Bridge										
RFD_004	14.99	6.1	15.12	6.2	15.19	6.2	15.00	5.9	15.00	5.7
RFD_005	15.00	6.1	15.13	6.2	15.19	6.2	15.01	5.9	15.01	5.6

Junction with RFE_001

RFD_006	15.00	3.6	15.13	3.6	15.19	3.6	15.01	3.3	15.01	3.0
RFD_007	14.99	3.6	15.12	3.6	15.18	3.6	15.00	3.3	15.00	3.0
RFD_008	15.71	3.6	15.72	3.6	15.72	3.6	15.73	3.3	15.75	3.0

Junction with RFC_009

RFD_008A	15.71	5.4	15.72	5.4	15.72	5.4	15.73	5.1	15.75	4.7
RFD_009	15.78	6.6	15.78	6.6	15.79	6.6	15.79	6.4	15.80	6.3
RFD_010	15.90	7.0	15.90	7.0	15.90	7.0	15.90	6.8	15.90	6.6
RFD_011	16.00	7.0	16.00	7.0	16.00	7.0	16.00	6.8	15.99	6.6

Junction with RFE_005

RFD_012	16.00	7.6	16.00	7.6	16.00	7.6	16.00	7.3	15.99	7.0
RFD_013	16.10	9.1	16.11	9.2	16.11	9.2	16.10	8.6	16.09	7.9
RFD_014	16.23	9.1	16.23	9.2	16.23	9.2	16.21	8.5	16.19	7.9
RFD_015	16.41	9.1	16.41	9.1	16.42	9.2	16.38	8.5	16.35	7.8
RFD_016	16.58	9.1	16.59	9.1	16.59	9.2	16.55	8.5	16.52	7.8
RFD_017	16.76	9.1	16.76	9.1	16.76	9.1	16.73	8.5	16.69	7.8

Junction with RFG_001

RFD_018	16.76	6.9	16.76	6.9	16.76	6.9	16.73	6.4	16.69	5.9
RFD_019	16.99	6.9	16.99	6.9	16.99	6.9	16.95	6.4	16.91	5.9
Bonds Mill Culvert										
RFD_020	19.22	6.9	19.22	6.9	19.23	6.9	19.26	6.4	19.30	5.9

Junction with RFG_006

RFD_021	19.22	9.1	19.22	9.1	19.23	9.1	19.26	8.5	19.30	7.8
RFD_022	19.29	9.1	19.30	9.1	19.30	9.1	19.32	8.5	19.34	7.8
RFD_023	19.36	9.2	19.36	9.2	19.36	9.3	19.37	8.7	19.38	8.3
RFD_024	19.43	10.1	19.43	10.3	19.43	10.4	19.43	9.8	19.43	9.4
RFD_025	19.50	12.3	19.51	12.6	19.51	12.8	19.50	12.0	19.50	11.6

GWR Bridge						
RFD_026	19.93	12.3	19.95	12.6	19.96	12.8
Ocean Pool Bridge						
RFD_027	20.67	12.3	20.72	12.6	20.77	12.8
RFD_028	20.69	11.8	20.75	11.8	20.79	11.8
RFD_029	20.70	17.1	20.75	17.0	20.79	17.0
RFD_030	20.72	15.3	20.77	15.4	20.81	15.5
RFD_031	20.74	18.9	20.79	19.0	20.82	19.1
Junction with RFJ_001						
RFD_032	20.74	14.8	20.79	15.0	20.82	15.1
RFD_033	20.81	15.1	20.85	15.7	20.87	16.0
Junction with RFK_001						
RFD_034	20.81	4.4	20.85	4.5	20.87	4.6
Bridgend Mill Side Sluices						
RFD_035	21.58	4.4	21.60	4.5	21.61	4.6
Junction with RFJ_003						
RFD_036	21.58	8.5	21.60	8.7	21.61	8.8
RFD_037	21.60	8.5	21.62	8.7	21.63	8.8
Bridgend Mill Bridge						
RFD_038	22.23	8.5	22.27	8.7	22.30	8.8
RFD_039	22.24	7.6	22.29	7.8	22.31	7.9
Junction with RFK_004						
RFD_040	22.24	11.5	22.29	11.9	22.31	12.1
RFD_041	22.25	12.8	22.30	13.3	22.32	13.5
RFD_042	22.27	13.0	22.31	13.4	22.34	13.6
RFD_043	22.32	11.5	22.36	11.3	22.39	11.3

Bridgend Kennels Bridge						
RFD_044	22.50	11.5	22.53	11.4	22.55	11.3
RFD_045	22.51	11.4	22.54	11.4	22.57	11.4
RFD_046	22.53	11.4	22.56	11.4	22.58	11.4
Junction with RFD_001						
RFD_047	22.53	6.5	22.56	6.5	22.58	6.5
Bridgend Kennels Sluices						
RFD_048	22.88	6.5	22.89	6.5	22.90	6.5
RFD_049	22.93	7.0	22.93	7.1	22.94	7.1
RFD_050	22.99	7.0	23.00	7.0	23.00	7.0
Downton Road Footbridge						
RFD_051	23.01	7.0	23.02	7.0	23.02	7.0
RFD_052	23.12	6.9	23.12	7.0	23.12	7.0
Upper Mills Footbridge						
RFD_053	23.26	6.9	23.27	6.9	23.27	7.0
RFD_054	24.07	6.9	24.07	6.9	24.07	6.9
Upper Mills Sluices						
RFD_055	25.11	6.9	25.11	6.9	25.11	6.9
RFD_056	25.14	7.2	25.15	7.2	25.15	7.2
RFD_057	25.16	9.6	25.16	9.6	25.17	9.7
RFD_058	25.25	9.6	25.25	9.6	25.25	9.6
RFD_059	25.28	9.5	25.29	9.6	25.29	9.6
RFD_060	25.31	9.5	25.31	9.6	25.32	9.6
Upper Mills Bridge						
RFD_061	25.36	9.5	25.37	9.6	25.37	9.6
RFD_062	25.40	9.5	25.41	9.6	25.41	9.6

RFD_063	25.44	9.5	25.45	9.6	25.45	9.6	25.43	9.1	25.41	8.6
RFD_064	25.50	9.5	25.51	9.6	25.51	9.6	25.49	9.1	25.47	8.6
RFD_065	25.54	11.5	25.55	11.6	25.55	11.7	25.53	10.7	25.51	9.8
RFD_066	25.58	13.5	25.59	13.6	25.59	13.8	25.57	12.3	25.55	10.9
Junction with RFL_016										
RFD_067	25.58	17.4	25.59	17.5	25.59	17.6	25.57	16.1	25.55	14.7

Junction with RFL_016

Ryeford Saw Mills Culvert										
RFD_068	27.65	17.4	27.73	17.5	27.75	17.5	27.71	16.1	27.75	14.6
RFD_069	27.72	17.0	27.73	17.1	27.75	17.1	27.75	15.8	27.78	14.8
RFD_070	27.84	19.1	27.84	19.3	27.85	19.5	27.85	18.6	27.86	18.1
RFD_071	27.88	19.2	27.89	19.4	27.89	19.7	27.89	18.7	27.89	18.3
RFD_072	27.97	21.0	27.98	21.5	27.99	22.1	27.98	20.6	27.98	20.2
RFD_073	28.06	21.0	28.08	21.4	28.08	22.0	28.06	20.6	28.06	20.1
RFD_074	28.14	21.0	28.16	21.4	28.17	22.0	28.14	20.5	28.13	20.1
RFD_075	28.20	20.9	28.21	21.4	28.23	22.0	28.19	20.5	28.19	20.1
RFD_076	28.39	18.6	28.41	19.0	28.43	19.6	28.38	17.8	28.37	17.0
RFD_077	28.46	20.5	28.48	21.1	28.50	22.0	28.45	19.2	28.44	18.0
RFD_078	28.57	20.4	28.59	21.2	28.61	22.3	28.55	19.2	28.53	18.0

Refuse Tip Weir 2

RFD_079	29.12	20.4	29.16	21.2	29.21	22.3	29.17	19.2	29.22	18.0
RFD_080	29.11	21.1	29.14	22.4	29.18	23.7	29.14	20.7	29.19	20.3

Refuse Tip Weir 3

RFD_081	29.45	21.1	29.50	22.4	29.56	23.7	29.53	20.7	29.62	20.3
RFE_001	15.00	2.5	15.13	2.5	15.19	2.5	15.01	2.5	15.01	2.6
RFE_002	15.07	1.1	15.18	1.1	15.24	1.1	15.08	1.1	15.09	0.9
RFE_003	15.08	0.7	15.19	0.7	15.24	0.7	15.09	0.6	15.09	0.5

	15.09	0.6	15.19	0.6	15.25	0.6	15.09	0.6	15.10	0.5
Marker Garden Weir										
RFE_004	16.00	0.6	16.00	0.6	16.00	0.6	16.00	0.5	15.99	0.5
RFF_005	18.54	0.6	18.55	0.7	18.56	0.8	18.54	0.6	18.53	0.6
RFF_001	18.54	0.6	18.55	0.7	18.56	0.8	18.54	0.6	18.53	0.6
RFF_002	18.54	0.6	18.55	0.7	18.56	0.8	18.54	0.6	18.53	0.6
Beards Mill Culvert										
RFG_003	20.44	0.6	20.49	0.7	20.52	0.8	20.49	0.6	20.52	0.6
RFG_001	16.76	2.2	16.76	2.2	16.76	2.2	16.73	2.1	16.69	1.9
RFG_002	16.82	2.2	16.82	2.2	16.82	2.2	16.79	2.1	16.75	1.9
RFG_003	16.92	2.2	16.92	2.2	16.92	2.2	16.89	2.1	16.86	1.9
RFG_004	17.10	2.2	17.10	2.2	17.10	2.2	17.08	2.1	17.05	1.9
RFG_005	17.23	2.2	17.23	2.2	17.23	2.2	17.21	2.1	17.19	1.9
Bonds Mill Side Sluices										
RFQ_006	19.22	2.2	19.22	2.2	19.23	2.2	19.26	2.1	19.30	1.9
RFH_001	29.80	15.9	29.85	16.7	29.91	17.3	29.81	15.5	29.85	15.0
RFH_002	29.86	16.4	29.92	16.9	29.97	17.1	29.87	15.8	29.90	14.7
RFH_003	29.95	16.6	30.00	16.9	30.04	17.1	29.95	15.8	29.97	14.7
Ebley Com Mill Culverts										
RFH_004	30.32	16.6	30.35	16.9	30.38	17.1	30.35	15.8	30.39	14.7
RFJ_001	20.74	4.0	20.79	4.1	20.82	4.2	20.76	3.8	20.76	3.7
RFJ_002	20.76	4.0	20.80	4.1	20.84	4.2	20.77	3.8	20.78	3.7
Bridgend Mill Culvert										
RFJ_003	21.58	4.0	21.60	4.1	21.61	4.2	21.61	3.8	21.66	3.7
RFK_001	20.81	10.6	20.85	11.2	20.87	11.4	20.82	10.5	20.82	10.2
RFK_002	21.12	3.9	21.15	4.1	" 21.17	" 4.2	21.12	3.6	21.11	3.2
RFK_003	21.15	3.9	21.18	4.1	21.19	4.2	21.14	3.6	21.13	3.2

Bridgeland Mill Bypass Culvert						
RFK_004	22.24	3.9	22.29	4.1	22.31	4.2
RFL_001	22.53	5.0	22.56	4.9	22.58	4.9
RFL_002	22.61	6.8	22.64	7.3	22.67	7.7
RFL_003	22.83	7.1	22.86	7.6	22.89	7.9
RFL_004	23.09	3.5	23.12	3.6	23.14	3.6
RFL_005	23.34	6.0	23.36	6.8	23.37	7.4
RFL_006	23.57	3.9	23.59	3.9	23.60	3.9
RFL_007	23.89	12.1	23.91	12.3	23.91	12.4
RFL_008	24.22	2.6	24.23	2.6	24.24	2.6
RFL_009	24.38	4.7	24.39	4.8	24.40	4.8
RFL_010	24.52	4.5	24.53	4.6	24.54	4.7
Benty Ditch Culvert						
RFL_011	25.37	4.7	25.38	4.8	25.38	4.8
RFL_012	25.38	4.6	25.39	4.7	25.39	4.6
RFL_013	25.38	4.8	25.39	4.8	25.40	4.8
RFL_014	25.40	4.8	25.41	4.8	25.42	4.8
Benty Ditch Weir						
RFL_015	25.58	4.8	25.58	4.8	25.58	4.8
RFL_016	25.58	4.8	25.59	4.8	25.59	4.8
RFM_001	23.45	0.1	23.47	0.1	23.47	0.1
RFM_002	23.45	0.0	23.47	0.0	23.47	0.0
RFM_003	23.45	0.0	23.47	0.0	23.47	0.0
RFN_001	35.15	2.2	35.20	2.2	35.23	2.2
RFN_002	35.16	2.1	35.21	2.2	35.24	2.2
RFN_003	35.18	2.1	35.22	2.2	35.25	2.2

RFN_004	35.19	2.1	35.24	2.2	35.26	2.2	35.20	1.9	35.21	1.9	35.21	1.7
Fromeball Mill Sluice												
RFN_005	36.83	2.1	36.86	2.2	36.88	2.2	36.85	1.9	36.87	1.9	36.87	1.7
RFN_006	36.83	2.1	36.86	2.2	36.88	2.2	36.85	1.9	36.87	1.9	36.87	1.7
RFX_001	32.69	14.3	32.71	15.0	32.72	15.8	32.69	14.3	32.69	14.3	32.69	14.3
RFX_002	32.71	14.3	32.72	15.0	32.74	15.8	32.71	14.3	32.71	14.3	32.71	14.3
RFX_003	32.75	14.3	32.77	15.0	32.79	15.8	32.75	14.3	32.76	14.3	32.76	14.3
Junction with NSA_001												
RFX_004	32.75	0.2	32.77	0.3	32.79	0.3	32.75	0.2	32.76	0.2	32.76	0.2
RFX_005	32.75	0.1	32.77	0.2	32.79	0.2	32.75	0.1	32.76	0.1	32.76	0.1
RFX_006	32.75	0.1	32.77	0.1	32.79	0.1	32.75	0.1	32.76	0.1	32.76	0.1
RFX_007	32.75	0.0	32.77	0.0	32.79	0.0	32.75	0.0	32.76	0.0	32.76	0.0
NSA_001	32.75	14.3	32.77	15.0	32.79	15.8	32.75	14.3	32.76	14.3	32.76	14.3
NSA_002	34.71	14.3	34.76	15.0	34.81	15.8	34.81	14.3	34.93	14.3	34.93	14.3
SCA_001	32.40	13.9	32.43	15.4	32.44	16.9	32.42	13.9	32.43	13.9	32.43	13.9
SCA_002	32.37	13.9	32.38	15.4	32.39	16.9	32.38	13.9	32.39	13.9	32.39	13.9
SCA_003	32.55	13.9	32.59	15.3	32.63	16.7	32.55	13.9	32.57	13.9	32.57	13.9
SCA_004	32.91	13.9	32.99	15.3	33.07	16.7	32.92	13.9	32.92	13.9	32.92	13.9
Duddridge Lock Weir												
SCA_005	35.00	13.9	35.08	15.3	35.17	16.7	35.09	13.9	35.20	13.9	35.20	13.9
SCA_006	36.49	12.3	36.54	13.5	36.59	14.7	36.50	12.3	36.50	12.3	36.50	12.3
Ruscombe Brook Weir												
SCA_007	37.56	12.3	37.63	13.5	37.71	14.7	37.64	12.3	37.74	12.3	37.74	12.3
SCA_008	37.83	12.3	37.90	13.5	37.98	14.7	37.86	12.3	37.92	12.3	37.92	12.3
SCA_009	37.97	12.3	38.05	13.5	38.12	14.7	38.00	12.3	38.04	12.3	38.04	12.3
SCA_010	38.05	12.3	38.14	13.5	38.22	14.7	38.08	12.3	38.11	12.3	38.11	12.3

SCA_011	38.19	12.3	38.28	13.5	38.36	14.8	38.21	12.3	38.24	12.3
SCA_012	38.34	5.5	38.44	6.0	38.53	6.6	38.36	5.5	38.38	5.5
Painswick Stream Weir										
SCA_013	38.41	5.5	38.50	6.1	38.60	6.6	38.43	5.5	38.47	5.5
SCA_014	38.42	5.6	38.52	6.2	38.61	6.8	38.44	5.6	38.48	5.6
Cainscross Road Weir										
SCA_015	40.23	5.7	40.28	6.2	40.33	6.8	40.29	5.7	40.35	5.7
SCA_016	40.43	5.7	40.48	6.2	40.53	6.8	40.46	5.7	40.50	5.7

Model Cell	100 Year Event (original)		100 Year Event + 10% flow		100 Year Event + 20% flow		100 Year Event - 10% coeffs		100 Year Event - 20% coeffs	
	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)
Cell 1	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00
Cell 2	8.10	0.00	8.10	0.00	8.10	0.00	8.10	0.00	8.10	0.00
Cell 3	8.51	0.81	8.67	0.97	8.96	1.26	8.49	0.79	8.54	0.84
Cell 4	8.51	0.41	8.67	0.57	8.97	0.87	8.49	0.39	8.54	0.44
Cell 5	8.40	0.00	8.64	0.24	8.98	0.58	8.40	0.00	8.40	0.00
Cell 6	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00	8.20	0.00
Cell 7	8.40	0.00	8.40	0.00	8.40	0.00	8.40	0.00	8.40	0.00
Cell 8	8.80	0.00	8.80	0.00	8.80	0.00	8.80	0.00	8.80	0.00
Cell 9	8.37	0.00	8.37	0.00	8.37	0.00	8.37	0.00	8.37	0.00
Cell 10	8.38	0.09	8.38	0.09	8.38	0.09	8.38	0.09	8.38	0.09
Cell 11	10.39	1.39	10.73	1.73	10.87	1.87	10.62	1.62	10.72	1.72
Cell 12	10.39	1.39	10.73	1.73	10.87	1.87	10.62	1.62	10.72	1.72
Cell 13	10.39	1.39	10.73	1.73	10.87	1.87	10.62	1.62	10.72	1.72
Cell 14	10.39	1.49	10.73	1.83	10.87	1.97	10.62	1.73	10.72	1.82
Cell 15	10.39	1.09	10.73	1.43	10.88	1.58	10.63	1.33	10.72	1.42
Cell 16	10.47	0.97	10.74	1.24	10.88	1.38	10.63	1.13	10.72	1.22
Cell 17	10.47	1.07	10.74	1.34	10.88	1.48	10.63	1.23	10.73	1.33
Cell 18	10.47	1.07	10.74	1.34	10.89	1.49	10.63	1.23	10.73	1.33
Cell 19	10.60	0.00	10.60	0.00	10.60	0.00	10.60	0.00	10.60	0.00
Cell 20	12.65	1.15	12.67	1.17	12.68	1.18	12.65	1.15	12.65	1.15
Cell 21	11.32	0.92	11.55	1.15	11.75	1.35	11.46	1.06	11.59	1.19
Cell 21A	11.36	0.36	11.56	0.56	11.75	0.75	11.47	0.47	11.59	0.59
Cell 22	12.65	1.15	12.67	1.17	12.68	1.18	12.65	1.15	12.65	1.15
Cell 23	11.32	0.92	11.55	1.15	11.75	1.35	11.46	1.06	11.59	1.19

Cell 24	12.65	1.65	12.67	1.67	12.69	1.69	12.65	1.65	12.65	1.65
Cell 25	11.64	0.74	11.66	0.76	11.76	0.85	11.65	0.75	11.66	0.76
Cell 26	12.65	1.65	12.67	1.67	12.69	1.69	12.65	1.65	12.65	1.65
Cell 27	11.50	0.00	11.50	0.00	11.73	0.23	11.50	0.00	11.50	0.00
Cell 28	12.65	1.15	12.67	1.17	12.69	1.19	12.65	1.15	12.65	1.16
Cell 29	12.00	0.00	12.00	0.00	12.09	0.09	12.00	0.00	12.00	0.00
Cell 30	13.53	2.03	13.55	2.05	13.57	2.07	13.53	2.03	13.55	2.05
Cell 31	12.50	0.00	12.50	0.00	12.65	0.15	12.50	0.00	12.50	0.00
Cell 32	13.53	1.53	13.56	1.56	13.57	1.57	13.53	1.53	13.55	1.55
Cell 33	13.20	0.00	13.20	0.00	13.20	0.00	13.20	0.00	13.20	0.00
Cell 34	13.54	1.04	13.56	1.06	13.58	1.08	13.54	1.03	13.56	1.06
Cell 35	14.40	0.90	14.41	0.91	14.42	0.92	14.38	0.89	14.41	0.91
Cell 36	13.55	1.05	13.57	1.07	13.59	1.09	13.54	1.04	13.57	1.07
Cell 37	14.47	0.97	14.50	1.00	14.51	1.01	14.47	0.97	14.48	0.98
Cell 38	13.70	0.20	13.82	0.32	13.84	0.34	13.56	0.06	13.82	0.32
Cell 39	14.30	0.00	14.30	0.00	14.30	0.00	14.30	0.00	14.30	0.00
Cell 40	14.25	0.00	14.27	0.01	14.49	0.24	14.25	0.00	14.25	0.00
Cell 41	15.02	0.52	15.09	0.59	15.13	0.63	15.02	0.52	15.02	0.52
Cell 42	15.05	1.15	15.11	1.21	15.15	1.25	15.06	1.16	15.05	1.16
Cell 43	15.09	0.69	15.15	0.75	15.19	0.79	15.10	0.70	15.10	0.69
Cell 44	15.22	0.72	15.26	0.76	15.28	0.78	15.22	0.72	15.22	0.72
Cell 45	15.76	1.36	15.77	1.37	15.78	1.38	15.77	1.36	15.76	1.36
Cell 46	15.90	1.50	15.92	1.52	15.93	1.53	15.90	1.50	15.90	1.50
Cell 47	16.27	0.52	16.28	0.53	16.28	0.53	16.27	0.52	16.27	0.52
Cell 48	16.45	0.45	16.47	0.47	16.48	0.48	16.46	0.46	16.46	0.46
Cell 49	17.01	0.26	17.02	0.27	17.02	0.27	17.01	0.26	17.01	0.26

Cell 50	17.30	0.30	17.31	0.31	17.32	0.32	17.30	0.30	17.30	0.30	0.30
Cell 51	17.78	0.33	17.79	0.34	17.80	0.35	17.78	0.33	17.78	0.33	0.33
Cell 52	18.47	0.57	18.48	0.58	18.48	0.58	18.47	0.57	18.47	0.57	0.57
Cell 53	17.45	0.25	17.47	0.27	17.48	0.28	17.46	0.26	17.46	0.26	0.26
Cell 54	17.68	0.68	17.69	0.69	17.70	0.70	17.68	0.69	17.69	0.69	0.69
Cell 55	17.86	0.11	17.88	0.13	17.89	0.14	17.87	0.12	17.88	0.12	0.12
Cell 56	18.36	0.10	18.37	0.12	18.38	0.13	18.36	0.11	18.37	0.12	0.12
Cell 57	19.80	0.80	19.80	0.80	19.81	0.81	19.80	0.80	19.80	0.81	0.81
Cell 58	20.68	1.68	20.73	1.73	20.77	1.77	20.70	1.70	20.71	1.71	1.71
Cell 59	20.69	1.69	20.74	1.74	20.79	1.78	20.71	1.71	20.72	1.72	1.72
Cell 60	20.70	1.29	20.75	1.35	20.79	1.39	20.72	1.32	20.73	1.33	1.33
Cell 61	20.72	0.22	20.78	0.28	20.82	0.32	20.74	0.24	20.75	0.25	0.25
Cell 62	21.29	0.48	21.30	0.50	21.31	0.51	21.29	0.49	21.29	0.49	0.49
Cell 63	21.66	0.46	21.67	0.47	21.68	0.48	21.66	0.46	21.66	0.46	0.46
Cell 64	20.70	0.90	20.76	0.96	20.80	1.00	20.73	0.93	20.73	0.94	0.94
Cell 65	20.73	0.73	20.78	0.78	20.82	0.82	20.75	0.75	20.76	0.76	0.76
Cell 66	21.64	1.25	21.65	1.25	21.66	1.26	21.65	1.25	21.65	1.25	1.25
Cell 67	22.25	0.75	22.29	0.79	22.32	0.82	22.27	0.77	22.29	0.79	0.79
Cell 68	22.27	0.72	22.31	0.76	22.34	0.79	22.29	0.74	22.31	0.76	0.76
Cell 69	22.52	0.72	22.55	0.75	22.57	0.77	22.53	0.73	22.53	0.73	0.73
Cell 70	22.56	0.66	22.59	0.69	22.61	0.71	22.57	0.67	22.57	0.67	0.67
Cell 71	22.60	0.60	22.64	0.64	22.66	0.66	22.61	0.61	22.61	0.61	0.61
Cell 72	23.33	0.33	23.34	0.34	23.35	0.35	23.34	0.34	23.34	0.34	0.34
Cell 73	23.70	0.50	23.74	0.54	23.77	0.57	23.72	0.52	23.73	0.53	0.53
Cell 74	22.85	0.85	22.86	0.85	22.86	0.86	22.85	0.85	22.84	0.84	0.84
Cell 75	23.15	0.65	23.18	0.68	23.19	0.69	23.16	0.66	23.16	0.66	0.66

Cell 76	23.32	0.32	23.35	0.35	23.36	0.36	23.33	0.33	23.33	0.33
Cell 77	23.54	0.43	23.56	0.46	23.57	0.47	23.54	0.44	23.54	0.44
Cell 78	24.23	0.33	24.24	0.34	24.24	0.34	24.23	0.33	24.23	0.33
Cell 79	24.35	0.55	24.37	0.57	24.39	0.59	24.36	0.56	24.37	0.57
Cell 80	24.57	0.32	24.59	0.34	24.60	0.35	24.58	0.33	24.59	0.34
Cell 81	24.99	0.59	25.01	0.61	25.02	0.62	25.00	0.60	25.01	0.61
Cell 82	24.57	0.97	24.59	0.99	24.60	1.00	24.58	0.98	24.59	0.99
Cell 83	25.38	1.38	25.39	1.39	25.39	1.39	25.32	1.32	25.23	1.23
Cell 84	25.40	1.30	25.41	1.31	25.41	1.31	25.34	1.24	25.25	1.15
Cell 85	27.84	0.94	27.85	0.95	27.86	0.96	27.85	0.95	27.86	0.96
Cell 86	27.10	0.00	27.10	0.00	27.10	0.00	27.10	0.00	27.27	0.17
Cell 87	26.40	0.00	26.40	0.00	26.40	0.00	26.40	0.00	26.40	0.00
Cell 88	26.39	0.99	26.64	1.24	26.81	1.41	26.67	1.27	26.96	1.56
Cell 88A	26.61	1.21	26.75	1.35	26.89	1.49	26.76	1.38	26.99	1.59
Cell 89	26.63	0.38	26.76	0.51	26.89	0.64	26.77	0.52	27.00	0.75
Cell 89A	26.63	0.38	26.76	0.51	26.89	0.64	26.77	0.52	27.00	0.75
Cell 90	27.67	0.92	27.71	0.96	27.73	0.98	27.68	0.94	27.70	0.95
Cell 90A	27.66	0.91	27.70	0.94	27.72	0.97	27.68	0.93	27.69	0.94
Cell 91A	27.50	0.00	27.50	0.00	27.82	0.32	27.50	0.00	27.50	0.00
Cell 92	28.42	0.52	28.44	0.54	28.45	0.55	28.42	0.52	28.43	0.53
Cell 93	29.86	0.61	29.92	0.67	29.97	0.72	29.87	0.62	29.90	0.65
Cell 93A	28.39	0.99	28.39	0.99	28.40	1.00	28.39	0.99	28.40	1.00
Cell 94	30.68	0.68	30.71	0.71	30.75	0.75	30.69	0.69	30.71	0.71
Cell 94A	28.38	1.13	28.39	1.14	28.40	1.15	28.39	1.14	28.40	1.15
Cell 95	30.78	1.48	30.77	1.48	30.81	1.51	30.78	1.48	30.76	1.46
Cell 95A	28.30	0.30	28.31	0.31	28.32	0.32	28.32	0.32	28.33	0.33

Cell 96	30.26	0.76	30.28	0.78	30.32	0.82	30.27	0.77	30.29	0.79
Cell 97	30.27	0.52	30.29	0.54	30.33	0.58	30.28	0.53	30.30	0.55
Cell 98	31.96	1.06	32.02	1.12	32.06	1.16	31.98	1.08	32.02	1.12
Cell 99	32.21	0.71	32.22	0.72	32.24	0.74	32.21	0.71	32.22	0.72
Cell 100	32.23	0.23	32.25	0.25	32.27	0.27	32.24	0.24	32.25	0.25
Cell 101	32.60	0.60	32.61	0.61	32.64	0.64	32.60	0.60	32.60	0.60
Cell 102	36.81	0.41	36.83	0.43	36.85	0.45	36.83	0.43	36.84	0.45
Cell 103	36.81	0.81	36.84	0.84	36.85	0.85	36.83	0.83	36.85	0.85
Cell 104	38.96	0.61	39.05	0.70	39.11	0.76	38.95	0.60	38.92	0.57

Section Label	100 Year Event (original)		100 Year Event + 10% flow		100 Year Event + 20% flow		100 Year Event - 10% coeffs		100 Year Event - 20% coeffs	
	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)	Level (mOD)	Flow (m³/s)
RFA_175	39.41	10.7	39.43	11.2	39.46	11.7	39.39	10.3	39.36	9.7
RFA_176	39.74	10.6	39.77	11.2	39.79	11.7	39.72	10.2	39.69	9.7
RFA_177	39.99	10.6	40.02	11.2	40.04	11.7	39.97	10.2	39.94	9.6
RFA_178	40.18	10.6	40.21	11.2	40.23	11.7	40.16	10.2	40.13	9.6
RFA_179	40.39	10.6	40.41	11.1	40.44	11.6	40.37	10.2	40.34	9.6
RFA_180	40.98	10.5	41.01	11.1	41.04	11.6	40.95	10.1	40.92	9.6
Railway Mill Weir										
RFA_181	41.81	10.5	41.84	11.1	41.86	11.6	41.84	10.1	41.88	9.6
RFA_182	41.90	10.5	41.93	11.1	41.96	11.6	41.92	10.1	41.94	9.6
RFA_183	41.96	10.5	41.99	11.1	42.01	11.6	41.97	10.1	41.98	9.6
Thames & Severn Canal Syphon										
RFA_184	43.64	10.5	43.86	11.1	44.07	11.6	43.89	10.1	44.17	9.6
RFA_185	43.64	10.1	43.87	10.2	44.08	10.2	43.90	9.4	44.17	8.6
RFA_186	43.65	10.1	43.87	10.2	44.08	10.2	43.91	9.4	44.16	8.7
Arundell Mill Structures										
RFA_187	43.95	10.1	44.06	10.2	44.20	10.2	44.09	9.4	44.29	8.7
RFA_188	44.01	10.1	44.10	10.2	44.23	10.3	44.12	9.5	44.30	8.8
RFA_189	44.03	10.1	44.11	10.2	44.23	10.3	44.13	9.5	44.30	8.8
Eagle Mills Culvert										
RFA_190	44.64	10.1	44.79	10.2	44.96	10.2	44.78	9.5	44.94	8.8
RFA_191	44.79	10.1	44.90	10.2	45.03	10.2	44.87	9.4	44.98	8.8
RFA_192	44.79	10.4	44.86	11.0	44.95	11.6	44.84	10.1	44.92	9.7
Butterow Hill Bridge										
RFA_193	45.58	10.4	45.80	11.0	46.02	11.6	45.68	10.1	45.80	9.7

RFA_194	45.58	10.4	45.80	11.0	46.01	11.6	45.68	10.1	45.80	10.1	45.80	9.7
Bowbridge Estate Bridge												
RFA_195	45.61	10.3	45.83	11.0	46.04	11.6	45.71	10.0	45.82	10.0	45.82	9.7
RFA_196	45.59	10.3	45.82	11.0	46.04	11.6	45.69	10.0	45.81	10.0	45.81	9.7
RFA_197	45.73	10.3	45.92	10.9	46.11	11.5	45.80	10.0	45.89	10.0	45.89	9.7
RFA_198	45.80	10.3	45.97	10.9	46.15	11.5	45.86	10.0	45.94	10.0	45.94	9.7
Bowbridge Estate Bridge 2												
RFA_199	45.83	10.3	46.01	10.9	46.27	11.5	45.89	10.0	45.97	10.0	45.97	9.7
RFA_200	45.85	10.3	46.03	10.9	46.28	11.5	45.91	10.0	45.99	10.0	45.99	9.6
RFA_201	45.92	10.3	46.08	10.9	46.32	11.5	45.97	10.0	46.03	10.0	46.03	9.6
RFA_202	45.98	10.3	46.13	10.9	46.35	11.5	46.01	10.0	46.07	10.0	46.07	9.6
RFA_203	45.99	10.3	46.13	10.9	46.35	11.5	46.02	10.0	46.08	10.0	46.08	9.7
Butterow Footpath Bridge												
RFA_204	46.25	10.3	46.33	10.9	46.47	11.5	46.28	10.0	46.32	10.0	46.32	9.7
RFA_205	46.28	10.2	46.36	10.9	46.48	11.5	46.31	10.0	46.34	10.0	46.34	9.7
RFA_206	46.28	10.2	46.36	10.9	46.48	11.5	46.31	10.0	46.34	10.0	46.34	9.7
RFA_207	46.42	10.2	46.47	10.9	46.56	11.5	46.43	9.9	46.44	9.9	46.44	9.6
Thrupp Works Weir												
RFA_208	47.20	10.2	47.25	10.9	47.29	11.5	47.25	9.9	47.30	9.9	47.30	9.6
RFA_209	47.20	10.2	47.24	10.9	47.28	11.5	47.24	9.9	47.29	9.9	47.29	9.6
Junction with RFO_001												
RFA_210	47.20	4.7	47.24	5.0	47.28	5.3	47.24	4.6	47.29	4.6	47.29	4.5
RFA_211	47.21	4.6	47.26	4.8	47.30	5.1	47.26	4.4	47.31	4.4	47.31	4.4
RFA_212	47.25	5.1	47.29	5.5	47.33	5.8	47.29	5.1	47.33	5.1	47.33	5.4
RFA_213	47.29	5.1	47.33	5.4	47.37	5.7	47.32	5.1	47.36	5.1	47.36	5.4
RFA_214	47.37	5.1	47.41	5.4	47.45	5.7	47.39	5.0	47.43	5.0	47.43	5.4

Griffin Mill Footbridge 1						
RFA_215	48.33	5.1	48.40	5.4	48.47	5.7
RFA_216	48.34	5.1	48.41	5.4	48.48	5.7
RFA_217	48.36	5.1	48.43	5.4	48.49	5.7
Griffin Mill Bypass						
RFA_218	48.60	5.0	48.63	5.3	48.67	5.7
Junction with RFO_012						
RFA_219	48.60	10.0	48.63	10.7	48.67	11.4
Griffin Mill Access Bridge						
RFA_220	48.65	10.0	48.68	10.7	48.72	11.4
RFA_221	48.79	10.0	48.82	10.6	48.86	11.3
Griffin Mill Footbridge 2						
RFA_222	48.80	10.0	48.84	10.6	48.87	11.3
Junction with RFP_001						
RFA_223	48.80	7.8	48.84	8.3	48.87	8.8
RFA_224	48.90	7.8	48.94	8.3	48.97	8.8
Brookside Bridge 1						
RFA_225	49.12	7.8	49.17	8.3	49.23	8.8
RFA_226	49.18	7.8	49.23	8.3	49.29	8.8
Hem Lock Footbridge						
RFA_227	49.38	7.8	49.46	8.3	49.54	8.8
RFA_228	49.41	7.8	49.48	8.3	49.55	8.8
Swimming Pool Bridge						
RFA_229	49.81	7.8	49.96	8.2	50.15	8.7
RFA_230	49.95	7.8	50.07	8.0	50.24	8.0
Phoenix Mill Bypass Sluices						

RFA_250	55.58	7.7	55.61	7.9	55.63	8.1	55.64	7.4	55.70	7.0
RFA_251	55.59	7.6	55.61	7.9	55.64	8.1	55.64	7.3	55.70	7.0
RFA_252	55.60	7.6	55.62	7.8	55.65	8.1	55.65	7.3	55.71	7.0
Brimsccombe Mill Chemical Works Culvert										
RFA_253	56.34	7.6	56.39	7.8	56.44	8.1	56.35	7.3	56.36	7.0
RFA_254	56.38	9.6	56.43	10.2	56.47	10.9	56.39	9.4	56.40	9.1
Brimsccombe Hill Bridge										
RFA_255	56.39	9.6	56.43	10.2	56.48	10.9	56.40	9.3	56.40	9.1
RFA_256	56.37	9.6	56.41	10.2	56.46	10.9	56.38	9.3	56.39	9.1
Burket Bridge (Port Industrial Estate)										
RFA_257	56.35	9.6	56.38	10.2	56.42	10.9	56.36	9.3	56.37	9.1
RFA_258	56.41	9.5	56.45	10.2	56.50	10.9	56.42	9.3	56.42	9.1
Bensons Culvert										
RFA_259	56.96	9.5	57.03	10.1	57.11	10.9	56.97	9.3	56.97	9.0
RFA_260	57.03	9.5	57.10	10.1	57.18	10.9	57.03	9.3	57.03	9.0
Bensons Bridge										
RFA_261	57.12	9.5	57.20	10.1	57.30	10.9	57.12	9.3	57.12	9.0
RFA_262	57.14	9.5	57.22	10.1	57.32	10.8	57.15	9.2	57.14	9.0
Port Industrial Estate Sluices										
RFA_263	57.29	9.5	57.36	10.1	57.45	10.8	57.31	9.2	57.34	9.0
Port Industrial Estate Bridge										
RFA_264	57.35	9.5	57.43	10.1	57.53	10.8	57.38	9.2	57.40	9.0
RFA_265	57.37	9.4	57.45	10.1	57.55	10.8	57.40	9.2	57.42	8.9
RFA_266	57.42	9.4	57.50	10.0	57.59	10.7	57.44	9.1	57.46	8.9
RFA_267	57.47	9.3	57.54	9.9	57.63	10.7	57.48	9.1	57.50	8.8
RFA_268	57.51	9.3	57.58	9.9	57.66	10.6	57.52	9.1	57.53	8.8

RFA_269	57.49	9.3	57.55	9.9	57.63	10.6	57.50	9.1	57.51	8.8
RFA_270	57.73	9.3	57.78	9.9	57.84	10.6	57.72	9.1	57.71	8.8
RFA_271	57.78	9.3	57.83	9.9	57.89	10.6	57.78	9.0	57.77	8.8

Junction with RFQ_001

RFA_272	57.78	6.5	57.83	7.0	57.89	7.7	57.78	6.5	57.77	6.5
RFA_273	57.95	6.5	57.98	7.0	58.02	7.6	57.94	6.5	57.94	6.4
RFA_274	58.24	3.5	58.26	3.6	58.28	3.8	58.23	3.2	58.22	2.9
RFA_275	58.29	3.4	58.31	3.6	58.33	3.8	58.28	3.2	58.26	2.9

Bourne Mills Bypass

RFA_276	58.55	3.4	58.56	3.6	58.58	3.8	58.56	3.2	58.56	2.9
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Junction with RFQ_004

RFA_277	58.55	9.2	58.56	9.8	58.58	10.5	58.56	8.9	58.56	8.7
RFA_278	58.73	9.1	58.75	9.7	58.78	10.5	58.73	8.9	58.72	8.6
RFA_279	58.93	7.6	58.96	8.6	59.00	9.4	58.93	7.5	58.92	7.1
RFA_280	59.07	7.6	59.11	8.6	59.15	9.4	59.06	7.5	59.04	7.1

Wimberley Mills Well

RFA_281	60.16	7.6	60.21	8.6	60.25	9.4	60.20	7.5	60.23	7.1
RFA_282	60.19	7.6	60.24	8.5	60.28	9.4	60.22	7.5	60.24	7.1
RFA_283	60.19	7.6	60.24	8.5	60.28	9.4	60.23	7.5	60.25	7.1

Wimberley Mills Culvert 1

RFA_284	60.37	7.6	60.44	8.5	60.50	9.4	60.40	7.5	60.40	7.1
RFA_285	60.40	7.6	60.47	8.5	60.52	9.4	60.42	7.5	60.43	7.1
RFA_286	60.49	7.6	60.55	8.5	60.60	9.3	60.50	7.5	60.50	7.1

Wimberley Mills Culvert 1

RFA_287	60.96	7.6	61.03	8.5	61.09	9.3	60.95	7.5	60.92	7.1
RFA_288	60.97	7.6	61.07	8.1	61.15	8.5	60.97	7.3	60.94	6.9

Wimberley Mill Culvert 2						
RFA_289	62.20	7.6	62.22	8.1	62.23	8.5
RFA_290	62.22	7.8	62.24	8.6	62.25	9.4
RFA_291	62.24	7.8	62.26	8.6	62.28	9.4
RFA_292	62.25	7.8	62.28	8.5	62.30	9.4
RFA_293	62.28	7.8	62.31	8.5	62.33	9.4
RFA_294	62.36	7.8	62.40	8.5	62.43	9.4
RFA_295	62.44	7.8	62.48	8.5	62.51	9.4
RFA_296	62.53	7.8	62.57	8.5	62.61	9.3
RFA_297	62.63	7.8	62.68	8.5	62.73	9.3
RFA_298	62.73	7.8	62.78	8.5	62.83	9.3
Junction with RFR_001						
RFA_299	62.73	2.6	62.78	2.8	62.83	2.9
RFA_300	62.93	2.6	62.93	2.8	62.93	2.9
St Marys Mill Canal Control Weir						
RFA_301	63.21	2.6	63.22	2.8	63.24	2.9
RFA_301A	63.22	2.7	63.23	2.8	63.25	3.0
St Marys Mill Bypass Sluices						
RFA_302	64.54	2.7	64.61	2.8	64.69	3.0
Junction with RFR_002						
RFA_303	64.54	7.9	64.61	8.6	64.69	9.4
St Marys House Culvert						
RFA_304	64.70	7.8	64.77	8.5	64.85	9.4
RFA_305	64.82	7.8	64.89	8.5	64.97	9.4

Illes Mill Railway Culvert						
RFA_306	64.88	7.8	64.95	8.5	65.03	9.4
RFA_307	64.93	7.8	65.00	8.5	65.09	9.4
Junction with RFS_001						
RFA_308	64.93	5.6	65.00	6.2	65.09	7.0
RFA_309	65.08	5.6	65.15	6.2	65.22	6.9
Illes Mill Bridge						
RFA_310	65.33	5.6	65.50	6.2	65.72	6.9
RFA_311	65.40	5.6	65.55	6.2	65.76	7.0
Junction with RFT_001						
RFA_312	65.40	5.6	65.55	6.2	65.76	6.9
RFA_313	65.55	5.6	65.66	6.2	65.83	6.9
RFA_314	65.98	2.0	66.01	2.2	66.06	2.3
RFA_315	66.06	2.0	66.09	2.2	66.13	2.3
Illes Mill Bypass Upper Weirs						
RFA_316	66.26	2.0	66.28	2.2	66.30	2.3
Junction with RFS_007						
RFA_317	66.26	7.8	66.28	8.5	66.30	9.4
RFA_318	66.41	7.8	66.45	8.5	66.49	9.4
Belvedere Mill Sluices						
RFA_319	68.27	7.8	68.31	8.5	68.36	9.4
RFA_320	68.27	7.8	68.31	8.5	68.35	9.4
Belvedere Mill Bridge						
RFA_321	68.28	7.8	68.32	8.5	68.38	9.4
RFA_322	68.44	7.8	68.49	8.5	68.55	9.4
RFA_323	68.49	7.8	68.54	8.5	68.62	8.9

Chalford Industrial Estate Sluices						
RFA_324	70.32	7.8	70.56	8.5	70.69	8.9
RFA_325	70.35	7.8	70.57	8.6	70.70	9.5
RFA_326	70.48	7.8	70.65	8.6	70.76	9.5
Chalford Chair & Culvert						
RFA_327	71.95	7.8	71.96	8.6	71.98	9.5
RFA_328	71.97	7.8	71.97	8.6	72.01	9.5
RFA_329	72.00	7.8	72.00	8.6	72.04	9.5
RFA_330	72.84	7.8	72.90	8.6	72.96	9.5
Thanet House Bridge						
RFA_331	73.66	7.8	73.73	8.6	73.81	9.5
RFA_332	73.77	7.8	73.84	8.6	73.91	9.5
Red Lion Bridge						
RFA_333	75.01	7.8	75.15	8.6	75.30	9.5
RFA_334	75.05	7.8	75.20	8.6	75.35	9.5
RFA_335	75.07	7.8	75.21	8.6	75.36	9.5
Brooklyn Bridge						
RFA_336	75.08	7.8	75.22	8.6	75.37	9.5
RFA_337	75.08	7.8	75.23	8.6	75.38	9.5
Sub-station Bridge						
RFA_338	75.09	7.8	75.23	8.6	75.38	9.5
RFA_339	75.09	7.8	75.24	8.7	75.39	9.6
RFA_340	75.11	7.8	75.25	8.7	75.40	9.6
RFA_341	75.11	7.8	75.25	8.7	75.40	9.6
RFA_342	75.12	7.9	75.26	8.7	75.41	9.6
RFA_343	75.13	7.9	75.27	8.7	75.41	9.6

Ridley Mill Weir			
RFA_344	77.49	7.9	77.56
RFA_345	77.49	7.9	77.56
RFA_346	77.62	7.9	77.68
RFA_347	77.95	7.9	78.02

Harley Lane Bridge

Harley Lane Bridge			
RFA_348	79.25	7.9	79.50
RFA_349	79.25	6.9	79.50
RFA_350	79.26	7.0	79.50
RFA_351	79.26	7.0	79.51
RFA_352	79.27	4.8	79.52
RFA_353	79.27	5.2	79.52
RFA_354	79.28	6.2	79.52
RFA_355	79.28	8.0	79.53
RFA_356	79.31	6.2	79.53

Ashmead Mill Sluices

Ashmead Mill Sluices			
RFA_357	79.70	6.2	79.81
RFA_358	79.73	8.0	79.83
RFA_359	79.87	8.0	79.96
RFA_360	80.09	8.0	80.16
RFA_361	80.32	8.0	80.38
RFA_362	80.63	7.9	80.68
RFA_363	81.10	7.9	81.17
RFA_364	81.30	7.9	81.37
RFA_365	81.60	7.0	81.67
RFA_366	81.69	7.0	81.76

Bakers Bridge	
RFA_367	83.08
RFA_368	83.13
RFA_369	83.39
Bakers Mill Sluices	
RFA_370	85.40
RFA_371	85.40
RFA_372	85.41
RFA_373	85.42
RFA_374	85.44
RFA_375	85.53
RFA_376	85.61
RFA_377	86.07
RFA_378	86.73
Puck Mill Culvert	
RFA_379	93.38
RFA_380	93.38
RFA_381	93.38
RFA_382	93.38
RFA_383	93.38
RFA_384	93.38
RFA_385	93.38
RFA_386	93.39
RFA_387	93.39
RFA_388	93.39
RFA_389	93.40

RFO_001	47.20	5.5	47.24	5.8	47.28	6.2	47.24	5.3	47.29	5.1
RFO_002	47.22	5.6	47.26	6.0	47.30	6.4	47.26	5.5	47.31	5.2
RFO_003	47.25	5.0	47.29	5.3	47.33	5.7	47.28	4.8	47.33	4.2
RFO_004	47.28	5.0	47.31	5.3	47.36	5.7	47.31	4.8	47.34	4.2
RFO_005	47.30	5.0	47.34	5.3	47.37	5.7	47.33	4.8	47.35	4.2

Griffin Mill Footbridge 3

RFO_006	47.33	5.0	47.39	5.3	47.46	5.7	47.37	4.8	47.39	4.2
RFO_007	47.34	5.0	47.40	5.3	47.47	5.7	47.37	4.8	47.40	4.2

Griffin Mill Weir 1

RFO_008	47.81	5.0	47.83	5.3	47.86	5.7	47.83	4.8	47.82	4.2
RFO_009	47.82	5.0	47.85	5.3	47.87	5.7	47.84	4.8	47.83	4.2

Griffin Mill Culvert

RFO_010	48.17	5.0	48.22	5.3	48.27	5.7	48.18	4.8	48.12	4.2
RFO_011	48.21	5.0	48.25	5.3	48.30	5.7	48.21	4.8	48.15	4.2

Griffin Mill Weir 2

RFO_012	48.60	5.0	48.63	5.3	48.67	5.7	48.63	4.8	48.72	4.2
RFP_001	48.80	2.2	48.84	2.3	48.87	2.5	48.81	2.0	48.85	1.9
RFP_002	48.81	2.2	48.85	2.3	48.88	2.5	48.82	2.0	48.86	1.9

Brookside Bridge 2

RFP_003	48.82	2.2	48.85	2.3	48.89	2.5	48.82	2.0	48.87	1.9
RFP_004	48.84	2.2	48.87	2.3	48.91	2.5	48.84	2.0	48.88	1.9

Phoenix Mill Culvert

RFP_005	50.19	2.2	50.27	2.3	50.35	2.5	50.23	2.0	50.27	1.9
RFP_006	50.19	2.2	50.27	2.7	50.35	4.6	50.23	2.0	50.27	2.2
RFQ_001	57.78	2.8	57.83	2.8	57.89	2.9	57.78	2.5	57.77	2.3
RFQ_002	57.84	2.8	57.87	2.8	57.92	2.9	57.83	2.5	57.81	2.3

Bourne Mills Sluice						
RFQ_003	58.51	2.8	58.53	2.8	58.55	2.9
RFQ_004	58.55	5.7	58.56	6.2	58.58	6.7
RFR_001	62.73	5.2	62.78	5.7	62.83	6.4
St Mary's Mill Culvert						
RFR_002	64.54	5.2	64.61	5.7	64.69	6.4
RFS_001	64.93	2.2	65.00	2.3	65.09	2.4
RFS_002	64.94	2.2	65.01	2.3	65.10	2.4
Iles Mill Culvert						
RFS_003	66.16	2.2	66.17	2.3	66.19	2.4
RFS_004	66.15	2.2	66.16	2.3	66.17	2.4
Junction with RFT_003						
RFS_005	66.15	2.2	66.16	2.3	66.17	2.5
RFS_006	66.18	5.8	66.19	6.4	66.20	7.0
RFS_007	66.26	5.8	66.28	6.4	66.30	7.0
RFT_001	65.40	0.0	65.55	0.0	65.76	0.0
RFT_002	65.40	0.0	65.55	0.0	65.76	0.0
Iles Mill Bypass Sluices						
RFT_003	66.15	0.0	66.16	0.0	66.17	0.0
SCB_001	43.91	0.0	44.01	0.0	44.19	0.0
SCB_002	43.91	0.4	44.01	1.0	44.19	2.1
SCB_003	43.91	0.4	44.01	1.0	44.19	2.1
SCB_004	43.91	0.4	44.01	1.0	44.19	2.1
SCB_005	43.91	0.4	44.02	1.0	44.20	2.1
SCB_006	43.92	0.1	44.02	0.1	44.20	0.1

Butterow Hill Canal Bridge

SCB_007	43.92	0.1	44.02	0.1	44.20	0.1	44.00	0.1	44.25	0.1
SCB_008	43.92	0.1	44.02	0.1	44.20	0.1	44.00	0.1	44.25	0.1

Bowbridge Lock Weir

SCB_009	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_010	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_011	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_012	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_013	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_014	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1
SCB_015	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1	46.34	0.1

Grimlings Mill Lock Weir

SCB_016	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.37	0.1
SCB_017	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.37	0.1
SCB_018	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.37	0.1
SCB_019	49.36	0.1	49.36	0.1	49.36	0.1	49.36	0.1	49.37	0.1

Ham Lock Weir

SCB_020	52.03	0.1	52.03	0.1	52.03	0.1	52.04	0.1	52.04	0.1
SCB_021	52.03	0.1	52.03	0.1	52.03	0.1	52.04	0.1	52.04	0.1
SCB_022	52.03	0.1	52.03	0.1	52.03	0.1	52.04	0.1	52.04	0.1
SCB_023	52.03	0.1	52.03	0.1	52.03	0.1	52.04	0.1	52.04	0.1
SCB_024	52.76	0.1	52.76	0.1	52.76	0.1	52.76	0.1	52.76	0.1
SCC_001	59.78	0.0	59.80	0.0	59.81	0.0	59.78	0.0	59.79	0.0
SCC_002	59.81	0.1	59.82	0.1	59.83	0.1	59.80	0.0	59.80	0.0
SCC_003	59.84	0.1	59.85	0.1	59.86	0.1	59.83	0.0	59.83	0.0
SCC_004	59.85	0.1	59.86	0.1	59.87	0.1	59.84	0.0	59.83	0.0
SCC_005	59.85	0.1	59.86	0.1	59.87	0.1	59.84	0.0	59.84	0.0

Wimberley Canal Weir						
SCC_006	63.09	0.1	63.09	0.1	63.10	0.1
SCC_007	63.09	0.1	63.09	0.1	63.10	0.1
SCC_008	63.09	0.1	63.09	0.1	63.10	0.1
SCC_009	63.09	0.1	63.09	0.1	63.10	0.1
SCC_010	63.09	0.1	63.09	0.1	63.10	0.1
SCC_011	63.09	0.1	63.09	0.1	63.10	0.1
SCC_012	63.09	0.0	63.09	0.0	63.10	0.0
SCC_013	63.09	0.0	63.09	0.0	63.10	0.0
Iles Mill Canal Culvert						
SCC_014	64.58	0.0	64.58	0.0	64.58	0.0
SCC_015	64.77	0.0	64.77	0.0	64.78	0.0
Iles Lock Weir						
SCC_016	67.37	0.0	67.37	0.0	67.37	0.0
SCC_017	67.40	0.0	67.40	0.0	67.41	0.0
Belvedere Mill Canal Culvert						
SCC_018	70.16	0.0	70.16	0.0	70.17	0.0
SCC_019	70.18	0.0	70.18	0.0	70.18	0.0
Chalford Canal Culvert 1						
SCC_020	70.51	0.0	70.51	0.0	70.51	0.0
SCC_021	70.52	0.0	70.52	0.0	70.53	0.0
Chalford Canal Culvert 2						
SCC_022	72.06	0.0	72.06	0.0	72.06	0.0
SCC_023	72.15	0.0	72.15	0.0	72.16	0.0
Chalford Chaltra Canal Culvert						
SCC_024	74.12	0.0	74.12	0.0	74.13	0.0
					74.11	0.0
					74.11	0.0

	74.34	0.0	74.34	0.0	74.36	0.0	74.30	0.0	74.27	0.0
SCC_025	74.44	0.0	74.45	0.0	74.47	0.0	74.39	0.0	74.34	0.0
Clowes Bridge Lock Well										
SCC_027	76.85	0.0	76.85	0.0	76.85	0.0	76.84	0.0	76.84	0.0
SCC_028	76.92	0.0	76.93	0.0	76.93	0.0	76.92	0.0	76.91	0.0
SCC_029	77.05	0.0	77.05	0.0	77.06	0.0	77.04	0.0	77.02	0.0
SCC_030	77.08	0.0	77.09	0.0	77.09	0.0	77.07	0.0	77.04	0.0
SCC_032	79.78	0.0	79.78	0.0	79.79	0.0	79.77	0.0	79.77	0.0
SCC_033	79.78	0.0	79.78	0.0	79.79	0.0	79.77	0.0	79.77	0.0
SCC_034	79.78	0.0	79.78	0.0	79.79	0.1	79.77	0.0	79.77	0.0
SCC_035	79.78	0.8	79.78	0.8	79.79	0.9	79.78	0.7	79.77	0.6
SCC_036	79.80	0.8	79.80	0.8	79.81	0.9	79.79	0.7	79.78	0.6
SCC_037	79.81	0.8	79.81	0.8	79.81	0.9	79.80	0.7	79.79	0.6
SCC_038	79.82	0.8	79.83	0.8	79.83	0.9	79.81	0.7	79.80	0.6
SCC_039	79.88	0.8	79.88	0.8	79.89	0.9	79.86	0.7	79.84	0.6
SCC_040	79.90	0.8	79.91	0.8	79.91	0.9	79.88	0.7	79.86	0.6
SCC_041	79.91	0.8	79.92	0.8	79.93	0.9	79.89	0.7	79.87	0.6
SCC_042	79.94	0.8	79.94	0.8	79.95	0.9	79.92	0.7	79.89	0.6
SCC_043	79.98	0.8	79.99	0.8	79.99	0.9	79.96	0.7	79.94	0.6
SCC_044	80.02	0.8	80.03	0.8	80.04	0.9	80.00	0.7	79.98	0.6
SCC_045	80.05	0.8	80.05	0.8	80.06	0.9	80.02	0.7	80.00	0.6
SCC_046	80.06	0.8	80.07	0.8	80.07	0.9	80.04	0.7	80.01	0.6
Bakers Mill Lower Lock Well										
SCC_047	83.17	0.8	83.17	0.8	83.18	0.9	83.16	0.7	83.16	0.6
SCC_048	83.17	1.7	83.17	1.8	83.18	2.0	83.16	1.6	83.16	1.4
SCC_049	83.17	1.7	83.17	1.8	83.18	2.0	83.16	1.6	83.16	1.4

SCC_050	83.17	1.7	83.17	1.8	83.18	2.0	83.16	1.6	83.16	1.4
Bakers Mill Upper Lock Weir										
SCC_051	85.44	1.7	85.46	1.8	85.49	2.0	85.45	1.6	85.45	1.4
SCC_052	85.44	3.9	85.46	4.3	85.48	4.6	85.45	3.7	85.45	3.5
SCC_053	85.45	3.9	85.47	4.3	85.49	4.6	85.45	3.7	85.46	3.5
SCC_054	85.46	3.9	85.48	4.3	85.51	4.6	85.46	3.7	85.46	3.5
SCC_055	85.48	3.9	85.50	4.3	85.53	4.7	85.48	3.7	85.48	3.5
SCC_056	85.49	3.9	85.52	4.3	85.55	4.6	85.49	3.7	85.49	3.5
SCC_057	85.51	3.9	85.53	4.3	85.56	4.6	85.50	3.7	85.50	3.5
Puck Mill Lower Lock Weir										
SCC_058	88.27	3.9	88.31	4.3	88.34	4.6	88.30	3.7	88.32	3.5
SCC_059	88.27	4.1	88.31	5.0	88.34	6.0	88.30	4.3	88.32	4.5
Puck Mill Upper Lock Weir										
SCC_060	91.02	4.1	91.11	5.0	91.20	6.0	91.09	4.3	91.17	4.5
SCC_061	91.73	4.1	91.79	5.0	91.84	6.0	91.66	4.3	91.61	4.5
Whitchell Lower Lock Weir										
SCC_062	93.36	4.1	93.52	5.0	93.68	6.0	93.49	4.3	93.62	4.5
SCC_063	93.38	3.4	93.54	4.1	93.70	4.9	93.50	3.6	93.64	3.7
SCC_064	93.38	2.9	93.54	3.5	93.70	4.0	93.50	3.0	93.64	3.2
SCC_065	93.38	3.3	93.54	3.8	93.70	4.3	93.51	3.3	93.64	3.3
SCC_066	93.38	3.2	93.54	3.6	93.70	4.0	93.51	3.2	93.64	3.2
SCC_067	93.39	3.4	93.55	3.9	93.71	4.3	93.51	3.5	93.64	3.4
SCC_068	93.39	3.3	93.56	3.7	93.71	4.1	93.51	3.4	93.64	3.4
SCC_069	93.39	2.8	93.55	3.3	93.71	3.6	93.51	2.9	93.64	3.0
SCC_070	93.39	0.0	93.55	0.0	93.71	0.0	93.51	0.0	93.64	0.0

Model Cell	100 Year Event (original)		100 Year Event + 10% flow		100 year Event + 20% flow		100 year Event - 10% coeffs		100 Year Event - 20% coeffs	
	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)
Cell 107	47.55	0.00	47.55	0.00	47.55	0.00	47.55	0.00	47.55	0.00
Cell 108	52.00	0.00	52.00	0.00	52.00	0.00	52.00	0.00	52.00	0.00
Cell 109	53.00	0.00	53.00	0.00	53.00	0.00	53.00	0.00	53.00	0.00
Cell 110	55.57	1.07	55.58	1.08	55.59	1.09	55.57	1.07	55.57	1.07
Cell 111	55.57	1.02	55.59	1.04	55.60	1.05	55.57	1.02	55.58	1.03
Cell 112	57.00	0.00	57.00	0.00	57.00	0.00	57.00	0.00	57.00	0.00
Cell 113	57.40	0.00	57.40	0.00	57.40	0.00	57.40	0.00	57.40	0.00
Cell 114	57.75	0.00	57.75	0.00	57.75	0.00	57.75	0.00	57.75	0.00
Cell 115	57.75	0.00	57.75	0.00	57.75	0.00	57.75	0.00	57.75	0.00
Cell 116	61.44	0.54	62.01	1.11	62.18	1.28	61.87	0.97	61.88	0.98
Cell 117	61.44	0.54	62.01	1.11	62.18	1.28	61.87	0.97	61.88	0.97
Cell 118	64.82	1.82	64.89	1.89	64.97	1.97	64.83	1.83	64.83	1.83
Cell 119	70.50	0.00	70.50	0.00	70.50	0.00	70.50	0.00	70.50	0.00
Cell 120	69.00	0.00	69.52	0.52	70.67	1.67	69.06	0.06	70.50	1.50
Cell 121	79.26	2.26	79.51	2.51	79.75	2.75	79.31	2.31	79.33	2.33
Cell 122	79.26	2.26	79.51	2.51	79.75	2.75	79.31	2.31	79.33	2.33
Cell 123	79.27	2.17	79.52	2.42	79.76	2.66	79.32	2.22	79.34	2.24
Cell 124	79.27	1.72	79.52	1.97	79.76	2.21	79.32	1.77	79.34	1.79
Cell 125	79.28	1.68	79.52	1.92	79.76	2.16	79.32	1.72	79.34	1.74
Cell 126	79.28	1.58	79.53	1.82	79.77	2.06	79.33	1.62	79.34	1.65
Cell 127	79.31	1.21	79.53	1.43	79.77	1.67	79.35	1.25	79.36	1.26
Cell 128	79.47	1.38	79.64	1.54	79.85	1.75	79.50	1.40	79.51	1.41
Cell 129	80.50	0.00	80.50	0.00	80.50	0.00	80.50	0.00	80.50	0.00
Cell 130	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00

Cell 131	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00	79.80	0.00
Cell 132	80.40	0.00	80.40	0.00	80.40	0.00	80.40	0.00	80.40	0.00
Cell 133	80.95	0.00	81.17	0.22	81.24	0.29	80.95	0.00	80.95	0.00
Cell 134	81.10	0.00	81.10	0.00	81.24	0.14	81.10	0.00	81.10	0.00
Cell 135	81.60	0.00	81.60	0.00	81.60	0.00	81.60	0.00	81.60	0.00
Cell 137	85.40	2.22	85.43	2.25	85.45	2.27	86.41	2.23	85.42	2.24
Cell 138	85.41	2.31	85.43	2.33	85.46	2.36	85.42	2.32	85.42	2.33
Cell 139	85.42	1.94	85.44	1.96	85.46	1.98	85.42	1.94	85.43	1.95
Cell 140	85.42	1.62	85.45	1.65	85.47	1.67	85.43	1.63	85.44	1.64
Cell 141	93.38	2.72	93.54	2.88	93.70	3.04	93.50	2.85	93.64	2.98
Cell 142	93.38	2.64	93.54	2.80	93.70	2.96	93.51	2.77	93.64	2.80
Cell 143	93.38	2.58	93.54	2.74	93.70	2.90	93.51	2.71	93.64	2.84
Cell 144	93.38	2.43	93.55	2.60	93.70	2.75	93.51	2.56	93.64	2.69
Cell 145	93.39	2.19	93.55	2.35	93.71	2.51	93.51	2.31	93.64	2.44
Cell 146	93.39	2.19	93.55	2.35	93.71	2.51	93.51	2.31	93.64	2.44
Cell 147	93.39	1.99	93.55	2.15	93.71	2.31	93.51	2.11	93.65	2.25

NSA_019	39.70	14.4	39.98	15.4	40.28	16.3	39.85	13.6	40.03	12.8
NSA_020	39.74	14.4	40.03	15.4	40.32	16.3	39.89	13.6	40.05	12.8
NSA_021	39.77	14.4	40.05	15.3	40.34	16.3	39.91	13.6	40.07	12.8
NSA_022	39.80	14.4	40.06	15.3	40.35	16.3	39.93	13.6	40.08	12.8

Cotswold House Bridge

NSA_023	39.96	14.3	40.16	15.3	40.41	16.3	40.04	13.6	40.15	12.8
NSA_024	39.98	14.3	40.16	15.3	40.41	16.3	40.05	13.6	40.15	12.8

New Tynings Footbridge

NSA_025	40.05	14.3	40.24	15.3	40.47	16.3	40.11	13.6	40.20	12.8
NSA_026	40.11	14.3	40.28	15.3	40.50	16.3	40.15	13.6	40.23	12.8
NSA_027	40.20	14.3	40.34	15.3	40.53	16.3	40.22	13.6	40.28	12.8

The Priory Bridge

NSA_028	40.55	14.3	40.65	15.3	40.78	16.3	40.55	13.6	40.56	12.8
NSA_029	40.58	14.3	40.69	15.3	40.82	16.3	40.58	13.6	40.59	12.8
NSA_030	40.65	14.3	40.75	15.3	40.87	16.3	40.65	13.6	40.65	12.8
NSA_031	40.68	14.3	40.78	15.3	40.90	16.3	40.67	13.6	40.67	12.8
NSA_032	40.72	14.3	40.82	15.3	40.94	16.3	40.71	13.6	40.70	12.8
NSA_033	40.75	14.3	40.84	15.3	40.96	16.3	40.74	13.6	40.73	12.8
NSA_034	40.80	14.3	40.88	15.3	40.99	16.3	40.78	13.6	40.76	12.8
NSA_035	40.86	14.3	40.95	15.3	41.05	16.3	40.84	13.5	40.82	12.8
NSA_036	40.85	14.2	40.93	15.3	41.03	16.3	40.83	13.5	40.81	12.8

Junction with NSB_001

	NSA_037	40.85	9.5	40.93	10.2	41.03	10.8	40.83	9.0	40.81	8.5
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Roosmoor III Culvan - Right

NSA_038	44.88	9.5	45.38	10.2	45.91	10.8	45.27	9.0	45.72	8.5
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Rooksmoor Mill Wör

NSA_039	44.92	9.5	45.42	10.2	45.95	10.8	45.30	9.0
							45.75	8.5
Junction with NSB_002								
NSA_040	44.92	14.3	45.42	15.3	45.95	16.3	45.30	13.6
NSA_041	44.92	14.4	45.42	15.5	45.95	16.6	45.30	13.7
NSA_042	44.92	14.4	45.42	15.7	45.95	16.7	45.30	13.8
NSA_043	44.92	14.5	45.42	15.9	45.95	16.9	45.30	14.0
NSA_044	44.92	14.6	45.42	16.0	45.95	17.1	45.30	14.0
Selsley Road Bridge								
NSA_045	44.94	14.6	45.43	16.1	45.95	17.2	45.31	14.1
							45.76	13.6
Selsley Road Weir								
NSA_046	45.06	14.6	45.54	16.1	46.05	17.2	45.42	14.1
NSA_047	45.07	14.7	45.54	16.3	46.05	17.4	45.42	14.3
							45.86	13.8
Pauls Rise Bridge								
NSA_048	45.14	14.7	45.57	16.4	46.06	17.6	45.45	14.3
NSA_049	45.14	14.8	45.57	16.6	46.06	17.9	45.46	14.4
NSA_050	45.16	14.8	45.58	16.7	46.07	18.2	45.47	14.5
NSA_051	45.17	14.8	45.58	16.9	46.07	18.5	45.47	14.6
							45.88	14.8
Railway Bridge								
NSA_052	45.40	14.9	45.83	17.0	46.24	18.7	45.69	14.7
NSA_053	45.43	15.0	45.85	17.1	46.25	18.9	45.71	14.8
							46.04	15.1
The Forge Weir								
NSA_054	45.71	15.0	46.10	17.2	46.46	19.0	45.97	14.8
NSA_055	45.73	15.0	46.11	17.2	46.46	19.0	45.98	14.8
							46.28	15.1
Birds Crossing								
NSA_056	46.12	15.0	46.41	17.2	46.56	19.1	46.33	14.9
NSA_057	46.15	15.1	46.42	17.2	46.57	19.1	46.34	14.9
							46.41	15.3

NSA_058	46.15	15.2	46.43	17.1	46.57	19.1	46.35	15.0	46.42	15.3
NSA_059	46.16	15.3	46.43	17.1	46.57	19.2	46.35	15.0	46.42	15.3
NSA_060	46.17	15.3	46.44	17.1	46.58	19.2	46.36	15.1	46.43	15.3
NSA_061	46.17	15.4	46.44	17.1	46.58	19.2	46.35	15.2	46.42	15.3
Station Road Works										
NSA_062	46.80	15.4	47.10	17.1	47.28	19.2	47.02	15.2	47.20	15.3
Station Road Bridge										
NSA_063	47.36	15.4	47.58	17.1	47.75	19.2	47.53	15.2	47.71	15.3
NSA_064	47.36	15.4	47.58	17.1	47.75	19.2	47.53	15.2	47.71	15.2
South Woodchester Works Bridge										
NSA_065	47.45	15.4	47.64	17.1	47.80	19.2	47.59	15.2	47.75	15.3
NSA_066	47.47	15.4	47.65	17.2	47.80	19.2	47.60	15.3	47.76	15.3
NSA_067	47.49	15.4	47.67	17.2	47.82	19.2	47.62	15.3	47.77	15.3
NSA_068	47.52	15.4	47.69	17.3	47.85	19.3	47.64	15.3	47.79	15.3
NSA_069	47.52	15.5	47.70	17.3	47.85	19.3	47.64	15.4	47.79	15.4
NSA_070	47.53	15.5	47.70	17.4	47.88	19.3	47.65	15.4	47.79	15.5
NSA_071	47.53	15.5	47.71	17.4	47.86	19.3	47.65	15.5	47.79	15.5
NSA_072	47.55	15.5	47.72	17.5	47.87	19.4	47.66	15.5	47.80	15.6
NSA_073	47.70	15.5	47.84	17.5	47.98	19.4	47.77	15.5	47.88	15.6
NSA_074	47.76	15.5	47.89	17.4	48.01	19.4	47.82	15.5	47.91	15.6
NSA_075	47.95	15.5	48.03	17.4	48.12	19.3	47.97	15.5	48.01	15.6
Frogmarsh Lane Bridge										
NSA_076	49.28	15.4	49.45	17.4	49.61	19.3	49.35	15.5	49.39	15.6
NSA_077	49.31	15.4	49.49	17.4	49.65	19.3	49.38	15.4	49.42	15.5
Bath Road Bridge										
NSA_078	49.33	15.4	49.51	17.4	49.77	19.3	49.40	15.4	49.45	15.5

NSA_079	49.34	15.4	49.52	17.4	49.78	19.3	49.41	15.4	49.46	15.5
NSA_080	49.38	15.4	49.55	17.4	49.80	19.3	49.44	15.4	49.48	15.5
NSA_081	49.38	15.4	49.55	17.4	49.79	19.3	49.44	15.4	49.48	15.4
NSA_082	49.40	15.4	49.57	17.4	49.81	19.4	49.46	15.4	49.50	15.4

Merretts Mills Bridge

NSA_083	49.62	15.4	49.82	17.4	50.03	19.4	49.70	15.4	49.76	15.4
NSA_084	49.66	15.4	49.85	17.4	50.05	19.4	49.73	15.4	49.79	15.4
NSA_085	49.70	15.3	49.88	17.4	50.07	19.4	49.76	15.4	49.81	15.4

Merretts Mills Culvert

NSA_086	50.92	15.3	50.94	17.3	50.95	19.4	51.02	15.3	51.09	15.4
NSA_087	50.93	15.2	50.94	17.3	50.96	19.4	51.02	15.3	51.09	15.3
NSA_088	50.92	15.2	50.94	17.3	50.95	19.3	51.01	15.3	51.09	15.3

Inchbrook Bridge

NSA_089	51.00	15.2	51.02	17.3	51.04	19.3	51.09	15.3	51.15	15.3
NSA_090	51.01	15.2	51.03	17.3	51.05	19.3	51.09	15.2	51.16	15.3
NSA_092	51.63	15.1	51.70	17.2	51.78	19.2	51.83	15.1	51.64	15.2

Critchleys Bridge 1

NSA_093	52.05	15.1	52.30	17.2	52.48	19.2	52.08	15.1	52.12	15.2
NSA_094	52.15	15.1	52.37	17.1	52.55	19.2	52.18	15.1	52.21	15.2

Junction with NSC_001

NSA_095	52.15	6.2	52.37	8.2	52.55	10.1	52.18	6.7	52.21	7.4
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Critchleys (New) Culvert

NSA_096	52.34	6.2	52.74	8.2	53.04	10.1	52.40	6.7	52.49	7.4
NSA_097	52.48	2.3	52.88	3.6	53.16	5.4	52.55	2.6	52.65	3.0

Critchleys Bridge 2

NSA_098	52.51	2.3	52.99	3.6	53.39	5.4	52.62	2.6	52.74	3.0
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NSA_099	52.52	2.3	52.99	3.5	53.41	4.8	52.62	2.6	52.75	3.0
NSA_100	52.56	1.3	53.03	1.3	53.43	1.4	52.66	1.2	52.79	1.1

Dunkirk Mills Culvert

NSA_101	55.96	1.2	56.09	1.3	56.19	1.3	56.05	1.2	56.15	1.1
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Junction with NSC_016

NSA_102	55.96	7.3	56.09	8.9	56.19	10.2	56.05	7.6	56.15	7.8
NSA_103	55.97	7.3	56.10	8.9	56.20	10.2	56.06	7.6	56.16	7.8
NSA_104	55.99	7.3	56.12	8.9	56.22	10.2	56.07	7.5	56.17	7.8
NSA_105	56.04	7.3	56.17	8.9	56.26	10.6	56.12	7.5	56.20	7.8
NSA_106	56.14	7.3	56.27	8.9	56.36	10.6	56.20	7.5	56.27	7.7
NSA_107	56.25	6.6	56.40	7.1	56.52	7.9	56.30	6.5	56.36	6.5
NSA_108	56.30	7.8	56.45	8.1	56.57	8.3	56.35	7.8	56.40	7.9
NSA_109	56.34	8.2	56.46	8.7	56.58	9.2	56.37	8.4	56.42	8.6
NSA_110	56.40	8.6	56.49	9.4	56.60	10.1	56.42	8.9	56.45	9.2
NSA_111	56.52	8.6	56.60	9.4	56.69	10.1	56.54	8.9	56.56	9.1
NSA_112	56.62	8.6	56.69	9.4	56.78	10.1	56.64	8.9	56.66	9.1
NSA_113	56.66	9.3	56.73	10.3	56.81	11.2	56.68	9.6	56.70	9.9

Junction with NSE_001

NSA_114	56.66	11.9	56.73	12.7	56.81	13.5	56.68	11.9	56.70	11.8
NSA_115	56.75	13.6	56.80	14.6	56.87	15.5	56.76	13.6	56.77	13.6
NSA_116	56.90	14.8	56.92	16.2	56.97	17.7	56.90	14.8	56.90	14.8
NSA_117	57.10	14.8	57.15	16.2	57.20	17.7	57.10	14.8	57.10	14.8
NSA_118	57.20	14.8	57.27	16.2	57.32	17.7	57.20	14.8	57.20	14.8

Garage Culvert

NSA_119	58.76	14.8	59.02	16.2	59.42	17.7	58.88	14.8	59.01	14.7
NSA_120	58.74	14.8	59.01	16.2	59.41	17.7	58.87	14.7	59.00	14.7

NSA_121	58.79	14.8	59.04	16.2	59.43	17.7	58.90	14.8	59.02	14.8
Egypt Mill Weir & Wheel										
NSA_122	58.94	14.8	59.17	16.2	59.53	17.7	59.06	14.8	59.19	14.8
NSA_124	58.92	14.8	59.16	16.3	59.53	17.7	59.05	14.8	59.18	14.8
NSB_001	40.85	4.8	40.93	5.1	41.03	5.5	40.83	4.5	40.81	4.3
Rooksmoor Mill Culvert - Left										
NSB_002	44.92	4.8	45.42	5.1	45.95	5.5	45.30	4.5	45.75	4.3
NSC_001	52.15	9.0	52.37	9.1	52.55	9.2	52.18	8.4	52.21	7.8
Critchley's Left Hand Culvert										
NSC_002	53.16	9.0	53.21	9.1	53.28	9.3	53.20	8.4	53.24	7.9
NSC_003	53.16	9.0	53.22	9.2	53.28	9.3	53.20	8.4	53.24	7.9
NSC_004	53.22	7.6	53.27	7.6	53.33	7.7	53.25	7.1	53.28	6.6
NSC_005	53.29	7.5	53.33	7.5	53.38	7.5	53.30	7.0	53.32	6.5
NSC_006	53.29	11.4	53.33	11.9	53.38	12.2	53.30	11.1	53.32	10.8
Junction with NSD_001										
NSC_007	53.29	6.1	53.33	6.5	53.38	6.8	53.30	6.0	53.32	5.9
Critchley's Bridge 3										
NSC_008	53.31	6.1	53.35	6.5	53.39	6.8	53.32	6.0	53.34	5.9
Critchley's Bridge 4										
NSC_009	53.45	6.1	53.52	6.5	53.58	6.8	53.48	6.0	53.51	5.9
NSC_010	53.47	6.1	53.53	6.6	53.59	7.3	53.49	6.0	53.52	6.0
NSC_011	53.47	7.1	53.54	8.9	53.59	10.7	53.50	7.5	53.52	7.9
Tennis Court Bridge 2										
NSC_012	53.50	7.1	53.57	8.9	53.64	10.7	53.76	7.5	53.56	7.9
NSC_013	53.50	7.1	53.57	8.8	53.63	10.6	53.75	7.5	53.55	7.8
NSC_014	53.56	6.1	53.65	7.6	53.74	8.9	53.79	6.4	53.62	6.7

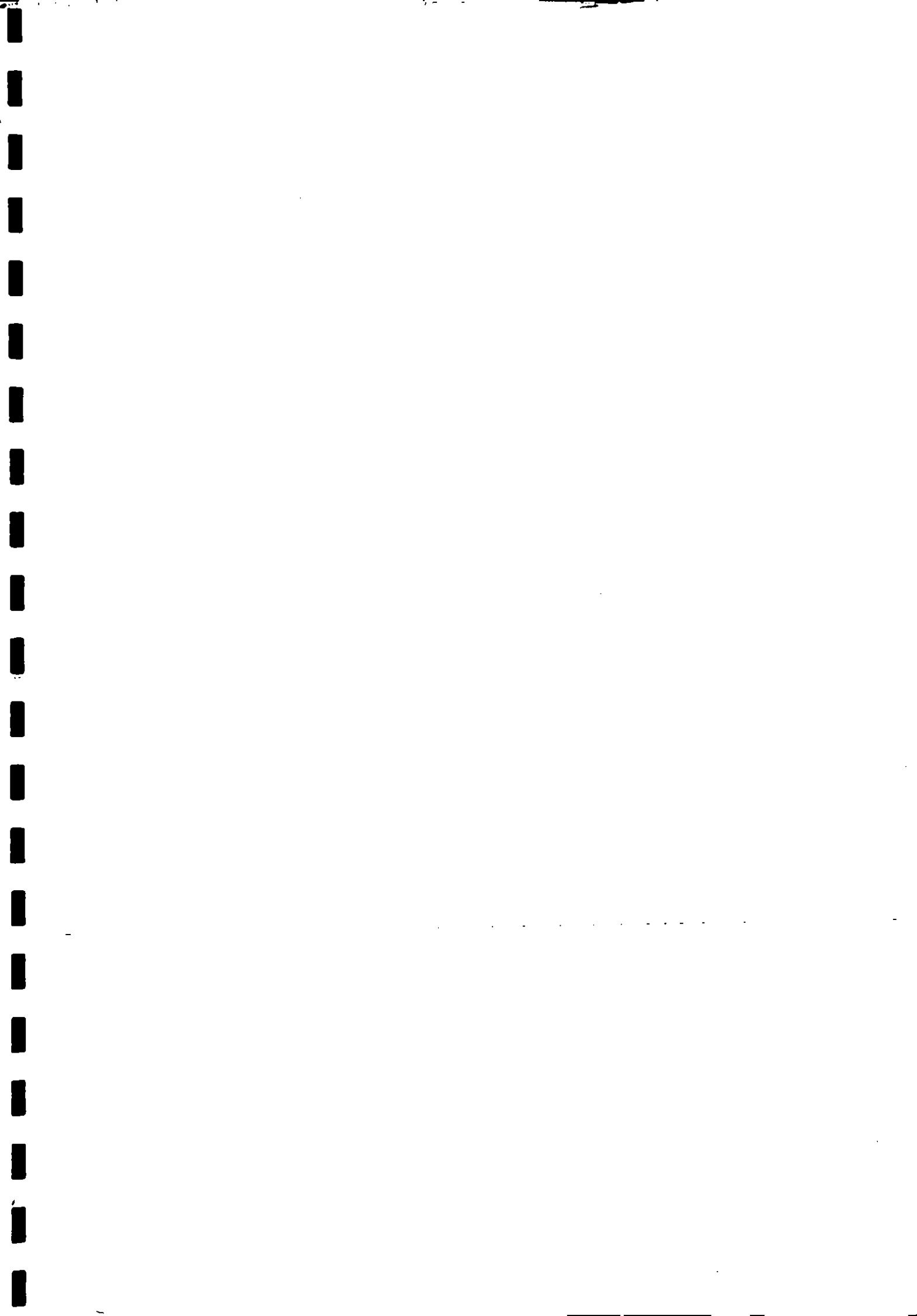
Dunkirk Mills Bridge 1						
NSC_015	53.68	6.1	53.84	7.6	54.00	8.9
Dunkirk Mills Side Sluices						
NSC_016	55.96	6.1	56.09	7.6	56.19	8.9
NSD_001	53.29	5.4	53.33	5.4	53.38	5.4
Critchleye Bridge 5						
NSD_002	53.72	5.4	53.75	5.4	53.78	5.4
NSD_003	53.77	5.4	53.80	5.4	53.82	5.4
NSD_004	53.83	5.3	53.85	5.4	53.87	5.4
NSD_005	53.88	5.3	53.90	5.4	53.91	5.5
Tennis Court Bridge 1						
NSD_006	54.22	5.3	54.24	5.4	54.27	5.5
NSD_007	54.22	6.3	54.23	6.6	54.26	7.2
Elm Brook Bridge 1						
NSD_008	54.59	6.3	54.61	6.6	54.62	7.2
NSD_009	54.60	6.3	54.62	6.6	54.63	7.2
The Gables Bridge						
NSD_010	54.63	6.3	54.65	6.6	54.67	7.2
NSD_011	54.66	6.3	54.68	6.6	54.70	6.8
Dunkirk Mills Entrance Bridge						
NSD_012	56.29	6.3	56.44	6.6	56.56	6.8
NSD_013	56.29	6.3	56.44	7.0	56.56	7.5
NSD_014	56.29	6.4	56.44	7.3	56.56	8.1
NSD_015	56.29	5.3	56.44	6.1	56.56	6.9
NSD_016	56.30	4.9	56.44	5.6	56.57	6.3
NSD_017	56.30	4.8	56.44	5.3	56.57	5.9

NSD_018	56.30	4.2	56.44	4.3	56.57	4.4	56.34	3.9	56.40	3.6
Filling Station Culvert										
NSD_019	56.63	4.2	56.71	4.3	56.80	4.4	56.66	3.9	56.68	3.6
NSD_021	56.66	5.6	56.73	6.1	56.81	6.5	56.68	5.3	56.70	5.1

Junction with NSE_002

NSD_022	56.66	2.9	56.73	3.5	56.81	4.4	56.68	2.9	56.70	3.0
NSD_023	56.68	1.2	56.76	1.6	56.84	2.4	56.70	1.2	56.72	1.2
NSD_024	56.69	0.0	56.77	0.0	56.86	0.1	56.71	0.0	56.73	0.0
NSE_001	56.66	4.7	56.73	4.7	56.81	5.0	56.68	4.5	56.70	4.1
NSE_002	56.66	4.6	56.73	4.7	56.81	5.0	56.68	4.5	56.70	4.1

Model Cell	100 Year Event (original)		100 Year Event + 10% flow		100 year Event + 20% flow		100 Year Event - 10% coeffs		100 Year Event - 20% coeffs	
	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)	Level (mOD)	Depth (m)
Cell 201	36.08	0.58	36.33	0.83	36.63	1.13	35.95	0.45	35.84	0.34
Cell 202	56.29	2.29	56.44	2.44	56.56	2.56	56.34	2.34	56.39	2.39
Cell 203	56.30	1.30	56.45	1.45	56.57	1.57	56.35	1.35	56.40	1.40
Cell 204	56.31	1.31	56.45	1.46	56.58	1.58	56.35	1.35	56.41	1.41
Cell 205	56.65	1.40	56.72	1.47	56.80	1.54	56.67	1.42	56.69	1.44



Address and Registered Office: **HR Wallingford Ltd**, Howbery Park, Wallingford, Oxon OX10 8BA, UK
Tel: +44 (0)1491 835381 Fax: +44(0)1491 824080

Wallingford Water is a joint venture operated by HR Wallingford Ltd and Institute of Hydrology